

# CONTROL

SARAH ALKASASBEH

POWERUNIT

\* Real time systems :- systems are subjected to real-time, i.e., the response should be guaranteed within a specified timing constraint or the system should meet the specified deadline

• characteristics of real-time systems :-

- 1) Time constraints  $\rightarrow$  the task should be completed within time interval (meet the specified deadline) / (fast response)
- 2) A task in the real-time systems must not start before its specified time.

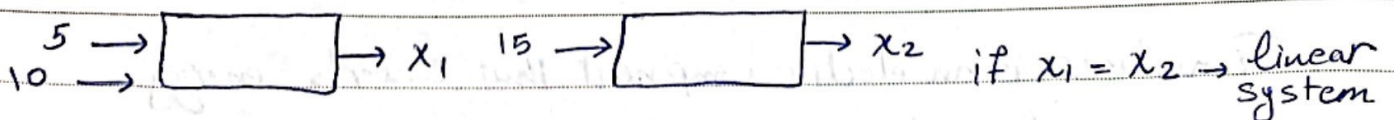
• Notes:- • Not every embedded system is a real time system

↳ • Not every embedded system is control system

↳ • real-time systems (some of them) may not need controllers.

↳ • The response in controllers is slow compared to the response in embedded systems.

• linear time-invariant systems (LTI)  $\rightarrow$  both linear and time invariant where linear systems are systems whose outputs for a linear combination of inputs are the same as a linear combination of individual responses to those inputs. for example:-



• Time invariant system is one whose response to inputs doesn't change with time.

تسمى أنظمة التحكم بالخطية (LTI) ، بينما الأنظمة الطبيعية مع الخصائص غير الخطية.

non-linear ← تم حل الأنظمة تقريباً (approximation)

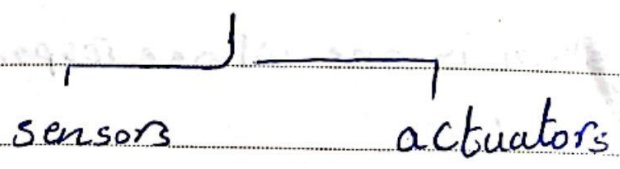
علاقة بين linear model و non-linear model

- Analog Control system → the Controller is made up of resistors, and capacitors (Complex), (hard to modify), (and they are subject to noise and distortion)  
↳ highly sensitive
- Digital Control system → uses digital computers, microcontrollers, microprocessors ... etc.
- ex:- Basic analog control system :- Potentiometers (Variable ~~resistor~~ resistor)

• In digital control systems, Computer functions may be passive or supervising, or ~~they~~ they may be active controllers (PLC "Programmable Logic Controllers")

• SCADA systems → used for controlling, monitoring, and analyzing devices and processes (both active and passive)

• Transducer is an electric component that converts energy from one form to another.



- sensors  $\rightarrow$  convert temperature to voltage or current (example)
- actuators  $\rightarrow$  convert voltage or current to another physical form.

Note :- digital control systems are less susceptible to noise as well as there is no tolerance effect.

- sampling frequency =  $2 \times$  frequency of the signal  
 $\hookrightarrow$  when converting from analog to digital

$\uparrow$  frequency     $\uparrow$  power consumption

• Two types of control systems: 1) open loop 2) closed loop

• Open loop control system → there is no feedback path  
Provided (non-feedback control system)

تؤدي الوظيفة  
بأسهل الطرق والحلول

↳ there is no sensors

↳ we don't know anything about the quality  
or the state of the control

↳ it only gives commands

↳ one forward path (Feed Forward path) from  
input to output

↳ unable to deal with any external changes  
(refer to the slides)

• disturbances :-

1) noise → affects the control signal

2) disturbances at the output

~~stress~~

• Closed loop control systems → there is a feedback path in addition

↳ 1) negative to Feed Forward path.  
↳ works on (target - sensor output)

↳ feedback path

• Closed loop control systems → has the ability to self-correct  
while the open-loop system doesn't.

Two types 1) negative → (target - feedback path)  
error signal

• the target and feedback ~~must~~ must be the  
same unit.

2) Positive  $\rightarrow$  (Target + Feedback path)

↓ not preferred

↳ actuating signal here is not the error signal

notes:-

• Open loop control systems have fast response because there is no measurement and feedback of output. The response of the closed loop control systems is slow due to presence of feedback.

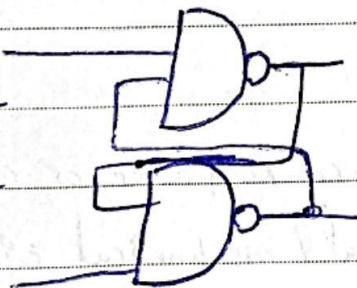
• Closed loop control systems require more maintenance (more expensive)

• Closed loop control systems are more accurate

• Closed loop control systems are less stable (unstability)

• positive closed loop control systems example  $\rightarrow$  latches

• There is a feedback path and the latch value remains the same.



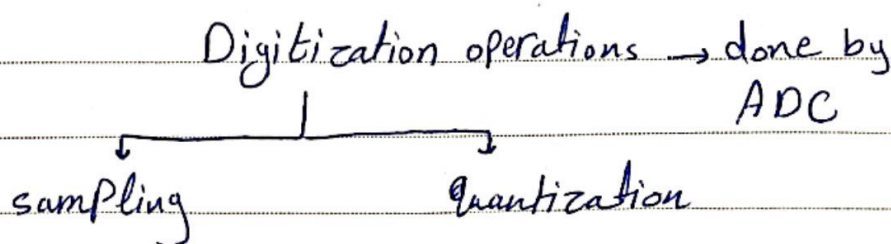
• There may be multiple feedback paths from different sources or from the same source. Some of them may be used in the control process or not.

- Why do we rarely see HDDs with speeds more than 7200 RPMs?
  - because when the speed increases, the force on the disc increases, which may damage it. it also brings negative effects such ~~as~~ as temperature increase.
- " " " " " " more than 5400 in laptops?
  - because it's portable, when the speed increases it'll be more sensitive to any external effects while it's working
- steady-state error :- the difference between the input command and the output of a system
- in HDDs, the steady-state error must be <sup>almost</sup> zero percent.

- natural response :- unforced response or characteristic response
    - ↳ has physical / mechanical equations that control it.
    - ↳ with time, the effect of the system disappears, and the output only affected by the input.
- stable system ←

- Forced response <sup>the system is</sup> → stable if the input is within its range

~~Dis~~

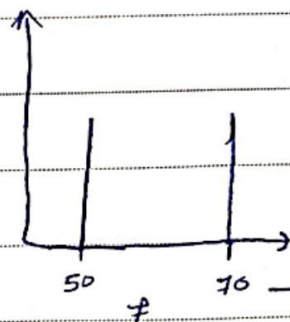


- Sampling  $\rightarrow$  discretization of time
- Quantization  $\rightarrow$  discretization of range (ex: if temperature is between 0 and 1 consider it 1).
- if we use the sampling frequency less than twice the maximum frequency component in the signal, that is called undersampling

$$f_{\text{sampling}} = 2 \times f_{\text{max}} \quad \text{undersampling results in data loss.}$$

- Fourier transform is a mathematical model which helps to transform the signals between different domains (from time domain to frequency domain or vice versa.)

$$\text{ex :- } \sin(50t) + \sin(70t)$$



or sampling rate

$$f_{\text{sampling}} = 2 \times 70 = 140 \text{ Hz}$$

50  $f$  70  $\rightarrow$  max frequency component.

$$T_{\text{processing}} \leftarrow T_{\text{sampling}}$$



• original signal max frequency  $\leq \frac{f_{sampling}}{2}$   
التردد الأقصى للإشارة الأصلية  $\leq \frac{f_{sampling}}{2}$

• distance between samples =  $1/f_{sampling} = T_s$   
المسافة الزمنية بين العينات =  $1/f_{sampling} = T_s$

• Cycle time =  $1/processor\ frequency$

$T_{processing} = cycle\ time \times \#\ of\ instructions \times \#\ of\ cycles$

$T_{processing} < T_{sampling}$   
 $\hookrightarrow 1/f_{sampling}$

• if  $T_{processing} > T_{sampling}$  we can use faster processor but this solution is considered expensive, or we can decrease the size of our program / using Algorithms (with better performance ex:  $O(\log n)$ ) / Compiler optimization

$\hookrightarrow$  الـ Algorithm

Compiler optimization

Speed  
if memory is large enough

Size  
if memory size is small

Deadlines

relative  
الـ deadline النسبي  
الـ event النسبي

absolute  
عبر مرتبة الـ event وليس مرتبة بالوقت سواء في الـ event 1 8 21 ليس deadline

$\hookrightarrow$  الـ event النسبي الـ deadline النسبي

• Functional Requirements → "essential"

A. Data Collection / Acquisition → through feedback loops (sensors)

↳ if Analog → use Analog to digital converter.

B. Signal Conditioning → amplification / filtering / Converting and any other processes required to make sensor output suitable for processing.

C. Plant / Process Control → Controlling

D. Alarm monitoring / Data logging / Man Machine interaction → safety systems  
↳ optional.

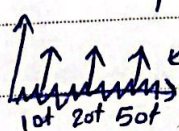
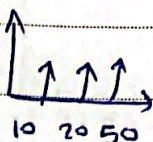
• Analog signals are more sensitive to noise (gaussian noise)

• ECC → error detection and correction.

• Low Pass filter → is a filter that passes signals with a frequency lower than a selected cutoff frequency and attenuates signals with frequencies higher. (RC circuits)

$$\sin(10t) + \sin(20t) + \sin(50t)$$

Fourier transform →



we can't determine the max. freq.  
so we have to get rid of this noise before sampling using Low Pass filters.

actual signal due to noise

• High pass filter  $\rightarrow$  filter designed to pass all frequencies above its cut-off frequency, and attenuates signals with frequencies lower.

• Band pass filter  $\rightarrow$  Passes frequencies within a certain range.

• Non-Functional Requirements.

1. Dependability  $\rightarrow$  the quality of being able to be trusted and being very likely to do what

Reliability      Safety      People expect.

fault-tolerance      Security

"survivability"

• Reliability  $\rightarrow$  the probability that a product or system will perform its intended function adequately for a specified period of time.

• Note  $\times$  Slide 49  $\rightarrow$  survival function 4 is the best one / survival function 1 more realistic in the industry (years instead of months)

•  $\lambda \rightarrow$  constant failure rate  $< 10^{-7}$  (high reliability)

$$\lambda = \frac{\text{\# of failures}}{\text{\# of systems} \times \text{operating time}}$$

- Fault tolerance → the ability of a system to continue operating without interruption when one or more of its components fail  
↳ ex:- odd number of sensors / lockstep processor

Note: lockstep processor → fault-tolerant that run the same set of operations at the same time in parallel, the output from lockstep operations can be compared to determine if there has been a fault if there are at least two systems, and the error can be corrected if there are at least three systems.

- safety stands for accident avoidance (unintentional harm), and security for crime prevention (intentional harm).

- Fail-safe system → in the event of any fault appearing, the system will always go to a safe status. (another action to do to reach the safe state.)
- Fail-operational → guarantee the full or degraded operation of a function even if a failure occurs. (يسمى بـ الوظيفة الآمنة)

• SCADA system (hybrid system) "Supervisory Control and Data Acquisition system" → used for controlling, monitoring, and analyzing industrial devices and processes. The system consists of both software and hardware components.

• SCADA System Architecture layers :-

1. Level 0 (Field level) → the lowest level and includes the physical devices that gather data from the processes. (sensors / actuators)
2. Level 1 (Programmable Devices for direct control)
  - ↳ PLCs → local
  - ↳ RTUs → Remote
3. Level 2 (Local plant control and HMI) → observation and local control
  - ↳ "Human Machine interface"
4. Level 3 (Coordination and Production control)
  - ↳ sending commands to PLCs and RTUs
5. Level 4 (Central control and Production Scheduling) → more software

"end of chapter 1"

• System modeling is the process of developing abstract models of a system. (تصميم عن الشكل الرياضي)

• Laplace: A mathematical tool that converts any differential and integral equations into algebraic equations. (from time domain to frequency domain).

• The superposition property of linear systems states that the response of a linear system to a sum of signals is the sum of the responses to each individual input signal.

• linear systems must apply the superposition principle.

• A homogeneous system of linear equations is one in which all of the constant terms are zero. (no constant term)

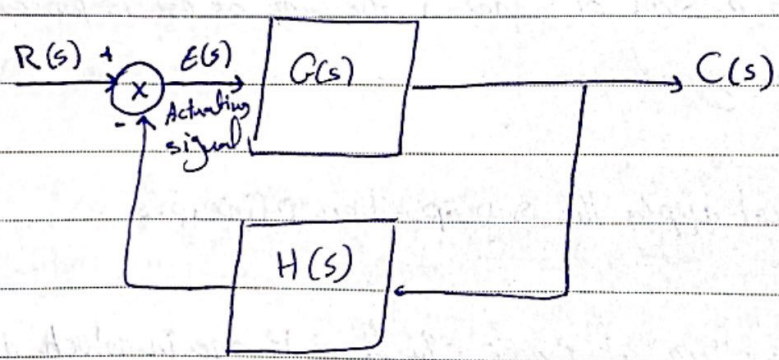
$$\text{Laplace equation} \rightarrow \mathcal{L}_t [f(t)](s) = \int_0^{\infty} f(t) e^{-st} dt$$

$$s = \sigma - j\omega t \quad \text{if } \sigma = 0 \rightarrow \text{Fourier transform}$$

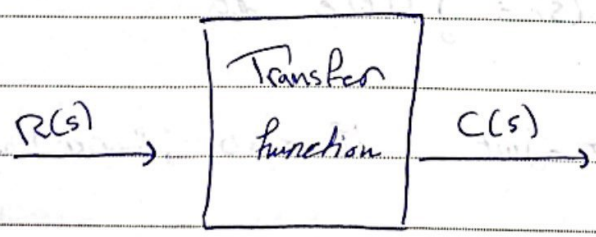
• Transfer function  $\rightarrow$  represents the relationship between the output signal of a control system and the input signal.

• Actuating signal  $\rightarrow$  An algebraic ~~sum~~ addition or subtraction of input signal and feedback signal.  
 Positive feedback system  $\downarrow$  negative feedback system

•  $R(s)$   $\rightarrow$  reference input /  $C(s)$   $\rightarrow$  controlled output



$\Downarrow$  we need to simplify it to  $\rightarrow$



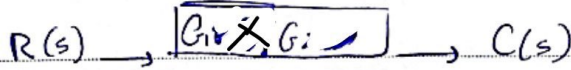
if we have n-systems  
 we have  $n \frac{C}{R}$   
 $\frac{C_1(s)}{R_1(s)} + \frac{C_2(s)}{R_2(s)} + \dots + \frac{C_n(s)}{R_n(s)}$

• negative feedback system  $\rightarrow \frac{C(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)}$   
 • Positive feedback system  $\rightarrow \frac{C(s)}{R(s)} = \frac{G(s)}{1 - G(s)H(s)}$   
 }  $\rightarrow$  Transfer functions of positive and negative feedback systems

• Block Manipulation

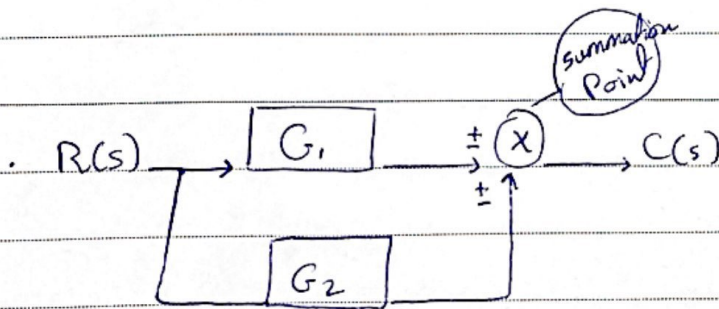


↓ simplify

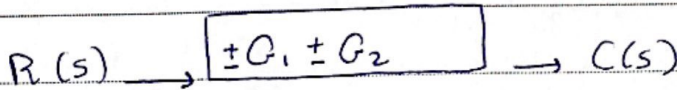


• Cascade systems "series"

• multiplication

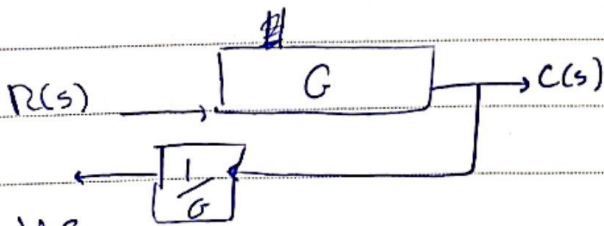
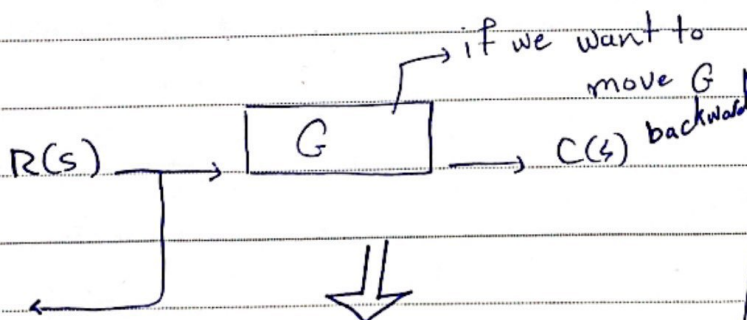


↓ simplify

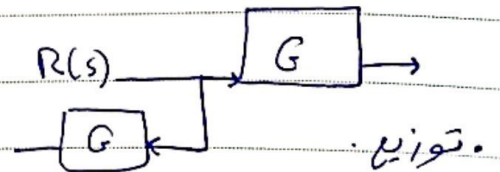
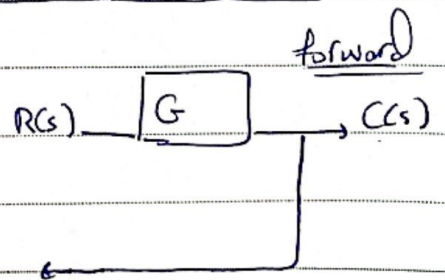


• Parallel system

• addition or subtraction according to ~~the~~ the sign enters the summation point



عكس كالتالي  
تأثير

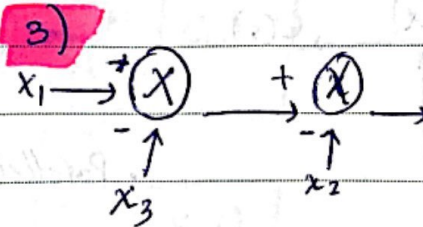
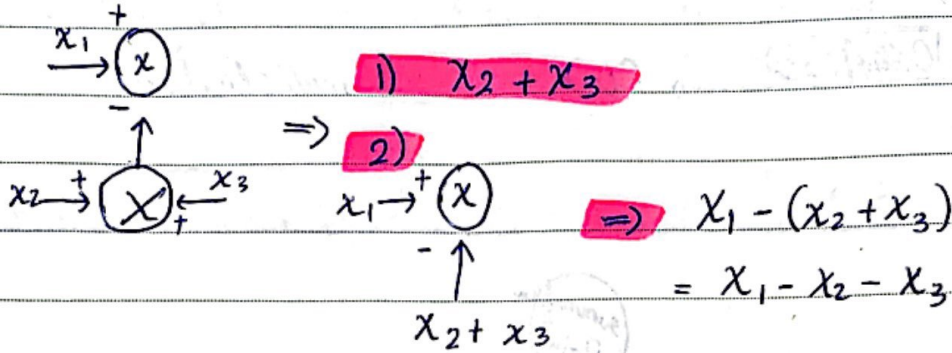


توزيع

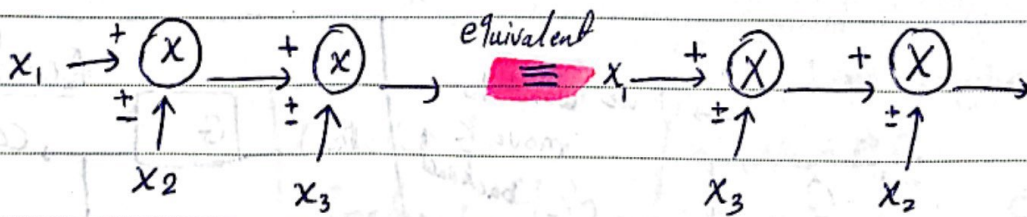


# Moving a Summing Point

## Rule 1:- Rearrangement of summing points

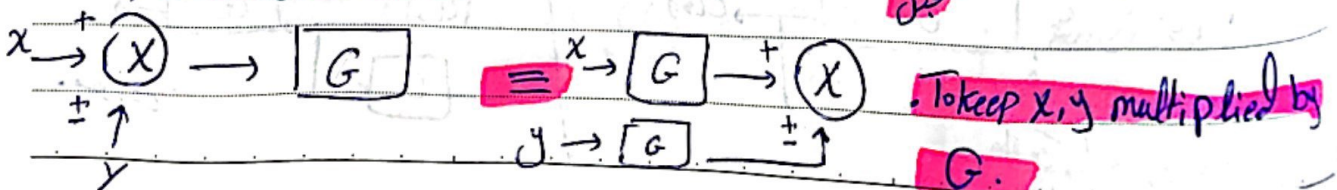


## Rule 2:- Interchanging of summing points → الترتيب ما يفرق



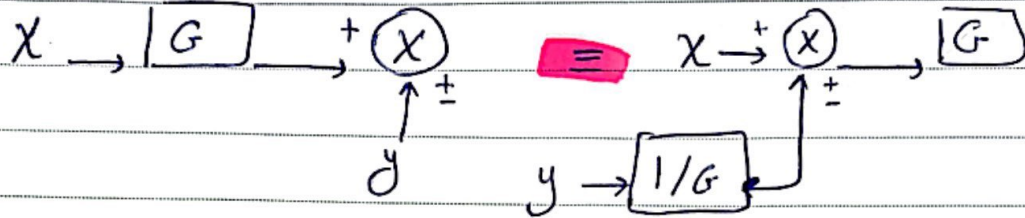
## Rule 3:- Moving a summing point ahead of a block

→  $Gx \pm Gy$  بالاول عبارة عن (Summation point قبل block قبل)



**Rule 4:** Moving a summing point beyond a block.  
 (Summation Point  $\rightarrow$  block  $\rightarrow$  Summation Point)

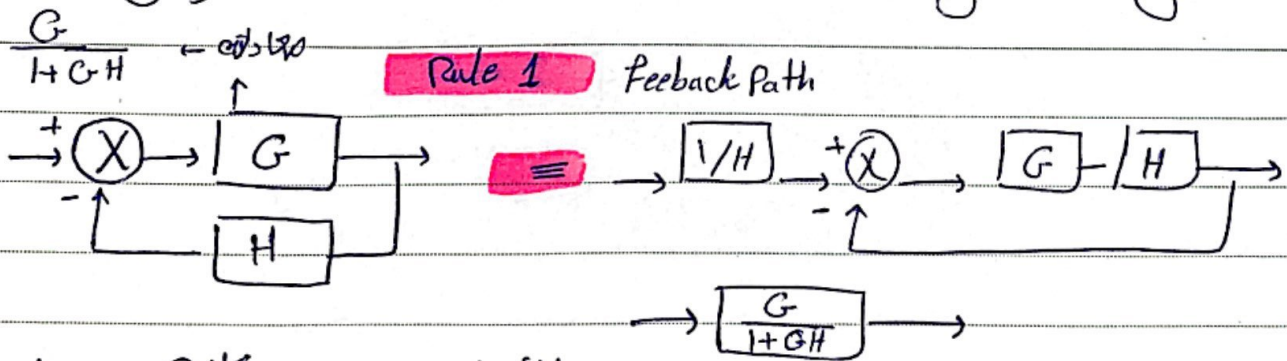
$G \rightarrow$  block  $\rightarrow$  Summation Point



• To keep only X multiplied with G.

**Unity path**  $\rightarrow$  a path that doesn't contain any block, whether it's forward path or feedback path.  $\equiv$  "block with 1"

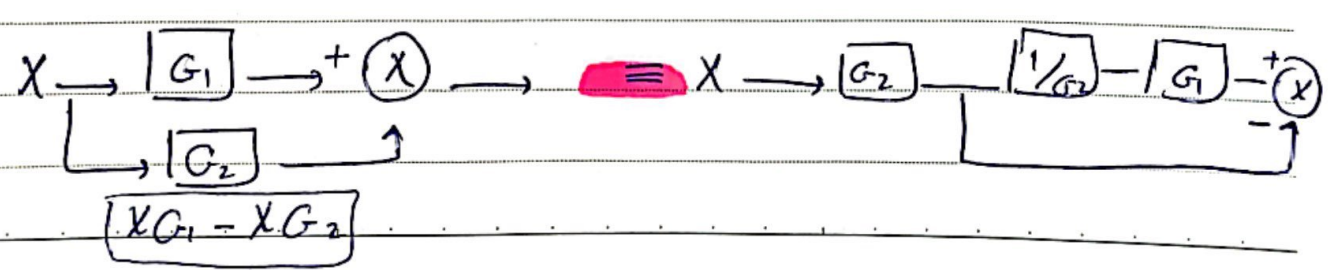
• Changing feedback and forward path (Converting to a unity path).



$\frac{1}{H} \cdot \frac{GH}{1+GH}$   $\rightarrow$  block  $\rightarrow$  Summation Point

$\rightarrow$  block  $\rightarrow$  Summation Point

**Rule 2** Forward Path

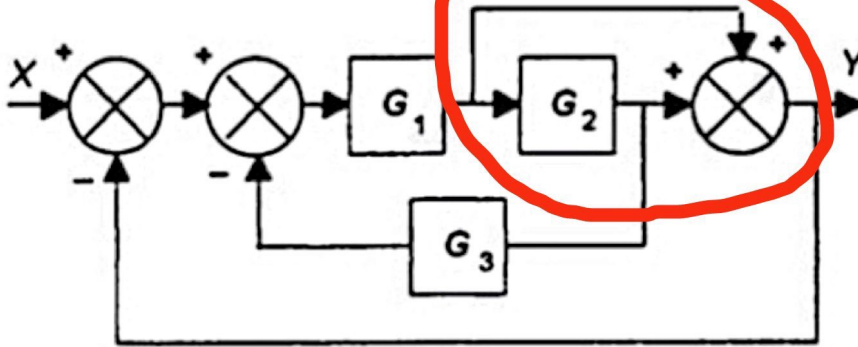


## Example 1 on Control System Block Simplification

9

Simplify the following control circuit using the block manipulation rules:

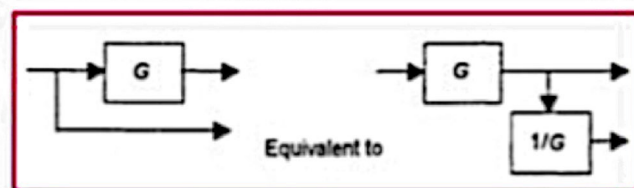
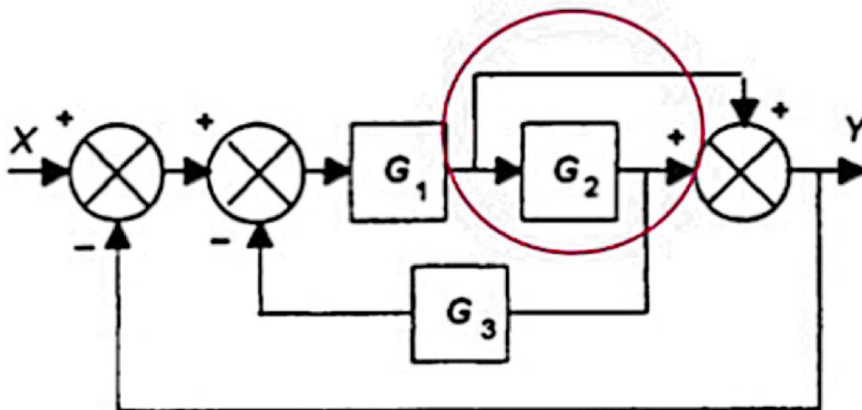
نقطة البداية  
لازم نتخلص من نقاط التشعب او  
التفرعات (G2 و G1 يكونوا series)



## Example 1 on Control System Block Simplification

10

Simplify the following control circuit using the block manipulation rules:

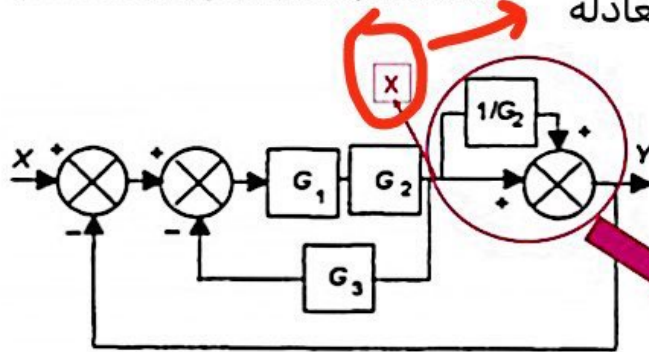


## Example 1 on Control System Block Simplification

11

Simplify the following control circuit using the block manipulation rules:

افتراضناه لنحل المعادلة



حل المعادلة رياضيا

$$Y = X + \frac{X}{G_2}$$

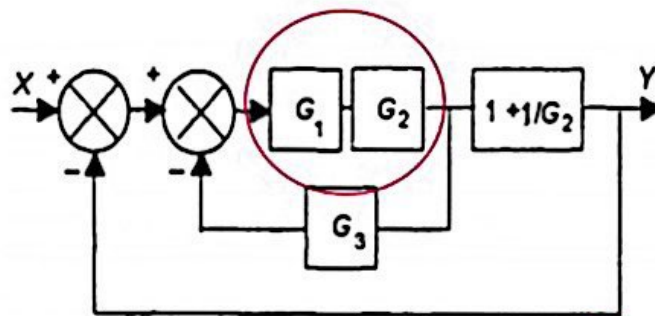
$$Y = X\left(1 + \frac{1}{G_2}\right)$$

$$\frac{Y}{X} = 1 + \frac{1}{G_2}$$

## Example 1 on Control System Block Simplification

12

Simplify the following control circuit using the block manipulation rules:

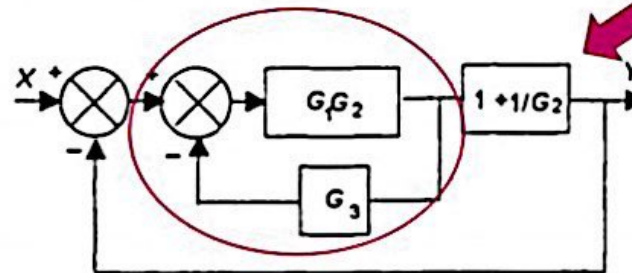


$$G_{\text{overall}} = G_1 G_2$$

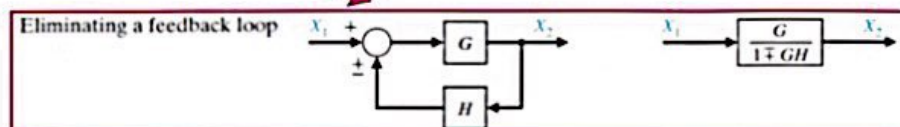
## Example 1 on Control System Block Simplification

13

Simplify the following control circuit using the block manipulation rules:



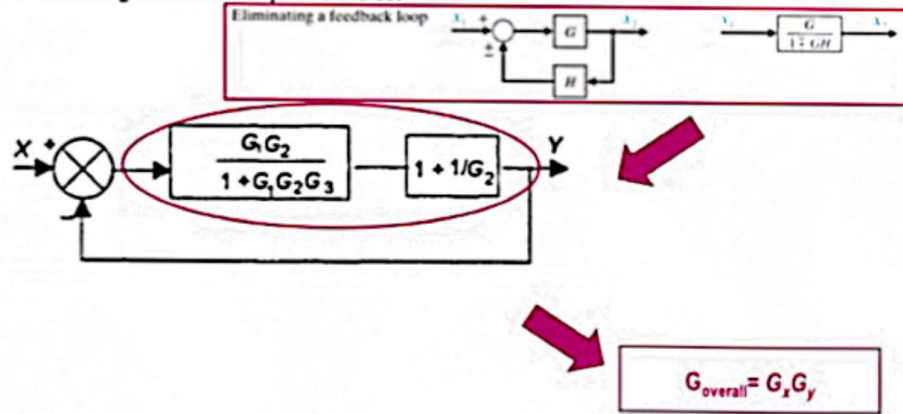
$$G_{\text{overall}}(s) = G_1 G_2$$



## Example 1 on Control System Block Simplification

14

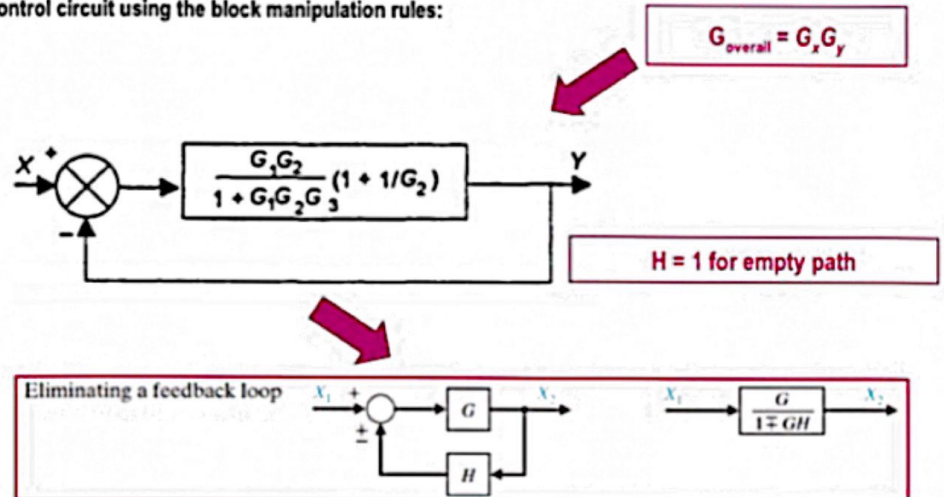
Simplify the following control circuit using the block manipulation rules:



## Example 1 on Control System Block Simplification

15

Simplify the following control circuit using the block manipulation rules:

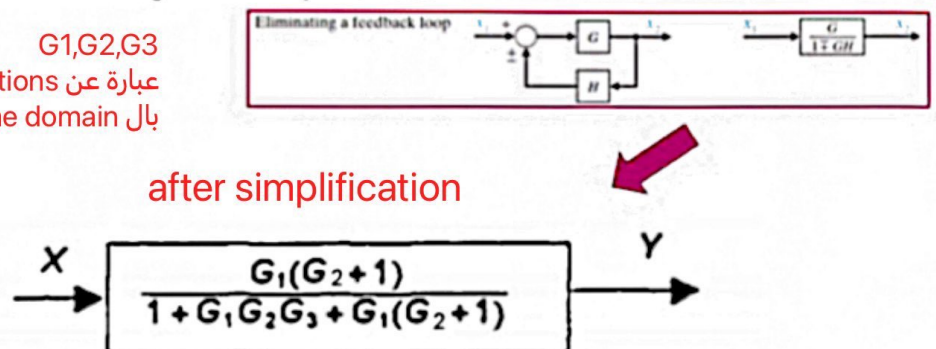


## Example 1 on Control Block Simplification

16

Simplify the following control circuit using the block manipulation rules:

$G_1, G_2, G_3$   
عبارة عن functions كانوا بالاساس  
بال time domain

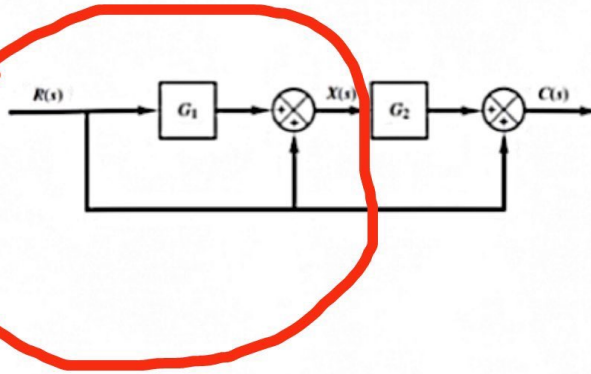


## Example 2 on Control System Block Simplification

17

Simplify the following control circuit using the block manipulation rules:

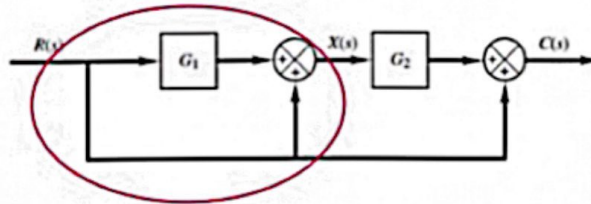
Start from here



## Example 2 on Control Block Simplification

18

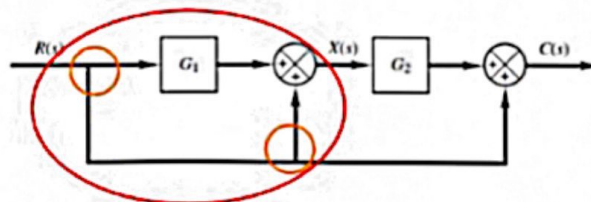
Simplify the following control circuit using the block manipulation rules:



## Example 2 on Control Block Simplification

19

Simplify the following control circuit using the block manipulation rules:

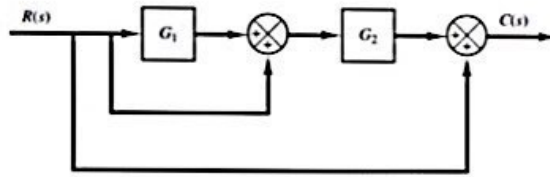


رتبهم بطريقة افضل

## Example 2 on Control Block Simplification

20

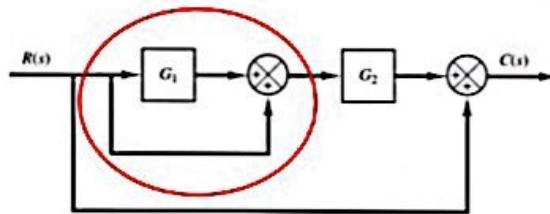
Simplify the following control circuit using the block manipulation rules:



## Example 2 on Control Block Simplification

21

Simplify the following control circuit using the block manipulation rules:

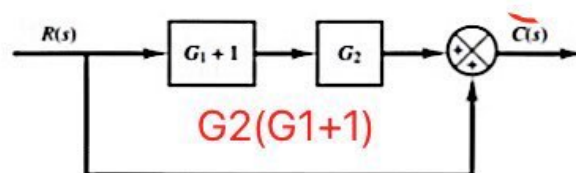


$$y = XG_1 + X$$
$$y = X(G_1 + 1)$$
$$y/X = G_1 + 1$$

## Example 2 on Control Block Simplification

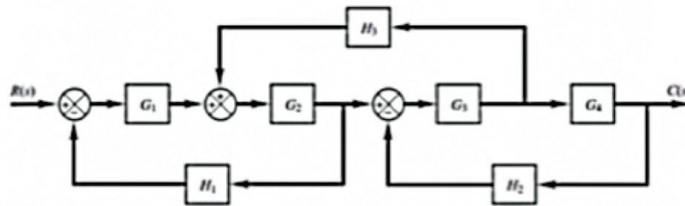
22

Simplify the following control circuit using the block manipulation rules:



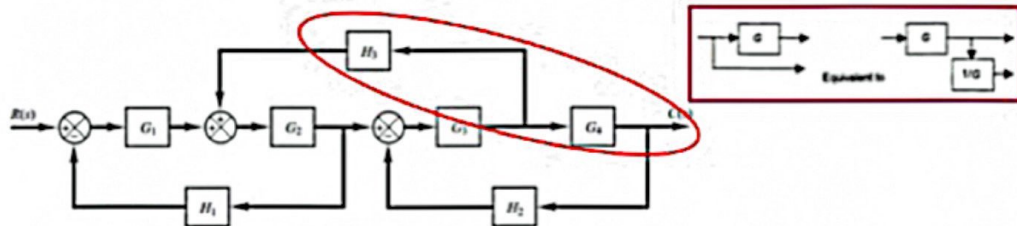
### Example 3 on Control Block Simplification

Simplify the block diagram shown in the Figure. Then obtain the closed-loop transfer function  $C(s)/R(s)$ .



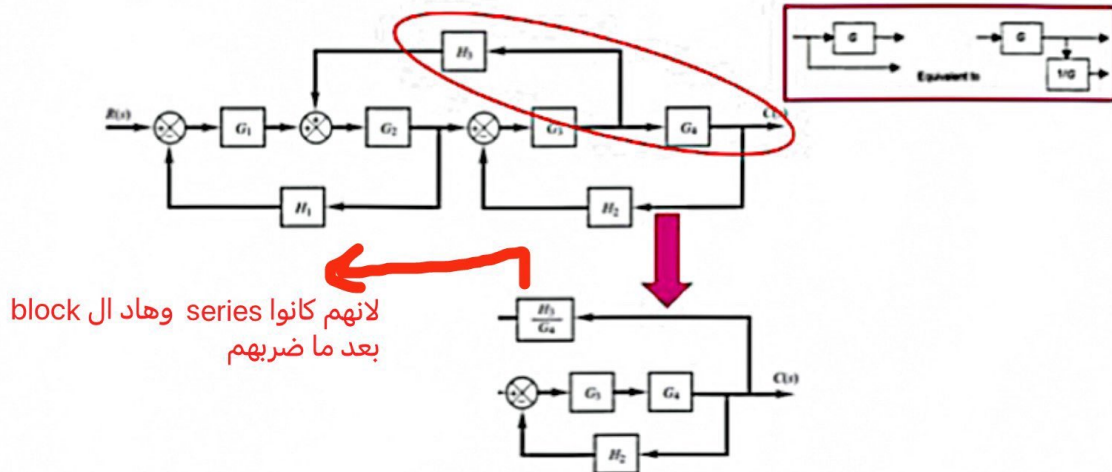
### Example 3 on Control Block Simplification

Simplify the block diagram shown in the Figure. Then obtain the closed-loop transfer function  $C(s)/R(s)$ .



### Example 3 on Control Block Simplification

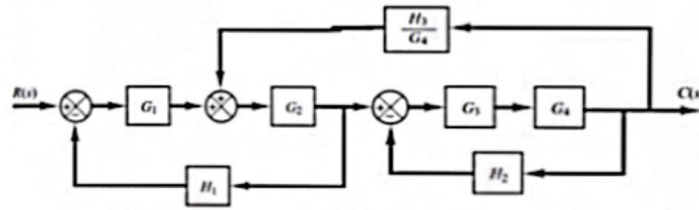
Simplify the block diagram shown in the Figure. Then obtain the closed-loop transfer function  $C(s)/R(s)$ .





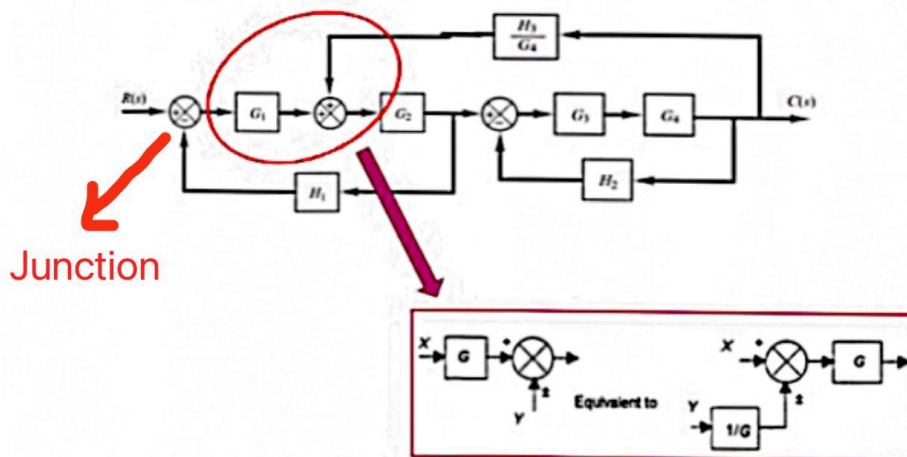
### Example 3 on Control Block Simplification

Simplify the block diagram shown in the Figure. Then obtain the closed-loop transfer function  $C(s)/R(s)$ .



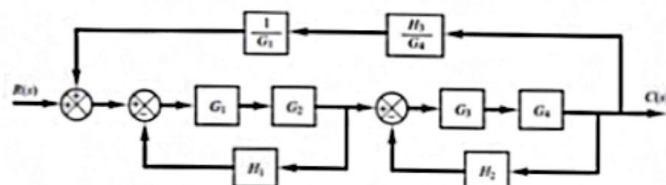
### Example 3 on Control Block Simplification

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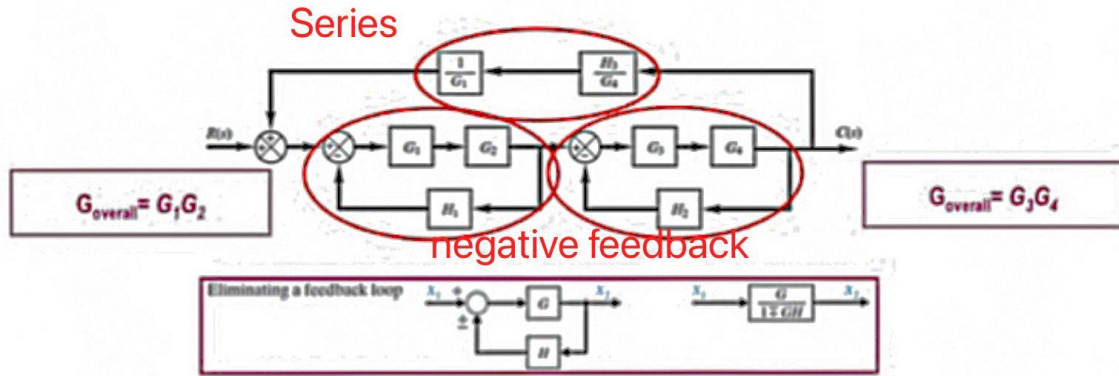
### Example 3 on Control Block Simplification

Simplify the block diagram shown in the Figure. Then obtain the closed-loop transfer function  $C(s)/R(s)$ .



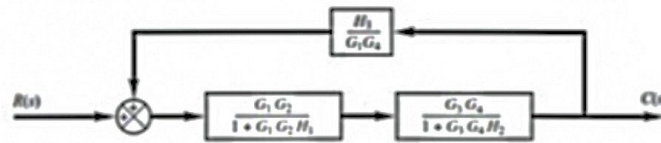
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Simplify the block diagram shown in the Figure. Then obtain the closed-loop transfer function  $C(s)/R(s)$ .



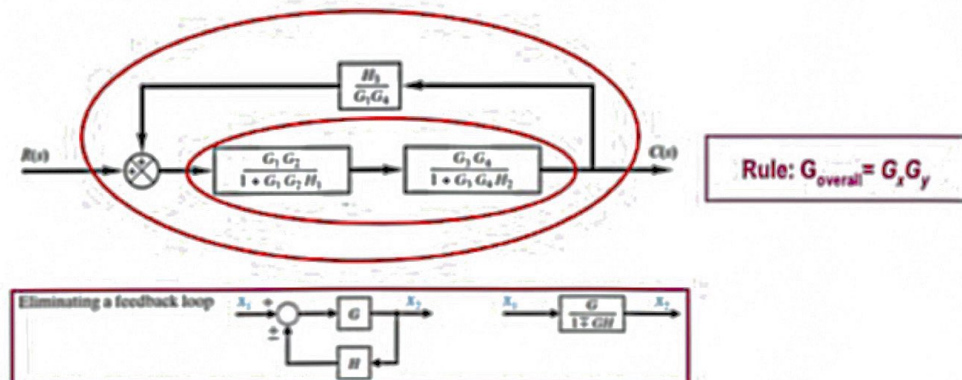
### Example 3 on Control Block Simplification

Simplify the block diagram shown in the Figure. Then obtain the closed-loop transfer function  $C(s)/R(s)$ .



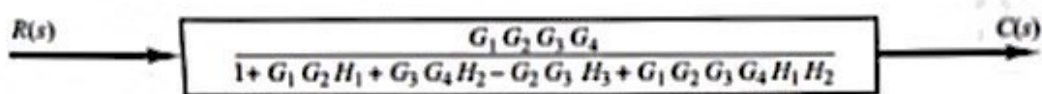
### Example 3 on Control Block Simplification

Simplify the block diagram shown in the Figure. Then obtain the closed-loop transfer function  $C(s)/R(s)$ .



### Example 3 on Control Block Simplification

Simplify the block diagram shown in the Figure. Then obtain the closed-loop transfer function  $C(s)/R(s)$ .

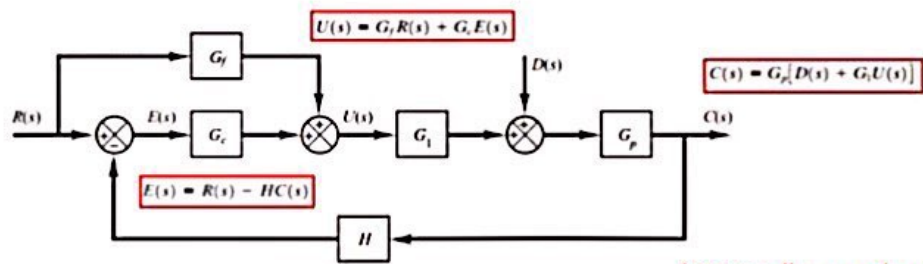


## Example 4 on Control Block Simplification

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### Using Equations

Mathematically obtain transfer functions  $C(s)/R(s)$  and  $C(s)/D(s)$  of the system shown in the Figure:



- This is a MIMO system
- D(s) is disturbance
- We have 2 transfer functions

بنصفر واحد من ال inputs  
عشان نحصل على C/R بنصفر D بالنهاية  
وعشان نحصل على C/D بنصفر R بالنهاية  
باستخدام superposition كونه linear

## Example 4 on Control Block Simplification

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### Using Equations

Mathematically obtain transfer functions  $C(s)/R(s)$  and  $C(s)/D(s)$  of the system shown in the Figure:

Substitute  $U_s$  into  $C_s$

$$C(s) = G_p D(s) + G_1 G_p [G_f R(s) + G_c E(s)]$$

Substitute  $E_s$  into the above equation:

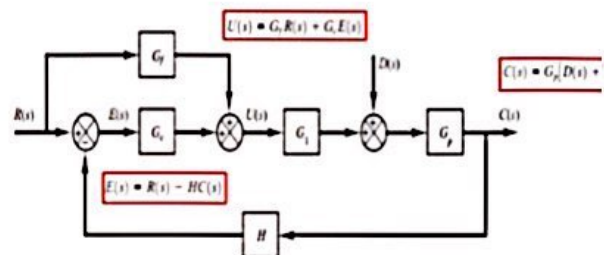
$$C(s) = G_p D(s) + G_1 G_p [G_f R(s) + G_c [R(s) - HC(s)]]$$

Solve for  $C_s$ :

$$C(s) + G_1 G_p G_c H C(s) = G_p D(s) + G_1 G_p (G_f + G_c) R(s)$$

Rearrange:

$$C(s) = \frac{G_p D(s) + G_1 G_p (G_f + G_c) R(s)}{1 + G_1 G_p G_c H}$$



دايما بنحاول نخلي ال outputs  
على جهة وال inputs على جهة

## Example 4 on Control Block Simplification

36

### Using Equations

Mathematically obtain the transfer functions  $C(s)/R(s)$  and  $C(s)/D(s)$  of the system shown in the Figure:

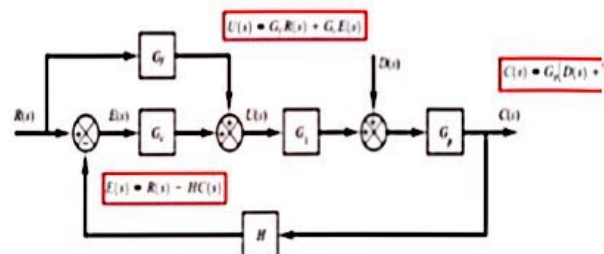
$$C(s) = \frac{G_p D(s) + G_1 G_p (G_f + G_c) R(s)}{1 + G_1 G_p G_c H}$$

Notice that this is a multiple input system, one for the actual input  $R(s)$ , and another for some disturbance  $D(s)$

To obtain the transfer functions  $C(s)/R(s)$  and  $C(s)/D(s)$ , we must only let one input present, and all other inputs are 0, therefore:

$$C(s)/R(s) = \frac{C(s)}{R(s)} = \frac{G_1 G_p (G_f + G_c)}{1 + G_1 G_p G_c H}$$

$$C(s)/D(s) = \frac{C(s)}{D(s)} = \frac{G_p}{1 + G_1 G_p G_c H}$$



## Example 5 on Control Block Simplification MIMO system Using Equations

Figure 2-24 shows a system with two inputs and two outputs. Derive  $C_1(s)/R_1(s)$ ,  $C_1(s)/R_2(s)$ ,  $C_2(s)/R_1(s)$ , and  $C_2(s)/R_2(s)$

Solution:

-We have 4 transfer functions because there are 2 inputs and 2 outputs

$$C_1 = G_1(R_1 - G_3C_2)$$

$$C_2 = G_4(R_2 - G_2C_1)$$

Substitute  $C_2$  into  $C_1$

$$C_1 = G_1[R_1 - G_3G_4(R_2 - G_2C_1)]$$

Substitute  $C_1$  into  $C_2$

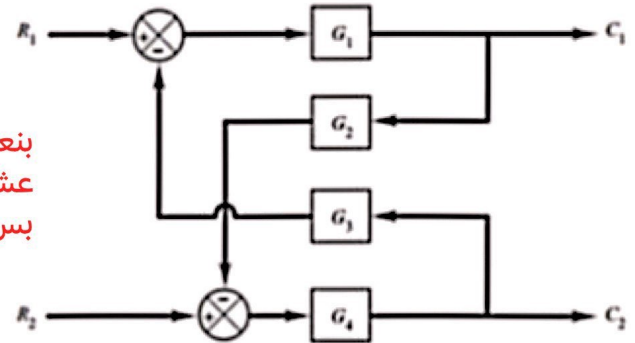
$$C_2 = G_4[R_2 - G_2G_1(R_1 - G_3C_2)]$$

Solve the equation for  $C_1$

$$C_1 = \frac{G_1R_1 - G_1G_3G_4R_2}{1 - G_1G_2G_3G_4}$$

Solve the equation for  $C_2$

$$C_2 = \frac{-G_1G_2G_4R_1 + G_4R_2}{1 - G_1G_2G_3G_4}$$



بنعوض C1 بمعادلة C2 او العكس  
عشان بهمنا يكون في output واحد  
بس بالمعادلة

## Example 5 on Control Block Simplification Using Equations

Figure 2-24 shows a system with two inputs and two outputs. Derive  $C_1(s)/R_1(s)$ ,  $C_1(s)/R_2(s)$ ,  $C_2(s)/R_1(s)$ , and  $C_2(s)/R_2(s)$

We now have these two relationships:

$$C_1 = \frac{G_1R_1 - G_1G_3G_4R_2}{1 - G_1G_2G_3G_4} \quad C_2 = \frac{-G_1G_2G_4R_1 + G_4R_2}{1 - G_1G_2G_3G_4}$$

We can derive the transfer functions of  $C_1(s)/R_1(s)$  and  $C_2(s)/R_1(s)$  by setting  $R_2$  to 0, so

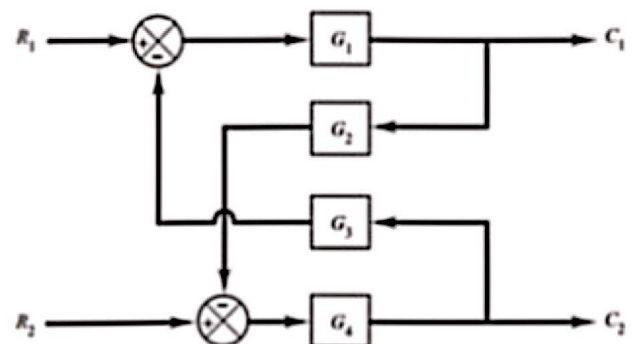
$$\frac{C_1(s)}{R_1(s)} = \frac{G_1}{1 - G_1G_2G_3G_4}$$

$$\frac{C_2(s)}{R_1(s)} = -\frac{G_1G_2G_4}{1 - G_1G_2G_3G_4}$$

Similarly, we can derive the transfer functions of  $C_1(s)/R_2(s)$  and  $C_2(s)/R_2(s)$  by setting  $R_1$  to 0, so

$$\frac{C_1(s)}{R_2(s)} = -\frac{G_1G_3G_4}{1 - G_1G_2G_3G_4}$$

$$\frac{C_2(s)}{R_2(s)} = \frac{G_4}{1 - G_1G_2G_3G_4}$$

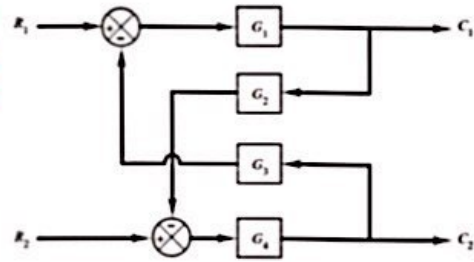
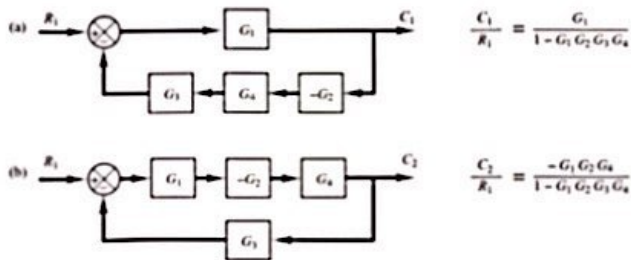


## Example 5 on Control Block Simplification *طريقة ثانية للحل* Using Equations – *Alternative Solution*

39

When setting  $R_2 = 0$ , the block diagram can actually be simplified to:

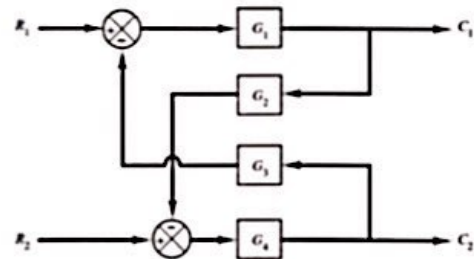
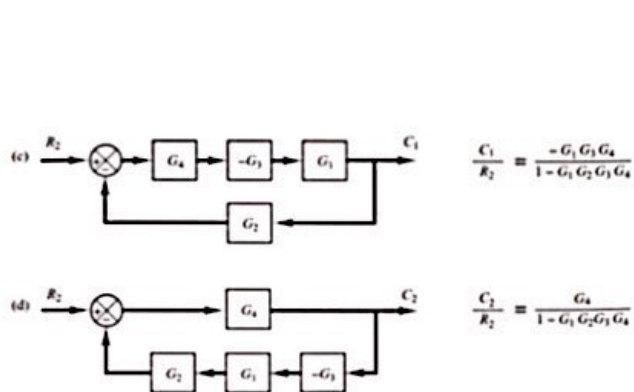
مرة صفرنا  $R_2$  وطلعنا معادلة  $R_1$   
 $C_1/R_1, C_2/R_1$   
ومرة صفرنا  $R_1$  وطلعنا معادلة  $R_2$



## Example 5 on Control Block Simplification Using Equations – *Alternative Solution*

40

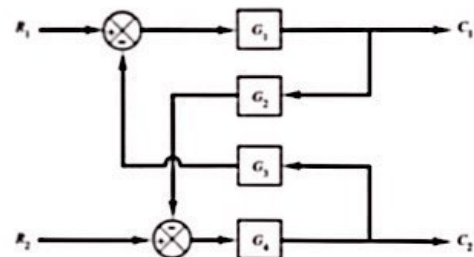
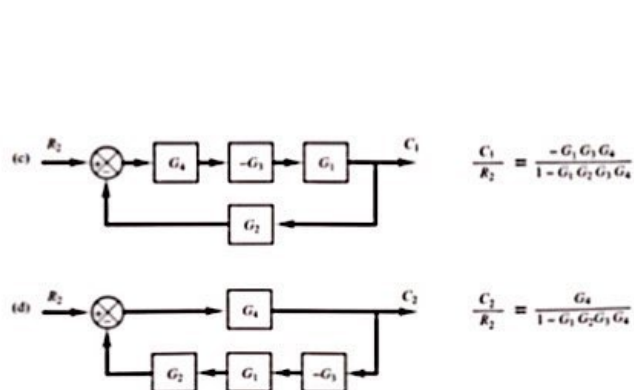
When setting  $R_1 = 0$ , the block diagram actually can be simplified to:



## Example 5 on Control Block Simplification Using Equations – *Alternative Solution*

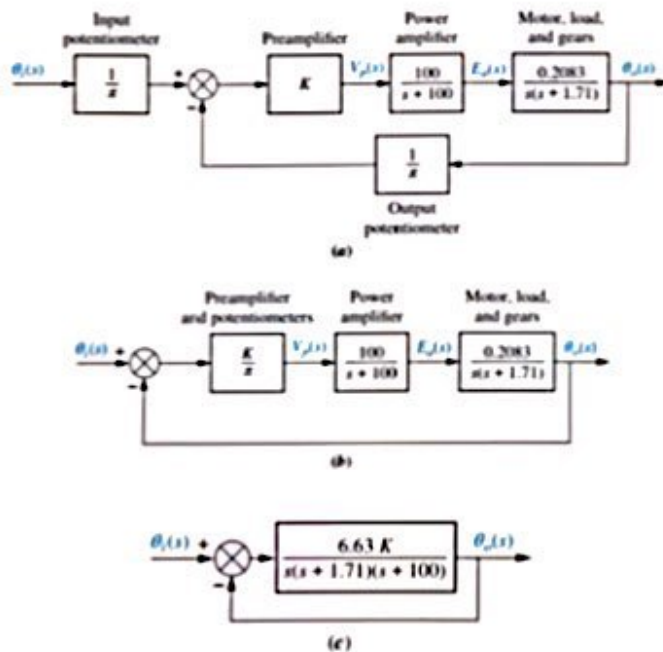
41

When setting  $R_1 = 0$ , the block diagram actually can be simplified to:

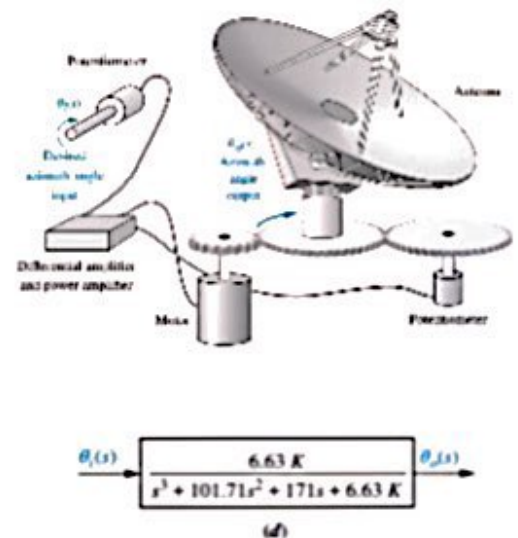


## Example 6 on Control Block Simplification

### Antenna Azimuth Control System



Layout



## References and Textbook Material

The material in these slides are based on:

**Control Systems Engineering**, Norman S. Nise, 7<sup>th</sup> Edition (2014), John Wiley And Sons

- **Chapter 5 – Reduction of Multiple Subsystems**  
Sections 5.1, 5.2

**Instrumentation and Control Systems**, 1<sup>st</sup> Edition, 2004, Elsevier (Newer versions available 3<sup>rd</sup> edition 2021, but I used the first one)

- **Chapter 9 – Transfer Function**  
Sections 9.1, 9.2, 9.3, 9.4, 9.5

Time Response

Time response → The amount of time required for the outputs to respond or react to the inputs.

• Forced response is what the system does ~~with the input~~ when turned on, but with the initial condition set to zero (from state to state "steady state") also called steady-state response. "input"

• Natural response is how does the system <sup>transfer</sup> from a state to the steady-state but with the influence of the system's properties, and how its properties affect the transition process. This effect must decrease over time until it disappears so that we can reach the steady-state. "شكل الانتقال"

• First order system →  $\frac{1}{s}$  "الجزء" المقام من الدرجة الأولى مثلاً  
"درجة في المقام هي 1"

• Second order system →  $\frac{1}{s^2}$  "الجزء" المقام من الدرجة 2 مثلاً

• Poles → أقطاب / zeros → أصفاء

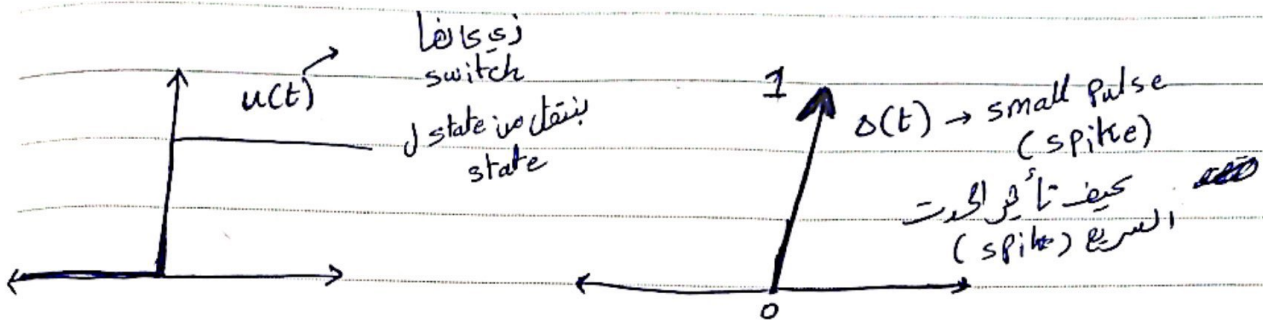
↳ they will determine if the system is stable or not, so we'll focus on them

↳ representation of blocks

in s-plane → Poles are represented by an (X), and zeros are represented by (O). s-plane هي، في transfer function

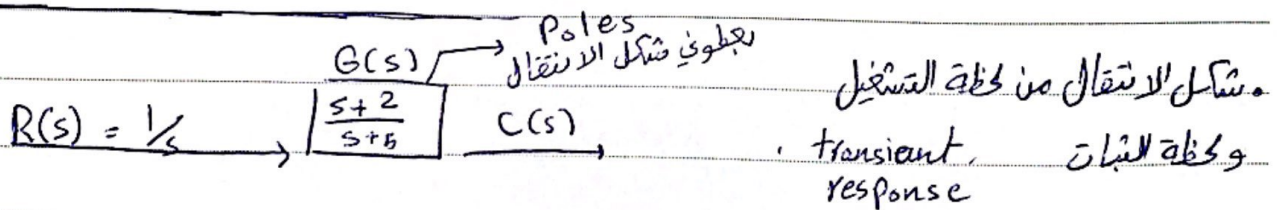


جب ان يكون جميع ال Poles في left half من s-plane ليكون stable.



time domain  $u(t)$   $\rightarrow$  s-domain  $\frac{1}{s}$ , so when the input of a system is  $\frac{1}{s}$ , consider it a switch.

- ex:
- input  $\frac{1}{s} \rightarrow$  forced input response
  - Natural response  $\rightarrow$  شكل الانتقال | is it linear / smooth... etc  
 determined by the transfer function of a system.



$$C(s) = \frac{(s+2)}{s(s+5)} = \frac{2/5}{s} + \frac{3/5}{s+5}$$

Partial Fraction (in math)   
 حساب من E.O. function لا يتم ونستخدم Laplace table

from table:  $C(t) = \frac{2}{5} + \frac{3}{5} e^{-5t}$

يختفي مع الزمن  $\rightarrow$   $\frac{2}{5}$  is the steady-state

zeros with poles generate the final amplitudes

inputs  $\rightarrow$  to reach the steady-state

Poles  $\rightarrow$  الطريقة التي وصلنا فيها  $\frac{2}{5}$  وكان  $e^{-5t}$  smooth line

• كل ما كان ال Poles اجه باجاء left x-axis يكون الاخر اجر  
 ويوصل ال system ال steady-state بشكل ايسر

• ال right half plane يعني ليس *unstable* output يكون

$$\frac{k_2}{s+2} \rightarrow k_2 e^{-2t} \quad / \quad \frac{k}{s+3} \rightarrow k e^{-3t} \quad \dots \text{etc}$$

↳ natural response ~~which~~ will decay over time.

• ~~هو~~ time-domain ~~هو~~ اذا ال system يكون stable

•  $a \rightarrow$  exponential frequency  $\rightarrow$  time to reach steady state.  
 • as  $a$  increases, the system reaches the steady-state faster.

• time constant =  $\frac{1}{a}$

• لو عني  $e^{-5t}$  فال Time constant يساوي  $\frac{1}{5}$  يعني هو  $\frac{1}{5}$  ثانية

• ال system يوصل ل 63% من ال steady-state

• Note :- ilaplace (F) command in matlab returns the inverse laplace transform of F (in time domain).

• rise time  $\rightarrow$  The time for a signal to go from 10% of its value to 90% of its value.

$$T_r = t_{90} - t_{10}$$

- settling time  $\rightarrow$  time to reach 2% of the final value.

Rise time, settling time, Time const  $\parallel$  Lap } first order systems  $\parallel$   $\bullet$

- Rise time ( $T_r$ ) =  $t_{90} - t_{10} = \frac{2.2}{a}$
  - settling time ( $T_s$ ) =  $4/a$
- }  $\rightarrow$  من كلوب  
الاستقرار

### problem

- A system has a transfer function  $G(s) = 50/s + 50$  find the time constant  $T_c$ , settling time  $T_s$ , and rise time  $T_r$ .

Answer :-  $a = 50$ , so time constant  $T_c = \frac{1}{50} = 0.02$

$$T_r = 2.2 / 50 = 0.044$$

$$T_s = 4/a = 0.08$$

- In second order systems  $\rightarrow$  Changing  $a$  will change the form of the response not only the speed.

- overdamped  $\rightarrow$  This function has a pole that comes from from the unit step function (steady-state) and Two real poles  $-a_1, -a_2$  that come from the system. (no complex roots)

• Note : euler identity  $\rightarrow e^{j\omega} = \sin(\omega t) + j\cos(\omega t)$

• Underdamped → roots are real and complex (Poles).

↳ <sup>sin wave</sup> بالتردد يتكون

amplitude موج الزمن ال

exp. enveloped

half ← <sup>تكون بال</sup>

18/4

• Undamped → Purely imaginary poles without a real part  
(no exponential parts)

↳ so, sin wave

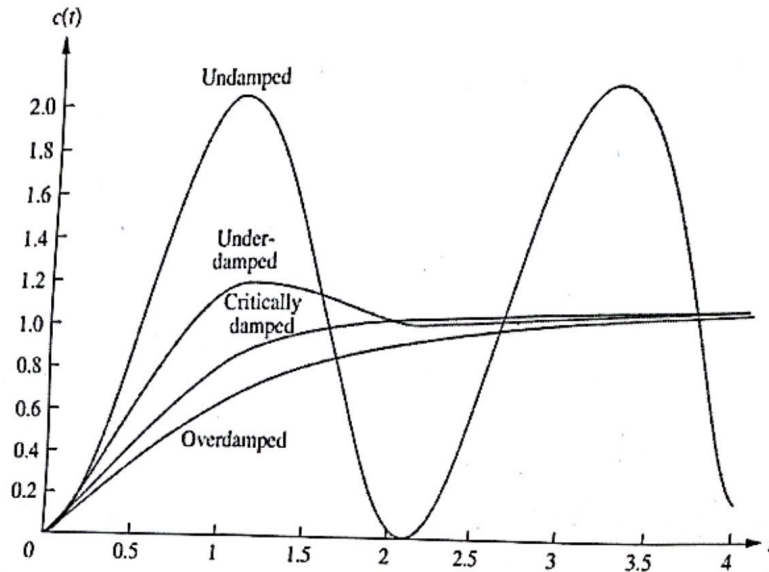
• Critically damped → both roots are the same. (متساويين)

• over damped به الاقواس والاضح اكثر.

• The output can be estimated as →  $c(t) = k_1 e^{-\sigma_1 t} + k_2 t e^{-\sigma_1 t}$

time variant, <sup>يعني</sup>  $k_1, k_2$  ← independent <sup>من</sup>  $t$  <sup>عبارة</sup> <sup>من</sup>  $t$  <sup>Variable</sup>

# Second Order Systems



فيما اظهر input و output ليوصل الى output بصورة  
منها في الاستجابة (بده وقت ليوصل للجواب)  
بسر بدنا نعلم نسيم يفر من هنا في الاستجابة بحيث  
تكون استجابته منا سوية

## The General Second Order System

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Natural Frequency,  $\omega_n$  of a second-order system is the frequency of oscillation of the system without damping

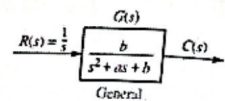
Damping Ratio,  $\zeta$  compares the exponential decay frequency of the envelope to the natural frequency

$$\zeta = \frac{\text{Exponential decay frequency}}{\text{Natural frequency (rad/second)}} = \frac{1}{2\pi} \frac{\text{Natural period (seconds)}}{\text{Exponential time constant}}$$

For the underdamped system, the complex poles have a real part,  $\sigma$

We can quickly derive the value of the real part of the poles from the second order equation  $s^2 + as + b$

The real part of the pole  $\sigma$  is equal to  $-a/2$ .



$$\zeta = \frac{\text{Exponential decay frequency}}{\text{Natural frequency (rad/second)}} = \frac{|\sigma|}{\omega_n} = \frac{a/2}{\omega_n} \rightarrow a = 2\zeta\omega_n$$

$$\omega_n = \sqrt{b}$$

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$\begin{matrix} a & & b \end{matrix}$

$$s_{1,2} = -\zeta\omega_n \pm \omega_n\sqrt{\zeta^2 - 1}$$

Underdamped systems  $\left\{ \begin{array}{l} \text{decay frequency (exp.)} \\ \text{natural frequency (sin wave)} \end{array} \right.$

$\zeta$  (overall damping ratio) =  $\frac{\text{decay frequency}}{\text{Natural frequency}} = \frac{\text{Natural period} \cdot \frac{1}{2\pi}}{\text{exp. time constant}}$

"How the exp. part is damping the sinusoidal part."

equivalent

second order system  $\cdot \frac{b}{s^2 + as + b} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$

$\omega_n^2 = b$
$2\zeta\omega_n = a$

natural frequency ( $\omega_n$ ) =  $\sqrt{\omega_n^2} = \sqrt{b}$

علاقة بين التردد الطبيعي / التردد التخميد  
natural freq. / exp. decay frequency

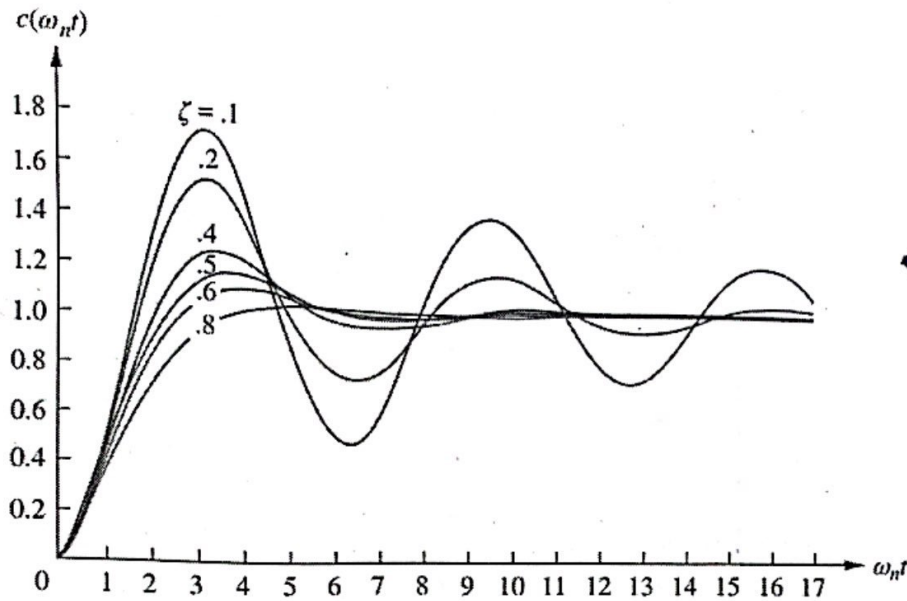
decay frequency ( $a$ ) =  $2\zeta\omega_n$

Note :- damping ratio  $\zeta$  يحدد الجزء التخميد والجزء التذبذب  
الجزء التذبذب هو  $\omega_n$  والجزء التخميد هو  $a$

- $\zeta = 0 \rightarrow$  Undamped
- $0 < \zeta < 1 \rightarrow$  Underdamped
- $\zeta = 1 \rightarrow$  Critically damped
- $\zeta > 1 \rightarrow$  Overdamped.

يُعرف  $\zeta$  بأنه نسبة التخميد إلى التردد الطبيعي

# Effect of $\zeta$ (dampening ratio) Visualized



لفظ  
ال  
Frequency  
( $\omega_n$ )

إذا كانت جميع ال Sin waves تتقاطع بنفس النقطة ← لفظ ال Frequency

↑  $\zeta$  ↑ damping

كلهم بالأخرى يصلوا إلى  
Steady state  
بس باختلاف طريقة الوصول

وبتغير ال poles  
كالشمال أكثر

## Finding $\zeta$ and $\omega_n$ For a Second-Order System - Example

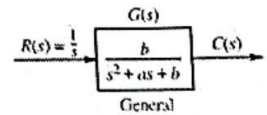
Given the transfer function of  $G(s)$ , find  $\zeta$  and  $\omega_n$ .

$$G(s) = \frac{36}{s^2 + 4.2s + 36}$$

$\omega_n^2 = 36$ , therefore  $\omega_n = 6$  rad/s

Also,  $2\zeta\omega_n = 4.2$ , so after substituting the value of  $\omega_n = 6$ , we get  $\zeta = 0.35$

هذا بقول الشكل العام  
البيسط في  $p$  وال مقام  
في  $b$   
غير هيك لازم نخلصها  
للكل  
العام



$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

→ speed of response

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• Other parameters associated with the underdamped response:-

- 1) Rise time ( $T_r$ ) → time to go from 0.1 to 0.9 of the final val
- 2) Peak time ( $T_p$ ) → time to reach the max. peak.
- 3) Percent overshoot → steady-state value  $\frac{\text{peak} - \text{steady-state}}{\text{steady-state}} \times 100\%$
- 4) settling time ( $T_s$ ) → reach and stay within 2% of the steady-state value  $\frac{\text{peak} - \text{steady-state}}{\text{steady-state}} \times 100\%$

Note  $T_r$  is an empirical study.  $T_r$  goes to 0 as  $\zeta$  increases.

• as the poles move in the vertical direction, the frequency changes. (envelope remains the same).

↳  $\zeta$  constant

• Changing frequency within the same envelope doesn't affect settling time, but it affects the overshoot (as frequency increases the overshoot increases and peak time decreases)

↑ frequency. Higher overshoot, lower peak time and rise time

• changing the damping ratio doesn't affect the peak time, but affects the overshoot and rise time.

↑ damping ratio ↓ overshoot ↑  $T_r$



- Changing the envelope and the frequency  $\rightarrow$  overshoots are the same / The farther the poles are from the origin, the more rapid the response.

- Third order system ~~above~~  $\rightarrow$  has 3 poles  
 $\hookrightarrow$  we'll assume that the third pole is a const. number.

- Case I  $\rightarrow$  third pole لا يكون ال قريباً من left half  
 طبق second order ال

- Case II  $\rightarrow$  " " " " } اواكز  
 " " " " } بعيدة بحدار 5 اختلاف  
 second order sys. ال  $\rightarrow$  عن ال roots الاساسية

- Case III  $\rightarrow$   $\infty$  = third pole اذا كان  
 second order system يعتبر

### • Additional real zero.

- اذا كان ال zero بعيد 5 اختلاف عن a يجوز تطبيق الحداد  
 وبتطبيق second order system

- if the zero is in the right half  $\rightarrow$  nonminimum - phase system

↓  
 يكون stable ال استجابة و لكن ال ال ال ال ال ال  
 لان ال roots ال left ال

## Exercise

- ▶ Find the step response of the following transfer functions and compare them. Which one of  $T_2$  or  $T_3$  can we apply the performance equations we learnt to?
- ▶ It is clear that  $T_1$  is a second-order system while  $T_2$  and  $T_3$  are third order systems
- ▶ There is a frequency component  $\omega_n = \sqrt{24.542} = 4.954$ , therefore  $\zeta = 4/(2 \cdot 4.954) = 0.4037$ , so  $T_1$  is an underdamped system
- ▶ We notice that  $T_2$  and  $T_3$  have identical complex poles like  $T_1$  but with extra real poles, one at -10 for  $T_2$ , and one at -3 for  $T_3$ , so expect the shapes of  $T_2$  and  $T_3$  to have similar shapes to  $T_1$ , but the effect of the dampening by the extra real pole will change them.
- ▶ We must know if the new shape will still resemble a second order system, so that we can approximate the third-order system as a second-order system and use the equations or not.

$$T_1(s) = \frac{24.542}{s^2 + 4s + 24.542}$$

$$T_2(s) = \frac{245.42}{(s+10)(s^2 + 4s + 24.542)}$$

$$T_3(s) = \frac{73.626}{(s+3)(s^2 + 4s + 24.542)}$$

فهل يمكن تطبيق المعادلات ههنا  
 الـ 10 ابعثر 5 مرات عن الـ 2 فبالتالي  
 second order

matlab نرسم Plot لكل system ونشوف اي واحد اقرب

ممكن باستخدام الـ  
 second order

## Solutions- Numerical

- ▶ We should find the location of the complex poles, and see if the real pole is five times further away to the left
- ▶ We know from the equations that the complex pole location will be at  $-\zeta \omega_n = -\sigma/2 = -0.4037 \times 4.954 = -2$
- ▶ For  $T_2$ ,  $\alpha_r = -10$  which five times larger than -2, so this system can be approximated as a 2<sup>nd</sup> order system. We can use the equations we learnt for settling time, overshoot, rise time, and peak time to **APPROXIMATE** the solutions.
- ▶ For  $T_3$ ,  $\alpha_r = -3$  which 1.5 times larger than -2, this system **cannot** be approximated as a 2<sup>nd</sup> order system. We cannot use the equations we learnt for settling time, overshoot, rise time, and peak time.

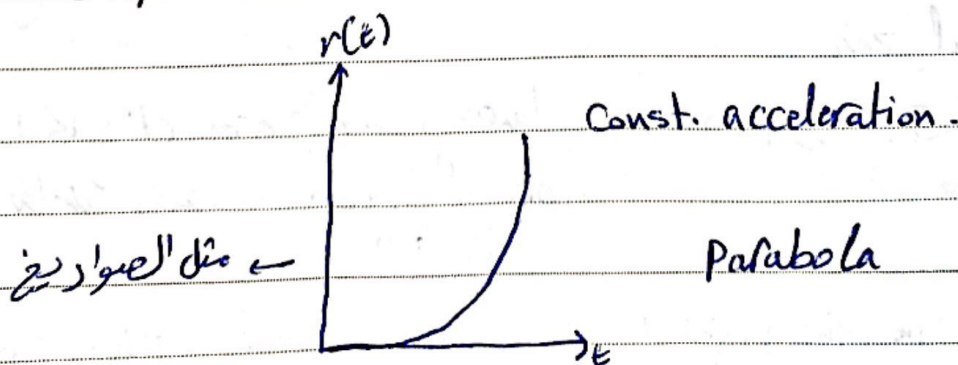
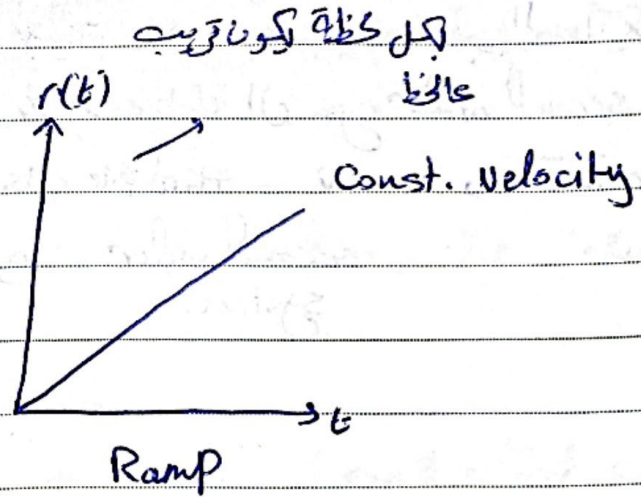
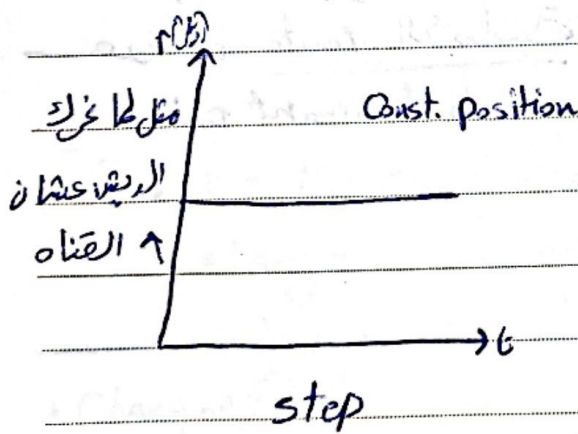
"steady-state error"

• Step inputs represent constant position and thus are useful in determining the ability of the control system to position itself with respect to target.

• Ramp inputs represent constant-velocity inputs to a position control system by their linearly increasing amplitude

• Parabolas, represent constant acceleration inputs to position control systems.

• So, inputs :-



• steady-state error reasons :-

- 1) our assumptions were that the systems are linear, but in reality they are not linear.
- 2) initially systems work as linear then non-linear
- 3) related to the design of the control systems

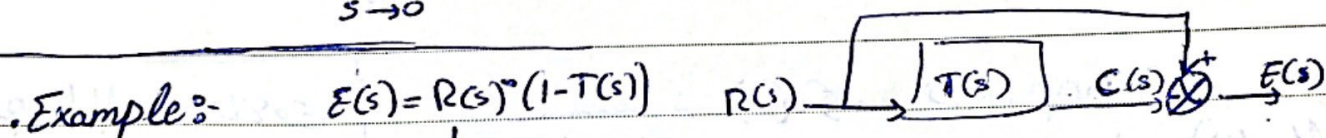
$$e_{\text{steady-state}} = \frac{1}{k} C_{\text{steady-state}}$$

• كلما زاد error قل خطأ و كلما زاد  $k \approx \infty$  و مستقر يكون  $\infty$

• Final Value Theorem

• هدفنا انه كل ما يقرب من الوقت ال error يقرب للعرض و عند  $t = \infty$  نعتبر "0"

$$e(\infty) = \lim_{s \rightarrow 0} s E(s)$$



$$E(s) = \frac{s^2 + 7s + 5}{s(s^2 + 7s + 10)}$$

$$e(\infty) = \lim_{s \rightarrow 0} s E(s)$$

```

in matlab
syms s
E = " "
limit(s * E, s, 0)
ans = 1/2
    
```

دائماً اول خطوة كان

نبدأ من ان ال system يكون stable عن

طريقة ال poles

لكل ال system (زائد مستقر) (stable)

↓ نعتبر قيمة عالية

ال system ال 50% عن ال steady-state

slide 9

$$e(\infty) = \lim_{s \rightarrow 0} \frac{S R(s)}{1+G(s)}$$

ideal

↳ the answer may = 0 → ~~the~~ case

↳ " " " be finite

↳ " " " be infinite (error ليس)

ال stability حسب ال  
system poles و zeros  
ال sys. و poles (s) f(s)

closed-loop system مع unity feedback

• يتغير R(s) بالانواع (step / ramp / parabola)

1) step input (on/off) →  $e(\infty) = \frac{1}{1 + \lim_{s \rightarrow 0} G(s)}$   $(\lim_{s \rightarrow 0} G(s)) = k_p$   
↳  $\frac{1}{s}$  (1 uct)

2) ramp input →  $e(\infty) = \frac{1}{\lim_{s \rightarrow 0} s(G(s))}$   
(1t uct) ↳  $\frac{1}{s^2}$

3) parabola input →  $\frac{1}{\lim_{s \rightarrow 0} s^2 G(s)}$   $k_v$   
(1t^2 uct) ↳  $\frac{1}{s^3}$

بمعنى ال stability  
يكون ال error = 0  
عن طريق ال poles  
فيكون ال error = ∞

↳  $\lim_{s \rightarrow 0} s^2 G(s) = k_a$

• يعني حسب  $k_p / k_v / k_a$  يكون ال error في كل نسبة ال poles ال  
و عشان تكون  $\lim_{s \rightarrow 0} G(s) = \infty$  لازم يكون في "s" اضافية و ال "s" اضافية  
↳ Integrator inputs ال ال

• في حال طلع لنا RHP poles، يعني ال system يكون unstable، عننا يكمل حل وها بنطلع  $e(\infty)$ .

• Note:  $k_v / k_p / k_a \rightarrow$  static error constants

- "Poly" Command  $\rightarrow$  roots ال  $\Delta$  استخدم ال roots
- "TF" Command  $\rightarrow$  transfer functions
- "Pole" Command  $\rightarrow$  same as roots ~~ال poles~~

• لما تكون "s" اضافية وحدة :- يكون ال step جوابه finite

ال ramp جوابه finite

ال parab. جوابه infinite

• لما تكون "s<sup>2</sup>" اضافية وحدة :- " " " " " " " " " " " "

" ramp " " " " " " " " " " " "

" parab. جوابه finite " " " " " " " " " " " "

• "dcgain" Command  $\rightarrow$  حساب ك ما بالاشارة

بسن لازم نكتبه حالة  $k_a / k_v$

• بتكون  $G(s)$  مخرجها بـ "s" و "s<sup>2</sup>" قبل dcgain

بسنستخبر  $\hookrightarrow$  com

• كل ما نزيد عدد ال integrators قبل ال error

و دا ئماً لما يكون عننا او مخرجنا قيم ال  $k$  يعني stable system

• Steady-State errors with disturbances ( $D(s)$ )

• we will assume that  $D(s) = \frac{1}{s}$  "step funct."

• when we apply Final Value theorem

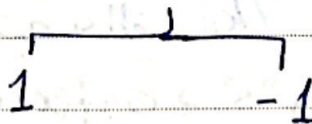
$$e_D = - \frac{1}{\lim_{s \rightarrow 0} \frac{1}{G_2(s)} + \lim_{s \rightarrow 0} G_1(s)} \quad (\text{error due to disturbance only})$$

↑ dc gain of  $G_1(s)$  ↓ error by disturbance  
 ↑ dc gain of  $G_2(s)$  ↓ error by disturbance

فإذا كان نقل الخطأ الكارثي من  $G_1$  ونقل  $G_2$  (dc gain) إلى الأمامية يتم تطبيقه على ال forward path. وال  $conv$  لا يكون بين المسارين  $G_1$  و  $G_2$  يعني سلاسل  $G_1$  و  $G_2$  في خط.

• Steady-state error for Nonunity feedback system

↳ ليحول إلى unity feedback



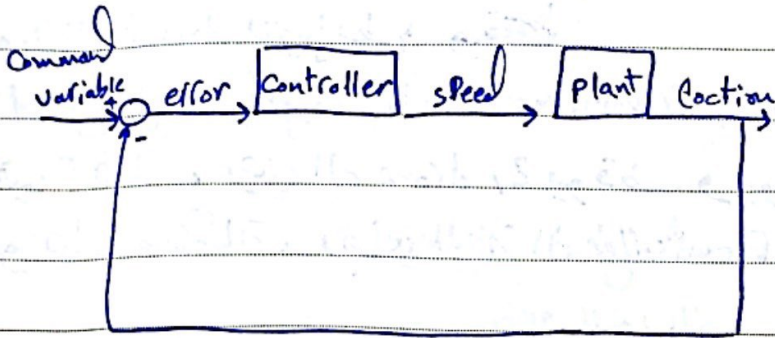
slide 27 →  $e(\infty) = -4$

↳ يعني لو ال steady-state كانت 5 وضواظلي 20 وهاد خطأ ليس.

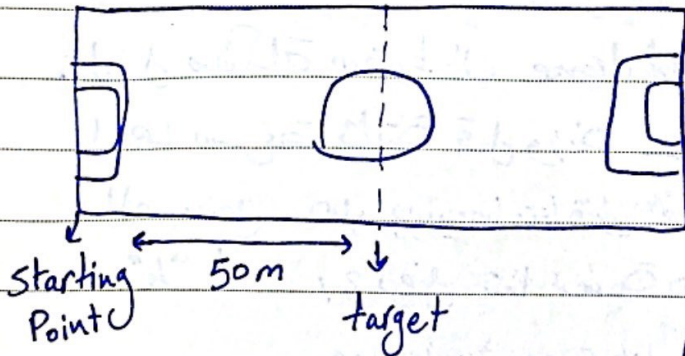
# "Quick Intro to PID Controllers"

.. PID controller → most famous type of controllers that is designed using software or hardware

.PID → 3 controllers



Proportional integral derivative  
 يمكن يكون P أو PI أو PD أو PID



⇒ input = target = 50m  
 feedback → target - current point = error  
 ↑ current point ↓ error

. Here the input command is Proportional with the error.

بالبداية ال controller يعطي امر بالحسي بسرعة باتجاه ال target، وكل ما قرب من ال target بتتغير الحركة ابطى كلما يوقف



Proportional control → مكون من block وحدة

يكون جواتفا "k" بالبداية بتكون ك كبيرة وبتقل لتوصل لوقف يعني Proportional لقيمة k.



target

هذا غيرنا ان application  
و صار drone .

50 meters

• سرعة المرواح بالبدائية يتكون

كالية لانه بعيد عن target

فال error عاي ، وكل ما يقرب

من target بتغير بطرئ

لما يوصل ال target ال Proportional 2 ، يعطي

قيمة صفر ، يعني ال drone 2 يوقف و يوقع .

و هاي مشكلة ، رهاي الحالة ال P controller ما بزيجا .

Start Point

عندما ال error  
يكون 50

• ال Proportional يعني Present control لانه بس يشتغل على الوضع الحالي .

• لنحل مشكلة سقوط ال drone لما يوصل ال target لازم يكون المرواح

الها سرعة ثابتة قبل وزنه . بس المشكلة هون هارت ان

ال gain هار يزيد ما يتناقص فليك و كمره بوصل ال drone ال 50

"k" 2 ، يعني عنا نسبة ثابتة (steady-state error)

→ lets assume we need 100 rpm to hover

$$\text{Error} \times \text{Gain} = 100 \text{ rpm (speed)}$$

$$50 \times 2 = 100$$

$$20 \times 5 = 100$$

$$10 \times 10 = 100$$

$$1 \times 100 = 100$$

ال حل - تحول من P-controller ل PI

• ال Integral controller بسحرم

They remember  
the Past

as is they have memory.

ال P-controller, 2 يعمل وظيفته ويوصل ال drone لارتفاعه

بتكون به تراقب كيف الخطأ يقل

ال I-controller يستعمل بعد ال P-controller، يشوف ال steady state error ويعطيه اوامر حتى يرفعه ال target ويقل يلف بسرعة محددة

ال إضافة ال integrator يعني إضافة block ال hardware او code

المشكلة صارت لما يعطي ال integrator امر معين انتقال ليس عن overshoot

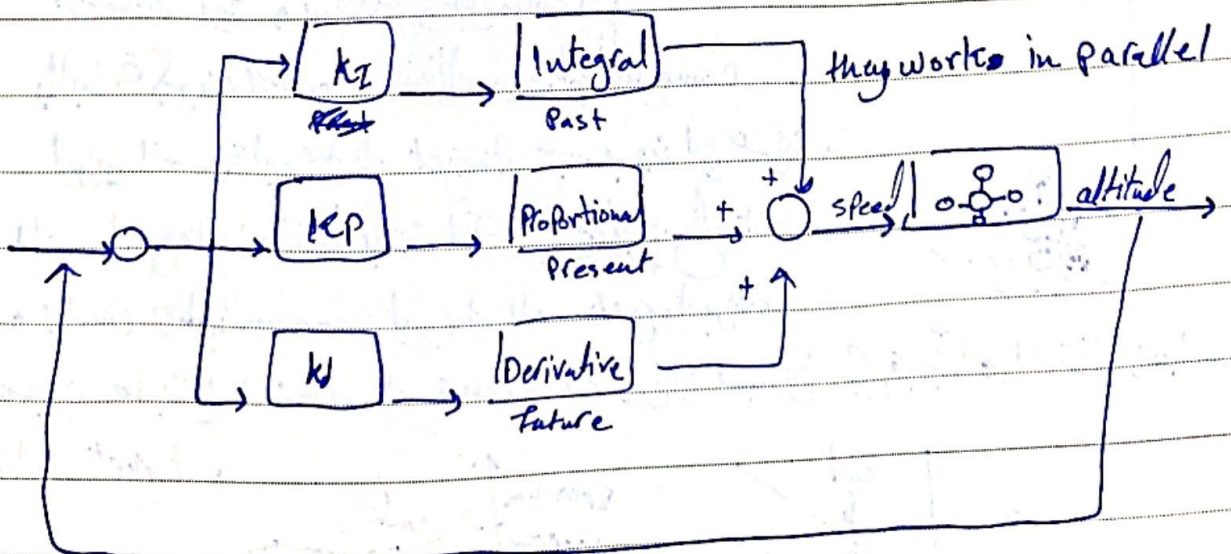
ويطلع عن ال target فلازمنا Controller يعرف المستقبل

فينستخدم ال derivative ال وظيفتها تراقب معدل التغير في الخطأ

وبناءً على معدل التناقص أو التسارع يعطي اوامر اذا ال drone

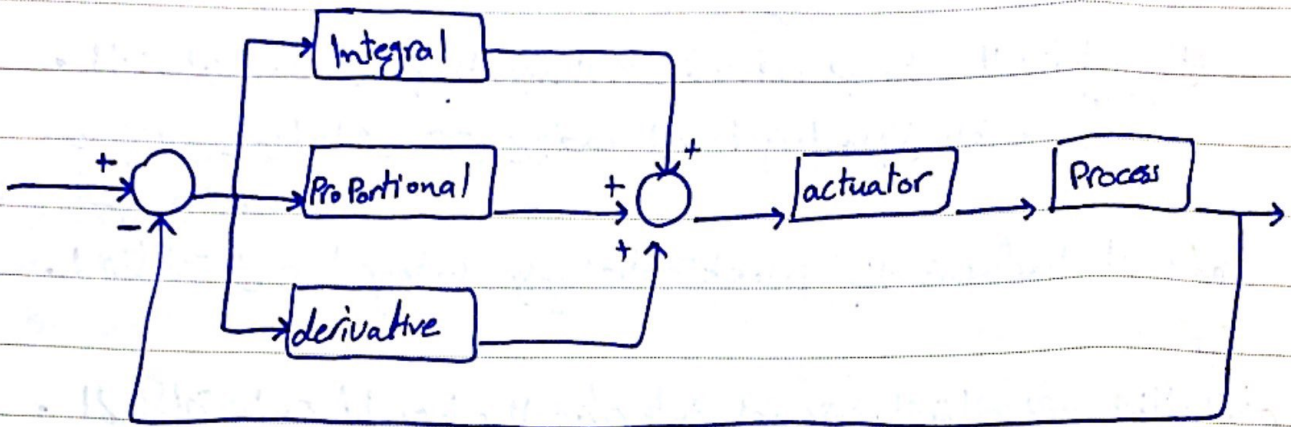
صارت بعدها تطلع عن ال 50 meter وليس يعطي اوامر باقائه معاكس

من شرط بكل ال Applications يكونوا ال 3 موجودة



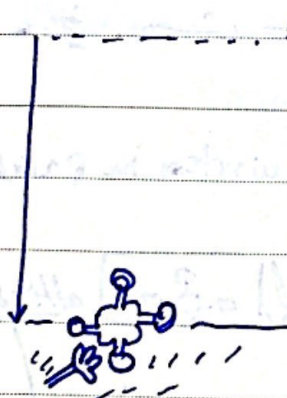
they work in parallel

# PID control



في مشاكل بتظهر ما يسمى ال integral wind

## Integral wind up problem



لتفرض نحتاج المثال انه شغله ما سلك ال drone ليه و شغله و فعل ما سلكه

بالدابة يكون P-controller شغال و يعطي command

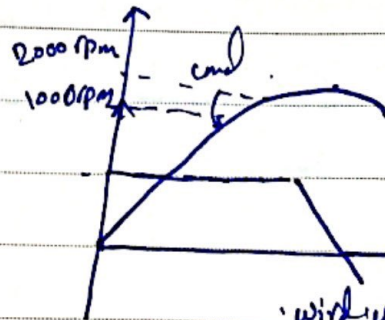
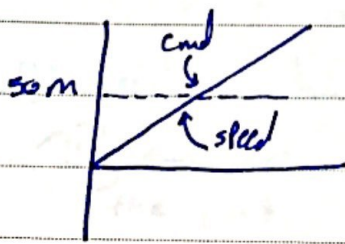
ليزيد السرعة ليوصل ل target بسرعة بدون اي مشكلة

ال integral وقتها بتفقد انه في steady-state error

و يبلش يعطي command ليوصل ل target برفيق

مجرد ما يترك الشغله ال drone 21 يرتفع لبطء جيت جيت و الانتقال يتجاوزه

ال target



تقدر ال 1000 و لبعه

ال 2000 لبقه ببطء

للموقع الصحيح wind up problem

How to solve the wind up Problem?  
using Clamping

Clamping → عبارة عن circuit أو if-statement بين ال Controller وال actuator

• بينما نتأكد انه الأوامر التي بتطبع من ال Controller بتجاوز طاقة ال actuator و 88. مثلا لو كانت سرعة الدوران الأقصى لل drone بتساوي 1000، لو أعطى ال Controller أمر أكثر من 1000 يضل 1000، ما بغير command بيزيد (كاسف if-statement).

كانا 1000 حسب المثال السابق.

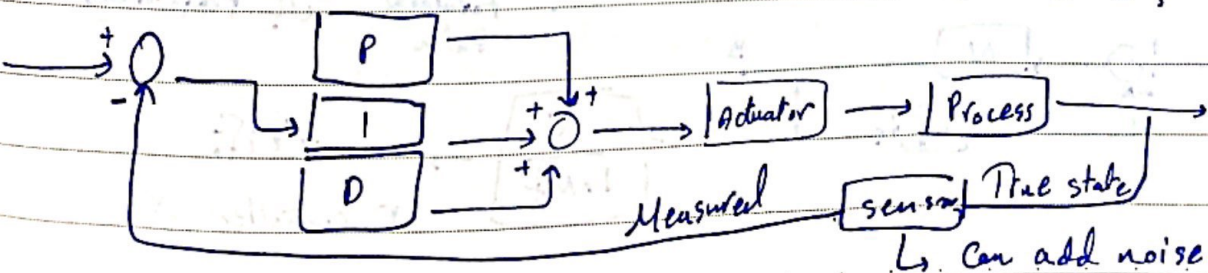
88 تحقق شرطية بال Clamping :-

1) يجب لو وصل ال saturation لفضل عندها  
2) إذا ~~كان~~ لازم يتحرك لطول وشارة ال error موجبة، او لازم يتحرك لتحت وشارة ال error سالبة، اذا تسادوا بالاشارة لازم ما يكمل حركة.

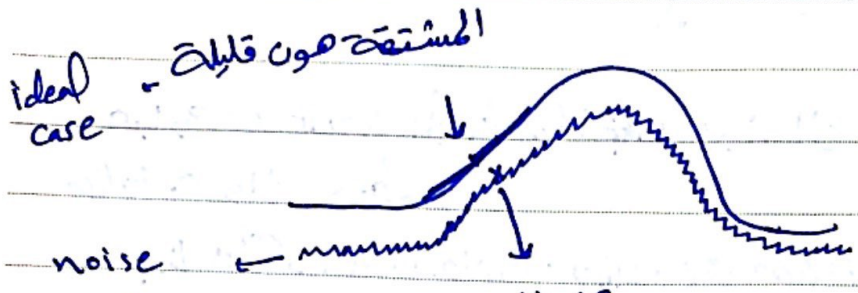
لما يتحقق الشرطية يفضل ال integrator

• شو القيمة التي لازم أعطها ال Clamping؟ مثلا لو كانت الطاقة الاستيعابية هي 1000 rpm، فهل ال Clamping اعطها 1000؟ دايماً بنحطه أقل (900) مثلا، لانه مع الزمن طاقتة الأقصى رح تقل.

المسائل التي بتواجه ال derivative سببها الرئيسي هو ال noise بال sensors



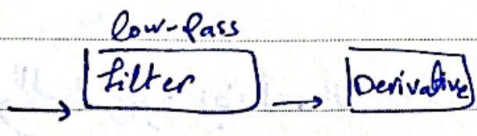
ال derivative يعتمد على معدل التغير في الخطأ ، و اي هو المشتقة



signal عند نفس النقطة ، ولانه ان  
 ما يلة هار معدل الخطأ كمين  
 واصبحت قراءات ال D خاطئة .

ال ال ← استخدام Filter ، و ههنا ال Low-pass Filter  
 attenuation يجب ان frequency العاليه

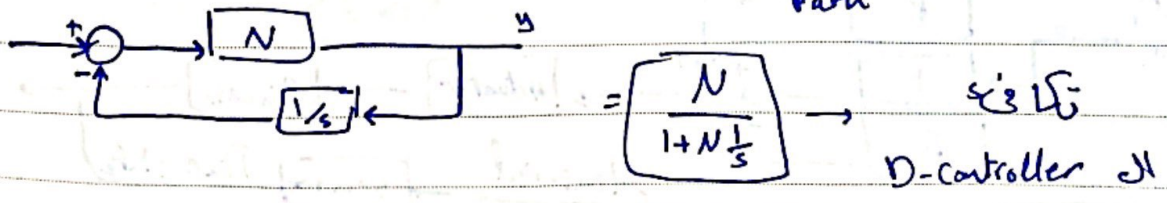
ال Low-pass filter ال cut-off freq. ال اي ههنا ال اي ههنا ال اي ههنا



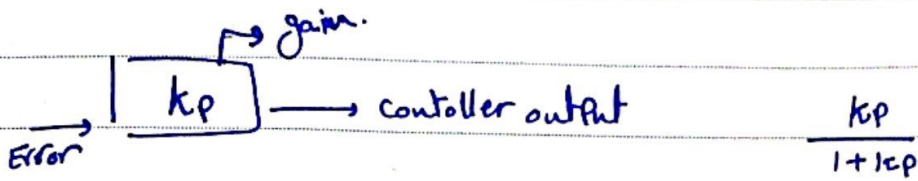
laplace	what is it
S	derivative
1/S	integral
N/(S+N)	low Pass with cut-off = N

المشتقة بنفرد بي والتكامل ننفرد س .  
 و ههنا انه التصفيم لنا ب ال filter  
 هو  $(\frac{N}{S+N})$  وال N هو ال cut-off

بنفرد ال low pass مع ال derivative ب استخدام ال integral ال feedback  
 ال Proportional ال Forward Path



## P-controller



- كلما زاد قيمة ال gain قل نسبة الخطأ
- كلما زاد ال gain قل نسبة الخطأ بـ مستحيل توصل للعز
- لو كانت ال gain تساوي  $\infty$  وفاد مستحيل

- أهمية وجود ال P انه يقلل من ال disturbances
- كلما ازيد قيمة kp يقل ال disturbance ~~و يقل damping~~ ~~و يقل overshoot~~
- ~~و ليس smoother~~ smoother

## PD-controller

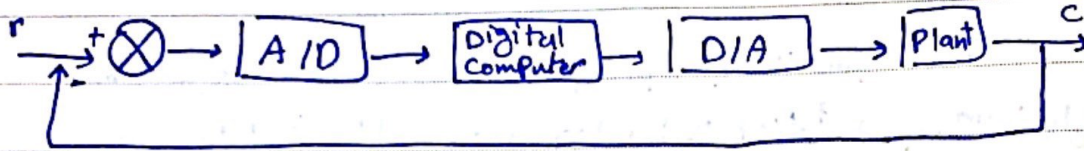
- ال P يقلل ال disturbance وال D يقلل ال oscillation
- ويقل smoothing ال signal وهذا اثر كبير مرغوب
- زيادة ال kd بتزيد ال damping ratio فيقل ال oscillation وال ~~under-damped effect~~
- " يقل damping ال overshoot "

## PI-controller

- ال I وظيفته الأساسية تمنع الخطأ من ال system وال steady-state

- اهتمنا، نوع ال controller بقدرى نوع ال system وطبيعته.

## "Brief Introduction to Digital control"



• digital control → based on software (digital computer)

- A/D → Analog to digital (from sensors)
- D/A → Convert the digital commands to analog (digital to analog).  
↳ ex:- PWM "Pulse width modulation".

• Analog signals are contin. in time and in range.

- A/D → discretization the analog signal  
↳ both time and range

A/D (2 circuits)

Sampling      Quantizing

take a sample and  
hold it (discretization of time)

↳ discretization of  
range

ex:-  $V(1 \rightarrow 2) = 0$

• remember :-  $f_{\text{sampling}} = 2f_{\text{max}}$

• n-bit A/D  $\rightarrow$  # of levels =  $2^n$

$\uparrow$  # of levels

• more accurate

• slower

• more expensive

• A/D  $\equiv$  ADC

• ZOH  $\rightarrow$  generates the stair-step approximation. (discrete values)  
 $\hookrightarrow$  sample and hold circuit.

• example: 3-bit A/D with range from 0V to 5V

$\hookrightarrow$  we have 8 levels

• range of each level  $\rightarrow \frac{5-0}{8} = 0.625$

•  $0 \rightarrow 0.625 \rightarrow 000$

•  $0.625 \rightarrow 1.25 \rightarrow 001$

•  $1.25 \rightarrow 1.875 \rightarrow 010$

!

etc

في مشكلة - نسبة خطأ عالية لانه صلا بعض 0 و 0.625 في الأخطاء  
مع انه الأقرب اليها 1 001 لكل تزيد ال resolution عن طريق  
زيادة عدد ال levels.

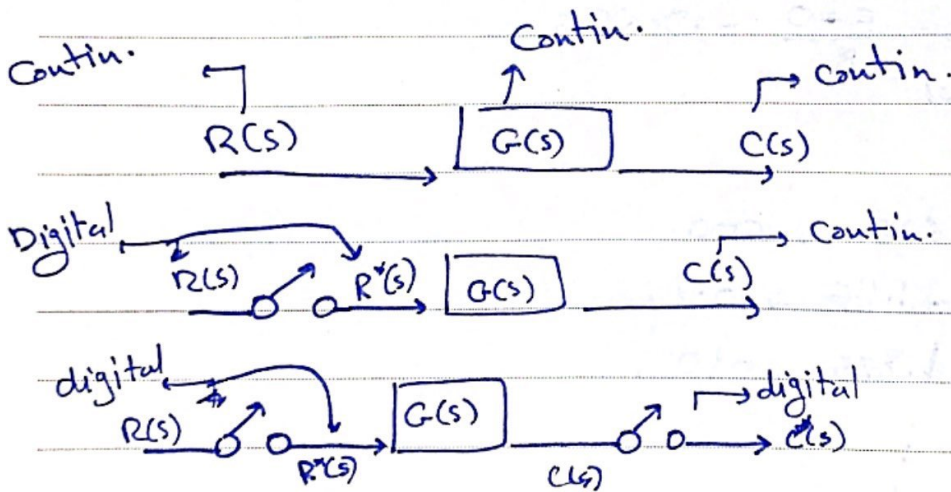
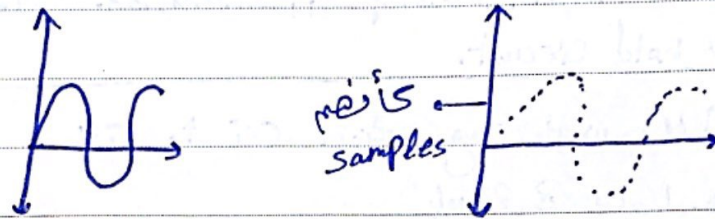
• The laplace transform for the zero-hold circuit is given by :-

$$G_h(s) = \frac{1 - e^{-Ts}}{s} \quad \text{where } T = \text{sampling period.}$$



• Ztrans (From time domain to frequency domain for discrete values/signals)  
 ↳ instead of Laplace command in Analog.

- $n \rightarrow$  instead of  $t$  / •  $z \rightarrow$  instead of  $s$
- Contin. time  $\sin(\omega t)$       • discrete time  $\sin(\omega n)$



↳ Phantom (imaginary)

"...physically ...  
 discrete ال تعبير عن"

- C2d  $\rightarrow$  convert the block to digital block  
 $G(s) \rightarrow G(z)$



↓  
Contin.

↓  
≡

$$R(z) \rightarrow \boxed{G_2 G_1(z)} \rightarrow C(z)$$

but if there is a sampling switch between  $G_1(s)$  and  $G_2(s)$

$$R(z) \rightarrow \boxed{G_2(z) G_1(z)}$$

أي رقم output و هو ال output ليس input  
 و رقم ثاني (يعني يكون output الثاني) - يعني  
 يعني Phantom sampler

Phantom يمكن تغييره على نظام التردد  
 sampler -> ب يكونوا على نفس ال sampling frequency

then we can start  
 with block simplification

- In digital systems stability

↳ take the magnitude of poles

- if the magnitude  $< 1 \rightarrow$  stable
- " " "  $> 1 \rightarrow$  unstable
- if there is only one "1"  $\rightarrow$  marginally stable
- if there are more than one root with magnitude  $= 1 \rightarrow$  unstable.

• remember :- magnitude of complex numbers

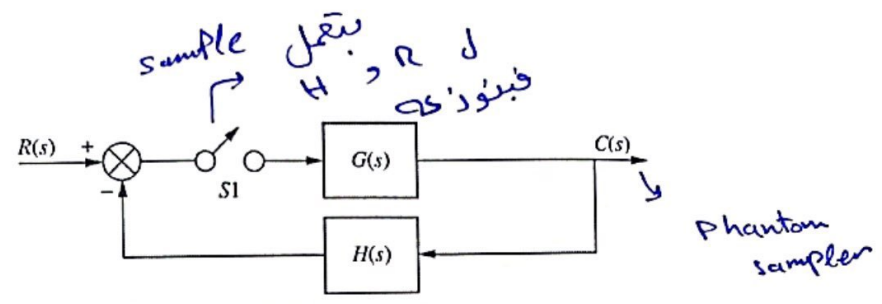
$$= \sqrt{a^2 + b^2} \quad \text{or use abs() command}$$

• why does the sampling rate affects the stability of the system?

• لماذا يؤثر معدل أخذ العينات على استقرار النظام؟  
تكون الأجزاء من سرعة التشغيل مستجابة للسرعة.

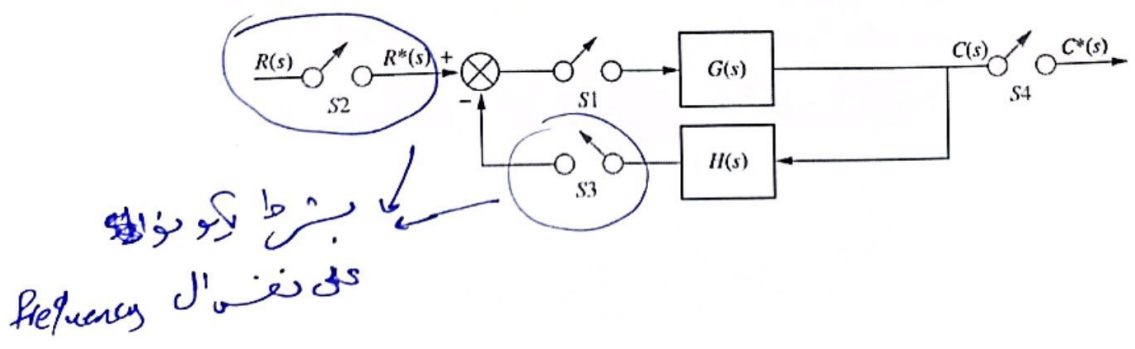
• Hardware in the loop  $\rightarrow$  in simulink "matlab", to test the hardware on sampling rate or parameter values

# Digital Block Simplification Example

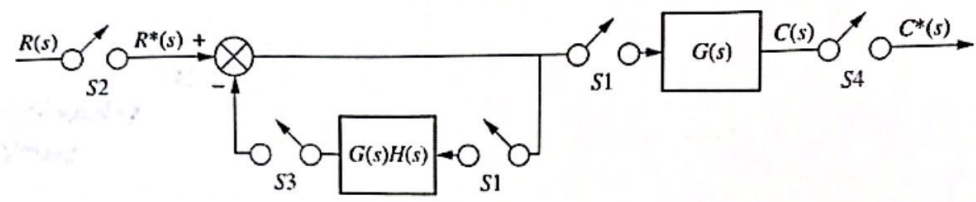


# Digital Block Simplification Example – cont.

► Adding Phantom samplers per the rules

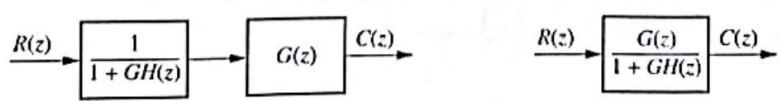
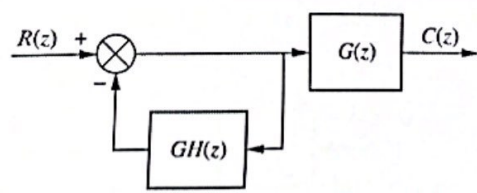


# Digital Block Simplification Example – cont.



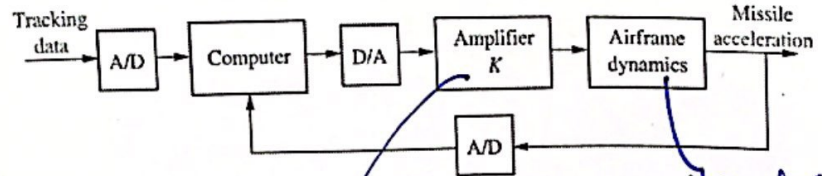
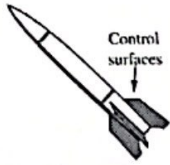
عشان نفقق شرط  
sample-block-sample

# Digital Block Simplification Example – cont.



# Example

- ▶ The missile shown can be aerodynamically controlled by torques created by the deflection of control surfaces on the missile's body. The commands to deflect these control surfaces come from a computer that uses tracking data along with programmed guidance equations to determine whether the missile is on track. The information from the guidance equations is used to develop flight control commands for the missile. A simplified model is shown as well.
- ▶ Here the computer performs the function of controller by using tracking information to develop input commands to the missile. An accelerometer in the missile detects the actual acceleration, which is fed back to the computer.
- ▶ Find the closed-loop digital transfer function for this system and determine if the system is stable for  $K = 20$  and  $K = 100$  with a sampling interval of  $T = 0.1$  second.

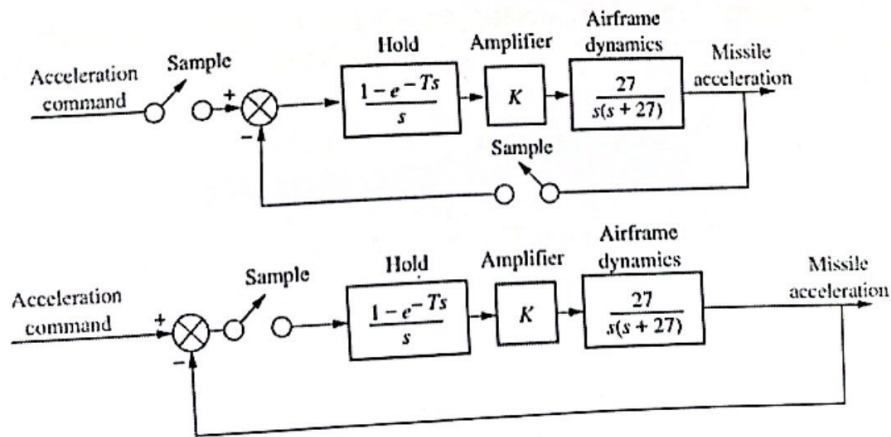


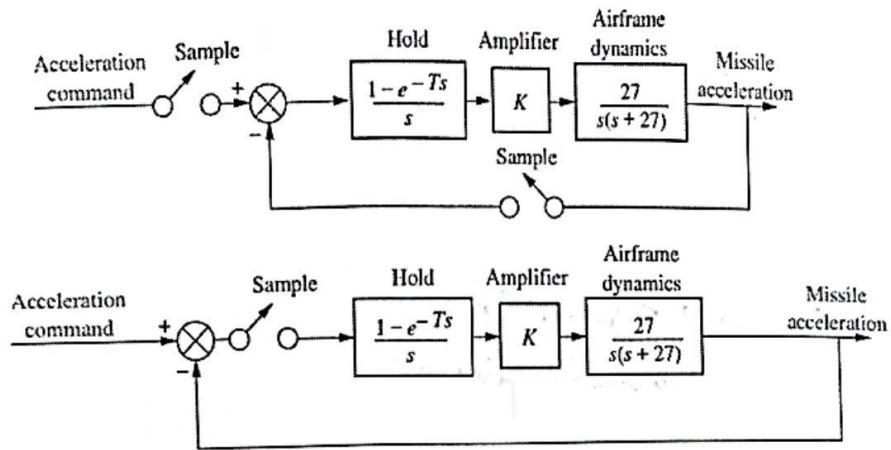
Computer  $\equiv$  ZOH circuit.

عشان تزیر ال Voltage  
 بكون ال قيمة متغير  
 مصنوعة تزیر عندها

Analog system

# Example - cont.





## Example MATLAB Solution I

30

بجاء في التمرين  
مع ال zoh في البداية

$s^2 + 27s$

```

numg=27;           % Define numerator of Ga(s).
deng=[1 27 0];    % Define denominator of Ga(s).
Ga=tf(numg,deng); % Create and display Ga(s).

Gz=c2d(Ga,0.1,'zoh') % Find G(z) assuming Ga(s) in cascade with z.o.h. and display.

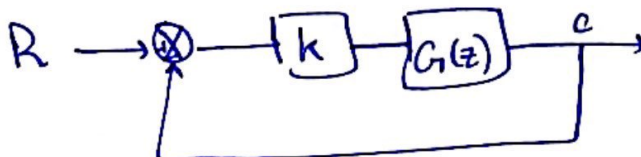
```

```

Gz =
      0.06545 z + 0.02783
-----
      z^2 - 1.067 z + 0.06721
Sample time: 0.1 seconds
Discrete-time transfer function.

```

↳ given  
التميز كجول  
L  
قياس K



## Example MATLAB Solution II

50 system

```

for K=1:0.1:50; % Set range of K to look for % stability.
    Tz=feedback(K*Gz,1); % Find T(z).
    r=pole(Tz); % Get poles for this value of K.
    rm=max(abs(r)); % Find pole with maximum absolute value for this value of K.
    if rm>=1, % See if pole is outside unit circle.
        break; % Stop if pole is found outside unit circle.
    end
end
display(K)

```

K = 33.6000

display(r)

```

r = 2x1 complex
   -0.5660 + 0.8257i
   -0.5660 - 0.8257i

```

→ في قيمة K هذه النظام unstable

## Steady-State Errors in Digital Systems

- ▶ Any general conclusion about the steady-state error is difficult because of the dependence of those conclusions upon the placement of the sampler in the loop.
- ▶ Remember that the position of the sampler could change the open-loop transfer function.
- ▶ In the discussion of analog systems, there was only one open-loop transfer function,  $G(s)$ , upon which the general theory of steady-state error was based and from which came the standard definitions of static error constants.
- ▶ For digital systems, however, the placement of the sampler changes the open-loop transfer function and thus precludes any general conclusions. In this chapter, we assume the typical placement of the sampler after the error and in the position of the cascade controller, and we derive our conclusions accordingly about the steady-state error of digital systems



Good  
Luck!

