



# EMI

DR YANAL ALFAOURI

DONE BY

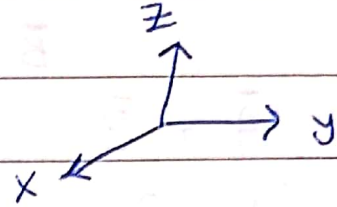
DANA ALMOGHRABI

 **POWERUNIT** 

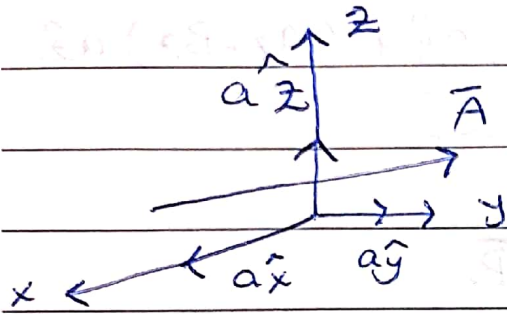
Vector  $\rightarrow$  magnitude and direction.  $(\vec{A})$

Scalar  $\rightarrow$  magnitude only.  $(A)$

in cartesian coordinate :-



mutually orthogonal axes



$\hat{a}_x$  = unit vector, has a magnitude that equals (1) and its direction is towards the x-axis.

$$\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z \quad (\text{This is the long format})$$

$A_x, A_y, A_z \rightarrow$  vector components

$\hat{a}_x, \hat{a}_y, \hat{a}_z \rightarrow$  unit vectors

$$\vec{A} = (A_x, A_y, A_z), \quad (\text{This is the short format})$$

vector magnitude  $|\vec{A}| :-$

$$|\vec{A}| = A = \sqrt{A_x^2 + A_y^2 + A_z^2}$$

vector direction :-

$$\hat{a}_A = \text{unit vector along } \vec{A} = \frac{\vec{A}}{A}$$

\* Operations on vectors :-

[1] Addition  $\Rightarrow \vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$

$\vec{B} = B_x \hat{a}_x + B_y \hat{a}_y + B_z \hat{a}_z$

$\vec{C} = \vec{A} + \vec{B}$

$= (A_x + B_x) \hat{a}_x + (A_y + B_y) \hat{a}_y + (A_z + B_z) \hat{a}_z$

$= C_x \hat{a}_x + C_y \hat{a}_y + C_z \hat{a}_z$

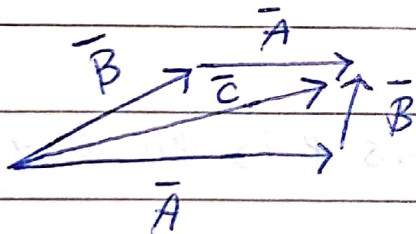
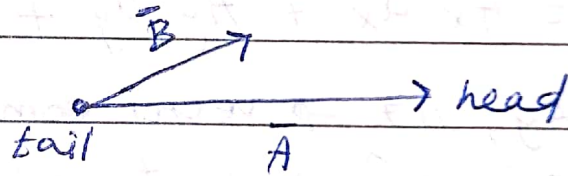
[2] Subtraction  $\Rightarrow \vec{D} = \vec{A} - \vec{B}$

$= (A_x - B_x) \hat{a}_x + (A_y - B_y) \hat{a}_y + (A_z - B_z) \hat{a}_z$

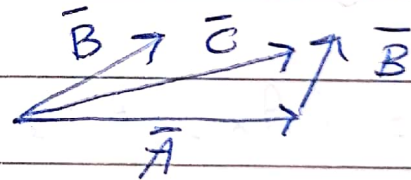
$= D_x \hat{a}_x + D_y \hat{a}_y + D_z \hat{a}_z$

Graphical :-

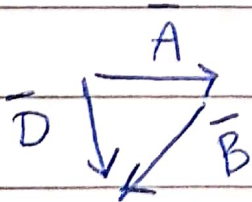
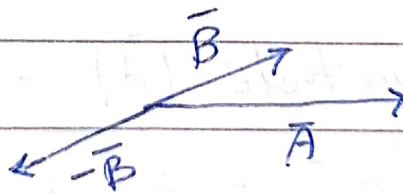
$\vec{C} = \vec{A} + \vec{B}$



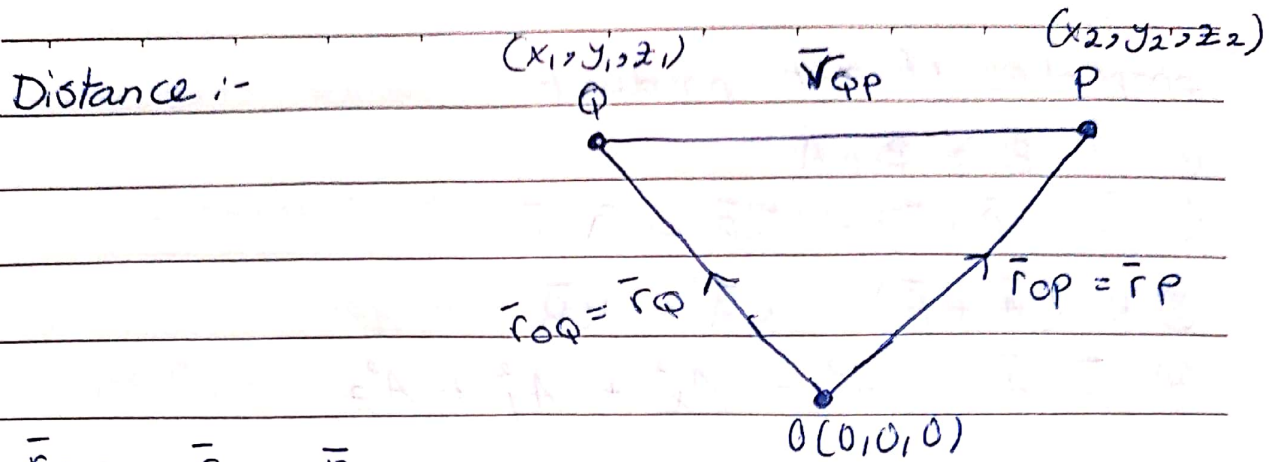
(or)



$\vec{D} = \vec{A} - \vec{B}$







$$\begin{aligned} \vec{r}_{QP} &= \vec{r}_P - \vec{r}_Q \\ &= (x_2, y_2, z_2) - (x_1, y_1, z_1) \\ &= (x_2 - x_1) \hat{a}_x + (y_2 - y_1) \hat{a}_y + (z_2 - z_1) \hat{a}_z \\ &= -\vec{r}_{PQ} \end{aligned}$$

$$r_{QP} = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$

$$\hat{a}_{r_{QP}} = \frac{\vec{r}_{QP}}{r_{QP}}$$

[3] Multiplication  $\Rightarrow$    
 $\left\{ \begin{array}{l} \text{Dot product (scalar)} \\ \text{cross product (vector)} \end{array} \right.$

(A) Dot product :-  $\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta_{AB}$

if  $\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$

$\vec{B} = B_x \hat{a}_x + B_y \hat{a}_y + B_z \hat{a}_z$

Then  $\vec{A} \cdot \vec{B} = A_x B_x + A_y B_y + A_z B_z$

$\hat{a}_x \cdot \hat{a}_x = (1)(1) \cos 0^\circ = 1$

$\hat{a}_x \cdot \hat{a}_y = (1)(1) \cos 90^\circ = 0$

$\cos \theta_{AB} = \frac{\vec{A} \cdot \vec{B}}{AB}$  then  $\theta_{AB} = \cos^{-1} \frac{\vec{A} \cdot \vec{B}}{AB}$

$\hat{a}_n \cdot \hat{a}_m = 0$  if  $n \neq m$   
 $= 1$  if  $n = m$



properties of dot product :-

$$\textcircled{1} \bar{A} \cdot \bar{B} = \bar{B} \cdot \bar{A}$$

$$\textcircled{2} \bar{A} \cdot (\bar{B} + \bar{C}) = \bar{A} \cdot \bar{B} + \bar{A} \cdot \bar{C}$$

$$\textcircled{3} K(\bar{A} + \bar{B}) = K\bar{A} + K\bar{B}$$

$$\textcircled{4} \bar{A} \cdot \bar{A} = A^2 = A_x^2 + A_y^2 + A_z^2$$

(B) Cross product :-  $|\bar{A} \times \bar{B}| = AB \sin \theta_{AB}$

$$\theta_{AB} = \sin^{-1} \frac{|\bar{A} \times \bar{B}|}{AB}$$

$\bar{A} \times \bar{B} =$	$a_x \hat{x}$	$a_y \hat{y}$	$a_z \hat{z}$
	$A_x$	$A_y$	$A_z$
	$B_x$	$B_y$	$B_z$

$$= a_x (A_y B_z - A_z B_y) - a_y (A_x B_z - A_z B_x) + a_z (A_x B_y - A_y B_x)$$

$$|a_x \hat{x} \times a_y \hat{y}| = (1)(1) \sin 90^\circ = 1$$

$$|a_x \hat{x} \times a_x \hat{x}| = 0$$

properties of cross product :-

$$\textcircled{1} \bar{A} \times \bar{B} \neq \bar{B} \times \bar{A}$$

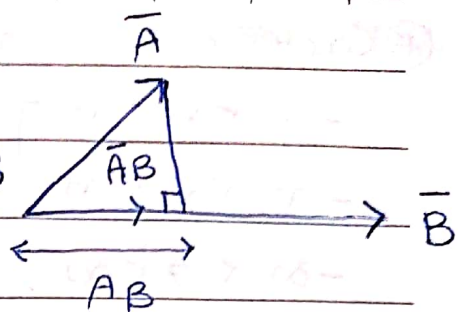
$$\textcircled{2} \bar{A} \times \bar{B} = -\bar{B} \times \bar{A}$$

$$\textcircled{3} \bar{A} \times (\bar{B} + \bar{C}) = (\bar{A} \times \bar{B}) + (\bar{A} \times \bar{C})$$

\* Components of a vector :-

$AB$  = scalar projection of  $A$  along  $B$

$\vec{AB}$  = vector projection of  $A$  along  $B$



$$\cos \theta_{AB} = \frac{AB}{A}$$

$$AB = A \cos \theta_{AB}$$

$$\cos \theta_{AB} = \frac{\vec{A} \cdot \vec{B}}{AB}, \quad \hat{a}_B = \frac{\vec{B}}{B}$$

$$= \frac{\vec{A} \cdot \hat{a}_B}{A}$$

$$AB = \vec{A} \cdot \hat{a}_B$$

so  $\vec{AB} = AB \hat{a}_B$

=  $(\vec{A} \cdot \hat{a}_B)$ , if scalar

=  $(\vec{A} \cdot \hat{a}_B) \hat{a}_B$ , if vector

Example :- Given  $\vec{A} = 3a_x + 4a_y + a_z$

$$\vec{B} = 2a_y - 5a_z$$

find :  $\theta_{AB}, AB, \vec{AB}$  ?

Sol  $\theta_{AB} = \cos^{-1} \frac{\vec{A} \cdot \vec{B}}{AB} = \cos^{-1} \left( \frac{3}{\sqrt{26} \sqrt{29}} \right) = 83.73^\circ$

$$\vec{A} \cdot \vec{B} = 0 + 8 + -5 = 3, \quad A = \sqrt{26}, \quad B = \sqrt{29}$$

$$AB = \vec{A} \cdot \hat{a}_B = \frac{8-5}{\sqrt{29}} = \frac{3}{\sqrt{29}} = 0.557, \quad \hat{a}_B = \frac{(0, 2, -5)}{\sqrt{29}}$$

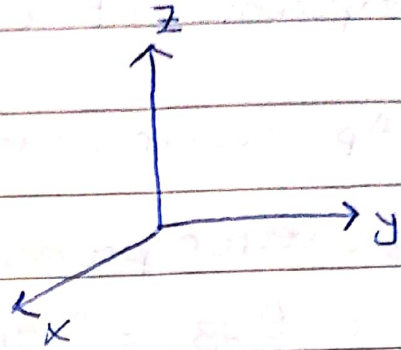
$$\vec{AB} = AB \hat{a}_B = \frac{3}{\sqrt{29}} \left( \frac{(0, 2, -5)}{\sqrt{29}} \right) = \frac{6a_y - 15a_z}{29}$$

$$= 0.207a_y - 0.517a_z$$

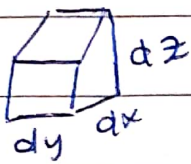


⊕ Cartesian coordinate :-

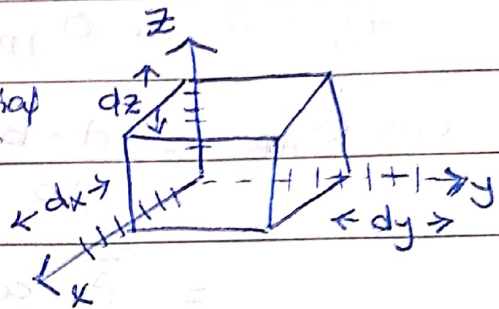
- $-\infty < x < \infty$
  - $-\infty < y < \infty$
  - $-\infty < z < \infty$
- } 3D object  
infinite solid  
box



unit vectors  $\rightarrow \hat{a}_x, \hat{a}_y, \hat{a}_z$



$dx, dy, dz$  :- differential elements



Differential length  $\Rightarrow$  vector quantity.  
 $(d\vec{l})$

$$d\vec{l} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

Differential normal surface area  $\Rightarrow$  vector quantity.  
 $(d\vec{s})$

$$d\vec{s}_{\text{front}} = dy dz \hat{a}_x$$

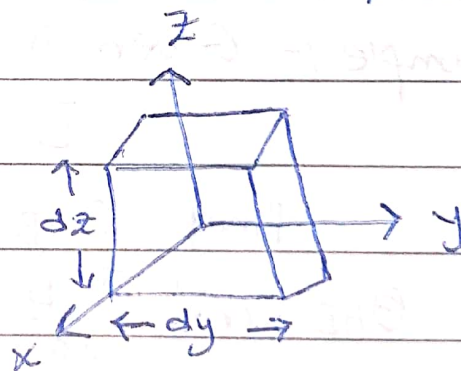
$$d\vec{s}_{\text{back}} = -dy dz \hat{a}_x$$

$$d\vec{s}_{\text{right}} = dx dz \hat{a}_y$$

$$d\vec{s}_{\text{left}} = -dx dz \hat{a}_y$$

$$d\vec{s}_{\text{top}} = dx dy \hat{a}_z$$

$$d\vec{s}_{\text{bottom}} = -dx dy \hat{a}_z$$



دالة الـ  $d\vec{s}$  الـ  $\hat{a}_x, \hat{a}_y, \hat{a}_z$



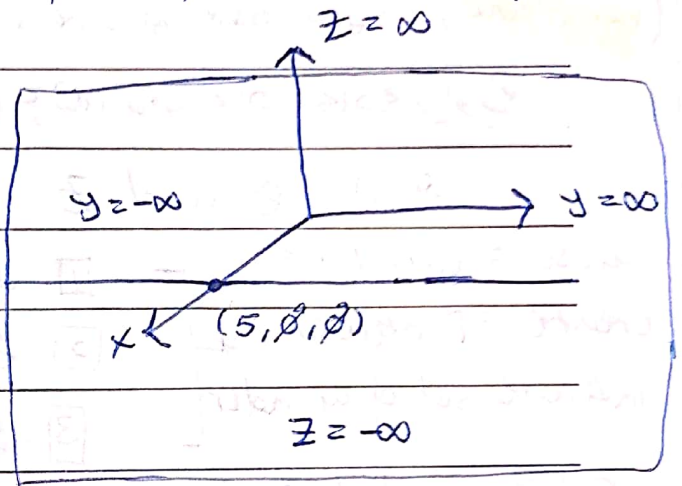
Differential volume ( $dv$ )  $\Rightarrow$  scalar quantity.

$$dv = dx dy dz$$

\* 2D Surface :- by fixing one variable, if  $x$  is constant then  $-\infty < \frac{y}{z} < \infty$

example:  $x=5$ , infinite plane parallel to  $yz$  plane.

parallel  $\rightarrow x \neq 0$   
 along  $\rightarrow x = 0$



$y = \text{constant} \rightarrow$  infinite plane along  $xz$  ( $y=0$ )

$\rightarrow$  infinite plane parallel to  $xz$  ( $y \neq 0$ )

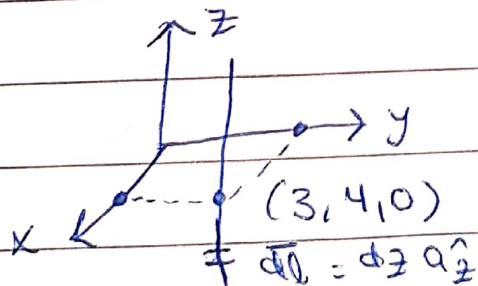
$z = \text{constant} \rightarrow$  infinite plane along  $xy$  ( $z=0$ )

$\rightarrow$  infinite plane  $\parallel$   $xz$  ( $z \neq 0$ )

\* 1D surface :- by fixing two variables

if  $x, y$  are constant then  $-\infty < z < \infty$

$$x=3, y=4$$



infinite line  $\parallel$   $z$  axis if  $x \neq 0, y \neq 0$

infinite line along  $x$  axis if  $x=0$  and  $y=0$

راديان  
 قطر سالک  
 $0 \leq r < \infty$

$0 \leq \theta < 2\pi$

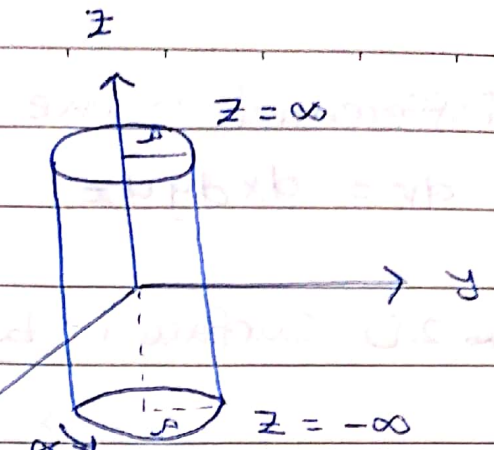
$-\infty < z < \infty$

$\theta = 0^\circ$  at x-axis

$\theta = 90^\circ$  at y-axis

الحركة تبدأ من x axis الى y axis

(x-y plane) -ve y axis الى -ve x axis



راديان :  $\theta$   
 ارتفاع :  $z$

قاعدة الاسطوانة فيها جزء من curvature عشان توصيفها كانه زاوية

$r \perp \theta$  and  $z$

whose 3 variables

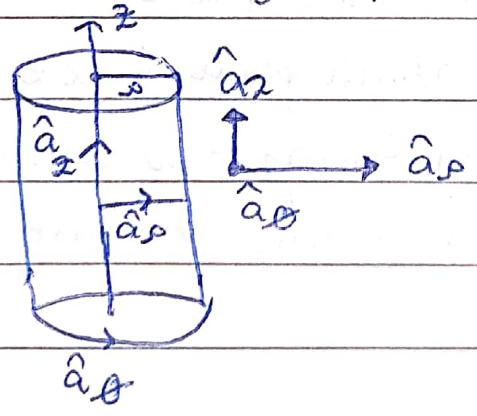
create 3D object;  
 infinite solid cylinder

- 1)  $r$
- 2)  $\theta$
- 3)  $z$

نقطه كذا على الـ  $r, \theta, z$

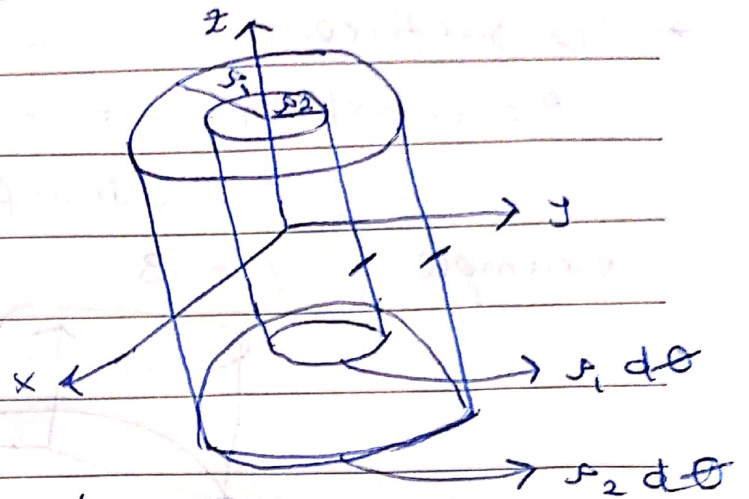
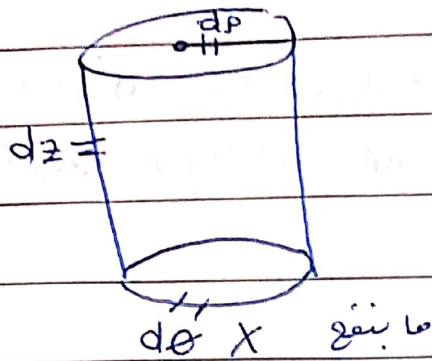
solid = filled from the inside.

unit vectors :  $\hat{a}_r, \hat{a}_\theta, \hat{a}_z$





Differential elements  $\Rightarrow dr, r d\theta, dz$   
 ما يفتقر إلى  $d\theta$  curvature



الأسطوانتين لهما نفس الارتفاع  $z_1 = z_2$

بسبب الاختلاف في نصف القطر  $r_2 > r_1$

المقطع الداخلي طول  $r_1 d\theta$   
 المقطع الخارجي طول  $r_2 d\theta$   
 بسبب اختلاف نصف القطر

$$d\vec{l} = dr \hat{a}_r + r d\theta \hat{a}_\theta + dz \hat{a}_z \text{ [vector]}$$

Differential normal surface area ( $d\vec{s}$ )

$$d\vec{s}_{side} = r d\theta dz \hat{a}_\theta, r = \text{constant}$$

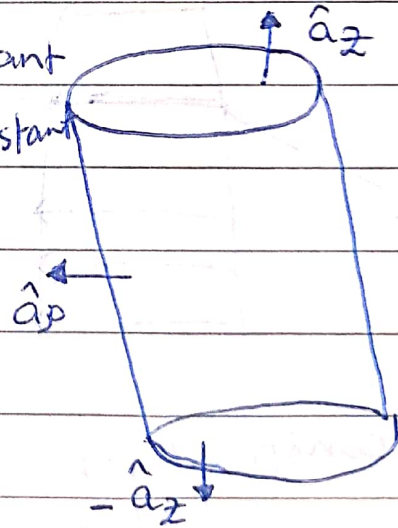
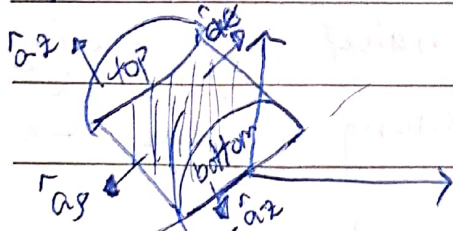
$$d\vec{s}_{top} = r dr d\theta \hat{a}_z$$

$$d\vec{s}_{bottom} = -r dr d\theta \hat{a}_z$$

$z = \text{constant}$

if  $\theta = \text{constant}$ , then:

$$d\vec{s}_{cut} = dr dz \hat{a}_\theta$$



هذا هو المقطع الذي يفتقر إلى  $d\theta$  بسبب ما يفتقر إلى  $d\theta$  بسبب ما يفتقر إلى  $d\theta$

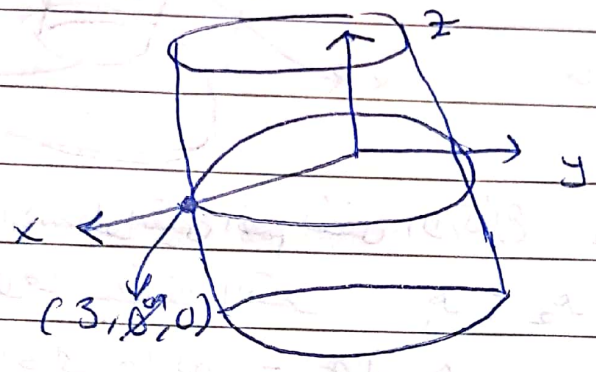


$dv = \rho d\rho \theta dz$  [scalar]

\* 2D Surface :-

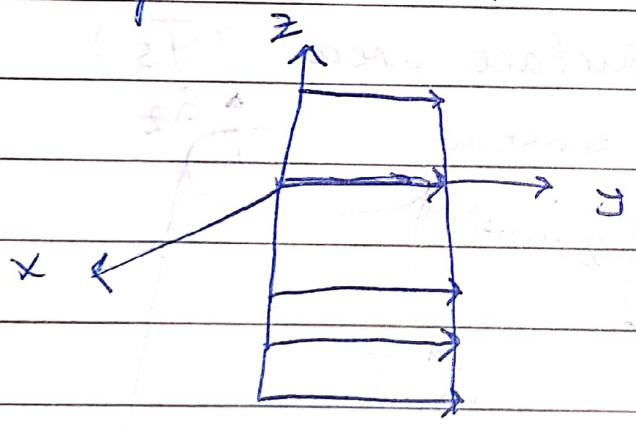
- $\rho = \text{constant}$ 
  - infinite hollow cylinder ( $\rho \neq 0$ )
  - infinite line along z-axis ( $\rho = 0$ )

example :-  $\rho = 3$

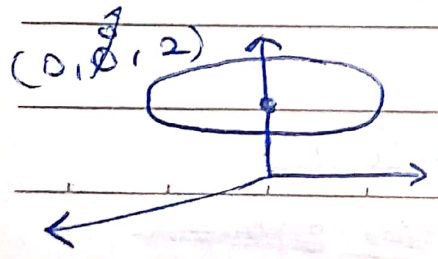


- $\theta = \text{constant}$ 
  - infinite plane along yz plane ( $\theta \neq 0$ )
  - infinite plane along xz plane ( $\theta = 0$ )

example :-  $\theta = 90^\circ$



- $z = \text{constant}$ 
  - infinite disk parallel to xy plane ( $z \neq 0$ )
  - infinite plane along xy plane ( $z = 0$ )

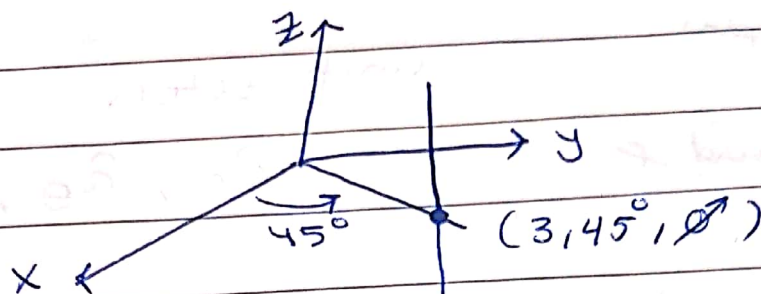


example ;  $z = 2$

\* 1D segment :

$\rho, \theta$  are constant  $\rightarrow$  infinite line // z-axis ( $\rho \neq 0$ )  
 $\rightarrow$  infinite line along z-axis ( $\rho = 0$ )

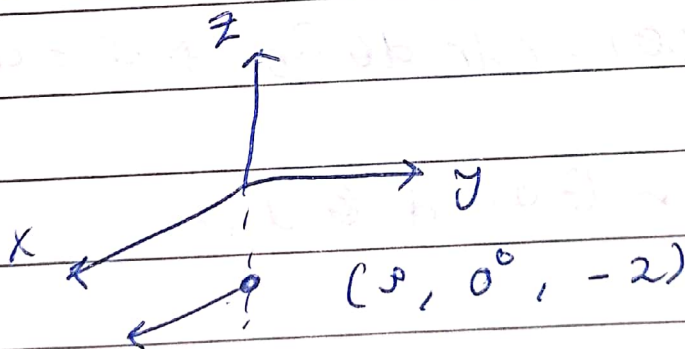
example :  $\rho = 3, \theta = 45^\circ$



$\rho, z$  are constant  $\rightarrow$  circle // xy plane ( $z \neq 0, \rho \neq 0$ )  
 $\rightarrow$  circle along xy plane ( $z = 0, \rho \neq 0$ )  
 $\rightarrow$  point if  $\rho = 0$

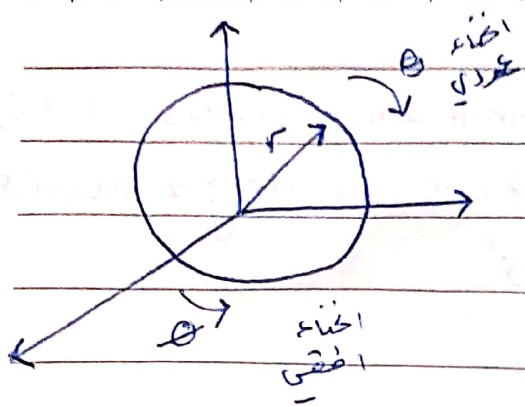
$\theta, z$  are constant  $\rightarrow$  semi-infinite line (ray)

example :  $\theta = 0^\circ, z = -2$



\* by fixing 3 variables  $\rightarrow$  point





$0 < r < \infty$   
 $0 < \theta < \pi$   
 $0 < \phi < 2\pi$

3D object;  
infinite solid sphere

unit vectors :

$\hat{r}, \hat{\theta}, \hat{\phi}$

Differential elements :-

$dr$  ,  $r d\theta$  ,  $r \sin \theta d\phi$   
 سبب اختلاف نصف القطر (radius difference)      سبب اختلاف المساحة (area difference)  
 (كل ما كبر نصف القطر يزيد طول arc)      القطع ونصف القطر

$$d\mathbf{l} = dr \hat{r} + r d\theta \hat{\theta} + r \sin \theta d\phi \hat{\phi}$$

$dS$  surface =  $r^2 \sin \theta d\theta d\phi \hat{r}$  →  $r = \text{constant}$

$dS$  horizontal cut ( $\theta$ ) =  $r \sin \theta dr d\phi \hat{\theta}$  →  $\theta = \text{constant}$

$dS$  vertical cut ( $\phi$ ) =  $r dr d\theta \hat{\phi}$  →  $\phi = \text{constant}$

$$dV = r^2 \sin \theta dr d\theta d\phi$$

\* 2D surface :-

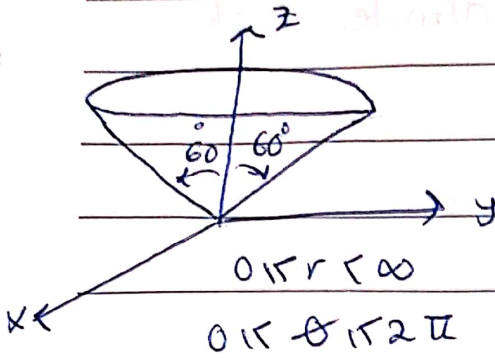
$r = \text{constant}$  → Hollow sphere ( $r \neq 0$ )  
 $(0 < \theta < \pi, 0 < \phi < 2\pi)$  → point ( $r = 0$ )



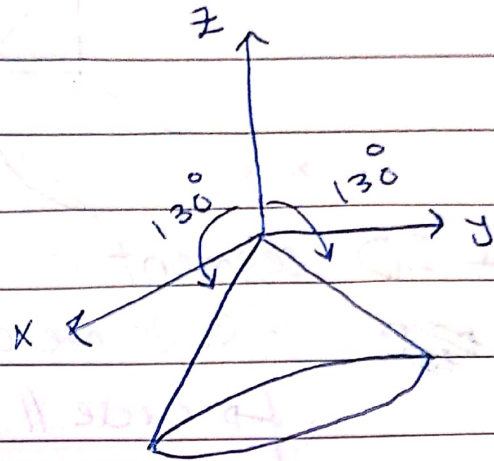
$\theta = \text{constant} \rightarrow$  infinite hollow cone

examples:

$\theta = 60^\circ$



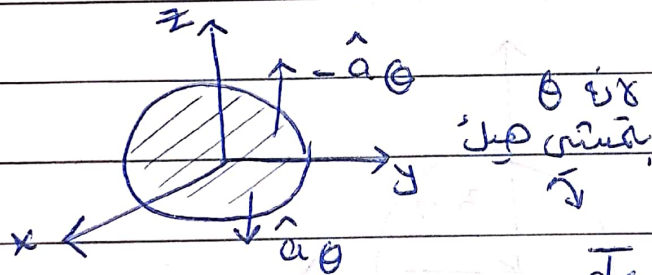
$\theta = 130^\circ$



Note:- if  $\theta$  is constant  $\rightarrow$  hollow  
 if  $\theta$  varies  $\rightarrow$  solid

Special Cases

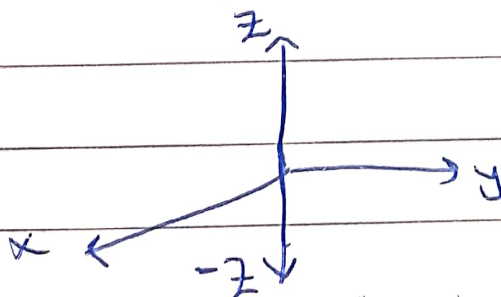
[1]  $\theta = 90^\circ \rightarrow$  infinite disk along xy-plane



$ds = r \sin \theta dr d\theta a_\theta$

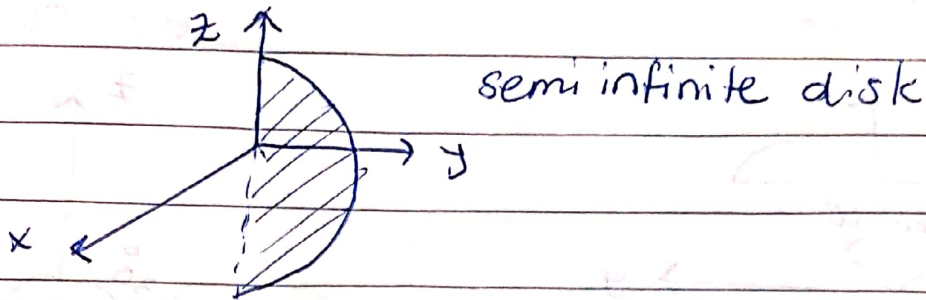
[2]  $\theta = 0^\circ \rightarrow$  positive z-axis

$\theta = 180^\circ \rightarrow$  negative z-axis



$\theta = \text{constant}$

example :  $\theta = 90^\circ$



\* 1D segment :-

~~\_\_\_\_\_~~  $r$  &  $\theta$  are constants

↳ circle || xy plane ( $r \neq 0, \theta \neq 90^\circ$ )

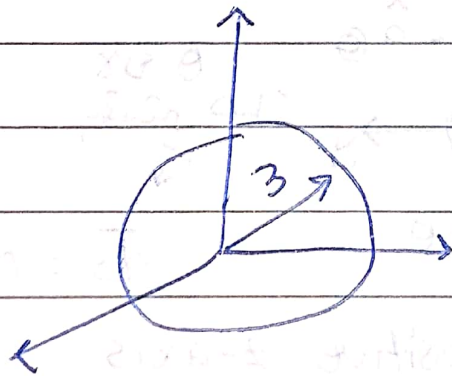
↳ circle along xy plane ( $r = 0, \theta = 90^\circ$ )

↳ point on the origin ( $r = 0, \theta = \rightarrow$ )

↳ on the positive z axis ( $\theta = 0^\circ$ )

↳ on the negative z axis ( $\theta = 180^\circ$ )

example :  $r = 3, \theta = 90^\circ$

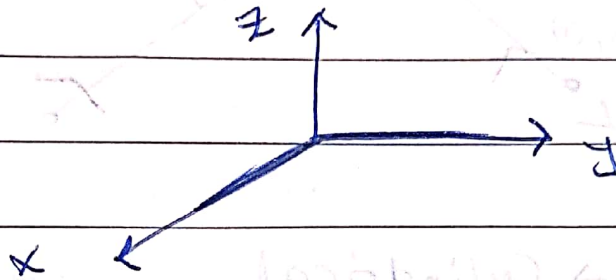


$$d\vec{l} = r \sin\theta d\theta \hat{a}_\theta$$

$r$  &  $\theta$  are constants  $\rightarrow$  half circle ( $r \neq 0$ )  
 $\rightarrow$  point ( $r = 0$ )

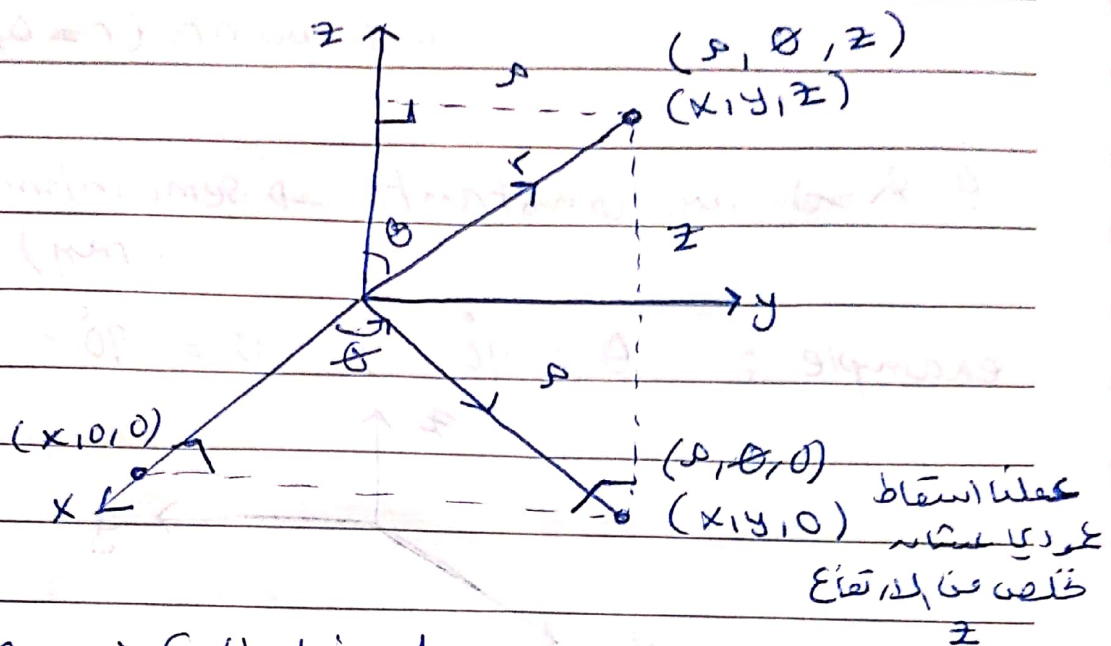
$\theta$  &  $\theta$  are constants  $\rightarrow$  semi infinite line  
(ray)

example :  $\theta = 90^\circ$  ,  $\theta = 90^\circ$





(\*) Point conversion :-



1] Cartesian  $\rightarrow$  Cylindrical.

$$(x, y, z) \rightarrow (\rho, \theta, z)$$

$$\rho = \sqrt{x^2 + y^2}$$

$$\theta \Rightarrow \sin \theta = \frac{y}{\rho}$$

$$\cos \theta = \frac{x}{\rho}$$

$$\tan \theta = \frac{y}{x} \quad \checkmark$$

$$\theta = \tan^{-1} \left( \frac{y}{x} \right)$$

$$z = z$$

2] Cylindrical  $\rightarrow$  Cartesian

$$(\rho, \theta, z) \rightarrow (x, y, z)$$

$$x = \rho \cos \theta$$

$$y = \rho \sin \theta$$

$$z = z$$

3] Cartesian  $\rightarrow$  Spherical

$$(x, y, z) \rightarrow (r, \theta, \phi)$$

$$r = \sqrt{x^2 + y^2 + z^2} = \sqrt{x^2 + y^2 + z^2}$$

$$\theta = \tan^{-1} \left( \frac{\sqrt{x^2 + y^2}}{z} \right)$$

$$\phi = \tan^{-1} \left( \frac{y}{x} \right)$$

$$\sin \theta = \frac{\rho}{r}$$

$$\cos \theta = \frac{z}{r}$$

$$\tan \theta = \frac{\rho}{z}$$

4] Spherical  $\rightarrow$  Cartesian

$$(r, \theta, \phi) \rightarrow (x, y, z)$$

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

$$z = r \cos \theta$$

5] Cylindrical  $\rightarrow$  Spherical

$$(\rho, \theta, z) \rightarrow (r, \theta, \phi)$$

$$r = \sqrt{\rho^2 + z^2}$$

$$\phi = \tan^{-1} \left( \frac{\rho}{z} \right)$$

$$\theta = \theta \quad \theta = \theta$$

6] Spherical  $\rightarrow$  Cylindrical

$$(r, \theta, \phi) \rightarrow (\rho, \theta, z)$$

$$\rho = r \sin \theta$$

$$\theta = \theta$$

$$z = r \cos \theta$$



⊛ Vector conversion :-

1] Cartesian  $\rightarrow$  Cylindrical

$$\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z \quad \text{remains the same}$$

$$\vec{A} = A_\rho \hat{a}_\rho + A_\theta \hat{a}_\theta + A_z \hat{a}_z$$

$$\begin{bmatrix} A_\rho \\ A_\theta \\ A_z \end{bmatrix}_{3 \times 1} = \begin{bmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}_{3 \times 3} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix}_{3 \times 1}$$

unknown                      conversion matrix                      given

Step 1

$$A_\rho = \cos \theta A_x + \sin \theta A_y$$

$$A_\theta = -\sin \theta A_x + \cos \theta A_y$$

$$A_z = A_z$$

Step 2 replace x, y by their point laws (in the previous pages)

2] Cylindrical  $\rightarrow$  Cartesian

$$\begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} = \begin{bmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A_\rho \\ A_\theta \\ A_z \end{bmatrix}$$

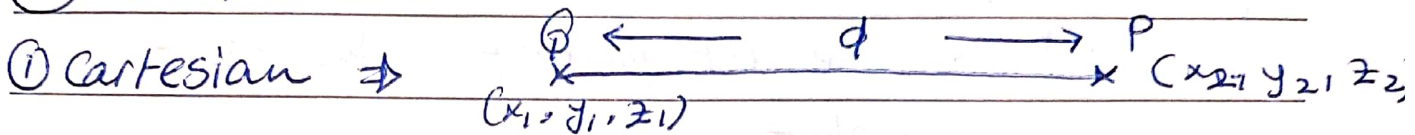
3] Cartesian  $\rightarrow$  Spherical

$$\begin{bmatrix} A_r \\ A_\theta \\ A_\phi \end{bmatrix} = \begin{bmatrix} \sin \theta \cos \phi & \sin \theta \sin \phi & \cos \theta \\ \cos \theta \cos \phi & \cos \theta \sin \phi & -\sin \theta \\ -\sin \phi & \cos \phi & 0 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix}$$

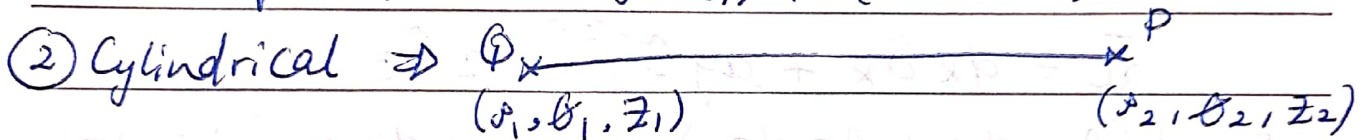
4) Cylindrical  $\rightarrow$  Spherical

$$\begin{bmatrix} Ar \\ A\theta \\ A\phi \end{bmatrix} = \begin{bmatrix} \sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \\ \cos\theta & -\sin\theta & 0 \end{bmatrix} \begin{bmatrix} Ar \\ A\theta \\ Az \end{bmatrix}$$

(\*) Distance :-



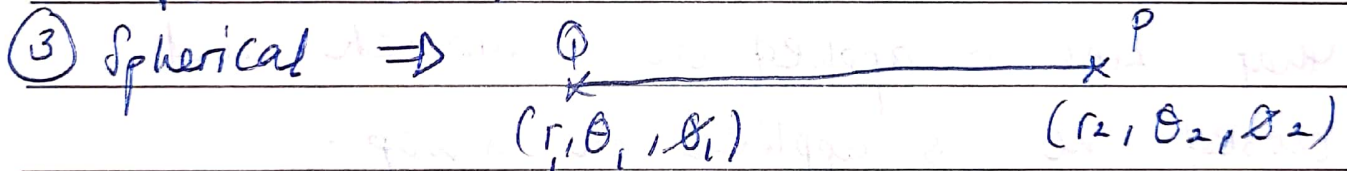
$$d = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$



$$d^2 = r_1^2 + r_2^2 - 2r_1r_2 \cos(\theta_2 - \theta_1) + (z_2 - z_1)^2$$

$z, r \rightarrow m$   
 $\theta \rightarrow \text{degree}$  بما يقع بينهما في الارتفاع Cartesian

$d = \sqrt{(r_2 - r_1)^2 + (z_2 - z_1)^2}$  : إذا  $\theta_1 = \theta_2$  بما يقع بينهما في الارتفاع



if  $\theta_1 = \theta_2$  and  $\phi_1 = \phi_2 \rightarrow d = \sqrt{(r_2 - r_1)^2}$

if they are not  $\rightarrow d^2 = r_2^2 + r_1^2 - 2r_1r_2 \cos\theta_2 \cos\theta_1 - 2r_1r_2 \sin\theta_2 \sin\theta_1 \cos(\phi_2 - \phi_1)$

Note:

spherical, cylindrical بما يقع بينهما في الارتفاع

Cartesian بما يقع بينهما في الارتفاع

distance بما يقع بينهما في الارتفاع



(\*) Integrals

II Line integral :-

differential length عنق line integral  
 القطر  $\downarrow$  كاط  $\downarrow$  القطر  
 القطر  $\downarrow$  طول كاط

$$\int_C \vec{A} \cdot d\vec{l}$$

we use dot product so the result is scalar.

example :  $\vec{A} = Ax \hat{a}_x + Az \hat{a}_z$

$$d\vec{l} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

$$\text{so } \int_C (Ax dx + Az dz) = \int_C Ax dx + \int_C Az dz$$

\* special case  $\Rightarrow$  Closed Line Integral :

difference between closed line and line is that line is applied on a branch and closed line is applied on a loop.

خطية (line) ليس خطية (line) بس، بس line خطية بس

circulation هو كاط

example :-

$$d\vec{l}_1 = dz \hat{a}_z$$

$$d\vec{l}_2 = dx \hat{a}_x$$

$$d\vec{l}_3 = dy \hat{a}_y$$

$$d\vec{l}_4 = dx \hat{a}_x$$

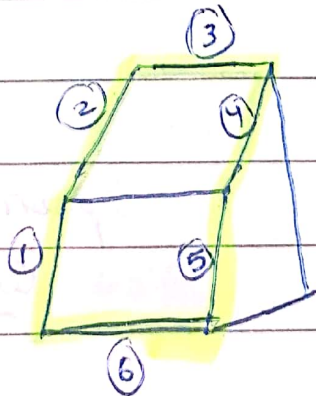
$$d\vec{l}_5 = dz \hat{a}_z$$

خطية (line) بس

خطية (line) بس

خطية (line) بس

خطية (line) بس



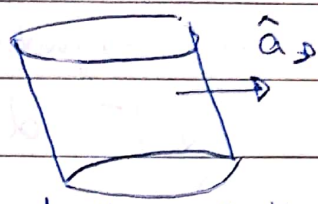
$$d\vec{l}_6 = dy \hat{a}_y$$

$$\oint_L \vec{A} \cdot d\vec{l} = \int_{l_1} \vec{A} \cdot d\vec{l}_1 + \int_{l_2} \vec{A} \cdot d\vec{l}_2 + \int_{l_3} \vec{A} \cdot d\vec{l}_3 + \int_{l_4} \vec{A} \cdot d\vec{l}_4 + \int_{l_5} \vec{A} \cdot d\vec{l}_5 + \int_{l_6} \vec{A} \cdot d\vec{l}_6$$

2 Surface integral :-

$$\int_S \vec{A} \cdot d\vec{s}$$

$$d\vec{s} = \rho d\theta dz \hat{a}_\rho$$



hollow cylinder

if A is in Cartesian then it should be converted to cylindrical.

$$\vec{A} = A \rho \hat{a}_\rho \quad \text{only}$$

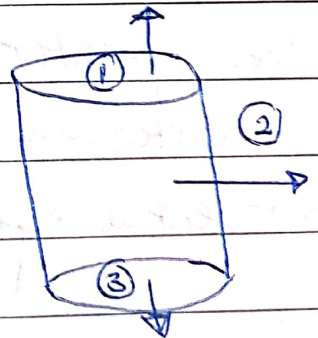
$$\rightarrow \int_{\theta} \int_z A \rho \hat{a}_\rho \cdot \rho d\theta dz \hat{a}_\rho$$

Note

\* special case  $\Rightarrow$  Closed Surface Integral :

$$\oint \vec{A} \cdot d\vec{s}$$

$$S = \int_{s_1} \vec{A} \cdot d\vec{s}_1 + \int_{s_2} \vec{A} \cdot d\vec{s}_2 + \int_{s_3} \vec{A} \cdot d\vec{s}_3$$



$$d\vec{s}_1 = \rho d\rho d\theta \hat{a}_z$$

$$d\vec{s}_2 = \rho d\theta dz \hat{a}_\rho$$

$$d\vec{s}_3 = -\rho d\rho d\theta \hat{a}_z$$

... ل ك ا ب ج د ه و ز ح ط ي ق ر س ت ث



[3] Volume integral :-

$$\int A \, du$$

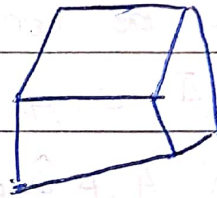
✓ scalar quantity so we do not need dot product

if A was given as a vector then we need to find its magnitude first then integrate,

$$\int |\vec{A}| \, du$$

example :

$$\int \int \int A \, dx \, dy \, dz$$



(\*) Del Operator ( $\nabla$ )

Del operator is a vector quantity.

- in cartesian :  $\nabla = \frac{\partial}{\partial x} \hat{a}_x + \frac{\partial}{\partial y} \hat{a}_y + \frac{\partial}{\partial z} \hat{a}_z$

differential elements (D.E)  $\rightarrow dx, dy, dz$

Partial  $\nabla$  is D.E is

Note:  $\partial$  : partial ,  $d$  : differential

- in cylindrical :  $\nabla = \frac{\partial}{\partial r} \hat{a}_r + \frac{\partial}{r \partial \theta} \hat{a}_\theta + \frac{\partial}{\partial z} \hat{a}_z$

- in spherical :  $\nabla = \frac{\partial}{\partial r} \hat{a}_r + \frac{\partial}{r \sin \theta} \hat{a}_\theta + \frac{\partial}{r \sin \theta \partial \theta} \hat{a}_\phi$

- Usage of Del operator  $\Rightarrow$
- ① Gradient ( $\nabla v$ )
  - ② Divergence ( $\nabla \cdot \vec{A}$ )
  - ③ Curl ( $\nabla \times \vec{A}$ )
  - ④ Laplacian ( $\nabla \cdot (\nabla u) = \nabla^2 u$ )

\* Gradient ( $\nabla u$ ) :-

$u$ : scalar,  $\nabla$ : vector  $\Rightarrow$  vector quantity  
 in Cartesian:  $\nabla u = \frac{\partial u}{\partial x} \hat{a}_x + \frac{\partial u}{\partial y} \hat{a}_y + \frac{\partial u}{\partial z} \hat{a}_z$   
 (as well as for spherical and cylindrical.)

\* Divergence ( $\nabla \cdot \vec{A}$ ) :-

$\nabla$ : vector,  $\vec{A}$ : vector, dot product  $\Rightarrow$  scalar

in Cartesian:  $\nabla \cdot \vec{A} = \left( \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right) (A_x, A_y, A_z)$   
 $= \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$

in cylindrical:  $\nabla \cdot \vec{A} = \frac{1}{r} \frac{\partial}{\partial r} (r A_r) + \frac{\partial A_\theta}{r \partial \theta} + \frac{\partial A_z}{\partial z}$

in spherical:  $\nabla \cdot \vec{A} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta A_\theta)$   
 $+ \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} (A_\phi)$



\* Curl ( $\nabla \times \bar{A}$ ) :-

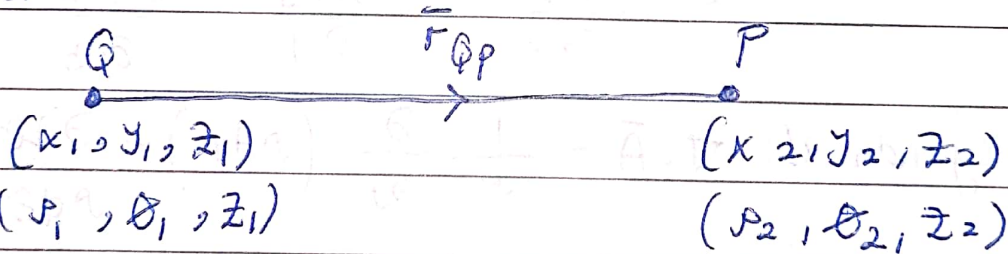
$\nabla$ : vector,  $\bar{A}$ : vector, cross product  $\rightarrow$  vector

in Cartesian:  $\nabla \times \bar{A} = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix}$

in cylindrical:  $\nabla \times \bar{A} = \frac{1}{\rho} \begin{vmatrix} \hat{a}_\rho & \rho \hat{a}_\theta & \hat{a}_z \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial z} \\ A_\rho & \rho A_\theta & A_z \end{vmatrix}$

in spherical:  $\nabla \times \bar{A} = \frac{1}{r^2 \sin \theta} \begin{vmatrix} \hat{a}_r & r \hat{a}_\theta & r \sin \theta \hat{a}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & A_\theta & r \sin \theta A_\phi \end{vmatrix}$

\* Distance :-



$d = |\bar{F}_{QP}|$

$d^2 = (x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2$  in Cartesian

in cylindrical,  $d^2 = \rho_2^2 + \rho_1^2 - 2\rho_1\rho_2 \cos(\theta_2 - \theta_1) + (z_2 - z_1)^2$

if  $\theta_2 = \theta_1 \rightarrow d^2 = (\rho_2 - \rho_1)^2 + (z_2 - z_1)^2$

in spherical,  $d^2 = (r_2 - r_1)^2$  if  $\theta_1 = \theta_2$

and  $\phi_1 = \phi_2$ .

# Chapter "4"

Subject Coulomb's Law Day \_\_\_\_\_ Date \_\_\_\_\_

\* Sources of electrostatics:

- 1) Point charge ( $Q$ ) [coulomb]
- 2) Line charge distribution ( $\rho_L$ )  $\rightarrow$  1D segment
- 3) Surface charge distribution ( $\rho_S$ )  $\rightarrow$  2D surface
- 4) Volume charge distribution ( $\rho_V$ )  $\rightarrow$  3D object
- 5) Electric dipole.
- 6) Polarized dielectric.

\* Major Laws  $\Rightarrow$  1) Coulomb's law.

2) Gauss's law (special case of Coulomb's law)

\* Coulomb's Law :-

$\vec{F}$  ( $\vec{F}_e$ ) : force

• The relation  $\rightarrow F \propto \frac{Q_1 Q_2}{R_{12}^2}$

• The law  $\rightarrow F = \frac{k Q_1 Q_2}{R_{12}^2}$  [N]

$\rightarrow$  the proportionality constant

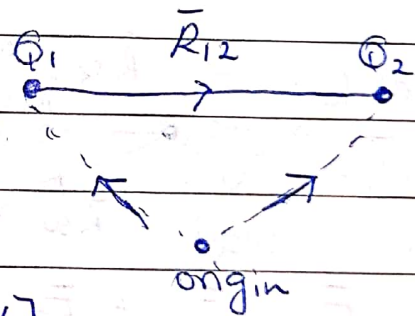
$$k = \frac{1}{4\pi\epsilon_0}$$

depends on  
the units used

$\rightarrow$  depends on the channel (dashed)

$\epsilon_0 =$  free space permittivity

$$= \frac{10^{-9}}{36\pi} \approx 8.858 \times 10^{-12} \left[ \frac{F}{m} \right]$$





-  $F$  as a magnitude  $\Rightarrow F = \frac{Q_1 Q_2}{4\pi \epsilon_0 R_{12}^2}$  [N]

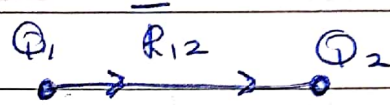
-  $F$  as a vector  $\Rightarrow \vec{F}_{12}$  = the force on  $Q_2$  due to  $Q_1$

$\vec{F}_{12} = -\vec{F}_{21}$

$|\vec{F}_{21}| = |\vec{F}_{12}|$

$\vec{F}_{12} = \frac{Q_1 Q_2}{4\pi \epsilon_0 R_{12}^2} \hat{a}_{R_{12}} \rightarrow \boxed{1}$

$\vec{F}_{12} = \frac{Q_1 Q_2 \vec{R}_{12}}{4\pi \epsilon_0 R_{12}^3} \rightarrow \boxed{2}$

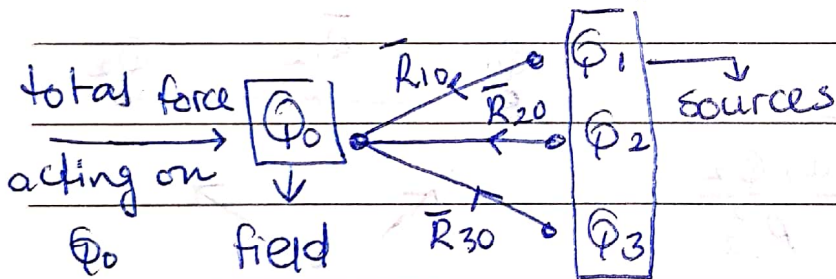


$\vec{F}_{12} = \frac{Q_1 Q_2 (\vec{r}_2 - \vec{r}_1)}{4\pi \epsilon_0 |\vec{r}_2 - \vec{r}_1|^3} \rightarrow \boxed{3}$

$\frac{\vec{R}_{12}}{R_{12}} = \hat{a}_{R_{12}}$

$\vec{R}_{12} = \vec{r}_2 - \vec{r}_1$

- For  $N$ -charges affecting on a certain charge :-



$\vec{F}_0 = \vec{F}_{10} + \vec{F}_{20} + \dots + \vec{F}_{N0}$

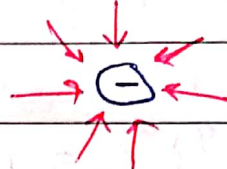
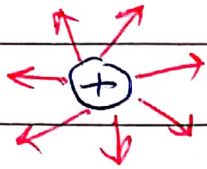
$\vec{F}_0 = \frac{Q_1 Q_0 (\vec{r}_0 - \vec{r}_1)}{4\pi \epsilon_0 |\vec{r}_0 - \vec{r}_1|^3} + \frac{Q_2 Q_0 (\vec{r}_0 - \vec{r}_2)}{4\pi \epsilon_0 |\vec{r}_0 - \vec{r}_2|^3} + \dots + \frac{Q_N Q_0 (\vec{r}_0 - \vec{r}_N)}{4\pi \epsilon_0 |\vec{r}_0 - \vec{r}_N|^3}$

$\vec{F}_0 = \frac{Q}{4\pi \epsilon_0} \sum_{k=1}^N \frac{Q_k (\vec{r}_0 - \vec{r}_k)}{|\vec{r}_0 - \vec{r}_k|^3}$  [N]

- Electric Field Intensity ( $\vec{E}$ ) :-

$$\vec{E} = \frac{\text{force}}{\text{charge (field)}} = \frac{\vec{F}}{q_{\text{test field}}} \quad \left[ \frac{N}{C} \right] \left[ \frac{V}{m} \right]$$

most used.

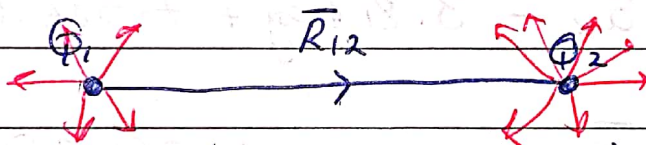


always exiting positive charge and entering negative charge

$\vec{E} \propto \frac{1}{r^2}$  → كلما اقتربنا من الشحنة

$\vec{E} \propto \frac{1}{r^2}$  → كلما ابتعدنا عن الشحنة

(as  $r \rightarrow 0$ ,  $E \rightarrow \infty$ ) (as  $r \rightarrow \infty$ ,  $E \rightarrow 0$ )



في قوة متبادلة بينهم ليسوا اصعب مجال يشوف من الشحنة اي يتاثر عندها العوض بالقانون.

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 R^2} \hat{a}_r$$

$$= \frac{Q}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|^3} \quad \begin{matrix} \text{The dash refers} \\ \text{to source} \\ \text{(without dash refers} \\ \text{to field)} \end{matrix}$$

Convention :- use dashes to represent the source and without dashes to represent the field point.

- For N-charges  $\Rightarrow \frac{1}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k (\vec{r} - \vec{r}'_k)}{|\vec{r} - \vec{r}'_k|^3}$



Example:- point charges  $1\text{mC}$  and  $-2\text{mC}$  located at  $(3, 2, -1)$  and  $(-1, -1, 4)$ . Find the force and electric field at a  $10\text{nC}$  charge located at  $(0, 3, 1)$  ?

field

$$\text{Sol } \vec{F} = \frac{(1 \cdot 10^{-3})(10 \cdot 10^{-9})}{4\pi \frac{10^{-9}}{36\pi}} \frac{(-3, 1, 2)}{\sqrt{(14)^3}} = \text{field-source}$$

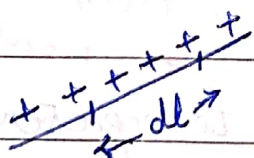
$$+ \frac{(-2 \cdot 10^{-3})(10 \cdot 10^{-9})}{4\pi \frac{10^{-9}}{36\pi}} \frac{(1, 4, -3)}{\sqrt{(26)^3}}$$

$$\vec{F} = -6.507 \hat{a}_x - 3.817 \hat{a}_y + 7.506 \hat{a}_z \text{ mN}$$

$$\vec{E} = \frac{\vec{F}}{Q_{\text{field}}} = \frac{\vec{F}}{10 \cdot 10^{-9}} = -650.7 \hat{a}_x - 381.7 \hat{a}_y + 750.6 \hat{a}_z \text{ KV/m.}$$

**(\*) Electric Field Due to Continuous Charge Distribution:-**

1) Line charge distribution (1D segment)

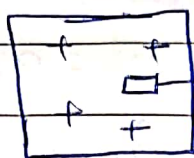


$\rho_L$ : line charge density  $[\frac{C}{m}]$

$$Q = \int_L \rho_L dl \rightarrow$$

vector  $\rho_L$  is scalar

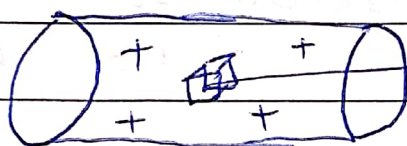
2) Surface charge distribution (2D surface)



$ds$   
 $\rho_s$  : surface charge density  
 $[\frac{C}{m^2}]$

$Q = \int_S \rho_s ds$  → *سکالر ہوتی ہے*  
*مجموع ہوتی ہے*

3) Volume charge distribution (3D object)

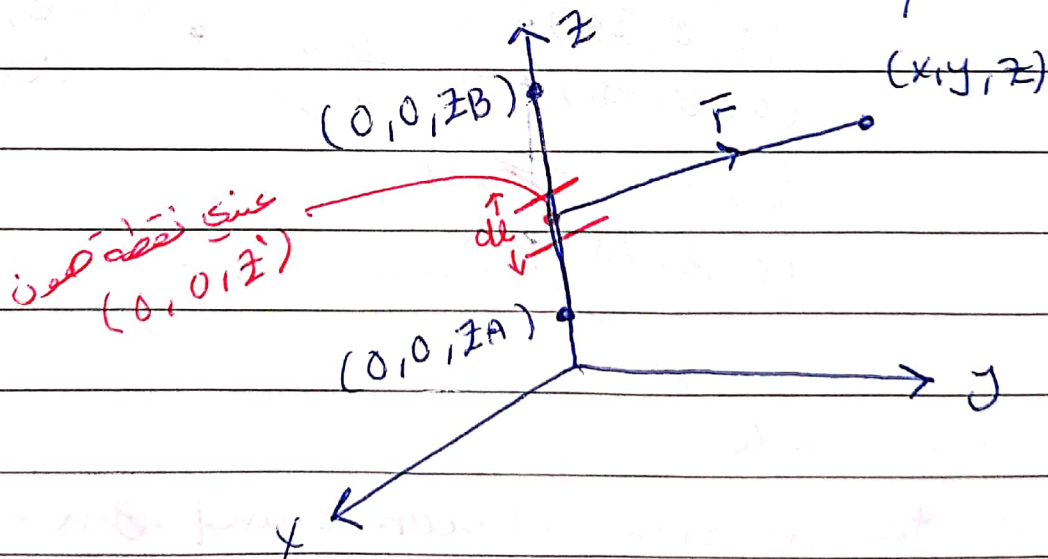


$dv$   
 $\rho_v$  : volume charge density  
 $[\frac{C}{m^3}]$

$Q = \int_V \rho_v dv$

Example (+ Derivation) :-

consider a finite line along z-axis carry charge  $\rho_L$  (C/m) - Find the electric field at point  $(x, y, z)$





$$Q = \int l \rho_L dl$$

$$\vec{E} = \int \frac{\rho_L dl}{4\pi\epsilon_0 r^2}$$

constant scalar  $\hat{a}_z$

$$dl = dz \hat{a}_z$$

$$\hat{a}_r = \frac{\vec{r}}{r}$$

$$= \frac{\rho_L}{4\pi\epsilon_0} \int_{z_A}^{z_B} \frac{x\hat{a}_x + y\hat{a}_y + (z-z')\hat{a}_z dz'}{(\sqrt{x^2 + y^2 + (z-z')^2})^3} r = \frac{\rho_L}{4\pi\epsilon_0} \frac{x\hat{a}_x + y\hat{a}_y + (z-z')\hat{a}_z}{r^2}$$

$$r = \sqrt{x^2 + y^2 + (z-z')^2}$$

by converting to cylindrical coordinate

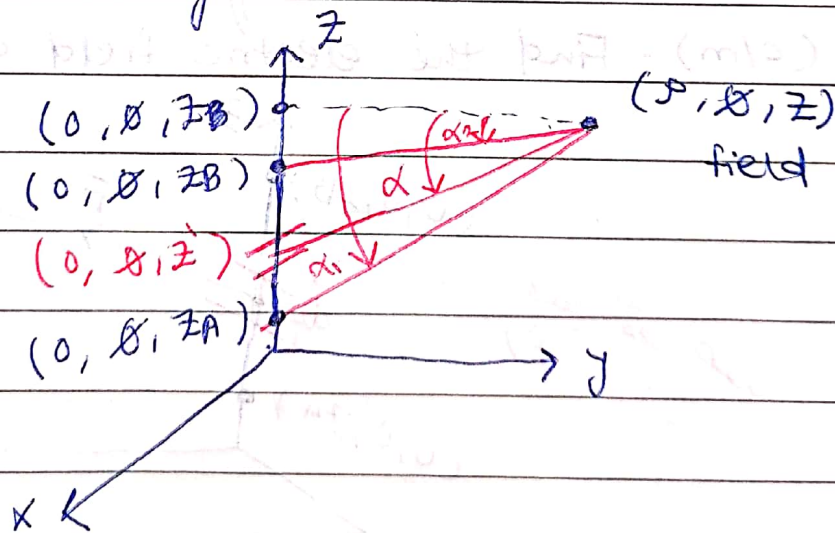
(cylindrical is sup is the line is)

$$\vec{r} = \rho \hat{a}_\rho + (z-z') \hat{a}_z$$

$$r = \sqrt{\rho^2 + (z-z')^2}, \quad dl = dz'$$

$$\vec{E} = \frac{\rho_L}{4\pi\epsilon_0} \int_{z_A}^{z_B} \frac{\rho \hat{a}_\rho + (z-z') \hat{a}_z}{[\rho^2 + (z-z')^2]^{3/2}} dz'$$

convert the integral limits :-

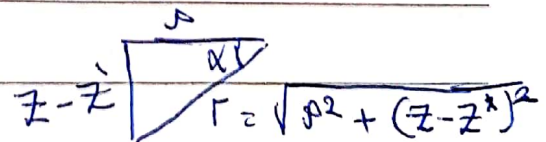


What is the relation between z and alpha?

$$\sin \alpha = (z-z') / r$$

$$\cos \alpha = \rho / r$$

$$\tan \alpha = (z-z') / \rho$$



الدالة  $z - z'$  على المسافة  $r$   $\tan \alpha = \rho / r$

$$z - z' = r \sin \alpha = \rho \tan \alpha$$

from  $z - z' = \rho \tan \alpha$

$$-dz' = \rho \sec^2 \alpha d\alpha$$

$$dz' = -\rho \sec^2 \alpha d\alpha$$

$$\begin{aligned} r^2 &= \rho^2 + (z - z')^2 \\ &= \rho^2 + \rho^2 \tan^2 \alpha \\ &= \rho^2 (1 + \tan^2 \alpha) \\ &= \rho^2 \sec^2 \alpha \end{aligned}$$

$$r^3 = \rho^3 \sec^3 \alpha = [\rho^2 + (z - z')^2]^{3/2}$$

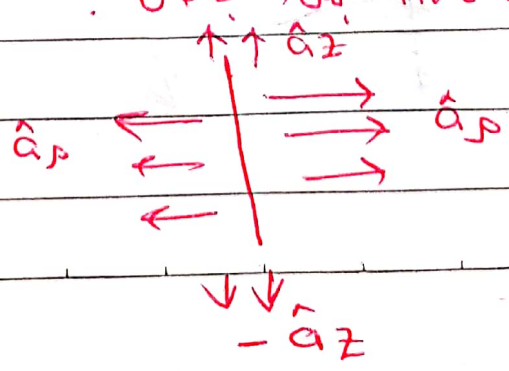
$$\begin{aligned} \text{So } \rho &= r \cos \alpha \\ z - z' &= r \sin \alpha \\ r &= \rho \sec \alpha \end{aligned}$$

$$\vec{E} = \frac{\rho L}{4\pi\epsilon_0} \int_{\alpha_1}^{\alpha_2} \frac{\rho \sec \alpha (\cos \alpha \hat{a}_\rho + \sin \alpha \hat{a}_z)}{\rho^3 \sec^3 \alpha} (-\rho \sec^3 \alpha d\alpha)$$

$$\vec{E} = \frac{-\rho L}{4\pi\epsilon_0 \rho} \left[ (\sin \alpha_2 - \sin \alpha_1) \hat{a}_\rho - (\cos \alpha_2 - \cos \alpha_1) \hat{a}_z \right] \frac{V}{m}$$

لأنه طرح على الكبار  $\alpha$  2 components  
 لا يكون عندك line along z-axis  
 electric field  $\hat{a}_z$   $\hat{a}_\rho$   $\hat{a}_\phi$   $\hat{a}_\theta$   $\hat{a}_r$   $\hat{a}_\theta$   $\hat{a}_\phi$   $\hat{a}_z$

This is finite line.

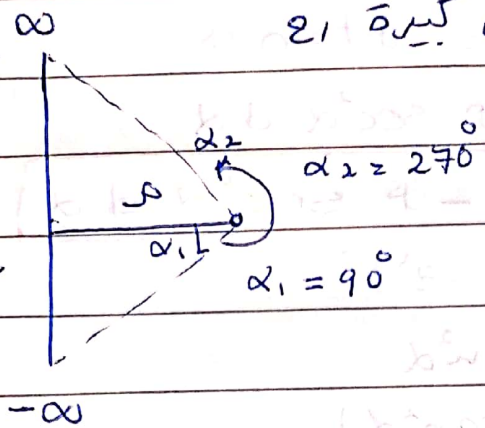




**Special case** infinite line

المسافة بين نقطة و line  
 بعض النظر عن ادواتك كبيرة و  
 نفس عملها مع line

$\rho$ : the shortest distance between the field and the source or the extension of the source.



مع طول line

$$\vec{E} \text{ for infinite line} = \frac{\rho_l \vec{\rho}}{2\pi \epsilon_0 \rho^2} = \frac{\rho_l}{2\pi \epsilon_0} \hat{a}_\rho$$

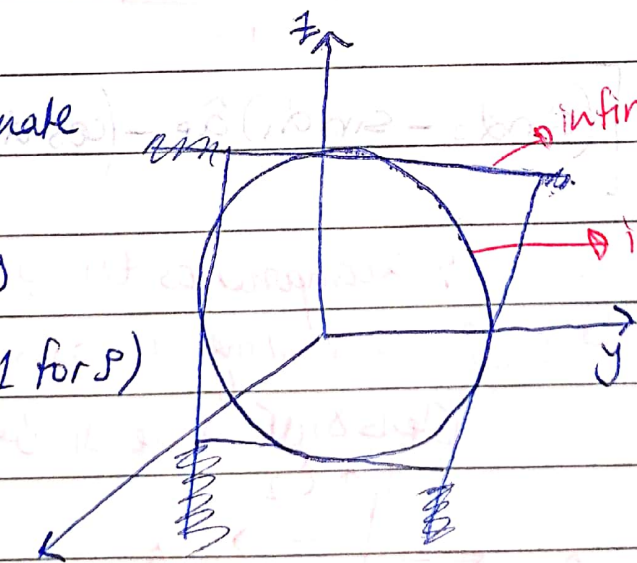
always for any infinite line.

- Electric field for surface charge distribution :-

Example; consider infinite  $(z=0)$  plane carry a charge distribution of  $\rho_s \frac{C}{m^2}$ . find  $\vec{E}$  at  $(0,0,h)$  and  $(0,0,-h)$ ?

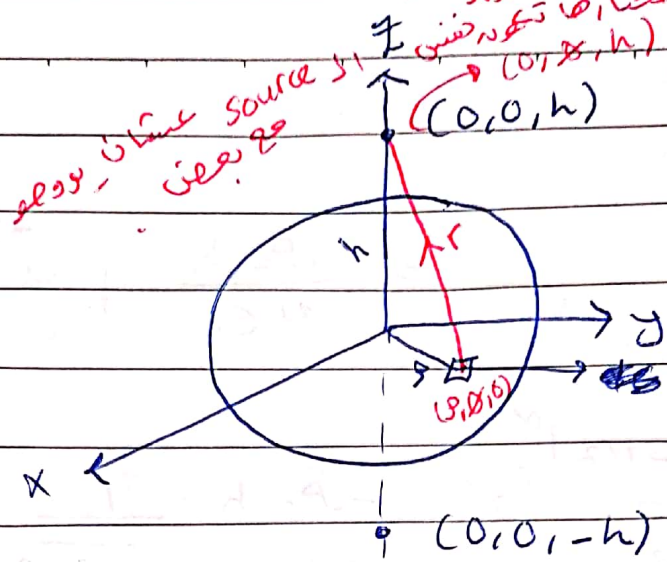
Cartesian coordinate

has 6 DOF but cylindrical has 3 (2 for  $z$ , 1 for  $\rho$ ) so its easier to use the disk.



infinite plane (Cartesian)  
 infinite disk (cylindrical)

یہ ذریعہ ہے، اس لیے اسے source کہتے ہیں۔  
 (0, 0, h)  
 (0, 0, -h)



$$\vec{r} = -\rho \hat{a}_\rho + h \hat{a}_z$$

$ds$  (scalar quantity)  $ds = \rho d\rho d\theta$

$$\vec{E}_{\text{point charge}} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \rightarrow Q = \int_{\text{surface}} \rho_s ds$$

$$\text{So } \vec{E}_{\text{surface}} = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r^2} \hat{a}_r$$

constant

$$\vec{E} = \int_S \frac{\rho_s ds \vec{r}}{4\pi\epsilon_0 r^3}, \quad \vec{r} = -\rho \hat{a}_\rho + h \hat{a}_z$$

$$r = \sqrt{\rho^2 + h^2}$$

$$\vec{E} = \frac{\rho_s}{4\pi\epsilon_0} \int_0^{2\pi} \int_0^\infty \frac{-\rho \hat{a}_\rho + h \hat{a}_z}{[\rho^2 + h^2]^{3/2}} \rho d\rho d\theta$$

ناظرہ بعد کے  
ذریعہ کے

The  $\rho$  component will be cancelled due to symmetry (only when the graph is symmetrical around the origin)

$$\vec{E} = \frac{\rho_s h (2\pi)}{2 \cdot 4\pi\epsilon_0} \int_0^\infty \frac{1}{[\rho^2 + h^2]^{3/2}} \rho d\rho \hat{a}_z$$



$$\text{let } u = \rho^2 + h^2$$

$$du = 2\rho d\rho$$

$$\vec{E} = \frac{\rho_s h}{2\epsilon_0} \int \frac{du}{2(u)^{3/2}} = \frac{\rho_s h}{4\epsilon_0} \int u^{-3/2} du$$

$$\vec{E} = \frac{\rho_s h}{4\epsilon_0} \left[ \frac{u^{-1/2}}{-1/2} \right]_0^\infty \hat{a}_z = \frac{-\rho_s h}{2\epsilon_0} \left[ \frac{1}{\sqrt{\rho^2 + h^2}} \right]_0^\infty \hat{a}_z$$

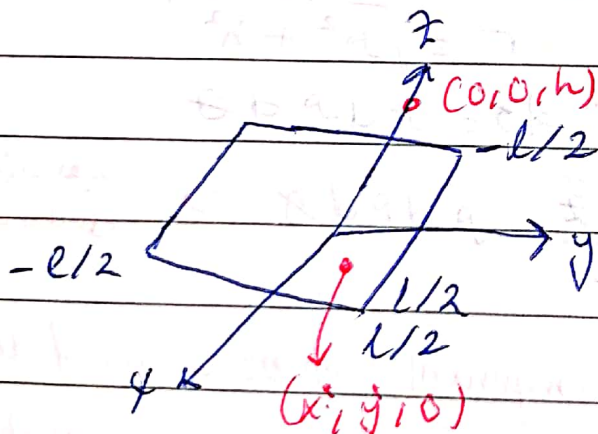
$$\vec{E} = \frac{-\rho_s h}{2\epsilon_0} \left( 0 - \frac{1}{h} \right) \hat{a}_z = \frac{\rho_s}{2\epsilon_0} \hat{a}_z = \frac{V}{m}$$

for  $(0,0,h) \rightarrow \hat{a}_z$   
for  $(0,0,-h) \rightarrow -\hat{a}_z$

For any infinite sheet :-

$$\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_{\text{normal}}$$

always for  
any infinite  
sheet.



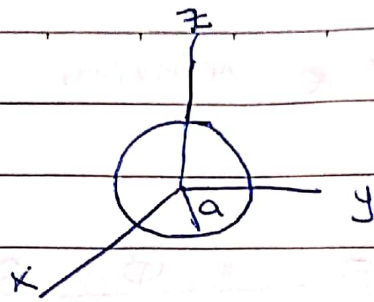
sheet is not infinite  
it must be solved in  
Cartesian coordinate  
x, y both cancel due  
to symmetry.

$$\vec{E} = \int_S \frac{\rho_s ds \vec{r}}{4\pi\epsilon_0 r^3}$$

$$ds = dx dy$$

$$\vec{r} = -x\hat{a}_x - y\hat{a}_y + h\hat{a}_z$$

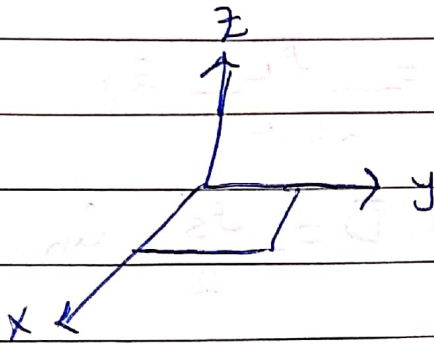
$$r = \sqrt{x^2 + y^2 + h^2}$$



finite disk of radius (a)

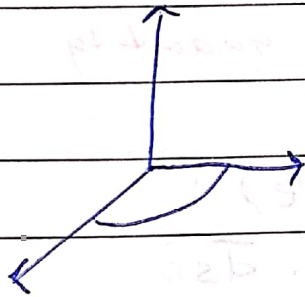
solved on cylindrical  
coordinate

there's symmetry on  $\phi$  component



solved on Cartesian

there is no symmetry

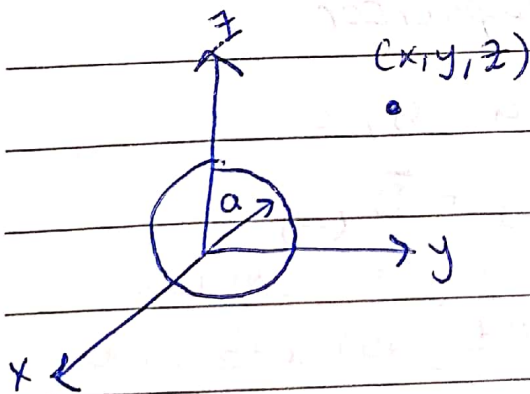


quarter disk

solved on cylindrical

there is no symmetry

- Electric Field Due to Volume Charge Distribution :-



$$Q = \int \rho_v dv$$

$$\vec{E} = \int \frac{\rho_v dv}{4\pi\epsilon_0 r^2} \hat{a}_r$$

~~we~~ volume charge delayed till  
we study Gauss law.



$\vec{D} = \epsilon_0 \vec{E}$  → constitutive relation

$[\vec{D}] = \frac{C}{m^2}$

for a point charge →  $\vec{D} = \frac{Q}{4\pi r^2} \hat{a}_r$

for an infinite line →  $\vec{D} = \frac{\rho_L}{2\pi r} \hat{a}_\rho$

for an infinite sheet →  $\vec{D} = \frac{\rho_S}{2} \hat{a}_n$

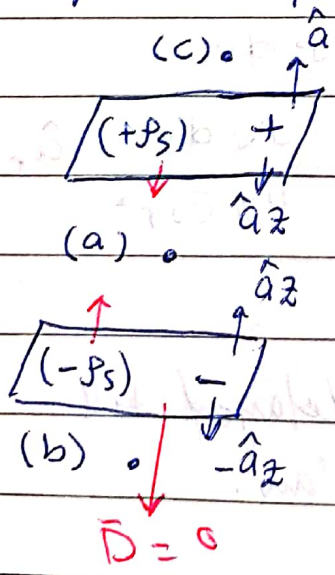
electric flux density ⇒ vector quantity

electric flux ⇒ scalar quantity

Electric flux  $\Psi$  (later  $\Psi_e$ ):

$\Psi = Q_{enclosed} = \int_S \vec{D} \cdot d\vec{s}$

example: for parallel plate capacitor



$\vec{D}$  at a, b, c

$D_a = \vec{D}_{(+)} + \vec{D}_{(-)}$

field of source is  $\hat{a}_z$  and  $-\hat{a}_z$  direction.   
 field of  $+$  is  $\hat{a}_z$  and field of  $-$  is  $-\hat{a}_z$ .

$= \frac{\rho_S}{2} (-\hat{a}_z) + \frac{-\rho_S}{2} (\hat{a}_z)$

$= \rho_S (-\hat{a}_z) \frac{C}{m^2}$

في كل نقطة بين الصفيحتين  $\vec{D}$  هو صفر   
 في كل نقطة فوق الصفيحة  $+$   $\vec{D}$  هو  $-\rho_S \hat{a}_z$    
 في كل نقطة تحت الصفيحة  $-$   $\vec{D}$  هو  $-\rho_S \hat{a}_z$

$$\vec{D} = \rho_s \hat{a}_n$$

$$\vec{D} \cdot \hat{a}_n = \rho_s \hat{a}_n \cdot \hat{a}_n$$

$$\vec{D} \cdot \hat{a}_n = \rho_s$$

↓ field
↓ source

example: find  $\vec{D}$  at (4, 0, 3) <sup>field</sup> if there is a point charge  $-5\pi$  mC at (4, 0, 0) and a line charge  $3\pi$  mC/m along y-axis?

infinite :- باعتبار طول من طول y-axis

Sol  $\vec{D} = \vec{D}_q + \vec{D}_l$

$$\vec{D}_q = \frac{q}{4\pi r^2} \hat{a}_r = \frac{q \vec{r}}{4\pi r^3} = \frac{-5\pi 10^3 (3\hat{a}_z)}{(4\pi)(27)}$$

$$= -0.138 \hat{a}_z \frac{C}{m^3}$$

$$\vec{D}_l = \frac{\rho_l}{2\pi r} \hat{a}_\rho = \frac{\rho_l \vec{r}}{2\pi r^2}$$

$$= \frac{3\pi 10^3 (4, 0, 3)}{2\pi (25)}$$

$$= 0.24 \hat{a}_x + 0.18 \hat{a}_z \frac{mC}{m^2}$$

$$\vec{r} = (4, 0, 3) - (0, y, 0)$$

Shortest distance is when  $y=0$

$$\vec{r} = 4\hat{a}_x + 3\hat{a}_z$$

$$r = 5$$

$$\vec{D}_{total} = 240 \hat{a}_x + 42 \hat{a}_z \frac{\mu C}{m^2}$$



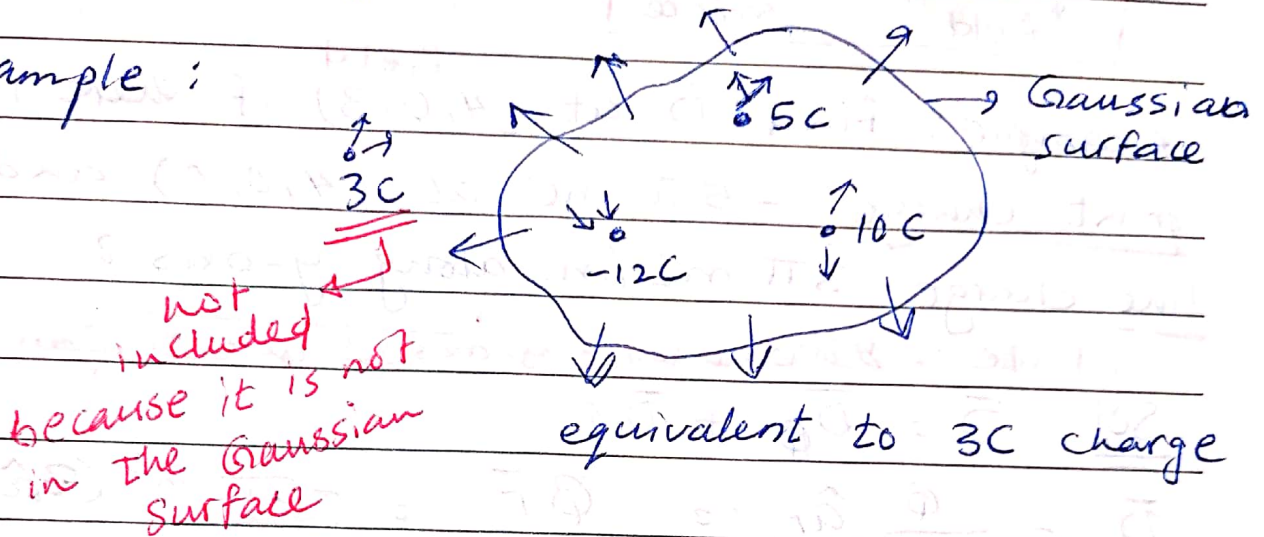
Gauss's law states that:

$$\oint_S \vec{D} \cdot d\vec{s} = \Phi_{\text{enclosed}}$$

→ *fixed area, gauss eqn do*

$$\vec{D} = \vec{E} \epsilon_0 \rightarrow \oint_S \vec{E} \epsilon_0 \cdot d\vec{s} = \Phi_{\text{enclosed}}$$

example:



→ This law is also called "Maxwell's 1<sup>st</sup> equation in integral form"

$\Phi_{\text{enclosed}}$  has four states →  $\Phi$  (point charge)  
 Gauss's law only works on  $\int \rho dl$  (line charge)  
infinite line and infinite sheet, but both of them  $\int \rho ds$  (surface charge)  
 have laws derivated from  $\int \rho dv$  (volume charge)  
 Coloumb's law so it is redundant to apply  
 Gauss's law on them.

# The main goal from Gauss law is to solve Volume charge density distribution questions.

\* source of the field is enclosed by the surface \*

Subject \_\_\_\_\_ Day \_\_\_\_\_ Date \_\_\_\_\_

$$\oint_S \vec{D} \cdot d\vec{s} = Q_{\text{enclosed}} = \int_V \rho_v dv$$

by applying the divergence theorem

للتكامل من  
السطح على السطح  
مغلق

$$\oint_S \vec{D} \cdot d\vec{s} = \int_V \nabla \cdot \vec{D} dv = \int_V \rho_v dv$$

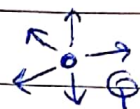
$$\nabla \cdot \vec{D} = \rho_v$$

$$\rho_s = \vec{D} \cdot \hat{a}_n$$

⇒ Maxwell's 1<sup>st</sup> equation in differential form (point form)

\* Applications of Gauss's law :-

1)  $\vec{E}$  or  $\vec{D}$  for a point charge

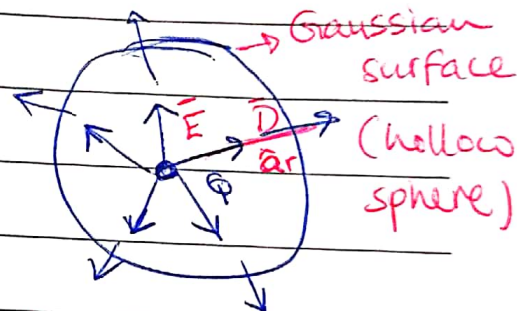


$$\oint_S \vec{D} \cdot d\vec{s} = Q_{\text{enclosed}}$$

$$Q_{\text{enclosed}} = Q$$

$$\vec{D} = D_r \hat{a}_r + D_\theta \hat{a}_\theta + D_\phi \hat{a}_\phi$$

because  $\vec{D}$  will be in  $r$  direction only



$d\vec{s}$  (السطح المغلق) ⇒ we get hollow sphere when  $r = \text{constant}$

so the normal will be  $\hat{a}_r$

$$d\vec{s} = r^2 \sin \theta d\theta d\phi \hat{a}_r$$

the sphere must be hollow because Gaussian surface is always 2D  
hollow → 2D  
solid → 3D

$$\int_0^{2\pi} \int_0^\pi D_r \hat{a}_r \cdot r^2 \sin \theta d\theta d\phi \hat{a}_r = Q$$

$$D_r r^2 \int_0^\pi \sin \theta d\theta \int_0^{2\pi} d\phi = Q$$

$$D_r r^2 (-\cos \theta \Big|_0^\pi) (\theta \Big|_0^{2\pi}) = Q$$

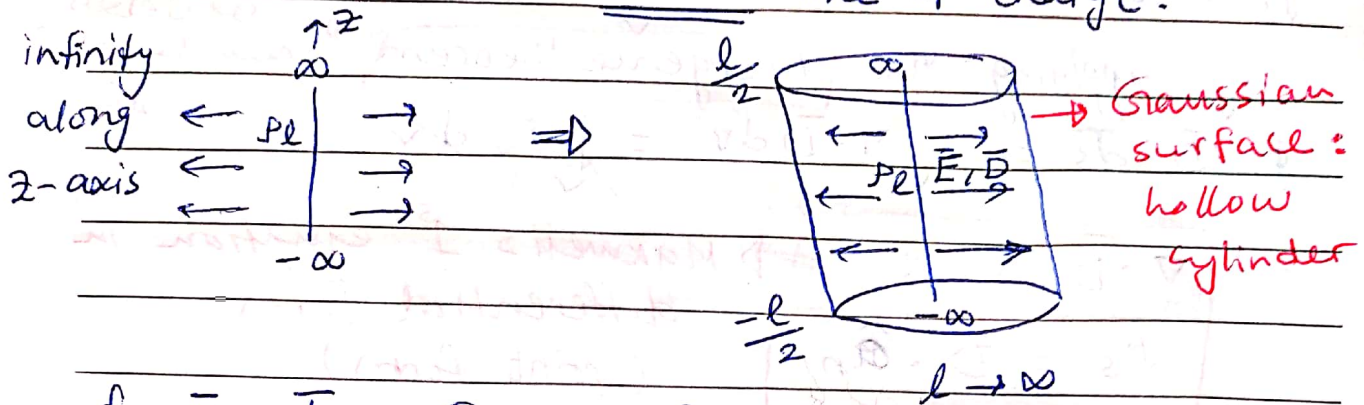
$$4\pi r^2 D_r = Q \Rightarrow D_r = \frac{Q}{4\pi r^2}$$

$$\vec{D} = \frac{Q}{4\pi r^2} \hat{a}_r, \quad \vec{E} = \frac{\vec{D}}{\epsilon_0} = \frac{Q}{4\pi \epsilon_0 r^2} \hat{a}_r$$

مساحة السطح



2)  $\vec{E}$  or  $\vec{D}$  for an infinite line of charge.



$$\oint_S \vec{D} \cdot d\vec{s} = Q_{enc} = \int \rho l \, dl$$

$$\vec{D} = D_\rho \hat{a}_\rho + \cancel{D_\theta \hat{a}_\theta} + \cancel{D_z \hat{a}_z}$$

*rho o b l k q e b k a b i s , o u r*

$$dl = dz \quad (\text{scalar because of } \theta)$$

$$d\vec{s} = \rho \, d\theta \, dz \, \hat{a}_\rho$$

$$\int_{-l/2}^{l/2} \int_0^{2\pi} D_\rho \hat{a}_\rho \cdot \rho \, d\theta \, dz \, \hat{a}_\rho = \int_{-l/2}^{l/2} \rho l \, dz$$

$$D_\rho \rho (2\pi) (l) = \rho l \, l$$

*المساحة الجائسة للسطح*

$$D_\rho = \frac{\rho l}{2\pi \rho}$$

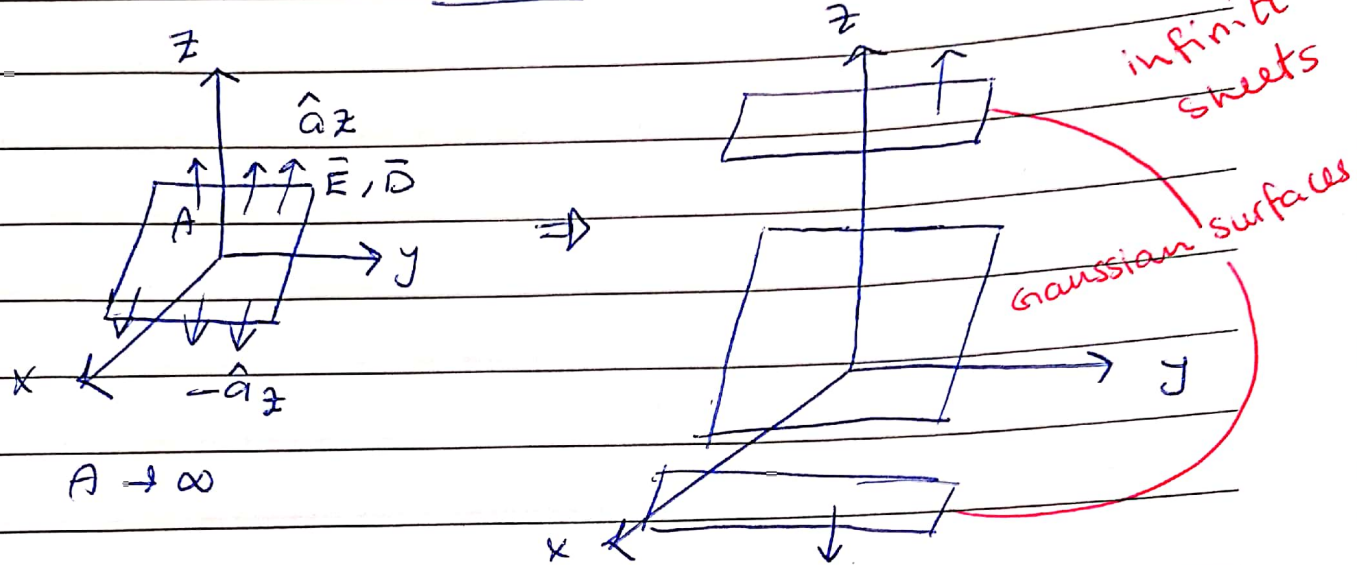
*وحيث ان l هي طول السطح الجائس و rho هي نصف قطر السطح الجائس و 2 pi rho هي المساحة الجائسة للسطح الجائس و l = infinity*

$$\vec{D} = \frac{\rho l}{2\pi \rho} \hat{a}_\rho$$

$$\vec{E} = \frac{\rho l}{2\pi \epsilon_0 \rho} \hat{a}_\rho$$

if the line is finite or with curvature, then use Coulomb's law to find  $\vec{E}$ ,  $\vec{D}$ , ...

3)  $\vec{E}$  or  $\vec{D}$  for an infinite sheet of charge.



$$\oint_S \vec{D} \cdot d\vec{s} = Q_{enc.} = \int_S \rho_s ds$$

$$\vec{D} = \begin{cases} Dz \hat{a}_z, & z > 0 \\ Dz (-\hat{a}_z), & z < 0 \end{cases} \quad ds = dx dy$$

$$d\vec{s}_{top} = dx dy \hat{a}_z$$

$$d\vec{s}_{bottom} = -dx dy \hat{a}_z$$

$$\int_{S_{top}} \vec{D} \cdot d\vec{s}_{top} + \int_{S_{bot.}} \vec{D} \cdot d\vec{s}_{bot.} = \int_S \rho_s ds$$

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} Dz \hat{a}_z \cdot dx dy \hat{a}_z + \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} Dz (-\hat{a}_z) \cdot dx dy (-\hat{a}_z) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \rho_s dx dy$$

$$Dz A + Dz A = \rho_s A, \quad \text{where } A = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} dx dy$$

$$2Dz = \rho_s \rightarrow Dz = \frac{\rho_s}{2}$$

$$\vec{D} = \begin{cases} \frac{\rho_s}{2} \hat{a}_z, & z > 0 \\ \frac{\rho_s}{2} (-\hat{a}_z), & z < 0 \end{cases} = \frac{\rho_s}{2} \hat{a}_n$$

$$\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_n$$

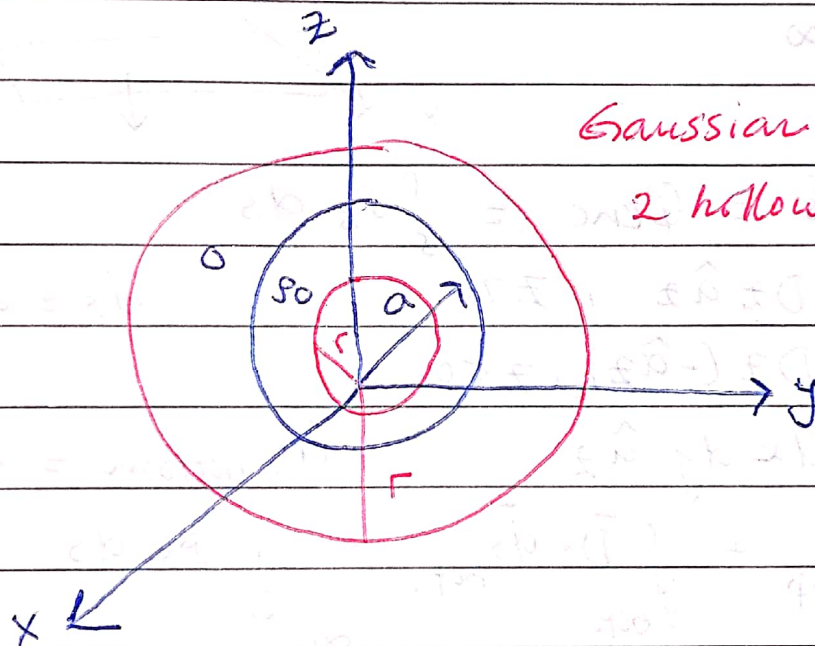


4)  $\vec{E}$  or  $\vec{D}$  for a uniform volume charge distribution:-  
 example; consider a sphere of radius  $a$  that carries a charge  $\rho_v = \begin{cases} \rho_0, & r < a \\ 0, & r > a \end{cases}$

find  $\vec{E}$  or  $\vec{D}$  everywhere?

↳ this indicates that we need to use Gauss's law.

Sol



Gaussian surface:  
2 hollow spheres

for  $0 < r < a$  ( $r = \bar{a}$ )  $\Rightarrow \oint \vec{D} \cdot d\vec{s} = Q_{enc} = \int \rho_v dv$

$\vec{D} = D r \hat{a}_r$

$d\vec{s} = r^2 \sin\theta d\theta d\phi \hat{a}_r$

$dv = r^2 \sin\theta dr d\theta d\phi$

$\oint_S \vec{D} \cdot d\vec{s} = \int \rho_v dv$

$\int_0^{2\pi} \int_0^\pi \int_0^r D r \hat{a}_r \cdot r^2 \sin\theta d\theta d\phi \hat{a}_r = \int_0^{2\pi} \int_0^\pi \int_0^r \rho_0 r^2 \sin\theta dr d\theta d\phi$

$4\pi r^2 D r = \rho_0 \left( \frac{4\pi r^3}{3} \right) \rightarrow \rho_0 \frac{4\pi r^3}{3}$

$D r = \frac{\rho_0 r}{3}$

$$\left. \begin{aligned} \bar{D} &= \frac{\rho_0 r}{3} \hat{a}_r \\ \bar{E} &= \frac{\rho_0 r}{3\epsilon_0} \hat{a}_r \end{aligned} \right\} \rightarrow 0 < r < a$$

at  $r = a \rightarrow \bar{D} = \frac{\rho_0 a}{3} \hat{a}_r$  از اطراف، کجای نیست  
عنه  $r > a$  يكون

$$\bar{E} = \frac{\rho_0 a}{3\epsilon_0} \hat{a}_r$$

الاقصان متصل

for  $a < r < \infty \Rightarrow \oint_s \bar{D} \cdot d\bar{s} = \int_v \rho_v dv$

$$4\pi r^2 D_r = \int_0^{2\pi} \int_0^{\pi} \int_0^a \rho_0 r^2 \sin\theta d\theta d\phi dr + \cancel{\int_0^{2\pi} \int_0^{\pi} \int_r^{\infty} \rho_0 r^2 \sin\theta d\theta d\phi dr} \text{ zero}$$

$$4\pi r^2 D_r = \left( \frac{4\pi a^3}{3} \right) \rho_0$$

$$D_r = \frac{\rho_0 a^3}{3r^2}$$

$$\left. \bar{D} = \frac{\rho_0 a^3}{3r^2} \hat{a}_r \right\} \rightarrow a < r < \infty$$

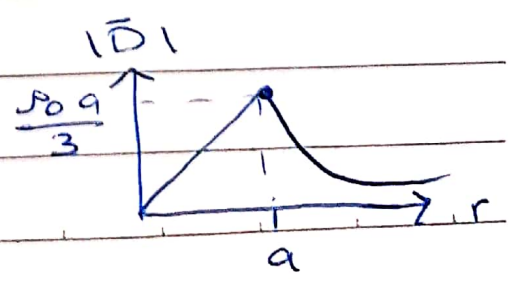
$$\bar{E} = \frac{\rho_0 a^3}{3\epsilon_0 r^2} \hat{a}_r$$

at  $r = a \rightarrow \bar{D} = \frac{\rho_0 a}{3} \hat{a}_r$  طرح نیست ای  
متعلق عننا صا

$$\bar{E} = \frac{\rho_0 a}{3\epsilon_0} \hat{a}_r$$

متصل

$$\bar{D} = \begin{cases} \frac{\rho_0 r}{3} \hat{a}_r, & 0 < r < a \\ \frac{\rho_0 a^3}{3r^2} \hat{a}_r, & a < r < \infty \end{cases}$$





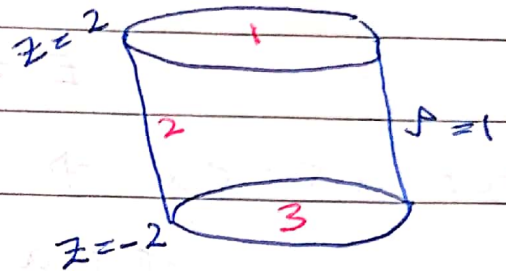
Example; Given  $\vec{D} = z\rho \cos^2 \theta \hat{a}_z \frac{C}{m^2}$ , calculate the total charge enclosed by the cylinder of radius 1m with  $-2 \leq z \leq 2$ ?

Sol  $Q_{\text{enclosed}} = \oint_S \vec{D} \cdot \vec{ds} = \int_V \rho_V dv = Q$

$$\vec{ds}_1 = \rho d\theta d\rho \hat{a}_z$$

$$\vec{ds}_2 = \rho d\theta dz \hat{a}_\rho$$

$$\vec{ds}_3 = -\rho d\rho d\theta \hat{a}_z$$



$$Q = \int_{S_1} \vec{D} \cdot \vec{ds}_1 + \int_{S_2} \vec{D} \cdot \vec{ds}_2 + \int_{S_3} \vec{D} \cdot \vec{ds}_3$$

equal zero because  $\vec{D}$  given is

in the direction of  $\hat{a}_z$

$$Q = \int_0^{2\pi} \int_0^1 z\rho \cos^2 \theta \rho d\rho d\theta + \int_{-2}^2 \int_0^{2\pi} -z\rho \cos^2 \theta \rho d\rho d\theta$$

$$Q = \frac{2\pi}{3} + \frac{2\pi}{3} = \frac{4\pi}{3} C$$

Surface charge density  $\rightarrow \rho_s = \vec{D} \cdot \hat{a}_n \rightarrow \hat{a}_z$  (top)  $\rightarrow -\hat{a}_z$  (bottom)

$$\vec{F} = q \vec{E}$$

Work (W) = Force ( $\vec{F}$ ) \* Distance ( $\vec{l}$ )

$$dW = - \vec{F} \cdot d\vec{l}$$

↳ the work is done by an external agent

$$\int dW = - \int q \vec{E} \cdot d\vec{l}$$

$$W = - q \int \vec{E} \cdot d\vec{l}$$

$$\frac{W}{q} = V = - \int \vec{E} \cdot d\vec{l}$$

عشان نفهم، خذنا على فرق جهد  
 مثلا، 1V كذا 1 كولوم بيتولد 1 جول  
 مثلا، 4J لنتقل شحنة 4 كولوم

$$V_{AB} = V_B - V_A$$

↳ if  $V_{AB}$  is positive →  $\uparrow$  gain in potential.

2) work is done by the external field.

↳ if  $V_{AB}$  is negative →  $\downarrow$  drop in potential.

2) work is done by the field itself.

For a point charge ⇒  $V_{AB} = - \int \vec{E} \cdot d\vec{l}$

$$= - \int_{r_A}^{r_B} \frac{q}{4\pi\epsilon_0 r^2} \hat{r} \cdot dr \hat{r}$$

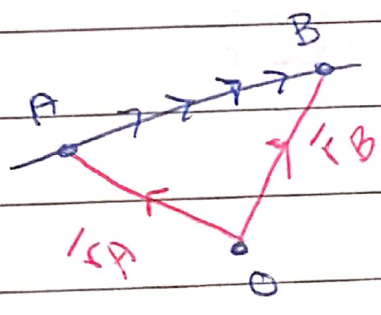
$$= \frac{q}{4\pi\epsilon_0} \left[ \frac{1}{r} \right]_{r_A}^{r_B}$$

$$= \frac{q}{4\pi\epsilon_0 r_B} - \frac{q}{4\pi\epsilon_0 r_A}$$

if point A is located

at  $\infty$  then  $V_A = 0$ ,  $r \rightarrow \infty$

$$= V_B - V_A$$





$$V_{AB} = V_{\infty B} = V_B - V_{\infty} = V_B - 0 = V_B$$

$V_{\infty} = 0$  when  $r_{\infty} \rightarrow \infty$  → reference reference

•  $V_{\infty}$  potential  $\infty$   $\rightarrow$   $V_{\infty} = 0$  (reference)

$$V = \frac{Q}{4\pi\epsilon_0 r} \quad \text{if reference is at } \infty \text{ (point charge case)}$$

For line charge  $\Rightarrow V = \int \frac{\rho_l dl}{4\pi\epsilon_0 r}$

For surface charge  $\Rightarrow V = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r}$

For volume charge  $\Rightarrow V = \int_V \frac{\rho_v dv}{4\pi\epsilon_0 r}$   
 potential  $\leftarrow$   $\leftarrow$  volume

in the book dash is used to refer to the volume,  $V(\vec{r}) = \int_{V'} \frac{\rho_v(\vec{r}')}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|} d\tau'$

For N-point charges  $\Rightarrow V = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k}{|\vec{r} - \vec{r}'_k|}$

$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$  but  $V = \frac{Q}{4\pi\epsilon_0 r}$

Example; Two point charges  $-4\mu\text{C}$  and  $5\mu\text{C}$  are located at  $(2, -1, 3)$  and  $(0, 4, -2)$ . find the potential at  $(1, 0, 1)$

Sol reference is at  $\infty$ ,  $V_{\infty} = \text{zero}$

$$V = V_1 + V_2$$

$$= 4 \cdot 10^{-6}$$

$$+ 5 \cdot 10^{-6}$$

$$4\pi \left( \frac{10^{-9}}{36\pi} \right) |(-1, 1, -2)|$$

$$4\pi \left( \frac{10^{-9}}{36\pi} \right) |(1, -4, 3)|$$

$$V = \ominus 5.872 \text{ KV}$$

work is done by the field itself.

Example; a point charge of  $5\text{nC}$  located at  $(-3, 4, 0)$  and a line  $y=1, z=1$  carries a uniform charge of  $2\text{nC/m}$ . if  $V = 100 \text{ V}$  at B  $(1, 2, 1)$ . find V at point C  $(-2, 5, 3)$

reference

Sol  $V_{BC} = V_C - V_B$

$$= V_C - 100 \rightarrow V_C = V_{BC} + 100$$

$$V_{BC} = V_Q + V_L$$

$$V_Q = - \int_{r_B}^{r_C} \vec{E} \cdot d\vec{r} = - \int_{r_B}^{r_C} \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \cdot dr \hat{a}_r$$

$$= \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_C} - \frac{1}{r_B} \right)$$

$$r_C = |(-2, 5, 3) - (-3, 4, 0)| = |(1, 1, 3)| = \sqrt{11}$$

$$r_B = |(1, 2, 1) - (-3, 4, 0)| = |(4, -2, 1)| = \sqrt{21}$$

$$V_L = - \int_{p_B}^{p_C} \vec{E} \cdot d\vec{r} = - \int_{p_B}^{p_C} \frac{\rho L}{2\pi\epsilon_0 r} \hat{a}_p \cdot dp \hat{a}_p$$

$$= \frac{-\rho L}{2\pi\epsilon_0} (\ln p_C - \ln p_B)$$



$$= \frac{-\rho U}{2\pi \epsilon_0} \ln\left(\frac{\rho_C}{\rho_B}\right)$$

$$\rho_C = |(-2, 5, 3) - (x, 1, 1)| = |(0, 4, 2)| = \sqrt{20}$$

$$x = -2 \text{ fix } \underline{\text{solution}} \leftarrow$$

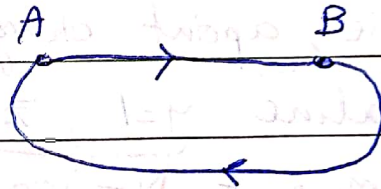
$$\rho_B = |(1, 2, 1) - (1, 1, 1)| = |(0, 1, 0)| = 1$$

$$V_{BC} = -50 \cdot 175 \text{ V}$$

$$V_C = V_{BC} + V_B = 49.825 \text{ V}$$

How to find  $\vec{E}$  from  $V$ ?

$$V_{AB} = -\int_A^B \vec{E} \cdot d\vec{l}$$



$$\oint \vec{E} \cdot d\vec{l} = -\oint \vec{E} \cdot d\vec{l}$$

for closed path

$$\oint \vec{E} \cdot d\vec{l} = -\int_A^B \vec{E} \cdot d\vec{l} + -\int_B^A \vec{E} \cdot d\vec{l}$$

$$= -\int_A^B \vec{E} \cdot d\vec{l} + \int_A^B \vec{E} \cdot d\vec{l}$$

$$= \text{zero}$$

$$\oint \vec{E} \cdot d\vec{l} = \text{zero}$$

always

equi-potential surface

$$V_{AA} = V_A - V_A = 0$$

2<sup>nd</sup> Maxwell's equation in integral form

to convert it into differential form, we use

$$\text{Stoke's theorem} \Rightarrow \oint_L \vec{E} \cdot d\vec{l} = \int_S \nabla \cdot \vec{E} \cdot d\vec{s} = 0$$

electric field

is irrotational  
(conservative)

$$\nabla \times \vec{E} = 0$$

2<sup>nd</sup> Maxwell's equation in differential form

let:  $\vec{E} = E_x \hat{a}_x + E_y \hat{a}_y + E_z \hat{a}_z$

$$d\vec{l} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

$$V = - \int_L \vec{E} \cdot d\vec{l} \rightarrow dV = - \vec{E} \cdot d\vec{l}$$

$$dV = - (E_x dx + E_y dy + E_z dz)$$

assume,  $dV = \frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz$

$$\frac{\partial V}{\partial x} dx = -E_x dx \rightarrow E_x = -\frac{\partial V}{\partial x}$$

$$E_y = -\frac{\partial V}{\partial y}$$

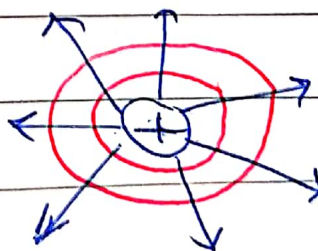
$$E_z = -\frac{\partial V}{\partial z}$$

$$\vec{E} = - \left( \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z \right) = - \nabla V \text{ (gradient)}$$

$$\vec{E} = - \nabla V$$

Equi-Potential Surface :-

potential





Example; Given the potential  $V = \frac{10}{r^2} \sin \theta \cos \theta$

(a) find  $\vec{D}$  at  $(2, \frac{\pi}{2}, 0)$

(b) calculate the work done in moving a  $10 \mu\text{C}$  charge from A  $(1, 30^\circ, 120^\circ)$  to B  $(4, 90^\circ, 60^\circ)$

Sol a)  $\vec{E} = -\nabla V$

$\vec{D} = \epsilon_0 \vec{E} = -\epsilon_0 \nabla V$

the source is unknown so we can't use Coulomb

$\vec{E} = -\left(\frac{\partial V}{\partial r} \hat{a}_r + \frac{\partial V}{r \partial \theta} \hat{a}_\theta + \frac{\partial V}{r \sin \theta \partial \phi} \hat{a}_\phi\right)$  or Gauss

$= \frac{20}{r^3} \sin \theta \cos \theta \hat{a}_r - \frac{10}{r^3} \cos \theta \cos \theta \hat{a}_\theta + \frac{10}{r^3} \sin \theta \hat{a}_\phi$

$\vec{D} = \epsilon_0 \vec{E} = \epsilon_0 \frac{20}{8} \hat{a}_r = 22.1 \text{ pC/m}^2$   
at  $(2, \frac{\pi}{2}, 0)$

b)  $W = Q V_{AB} = Q (V_B - V_A)$

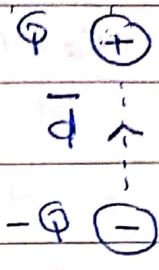
$= 10 \cdot 10^{-6} \left( \frac{10}{16} (1) \left(\frac{1}{2}\right) - \frac{10}{1} \left(\frac{1}{2}\right) \left(-\frac{1}{2}\right) \right)$

$= 10 \cdot 10^{-6} \left( \frac{45}{16} \right) = 28.125 \mu\text{J}$

Method 2  $\Rightarrow W = -Q \int \vec{E} \cdot d\vec{l}$

$= -Q \left[ \int_{r_A}^{r_B} E_r dr + \int_{\theta_A}^{\theta_B} E_\theta r d\theta + \int_{\phi_A}^{\phi_B} E_\phi r \sin \theta d\phi \right]$

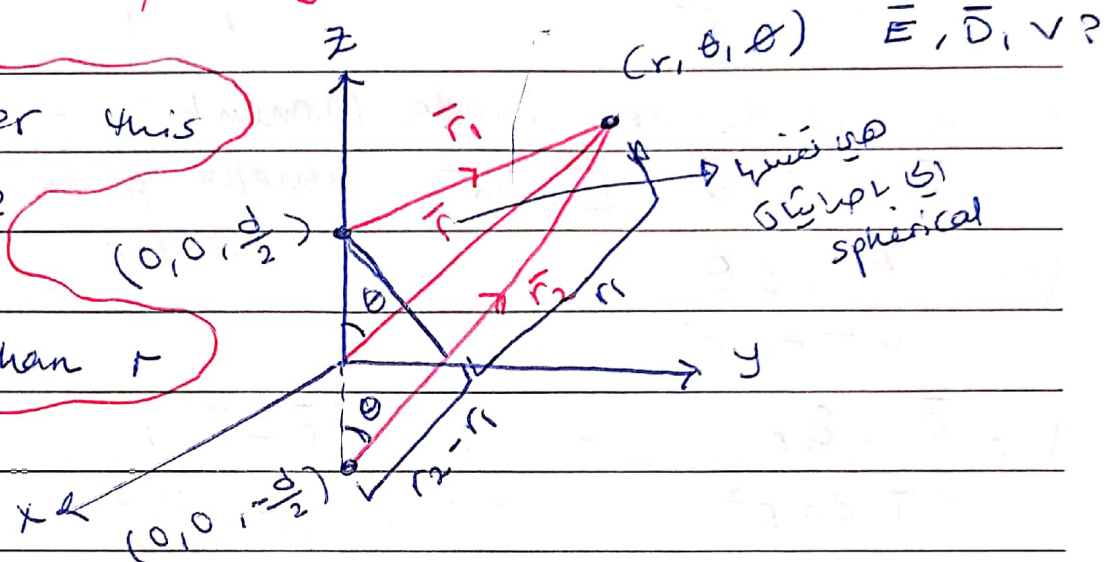
$\int_{r_A}^{r_B}$   $\int_{\theta_A}^{\theta_B}$   $\int_{\phi_A}^{\phi_B}$   
 هذه تكامل بالنسبة لـ  $r$   $\theta$   $\phi$   
 من  $r_A$  إلى  $r_B$   $\theta$  من  $\theta_A$  إلى  $\theta_B$   $\phi$  من  $\phi_A$  إلى  $\phi_B$   
 من  $(4, 30^\circ, 120^\circ)$  من  $(4, 90^\circ, 120^\circ)$  من  $(4, 90^\circ, 60^\circ)$   
 هذه  $\theta$   $\phi$   $r$   $\theta$   $\phi$   $r$   $\theta$   $\phi$   $r$   $\theta$   $\phi$



very small distance

$Q$  and  $-Q$  are equal in magnitude  
different in polarity.

To consider this as a dipole  $d$  must be much less than  $r$



$$V = V_+ + V_- \quad , \quad V_\infty = 0 \text{ (reference)}$$

$$= \frac{Q}{4\pi\epsilon_0 r_1} + \frac{-Q}{4\pi\epsilon_0 r_2}$$

$$= \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_1} - \frac{1}{r_2} \right)$$

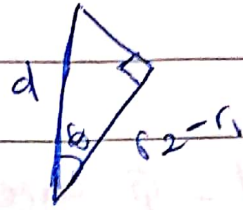
$$= \frac{Q (r_2 - r_1)}{4\pi\epsilon_0 r_1 r_2} \quad !! \quad \text{usually } Q \text{ and } d \text{ are not known}$$

$r_2 \approx r_1$  in the direction of  $z$ -axis extension is  $\theta$  angle  
 $r_2 \approx r_1$  in the direction of  $z$ -axis extension is  $\theta$  angle  
 $r \approx r_1 \approx r_2$

$$r_1 r_2 = r^2$$



$$\cos \theta = \frac{r_2 - r_1}{d}$$



$$r_2 - r_1 = d \cos \theta$$

$$V = \frac{Q (d \cos \theta)}{4 \pi \epsilon_0 r^2}$$

we still don't know  $Q$  and  $d$

so we will define "Dipole Moment" :-

$$\vec{p} = Q \vec{d} \quad [\text{C}\cdot\text{m}] \quad \text{usually given as a vector}$$

$$V = \frac{p \cos \theta}{4 \pi \epsilon_0 r^2}$$

$$V = \frac{\vec{p} \cdot \hat{a}_r}{4 \pi \epsilon_0 r^2} = \frac{\vec{p} \cdot (\vec{r} - \vec{r}')}{4 \pi \epsilon_0 |\vec{r} - \vec{r}'|^3}$$

For  $N$ -dipoles :

$$V = \frac{1}{4 \pi \epsilon_0} \sum_{k=1}^N \frac{\vec{p}_k \cdot (\vec{r} - \vec{r}'_k)}{|\vec{r} - \vec{r}'_k|^3}$$

field
center of the dipole

$$\vec{E} = \vec{E}_+ + \vec{E}_-$$

(or)  $\vec{E} = -\nabla V$  in spherical coordinate

$$= - \left( \frac{\partial V}{\partial r} \hat{a}_r + \frac{\partial V}{r \partial \theta} \hat{a}_\theta \right) \quad \text{since } V \text{ is independent on } \theta$$

scalar

$$\vec{E} = \frac{p}{4 \pi \epsilon_0 r^3} (2 \cos \theta \hat{a}_r + \sin \theta \hat{a}_\theta) \quad \frac{V}{m} \quad (\text{vector})$$

$$\vec{D} = \vec{E} \epsilon_0$$

$$V = \frac{\vec{p} \cdot \hat{a}_r}{4 \pi \epsilon_0 r^2} \quad (\text{scalar})$$

point charge

$$E \propto \frac{1}{r^2}$$

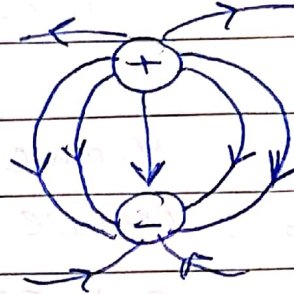
$$V \propto \frac{1}{r}$$

electric dipole

$$E \propto \frac{1}{r^3}$$

$$V \propto \frac{1}{r^2}$$

Flux Lines :



Example ; Two dipoles with dipole moments  $-5\hat{a}_z \text{ nC}\cdot\text{m}$  and  $9\hat{a}_z \text{ nC}\cdot\text{m}$  are located at  $(0,0,-2)$  and  $(0,0,3)$  find the potential and  $\bar{E}$  at the origin?

Sol  $V = \frac{\bar{P} \cdot (\bar{r} - \bar{r}')}{4\pi\epsilon_0 |\bar{r} - \bar{r}'|^3}$

reference is at  $\infty$ 

$$= \frac{(-5\hat{a}_z 10^{-9}) (2\hat{a}_z)}{4\pi \frac{10^{-9}}{36\pi} (8)} + \frac{(9\hat{a}_z 10^{-9}) (-3\hat{a}_z)}{4\pi \frac{10^{-9}}{36\pi} (27)}$$

$$= -20.25 \text{ V}$$

$$\bar{E}_1 = \frac{P_1}{4\pi\epsilon_0 r_1^3} (2\cos\theta \hat{a}_r + \sin\theta \hat{a}_\theta)$$

$r_1 = 2 \text{ m}$

$r_2 = 3 \text{ m}$

$$P_1 = 5 \text{ n}\cdot\text{m}$$

$$P_2 = 9 \text{ n}\cdot\text{m}$$

$\theta_1 = 180^\circ$

$\theta_2 = 180^\circ$

$\theta$  is the angle between  $\bar{P}_z$  and  $\bar{r}$

$$\left. \begin{array}{l} \bar{r}_1 = 2\hat{a}_z \\ \bar{P}_1 = -5\hat{a}_z \end{array} \right\} 180^\circ$$

$$\left. \begin{array}{l} \bar{r}_2 = -3\hat{a}_z \\ \bar{P}_2 = 9\hat{a}_z \end{array} \right\} 180^\circ$$

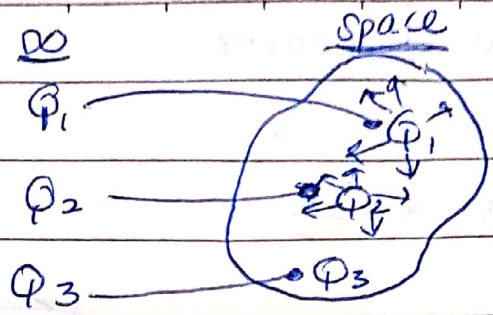


space کی  $\infty$  سے  $Q_1$  تک

ما،  $Q_1$  کے لیے  $Q_2$  کی طرف

force کی space

تک



$$W = QV = \text{zero}$$

$$Q_1 \rightarrow Q_2 \rightarrow Q_3$$

potential difference = zero because  $V_{\infty} = 0$   
 and  $V_{\text{space}} = 0$  because the space is empty

electric field intensity for  $Q_1$  کی  $Q_2$  کی طرف

force کی  $Q_1$  &  $Q_2$  کی  $Q_3$  کی طرف

$W_E$  = electrical energy

$$W_E = W_1 + W_2 + W_3$$

$$= Q_1(0) + Q_2 V_{12} + Q_3 (V_{13} + V_{23}) \dots \textcircled{1}$$

(if  $Q_1 \rightarrow Q_2 \rightarrow Q_3$ )

$$\text{if } (Q_3 \rightarrow Q_2 \rightarrow Q_1) \Rightarrow W_E = W_1 + W_2 + W_3$$

$$= Q_1 (V_{31} + V_{21}) + Q_2 V_{32} + 0 \dots \textcircled{2}$$

$$\textcircled{1} + \textcircled{2} \dots 2W_E = Q_1 (V_{21} + V_{31}) + Q_2 (V_{12} + V_{32}) + Q_3 (V_{13} + V_{23})$$

$$W_E = \frac{1}{2} [Q_1 V_1 + Q_2 V_2 + Q_3 V_3]$$

$$W_E = \frac{1}{2} \sum_{k=1}^N Q_k V_k \quad [\text{Joule}]$$





Energy Density ( $w_E$ )  $\rightarrow$   $w$  is small while in  $W$  is capital energy

$$w_E = \frac{W_E}{\text{volume}} \left[ \frac{J}{m^3} \right]$$

$$= \frac{1}{2} \vec{E} \cdot \vec{D} = \frac{1}{2} E^2 \epsilon_0 = \frac{1}{2} \frac{D^2}{\epsilon_0}$$

$$W_E = \int_V w_E dV$$

Example; The point charges  $-1\mu C$ ,  $4\mu C$  and  $3\mu C$  are located at  $(0,0,0)$ ,  $(0,0,1)$  and  $(1,0,0)$  find the energy in the system?

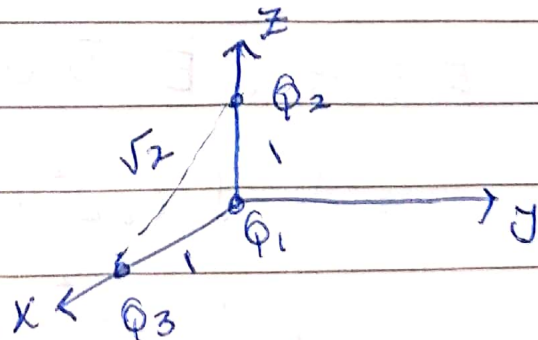
Sol  $W_E = \frac{1}{2} \sum_{k=1}^N Q_k V_k$

$$= \frac{1}{2} (Q_1 V_1 + Q_2 V_2 + Q_3 V_3)$$

$$= \frac{1}{2} [Q_1 (V_{21} + V_{31}) + Q_2 (V_{12} + V_{32}) + Q_3 (V_{13} + V_{23})]$$

$$= \frac{1}{2} \left[ Q_1 \left( \frac{Q_2}{4\pi\epsilon_0(1)} + \frac{Q_3}{4\pi\epsilon_0(1)} \right) + Q_2 \left( \frac{Q_1}{4\pi\epsilon_0(1)} + \frac{Q_3}{4\pi\epsilon_0(\sqrt{2})} \right) + Q_3 \left( \frac{Q_1}{4\pi\epsilon_0(1)} + \frac{Q_2}{4\pi\epsilon_0(\sqrt{2})} \right) \right]$$

$$= 13.37 \mu J$$





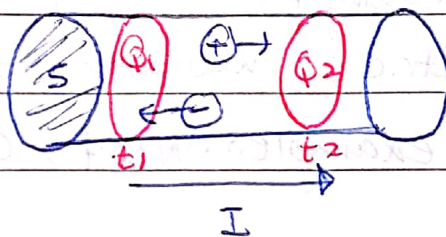


Electric Current :

$I = \frac{dQ}{dt}$  to get (1A) current, you need to move a charge of (1C) in duration of (1s)

for uniform cross section we use delta, if not we use  $ds$

$J = \frac{I}{\Delta s} \left[ \frac{A}{m^2} \right]$   
 ↳ Current density

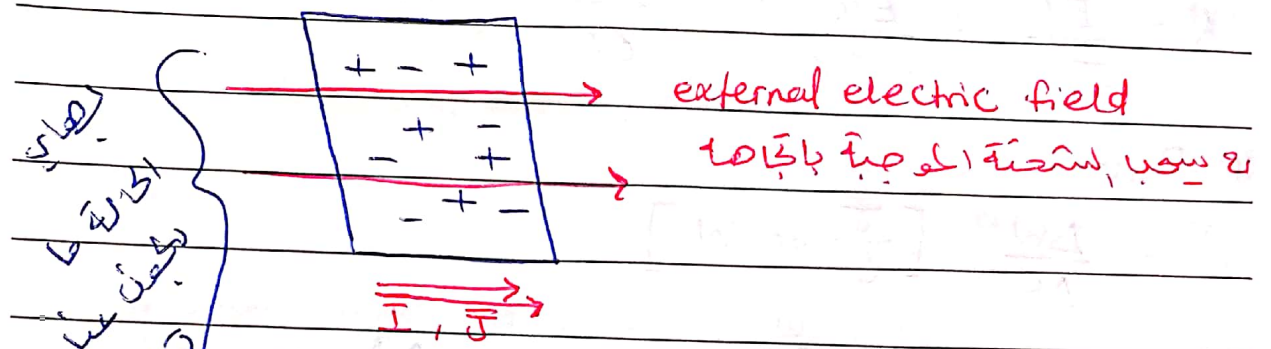


$J = \frac{dI}{ds}$

$\int dI = \int J ds$

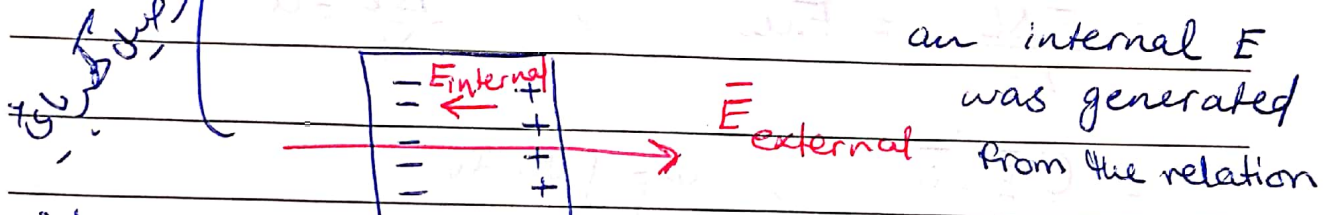
$I = \int_s \vec{J} \cdot d\vec{s} \rightarrow \text{scalar}$

$\Psi = \int \vec{D} \cdot d\vec{s}$



external electric field

ع سبب، لشحنة الموجبة باتجاه



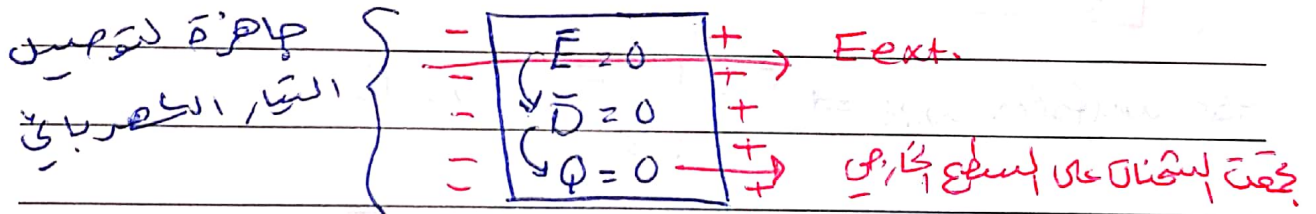
an internal  $E$  was generated from the relation

$$\vec{E} = -\nabla V$$

منه على فرق جهد (طرف موجب، طرف سالب)

التي  $E$  لا تكون صفر

$$\vec{E}_{total} = \text{zero} \quad \& \quad \vec{E}_{int.} = -\vec{E}_{ext.}$$



قوة لفرق الجهد  
التي، الكهرطيسي

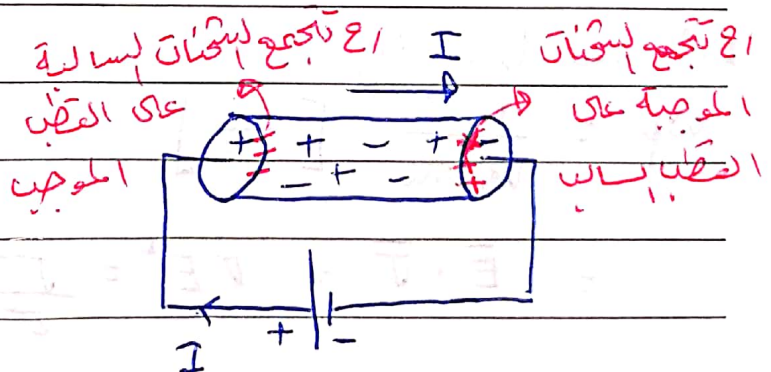
جهد إمكان على سطح كروي

للا دة على القطع على الأثران  $V_{difference} = 0$

So the conductor became equipotential body.

\* Resistance :-

$$R = \frac{V}{I} = \frac{\int_l \vec{E} \cdot d\vec{l}}{\int_s \vec{J} \cdot d\vec{s}}$$



$$R = \frac{l}{\sigma A} = \frac{\rho l}{A} \quad \text{where} \quad \rho = \frac{1}{\sigma}$$

for uniform cross section wire



$$R = \frac{EL}{Js} = \frac{EL}{\sigma E s} = \frac{l}{\sigma s} \quad (\text{because its uniform})$$

\* Power :

$$P = \frac{\Delta W}{\Delta t} \quad \left[ \frac{J}{s} \text{ or } W \right]$$

$$= \frac{F \Delta l}{\Delta t} = \bar{F} \cdot \bar{u} \quad , \quad \frac{\Delta l}{\Delta t} = u$$

$$= \Phi \bar{E} \cdot \bar{u} \quad , \quad \Phi = \int \rho_v dv$$

$$= \int \rho_v \bar{E} \cdot \bar{u} dv \quad , \quad \bar{J} = \rho_v \bar{u}$$

$$= \int_V \bar{E} \cdot \bar{J} dv \rightarrow \text{Joule's law}$$

for uniform wire  $\Rightarrow P = \int \int \bar{E} \cdot \bar{J} ds dl$

$$= - \int_l \bar{E} \cdot d\bar{l} \int_s \bar{J} \cdot d\bar{s}$$

$$P = V \cdot I = I^2 R$$

\* Power Density :-

$$\omega_p = \frac{\text{power}}{\text{volume}} \quad \left[ \frac{W}{m^3} \right]$$

$$= \bar{E} \cdot \bar{J} = \sigma E^2 = \frac{J^2}{\sigma}$$

Example; if  $\vec{J} = \frac{1}{3} (2\cos\theta \hat{a}_r + \sin\theta \hat{a}_\theta)$   $A/m^2$

find  $I$  for:

(a) a hemi-spherical shell of radius 20 cm with  $0 < \theta < \frac{\pi}{2}$

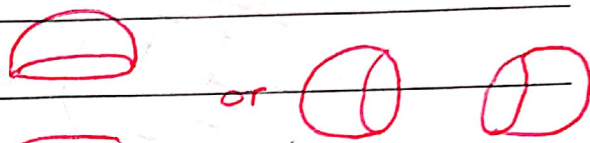
hemi (نصف)  $\rightarrow$  3D  
half  $\rightarrow$  1D

(b) a spherical shell of radius 10 cm.

Sol (a)  $I = \int_S \vec{J} \cdot d\vec{s}$

نصف الكرة على وجهي جالسيين

$d\vec{s} = r^2 \sin\theta d\theta d\phi \hat{a}_r$



$I = \int_0^{2\pi} \int_0^{\pi/2} \frac{1}{3} \sin 2\theta d\theta d\phi$   
 $r = 0.2m$

but  $\phi$  is complete horizontal rotation ( $0 < \phi < 2\pi$ )

$= 10\pi A$

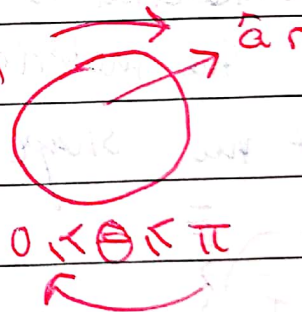
$\rightarrow$  so this shape that should be used.

(b)  $I = \int_S \vec{J} \cdot d\vec{s}$

النيار ابي، ع عيشه على الجزء العلوي على الكرة، ع

$I = \text{zero}$

عيشه نفسه ليس جالسي



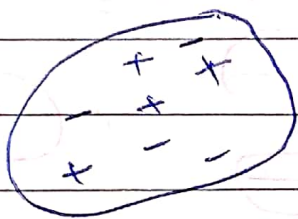
$0 < \theta < \pi$  | لا جابه على السطح السفلي للكرة .



Dielectrics  $\begin{cases} \rightarrow \text{non polar} \\ \rightarrow \text{polar (permanent dipoles)} \end{cases}$

$$\bar{P} = \lim_{\Delta V \rightarrow 0} \frac{\sum_{K=1}^N \bar{P}_K}{\Delta V}$$

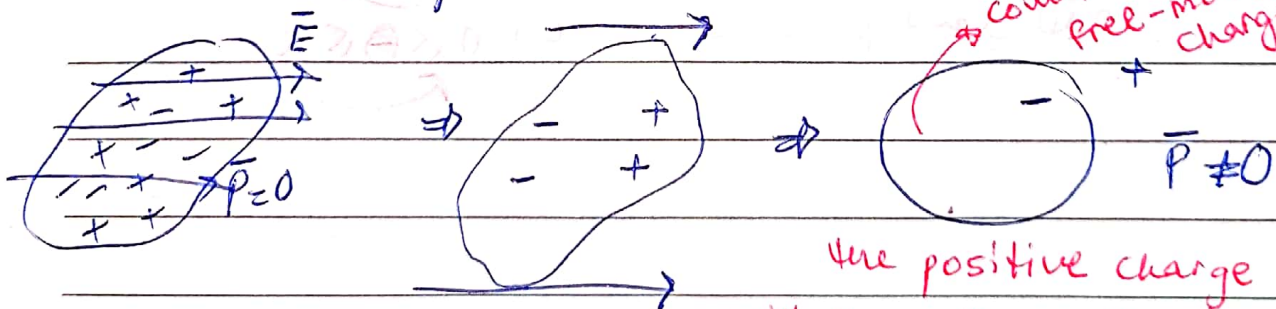
example; non polar dielectric ( $H_2, O_2, N_2$ , rare gases)



charges are not distributed on the sides of the material  $\rightarrow \Phi_{total} = 0$   
 so  $\bar{P} = 0$

$\bar{P} = 0$   $\begin{cases} \rightarrow \text{has dipoles with dipole moment} = 0 \\ \rightarrow \text{has no dipoles at all (nonpolar material)} \end{cases}$

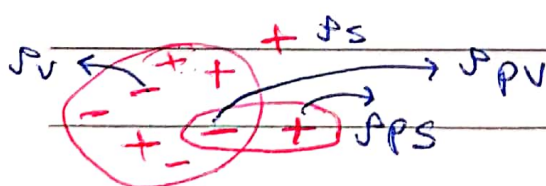
if this material is put under an external electric field, the material will exhibit a force that will effect the shape due to pressure.



$\rightarrow$  could contain free-moving charges

the positive charge will go on the outer perimeter of the surface

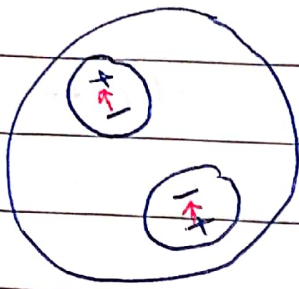
while the -ve charge will remain inside the surface



$J_s$ : free moving charge

$J_{pv} / J_{ps}$ : polarization

Polar :-

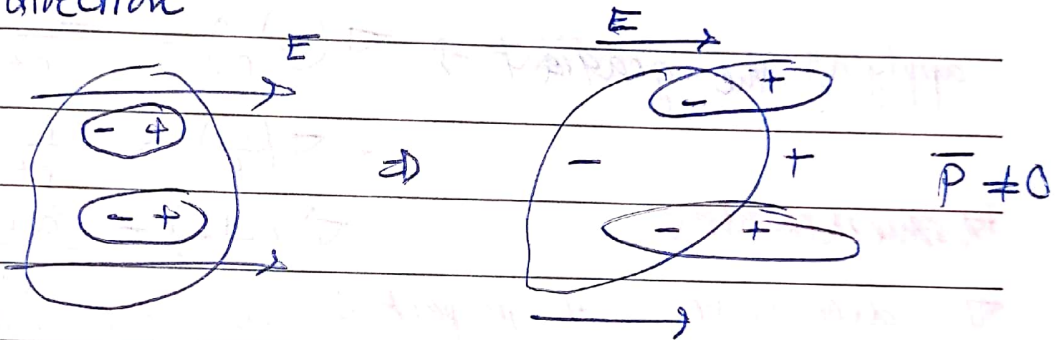


at equilibrium  $\rightarrow Q_{total} = 0$

These two dipoles have dipole moments in opposite directions so the sum equals zero.

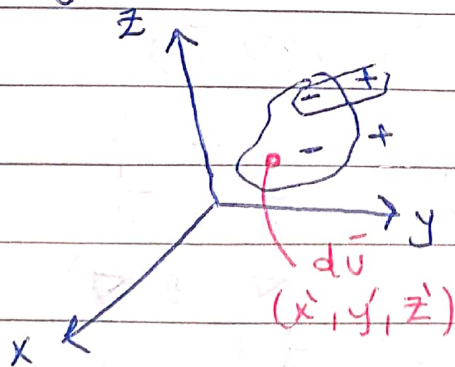
$\bar{P} = 0$

if this material is put under an external E.F, it will effect the positive charges to be aligned in the E.F direction



So, whatever the material was polar or non-polar, the result after electric field is applied will be always (Polarized Dielectric)

\* Finding the Potential / Electric Field  $\left\{ \begin{matrix} \text{density} \\ \text{intensity} \end{matrix} \right.$  :-



$(x, y, z)$

The potential at  $(x, y, z)$  will be due to bound surface charge distribution and free surface distribution

and bound volume C.D and free volume C.D

So we will need to see the effect of these four charge individually



$$dV = \frac{\bar{p} \cdot \hat{a}_r}{4\pi\epsilon_0 r^2} \quad (\text{due to one dipole})$$

so we need to integrate both sides in order to consider the whole volume

$$\int_V dV = \int_{V'} \frac{\bar{p} \cdot \hat{a}_r}{4\pi\epsilon_0 r^2}$$

$$V = \int_{V'} \frac{\bar{p} \cdot \hat{a}_r}{4\pi\epsilon_0 r^2} dV'$$

applying the gradient  $\rightarrow \nabla\left(\frac{1}{r}\right) = -\frac{1}{r^2} \hat{a}_r$

$$-\nabla\left(\frac{1}{r}\right) = \frac{1}{r^2} \hat{a}_r$$

~~to be derivative~~

$$\nabla'\left(\frac{1}{r}\right) = \frac{\hat{a}_r}{r^2}$$

$\nabla$ : derivative with respect to the field point  $(x, y, z)$

$\nabla'$ : " " " "  $(x', y', z')$

$$V = \int_{V'} \frac{\bar{p} \cdot \nabla'\left(\frac{1}{r}\right)}{4\pi\epsilon_0} dV'$$

in order to solve this integral, we need a certain identity  $\rightarrow \nabla \cdot \nabla A = \bar{A} \cdot \nabla U + \nabla(\nabla \cdot \bar{A})$

$$V = \int_{V'} \frac{\bar{p} \cdot \nabla'\left(\frac{1}{r}\right)}{4\pi\epsilon_0} dV' \quad \begin{array}{l} V \rightarrow \frac{1}{r} \\ \bar{A} \rightarrow \bar{p} \\ \nabla \rightarrow \nabla' \end{array}$$

$$= \int_{V'} \frac{\nabla' \cdot \bar{p}}{4\pi\epsilon_0} dV' + \int_{V'} \frac{-\frac{1}{r} \nabla' \cdot \bar{p}}{4\pi\epsilon_0} dV'$$

①

②

by applying the divergence theorem into integration (1):-

$$V = \int_S \frac{\bar{P} \cdot d\bar{s}}{4\pi\epsilon_0 r} + \int_V \frac{-\nabla \cdot \bar{P}}{4\pi\epsilon_0 r}, \quad d\bar{s} = ds \hat{a}_n$$

$$= \int_{S'} \frac{\bar{P} \cdot \hat{a}_n}{(r) 4\pi\epsilon_0} ds' + \int_V \frac{-\nabla \cdot \bar{P}}{4\pi\epsilon_0 r} dV'$$

these two terms are used to find the potential due to bound charges (polarized)

For free charges (if exists):-

$$V = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r} + \int_V \frac{\rho_v dv}{4\pi\epsilon_0 r}$$

$$\rho_{ps} = \bar{P} \cdot \hat{a}_n \quad (\text{equal to } \rho_s = \bar{D} \cdot \hat{a}_n)$$

$$\rho_{pv} = -\nabla \cdot \bar{P} \quad (\rho_v = \nabla \cdot \bar{D})$$

Bound Charges ( $Q_b$ ):-

$$Q_{b+} = \int_S \rho_{ps} ds$$

$$Q_{b-} = \int_V \rho_{pv} dv$$

Remember that for free charges:

$$Q_{b+} = \int_S \rho_s ds$$

$$Q_{b-} = \int_V \rho_v dv$$

$$Q_{b\text{total}} = Q_{b+} + Q_{b-}$$

if  $Q_{b\text{total}} = 0 \rightarrow$  electrically neutralized

$$\rho_{V\text{total}} = \rho_v + \rho_{pv} = \nabla \cdot \epsilon_0 \bar{E}$$

$$\rho_v = \rho_{V\text{total}} - \rho_{pv}$$

$$= \nabla \cdot \epsilon_0 \bar{E} - (-\nabla \cdot \bar{P}) = \nabla \cdot \bar{D}$$



$$\vec{D} = \epsilon_0 \vec{E} + \vec{P}$$

another way to calculate polarization :-

$$\vec{P} = \chi_e \epsilon_0 \vec{E} \rightarrow \text{this equation is valid for linear materials}$$

since the relation between  $\vec{E}$  &  $\vec{P}$  is linear.

$\chi_e$  = electrical susceptibility  $\rightarrow \chi_e = 0$  for air and conductive materials  
 $\rightarrow \chi_e \gg 1$  for dielectrics

$$D_{\text{dielectric}} > D_{\text{air}}, D_{\text{conductive}}$$

$$\rho_v = \nabla \cdot \vec{D}$$

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P}, \quad \vec{P} = \chi_e \epsilon_0 \vec{E}$$

$$\vec{D} = \epsilon_0 \vec{E} + \chi_e \epsilon_0 \vec{E}$$

$$= (1 + \chi_e) \epsilon_0 \vec{E}$$

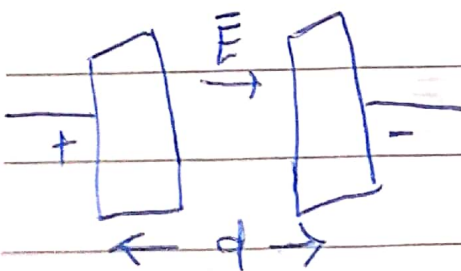
$$= \epsilon_r \epsilon_0 \vec{E}, \quad \epsilon_r = \text{relative permittivity}$$

$\epsilon_r = 1 \rightarrow$  for free space

$$\epsilon_r = 1 + \chi_e = \frac{\epsilon}{\epsilon_0}$$

$\epsilon$   $\rightarrow$  total permittivity  
 $\epsilon_0$   $\rightarrow$  free space permittivity

to measure  $\epsilon_r$  experimentally,



$$C_0 = \frac{\epsilon_0 S}{d}$$

$$C = \frac{\epsilon_0 \epsilon_r S}{d}$$

$$\frac{C}{C_0} = \epsilon_r$$

\* Dielectric Breakdown :-

Factors  $\Rightarrow$  1) Nature of the dielectric material  
 the dielectrics that we use are in this range  $\rightarrow 0 < \sigma < \infty$

2) Temperature (increasing Temp  $\rightarrow$  decreasing)

3) Humidity (as it increase,  $\sigma$  decrease) <sup>conductivity</sup>

4) Applied electric field (as it increase,  $\sigma$  increase)  
 every material has maximum E-field & this is called "Dielectric strength"

5) Time the  $\vec{E}$  is applied

Example ; a dielectric cube of length (l) centered at the origin has  $\vec{P} = a\vec{r}$  (a: constant) and  $\vec{r} = x\hat{a}_x + y\hat{a}_y + z\hat{a}_z$ . Find all bound charge densities and the total charge?

Sol  $\rho_{ps} = \vec{P} \cdot \hat{a}_n$  (we have 6 faces)

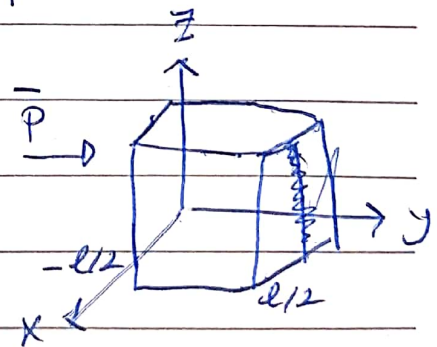
$\rho_{ps} \text{ front} = ax \hat{a}_x \cdot \hat{a}_x = ax = \frac{al}{2}$

$\rho_{ps} \text{ back} = \frac{al}{2}$

because :  $ax \hat{a}_x = -\hat{a}_x \Big|_{x = -\frac{l}{2}} = \frac{al}{2}$

all faces  $\Rightarrow \rho_{ps} = \frac{al}{2} \text{ C/m}^2$

since the position vector is identical in all directions





$$\rho_{ps \text{ total}} = -\nabla \cdot \vec{P} = -\frac{\partial P_x}{\partial x} + \frac{\partial P_y}{\partial y} + \frac{\partial P_z}{\partial z}$$

$$= -(a+a+a) = -3a \text{ C/m}^3$$

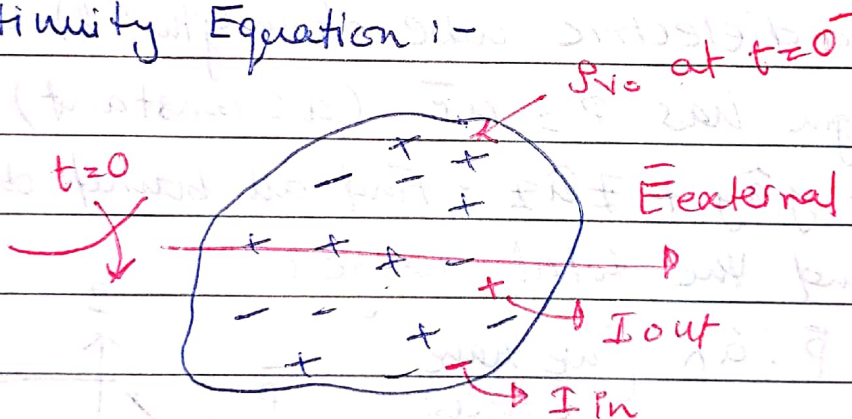
$$\Phi_{b+} = \oint_S \rho_{ps} ds = 6 \int_S \rho_{ps} ds = 6 \frac{al}{2} l^2$$

$$= 3al^3 c$$

$$\Phi_{b-} = \int_V \rho_{pv} dv = -3al^3 c$$

$$\Phi_{\text{total}} = \Phi_{b+} + \Phi_{b-} = \text{zero (electrically neutralized)}$$

\* Continuity Equation :-



KCQ:  $I_{out} = I_{in}$

$$\oint_S \vec{J} \cdot d\vec{s} = -\frac{dq_{in}}{dt} = -\frac{d}{dt} \int_V \rho_v dv = -\int_V \frac{\partial \rho_v}{\partial t} dv$$

↳ the charges inside the volume are decreasing

$$\oint_S \vec{J} \cdot d\vec{s} = \int_V -\frac{\partial \rho_v}{\partial t} dv$$

↳ continuity equation in integral form.

$$\oint_S \vec{J} \cdot d\vec{s} = - \int_V \frac{\partial \rho_V}{\partial t} dV$$

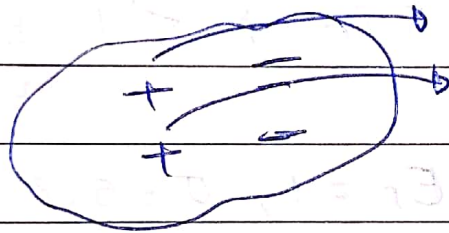
↳ applying the divergence theorem:

$$\int_V \nabla \cdot \vec{J} dV = - \int_V \frac{\partial \rho_V}{\partial t} dV$$

$$\nabla \cdot \vec{J} = - \frac{\partial \rho_V}{\partial t} \rightarrow \text{Continuity equation in differential form.}$$

\* Relaxation Time ( $\tau_r$ ) :-

The time needed for the charge to appear on the surface in order that the material become conductor



$$\nabla \cdot \vec{J} = - \frac{\partial \rho_V}{\partial t}$$

$$\vec{J} = \sigma \vec{E}$$

$$\vec{D} = \epsilon_0 \vec{E}$$

$$\nabla \cdot \sigma \vec{E} = \frac{\sigma \rho_V}{\epsilon_0} = - \frac{\partial \rho_V}{\partial t}$$

$$\rho_V = \nabla \cdot \vec{D}$$

$$\rho_V = \nabla \cdot \epsilon_0 \vec{E}$$

$$\int_{\rho_{V0}}^{\rho_V} + \frac{\partial \rho_V}{\rho_V} = \int_0^t \frac{-\sigma}{\epsilon_0} dt$$

$$\frac{\rho_V}{\epsilon_0} = \nabla \cdot \vec{E}$$

$$\ln(\rho_V - \rho_{V0}) = \frac{-\sigma}{\epsilon_0} t = \frac{-\sigma}{\epsilon} t$$

↳ for all materials

$$\ln\left(\frac{\rho_V}{\rho_{V0}}\right) = \frac{-\sigma}{\epsilon} t$$

$$\rho_V = \rho_{V0} e^{\frac{-\sigma}{\epsilon} t}$$

السعة التي بقيت داخل المادة بعد فترة من الزمن

$$\rho_V = \rho_{V0}, t=0$$

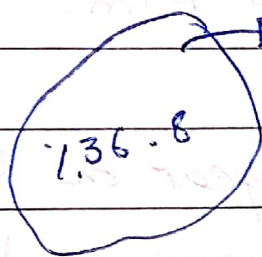


$$P_V = P_{V0} e^{-\frac{\sigma}{\epsilon} t}$$

$$P_V = P_{V0} e^{-t/Tr}$$

$$Tr = \frac{\epsilon}{\sigma} = \frac{\epsilon_0 \epsilon_r}{\sigma} \Rightarrow \text{Relaxation time. [s]}$$

at  $t = 1 Tr \rightarrow P_V = P_{V0} e^{-1} = 0.368 P_{V0}$



1 Tr

2 Tr  $\rightarrow$  1.14

3 Tr  $\rightarrow$  1.5

4 Tr  $\rightarrow$  1.8

5 Tr  $\rightarrow$  < 1% *المادة سوف تَبْقَى*

*in steady state*

Example; \*for copper  $\epsilon_r = 1$ ,  $\sigma = 5.8 \cdot 10^7$  S/m

so find Tr :

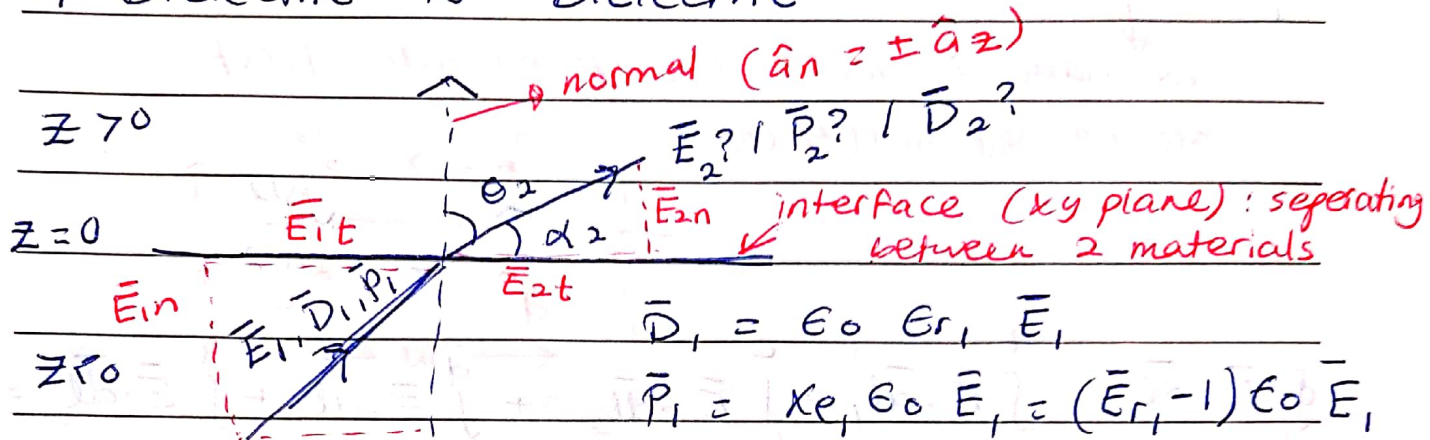
$$\text{Sol } Tr = \frac{\epsilon}{\sigma} = \frac{\frac{10^{-9}}{36\pi}}{5.8 \cdot 10^7} = 1.53 \cdot 10^{-19} \text{ s}$$

\* for fused quartz  $\epsilon_r = 5$ ,  $\sigma \approx 10^{-17}$  S/m.

$$\text{Sol } Tr = \frac{\epsilon}{\sigma} = 51.2 \text{ Days.}$$

Purpose: - عشان نعرف شوية عن المجال الكهربائي لما ينتقل من وسط لآخر  
 صيغتين معينتين اى وسط آخر ختلافه مع في الخصائص.

### 1) Dielectric to Dielectric



the characteristic of the milieu ( $z < 0$ ) is  $\epsilon_{r1}$  and for ( $z > 0$ ) is  $\epsilon_{r2}$ , where  $\epsilon_{r1}$  and  $\epsilon_{r2}$  are both greater than 1 (none of these materials is free space).

\* We start with the given  $\bar{E}$  :

$$\bar{E}_1 = \bar{E}_{1n} + \bar{E}_{1t}$$

$n \rightarrow$  normal

$t \rightarrow$  tangent

$$\hat{a}_n = \hat{a}_z$$

$$\bar{E}_{1n} = (\bar{E}_1 \cdot \hat{a}_n) \hat{a}_n$$

$$\bar{E}_{1t} = \bar{E}_1 - \bar{E}_{1n}$$

$$\theta_1 = \sin^{-1} \frac{|\bar{E}_{1t}|}{E_1} = \cos^{-1} \frac{|\bar{E}_{1n}|}{E_1} = \tan^{-1} \frac{E_{1t}}{E_{1n}}$$

$$\alpha_1 = 90^\circ - \theta_1$$

\* To find the field in region 2 ;

$$\bar{E}_2 = \bar{E}_{2n} + \bar{E}_{2t}$$

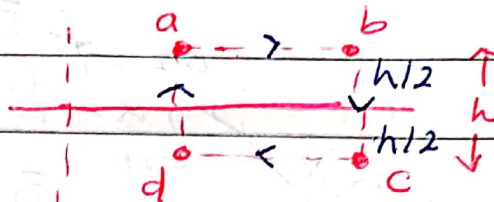
we need to apply 2 equations which are 1<sup>st</sup> and 2<sup>nd</sup> Maxwell's equations.



$$\oint_S \vec{D} \cdot d\vec{s} = \rho_{enclosed} = \int_S \rho_s ds \quad (\text{Gauss})$$

$$\oint_C \vec{E} \cdot d\vec{l} = 0 \quad (\text{equipotential surface})$$

we have to make the closed path first around the interface



$$\oint_C \vec{E} \cdot d\vec{l} = \int_a^b \vec{E} \cdot d\vec{l}_1 + \int_b^c \vec{E} \cdot d\vec{l}_2 + \int_c^d \vec{E} \cdot d\vec{l}_3 + \int_d^a \vec{E} \cdot d\vec{l}_4 = 0$$

$$0 = E_{2t}w - E_{2n} \frac{h}{2} - E_{1n} \frac{h}{2} - E_{1t}w + E_{1n} \frac{h}{2} + E_{2n} \frac{h}{2}$$

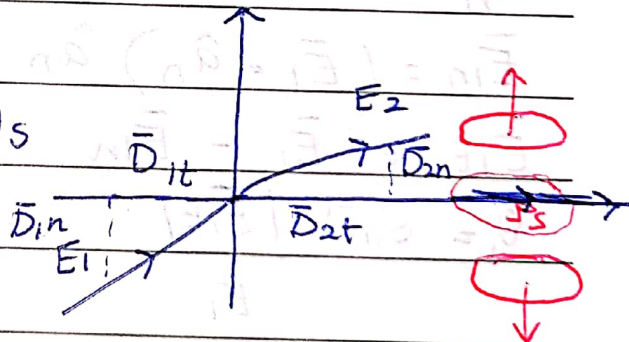
$$E_{2t}w - E_{1t}w = 0$$

$\vec{E}_{2t} = \vec{E}_{1t}$  → The tangential component of electric field must be continuous

To find  $E_{2n}$  :-

$$\oint_S \vec{D} \cdot d\vec{s} = \int_S \rho_s ds \quad (\text{at } z=0)$$

$$\int_{S_{top}} \vec{D} \cdot d\vec{s} + \int_{S_{bottom}} \vec{D} \cdot d\vec{s} = \rho_s ds$$



$$D_{2n} \Delta s - \Delta s D_{1n} = \rho_s \Delta s$$

$$D_{2n} - D_{1n} = \rho_s$$

assume of the area for all of them =  $\Delta s$   
 $\Delta s \rightarrow \infty$

if  $\rho_s = 0$  then  $D_{2n} = D_{1n}$

so  $\epsilon_0 \epsilon_{r2} E_{2n} = \epsilon_0 \epsilon_{r1} E_{1n}$

$$\vec{E}_{2n} = \frac{\epsilon_{r1}}{\epsilon_{r2}} \vec{E}_{1n}$$

$$\theta_2 = \sin^{-1} \left( \frac{E_{2t}}{E_2} \right)$$

$$\alpha_2 = 90^\circ - \theta_2$$

or  $\underline{E_{1t}} = \underline{E_{2t}}$

$$E_1 \sin \theta_1 = E_2 \sin \theta_2 \quad \dots \textcircled{1}$$

if  $\rho_s = 0 \rightarrow D_{2n} - D_{1n} = 0 \quad \epsilon_{r1} E_1 \cos \theta_1 = \epsilon_{r2} E_2 \cos \theta_2$

$$\underline{D}_{2n} = \underline{D}_{1n}$$

$$\epsilon_0 \epsilon_{r1} E_{1n} = \epsilon_0 \epsilon_{r2} E_{2n} \quad \dots \textcircled{2}$$

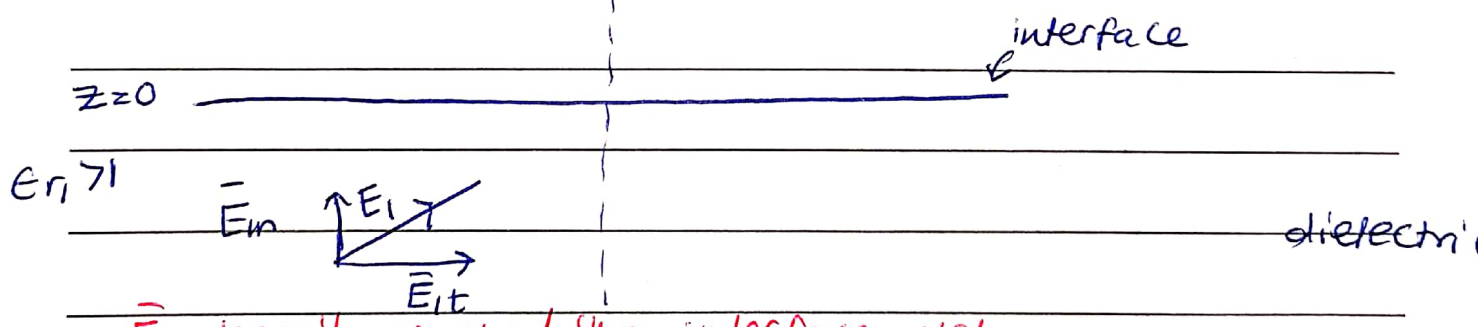
divide ① by ②  $\rightarrow \frac{\tan \theta_1}{\epsilon_{r1}} = \frac{\tan \theta_2}{\epsilon_{r2}}$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_{r1}}{\epsilon_{r2}} \quad \text{only if } \rho_s = 0$$

## 2] Conductor to Dielectric

$\sigma_2 \approx \infty$  (perfect conductor)  $\uparrow$   
 $\epsilon_{r2} = 1$

$\underline{E}_2 = 0 \rightarrow \underline{E}_{2n} = 0, \underline{E}_{2t} = 0$  conductor  
 $\underline{D}_2 = 0 \rightarrow \underline{D}_{2t} = 0, \underline{D}_{2n} = 0$



$\underline{E}_1$  hasn't reached the interface yet.

$\underline{E}_{1t} = \underline{E}_{2t} \rightarrow \underline{E}_{1t} = 0$  at  $z=0$  So the electric field will enter the interface with  $90^\circ$  (normal)

$$\underline{D}_{2n} - D_{1n} = \rho_s$$

$$D_{1n} = -\rho_s = \rho_s (-\hat{a}_n)$$

$$\underline{E}_{1n} = \frac{-\rho_s \hat{a}_n}{\epsilon_0 \epsilon_{r1}}$$

$\theta_2, \alpha_2$  doesn't exist

$$\theta_1 = 0^\circ$$

$$\alpha_1 = 90^\circ$$



isotropic: permittivity doesn't change with direction.

Subject \_\_\_\_\_ Day \_\_\_\_\_ Date \_\_\_\_\_

$\epsilon_r$  is constant everywhere inside the region

Example; Two homogeneous isotropic dielectrics meet

on plane  $z=0$ , for  $z > 0$ ,  $\epsilon_{r1} = 4$  and for  $z < 0$ ,

$\epsilon_{r2} = 3$ . if  $\vec{E}_1 = 5\hat{a}_x - 2\hat{a}_y + 3\hat{a}_z$   $\text{KV/m}$

exists for  $z > 0$ . find:

(a)  $\vec{E}_2$  for  $z < 0$ ?

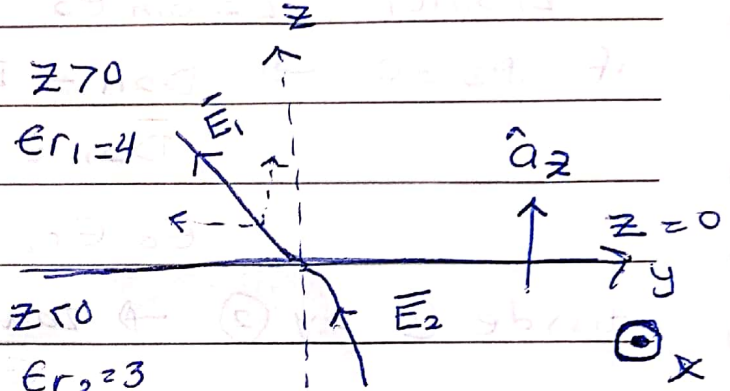
Sol  $\hat{a}_n = \hat{a}_z$

$$\vec{E}_{in} = (\vec{E}_1 \cdot \hat{a}_n) \hat{a}_n$$

$$= 3\hat{a}_z \text{ KV/m}$$

$$\vec{E}_{it} = \vec{E}_1 - \vec{E}_{in}$$

$$= 5\hat{a}_x - 2\hat{a}_y \text{ KV/m} = \vec{E}_{2t}$$



$$D_{2n} - D_{1n} = \rho_s = 0 \quad \text{since } \rho_s \text{ is not mentioned}$$

Most likely between dielectrics in the question and it said dielectric

there is no surface charge because the charges inside dielectrics need large relaxation time to reach the surface so usually there is no surface charge on the interface

$$\vec{E}_{2n} = \frac{\epsilon_{r1}}{\epsilon_{r2}} \vec{E}_{in} = \left(\frac{4}{3}\right) 3\hat{a}_z = 4\hat{a}_z \text{ KV/m}$$

$$\vec{E}_2 = \vec{E}_{2n} + \vec{E}_{2t} = 5\hat{a}_x - 2\hat{a}_y + 4\hat{a}_z \text{ KV/m}$$

(b) the angles  $E_1$  and  $E_2$  makes with the interface?

$$\text{Sol } \theta_1 = \sin^{-1} \frac{E_{it}}{E_1} = \sin^{-1} \frac{\sqrt{29}}{\sqrt{38}} = 60.9^\circ$$

$$\alpha_1 = 90^\circ - \theta_1 = 29.1^\circ$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{4}{3} \rightarrow \theta_2 = 53.4^\circ$$

$$\alpha_2 = 36.6^\circ$$

Note:-  
angles with the normal  $\rightarrow \theta_1 / \theta_2$   
angles with the interface  $\rightarrow \alpha_1 / \alpha_2$

(c) Energy densities in both dielectrics ?-

Sol  $w_{E1} = \frac{1}{2} \epsilon_1 E_1^2 = \frac{1}{2} \epsilon_0 \epsilon_{r1} E_1^2 = \frac{1}{2} \frac{10^{-9}}{36\pi} (4)^2 3810^6$   
 $= 672 \frac{\mu J}{m^3}$

$w_{E2} = \frac{1}{2} \epsilon_0 \epsilon_{r2} E_2^2 = \frac{1}{2} \frac{10^{-9}}{36\pi} (3)^2 4510^6 = 597 \frac{\mu J}{m^3}$

$|E_2| = \sqrt{45} \frac{KV}{m}$   
 $|E_1| = \sqrt{38} \frac{KV}{m}$  }  $E_2 > E_1$   
 $w_{E2} < w_{E1}$  because  $\epsilon_{r2}$  is greater than  $\epsilon_{r1}$

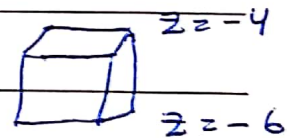
(d) The energy within a cube of side 2m centered at (3, 4, -5) ?  $z > 0$

Sol  $w_E = \int_V w_{E2} dv$

$= (597 \cdot 10^{-6})(8)$

$= 4.776 \text{ mJ}$

$z=0$



if the cube is centered at the origin  $\rightarrow w_E$  equals  $(w_{E1} \times 4) + (w_{E2} \times 4)$  since half the cube will be in region 1 and the other half will be in region 2.



Subject Boundary Value Problems Day (B.V.P) Date \_\_\_\_\_

Purpose! - we will use it as a fourth way to find electric field.

we can find  $\vec{E}$  using  $\rightarrow$  1) Coulomb's law } charge must  
 2) Gauss law } be known  
 3) potential  $\rightarrow \vec{E} = -\nabla V$

problem: if the charge or the potential are known for some part of the surface (not for the whole surface) so we can't use coulomb, gauss & potential  $\rightarrow$  we will use B.V.P.

$$\rho_v = \nabla \cdot \vec{D}, \vec{D} = \epsilon \vec{E}, \vec{E} = -\nabla V$$

$$\nabla \cdot (\epsilon \vec{E}) = \rho_v$$

$$\nabla \cdot (-\epsilon \nabla V) = \rho_v$$

$$\nabla \cdot \epsilon \nabla V = -\rho_v \text{ --- (1) Poisson's equation for non homogeneous media.}$$

$\epsilon$  is not a constant  
 ما يقدر نطلبها برا المتغير

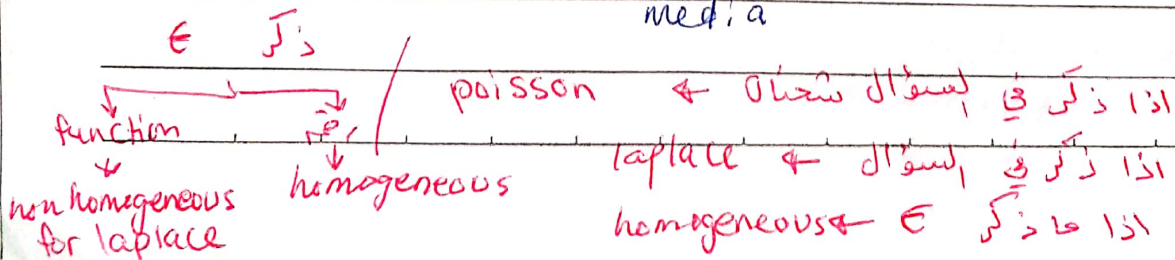
$$\epsilon \nabla \cdot \nabla V = -\rho_v$$

scalar quantity  $\nabla^2 V = \frac{-\rho_v}{\epsilon}$  --- (2) Poisson's equation for homogeneous media

if  $\rho_v = 0 \rightarrow$  source free region

$$\nabla \cdot \epsilon \nabla V = 0 \text{ --- (3) Laplace's equation for non homogeneous media}$$

$$\nabla^2 V = 0 \text{ --- (4) Laplace's equation for homogeneous media}$$







4) find other quantities  $\Rightarrow$  drift velocity  
 $\downarrow$  mobility

$$\bar{D} = \epsilon \bar{E}, \quad \bar{J} = \sigma \bar{E}, \quad \bar{u} = \mu \bar{E}$$

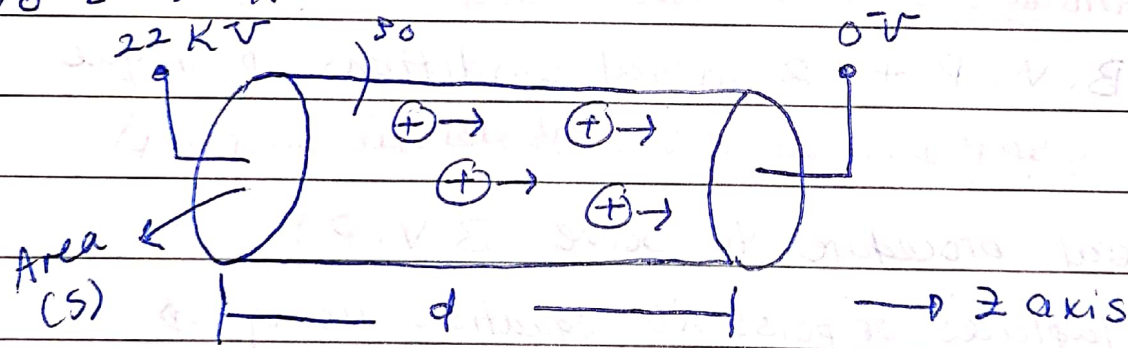
$$W_E = \frac{1}{2} \int_V \epsilon E^2 dV, \quad F = \phi \bar{E}$$

$$\text{pressure} = \frac{F}{\text{area}}, \quad \phi = \oint_S \epsilon \bar{E} \cdot d\bar{s}, \quad R = \frac{V}{I} = \frac{-\int_L \bar{E} \cdot d\bar{l}}{\int_S \sigma \bar{E} \cdot d\bar{s}}$$

$$C = \frac{\phi}{V} = \frac{\oint_S \epsilon \bar{E} \cdot d\bar{s}}{-\int_L \bar{E} \cdot d\bar{l}}, \quad P = \int_V \sigma E^2 dV$$

Example: an electrohydrodynamic (EHD) pumping has a uniform charge  $\rho_0$   $\text{C/m}^3$  exists between the two electrodes which is generated in the left electrode and collected at the right electrode calculate the pressure of the pump if  $\rho_0 = 25 \text{ mC/m}^3$

$$V_0 = 22 \text{ KV}$$



Sol  $\nabla^2 V = \frac{-\rho_0}{\epsilon} = \frac{-\rho_0}{\epsilon}$

$$\frac{d^2 V}{dz^2} = \frac{-\rho_0}{\epsilon}$$

integration

integrating  $\rightarrow \frac{dV}{dz} = \frac{-\rho_0}{\epsilon} z + A$  Constant

$$V = \frac{-\rho_0}{\epsilon} \frac{z^2}{2} + Az + B \rightarrow \text{General Solution.}$$

integration constant

$$V = \frac{-\rho_0}{\epsilon} \frac{z^2}{2} + Az + B$$

$$V|_{z=0} = V_0 \quad , \quad V|_{z=d} = 0$$

$$\boxed{B = V_0}$$

$$0 = \frac{-\rho_0}{\epsilon} \frac{d^2}{2} + Ad + V_0$$

$$\boxed{A = \left[ \frac{\rho_0 d^2}{2\epsilon} - V_0 \right] \frac{1}{d}}$$

$$V = \frac{-\rho_0 z^2}{2\epsilon} + \left( \frac{\rho_0 d}{2\epsilon} - \frac{V_0}{d} \right) z^2 + V_0 \rightarrow \text{Unique Solution}$$

$$\vec{E} = -\nabla V = -\frac{dV}{dz} \hat{a}_z = \frac{\rho_0 z}{\epsilon} - \frac{\rho_0 d}{2\epsilon} + \frac{V_0}{d} \hat{a}_z$$

pressure =  $\frac{|\vec{F}|}{\text{area}} = \frac{\rho_0 |\vec{E}|}{\text{area}}$   $\rho_0 = \int_V \rho_v dv$

*scalar quantity*

$$\vec{E} = \frac{\rho_0 z}{\epsilon} - \frac{\rho_0 d}{2\epsilon} + \frac{V_0}{d} \hat{a}_z$$

$$\vec{F} = \rho_0 \vec{E} = \int_V \rho_v \vec{E} dv = \rho_0 \int_S \int \vec{E} ds dz \quad , \quad \int_S ds = S$$

$$= \rho_0 S \int_z \vec{E} dz = \rho_0 S \left( \frac{\rho_0 z^2}{2\epsilon} - \frac{\rho_0 d z}{2\epsilon} + \frac{V_0 z}{d} \right) \Bigg|_{z=0}^{z=d}$$

$$= \rho_0 S \left( \frac{\rho_0 d^2}{2\epsilon} - \frac{\rho_0 d^2}{2\epsilon} + V_0 \frac{d}{d} \right) \hat{a}_z$$

$$= \rho_0 S V_0 \hat{a}_z \text{ N}$$

$$\text{pressure} = \frac{\rho_0 S V_0}{S} = \rho_0 V_0 = 550 \text{ N/m}^2$$



$$R = \frac{V}{I} = \frac{\oint_S \sigma \vec{E} \cdot d\vec{s}}{\int_l \vec{E} \cdot d\vec{l}}$$

always positive

$$C = \frac{Q}{V} = \frac{\oint_S \vec{E} \cdot d\vec{s}}{\int_l \vec{E} \cdot d\vec{l}}$$

It means that the integration must be from the lower potential to the higher potential

Procedure to find R and C :-

1] Choose a suitable coordinate system.

2] assume either  $V_0$  difference or a positive or negative charges

B.V.P  
Gauss method

3] solve B.V.P and apply the boundary conditions

4]  $\vec{E} = -\nabla V$

5]  $R = \frac{V_0}{\oint_S \sigma \vec{E} \cdot d\vec{s}}$  ,  $C = \frac{\oint_S \vec{E} \cdot d\vec{s}}{V_0}$

for B.V.P

for Gauss method :-

3]  $Q = \oint_S \epsilon \vec{E} \cdot d\vec{s}$

4]  $V = -\int_l \vec{E} \cdot d\vec{l}$

5]  $R = \frac{V}{I}$  ,  $C = \frac{Q}{V}$

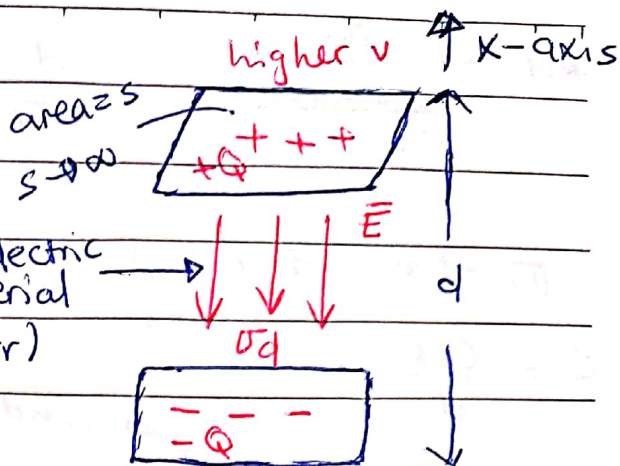
Gauss :-

$$\Phi = \oint_s \vec{E} \cdot d\vec{s}$$

$$\rho_s = \frac{\Phi}{s}$$

$$\vec{E}_{\text{infinite plate}} = \frac{\rho_s}{2\epsilon} (-\hat{a}_x)$$

dielectric material ( $\epsilon_r$ )



two plate  $\rightarrow \vec{E} = \frac{\rho_s}{2\epsilon_0} (-\hat{a}_x) + \frac{-\rho_s}{2\epsilon_0} (\hat{a}_x)$  lower v

$$= \frac{\rho_s}{\epsilon} (-\hat{a}_x), \quad \rho_s = \frac{\Phi}{s}$$

$$= \frac{\Phi}{s\epsilon} (-\hat{a}_x) \quad \frac{V}{m} \quad \text{step ③}$$

$$V = - \int_l \vec{E} \cdot d\vec{l} = - \int \frac{\Phi}{s\epsilon} (-\hat{a}_x) \cdot dk \hat{a}_x \quad \text{step ④}$$

$$= \frac{\Phi}{s\epsilon} d \quad V$$

$$C = \frac{\Phi}{V} = \frac{\Phi}{\frac{\Phi d}{s\epsilon}} = \frac{\epsilon s}{d} F, \quad \epsilon = \epsilon_0 \epsilon_r$$

$$R = \frac{V}{I}, \quad I = \oint_s \vec{J} \cdot d\vec{s} = \oint_s \sigma_d \vec{E} \cdot d\vec{s}$$

$$I = \iint_{z,y} \sigma_d \frac{\Phi}{s\epsilon} (-\hat{a}_x) \cdot dy dz (-\hat{a}_x)$$

$\rightarrow [\frac{s}{m}], \quad s = \frac{1}{\Omega}$

$$I = \frac{\sigma_d \Phi}{s\epsilon} s \Rightarrow I = \frac{\sigma_d \Phi}{\epsilon} \quad A$$

convection current

$$\text{Volt} = \left[ \frac{C}{F} \right] = \frac{\Phi}{C}$$



$$R_d = \frac{\frac{\Phi d}{\epsilon \epsilon_0}}{\frac{\sigma_d \Phi}{E}} = \frac{d}{\epsilon \sigma_d} \Omega \quad (\text{dielectric resistance})$$

$$\sigma_c \rightarrow \infty \Rightarrow R = \frac{\rho}{\sigma_c A} = \text{zero (ideal conductor)}$$

$$C = \frac{\epsilon S}{d}$$

$$R_d = \frac{d}{\sigma_d S}, \quad \text{Conductance } G = \frac{1}{R_d} = \frac{\sigma_d S}{d} [S]$$

نقطة الشحنة R  
C ليس نقطة  
بين د و E

$$W_E = \frac{1}{2} \int_V \epsilon E^2 dv = \frac{1}{2} \epsilon \frac{\Phi^2}{S^2 \epsilon^2} S d$$

Capacitor  
المساحة  $\times$  ارتفاع =  
d  $\times$  S

$$= \frac{\Phi^2 d}{2 \epsilon S} \frac{1}{\epsilon} = \frac{\Phi^2}{2C}, \quad C = \frac{\Phi}{V}$$

$$= \frac{1}{2} \Phi^2 V, \quad \Phi = CV$$

$$= \frac{1}{2} C V^2 [J] \quad \text{if uniform}$$

B.V.P :-

Cartesian  $\rightarrow \nabla^2 V = 0$

$$\frac{d^2 V}{dx^2} = 0$$

$$\frac{dV}{dx} = A \Rightarrow V = Ax + b$$

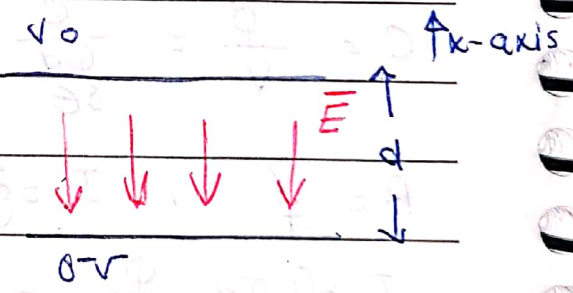
$$V|_{x=0} = 0 \Rightarrow B = 0$$

$$V|_{x=d} = V_0 \Rightarrow A = \frac{V_0}{d}$$

$$V = \frac{V_0}{d} x$$

General more than Gauss  
عند نقطة V بين اللوحين  
المساحة  $\times$

B.V.P. نقطة V عند أي مكان بين اللوحين



$$\vec{E} = -\nabla v = \frac{-dv}{dx} \hat{a}_x = \frac{-v_0}{d} \hat{a}_x \frac{V}{m}$$

$$Q = \int_S \epsilon \vec{E} \cdot d\vec{s} = \iint_{xy} \epsilon \left(\frac{-v_0}{d}\right) \hat{a}_x \cdot dy dz (-\hat{a}_x)$$

$$= \frac{\epsilon v_0 S}{d}$$

$$C = \frac{Q}{v_0} = \frac{\epsilon S}{d}$$

$$I = \iint_S \sigma_d \vec{E} \cdot d\vec{s} = \iint_{xy} \sigma_d \left(\frac{-v_0}{d}\right) \hat{a}_x \cdot dy dz (-\hat{a}_z)$$

$$= \frac{\sigma_d v_0 S}{d}$$

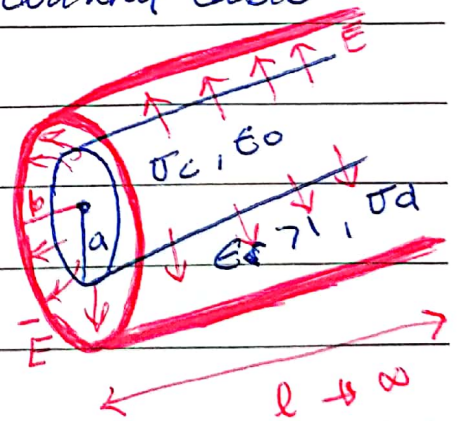
$$R_d = \frac{v_0}{\frac{\sigma_d v_0 S}{d}} = \frac{d}{\sigma_d S}$$

## (2) Cylindrical Capacitor 1-

also known as coaxial capacitor / coaxial cable

Gauss:

practically  $\rightarrow$  inner cable  $\rightarrow +Q$   
 $\rightarrow$  external cable  $\rightarrow -Q$



$$Q = \oint \epsilon \vec{E} \cdot d\vec{s}$$

$$= \iint_{\text{cylinder}} \epsilon \vec{E} \cdot \hat{a}_\rho \cdot \rho d\phi dz \hat{a}_\rho$$

$$= \epsilon E_\rho \rho (2\pi) (l) \Rightarrow \vec{E} = \frac{Q}{2\pi \epsilon \rho l} \hat{a}_\rho$$



$$V = -\frac{Q}{2\pi\epsilon l} \ln\left(\frac{a}{b}\right) \quad V = \frac{Q}{2\pi\epsilon l} \ln\left(\frac{b}{a}\right)$$

$$C = \frac{Q}{V} = \frac{2\pi\epsilon l}{\ln\left(\frac{b}{a}\right)} \quad F \quad (l \rightarrow \infty)$$

$$\frac{C}{l} = \frac{2\pi\epsilon}{\ln\left(\frac{b}{a}\right)} \quad \frac{F}{m}$$

$$R_d = \frac{V}{I}$$

$$= \frac{\ln\left(\frac{b}{a}\right)}{2\pi \cdot \sigma_d l}$$

$$I = \int \sigma_d \vec{E} \cdot d\vec{s}$$

$$= \int_0^l \int_0^{2\pi} \sigma_d \frac{Q}{2\pi\epsilon r l} \cdot r d\theta dz$$

$$= \frac{\sigma_d Q}{\epsilon}$$

$$W_E = \frac{1}{2} C V^2$$

$$W_E = \frac{1}{2} \int \epsilon E^2 dV$$

$$C = \frac{2\pi\epsilon l}{\ln\left(\frac{b}{a}\right)} \quad F$$

B.V.P :-

$$\nabla^2 v = 0$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial v}{\partial r} \right) = 0$$

$$\text{integrating} \rightarrow r \frac{dv}{dr} = A \rightarrow \frac{dv}{dr} = \frac{A}{r}$$

$$\text{integrating} \rightarrow A \ln r + B$$

$$V(r=a) = V_0$$

$$V(r=b) = 0$$

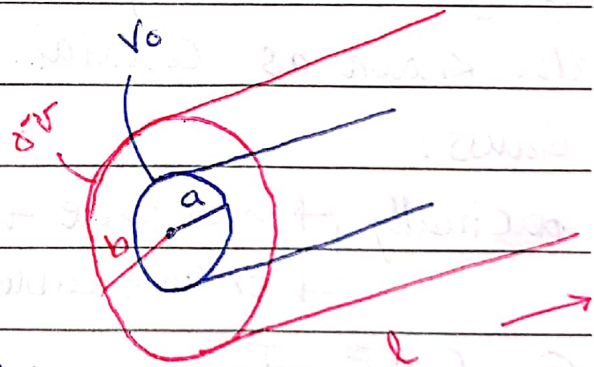
$$V_0 = A \ln a - A \ln b$$

$$0 = A \ln b + B$$

$$= A \ln \frac{a}{b}$$

$$\boxed{B = -A \ln b}$$

$$\boxed{A = \frac{V_0}{\ln \frac{a}{b}}}$$



$$V = \frac{V_0}{\ln\left(\frac{a}{b}\right)} \ln\left(\frac{\rho}{b}\right) \rightarrow \text{unique potential}$$

$$\vec{E} = -\nabla V = -\frac{\partial V}{\partial \rho} \hat{a}_\rho = \frac{-V_0}{\rho \ln\left(\frac{a}{b}\right)} \hat{a}_\rho$$

$$\begin{aligned} \Phi &= \oint_S \epsilon \vec{E} \cdot d\vec{s} = \int_0^l \int_0^{2\pi} \frac{\epsilon \left(-V_0 \hat{a}_\rho\right)}{\rho \ln\left(\frac{a}{b}\right)} \cdot \rho d\theta dz \hat{a}_\rho \\ &= \frac{-\epsilon V_0}{\ln\left(\frac{a}{b}\right)} 2\pi l \end{aligned}$$

$$C = \frac{\Phi}{V_0} = \frac{2\pi \epsilon l}{\ln\left(\frac{b}{a}\right)} \text{ F}$$

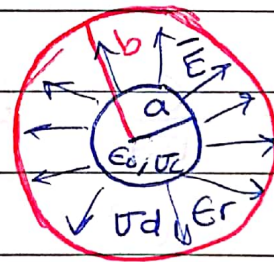
$$I = \oint_S \sigma_d \vec{E} \cdot d\vec{s}$$

$$R = \frac{V_0}{I}$$

### (3) Spherical Capacitor

Gauss :-

$$\begin{aligned} \Phi &= \oint_S \epsilon \vec{E} \cdot d\vec{s} \\ &= \int_0^{2\pi} \int_0^\pi \epsilon E r \hat{a}_r \cdot r^2 \sin\theta d\theta d\phi \hat{a}_r \\ &= \epsilon E r r^2 (2)(2\pi) \end{aligned}$$



$$\vec{E} = \frac{\Phi}{4\pi \epsilon r^2} \hat{a}_r$$

$$\begin{aligned} V &= -\int \vec{E} \cdot d\vec{l} = -\int_{r=b}^{r=a} \frac{\Phi}{4\pi \epsilon r^2} \hat{a}_r \cdot dr \hat{a}_r \\ &= \frac{\Phi}{4\pi \epsilon} \left( \frac{1}{a} - \frac{1}{b} \right) \end{aligned}$$



$$C = \frac{Q}{V} = \frac{4\pi\epsilon}{\frac{1}{a} - \frac{1}{b}} F$$

$$I = \oint_S \sigma_d \vec{E} \cdot d\vec{s} = \int_0^{2\pi} \int_0^{\pi} \sigma_d \frac{Q}{4\pi\epsilon r^2} \hat{a}_r \cdot r^2 \sin\theta d\theta d\phi a$$

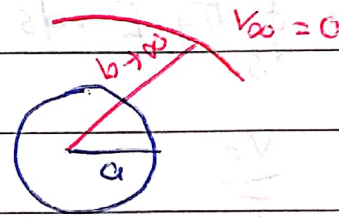
$$= \frac{\sigma_d Q}{\epsilon} A$$

$$R_d = \frac{Q}{4\pi\epsilon \sigma_d} \left( \frac{1}{a} - \frac{1}{b} \right) = \frac{1}{4\pi\epsilon \sigma_d} \left( \frac{1}{a} - \frac{1}{b} \right)$$

④ Isolated Capacitor (Isolated Sphere) :-

$$C = \frac{4\pi\epsilon}{\frac{1}{a} - \frac{1}{\infty}} = 4\pi\epsilon a F$$

$$R_d = \frac{1}{4\pi\sigma_d a} \Omega$$



$$Q = 4\pi\sigma_d a$$

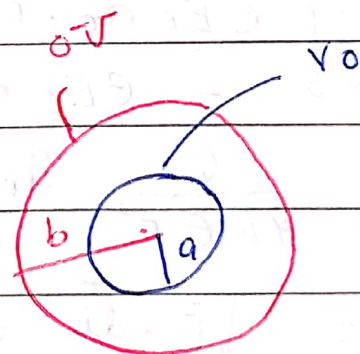
$$R_d C = \frac{\epsilon}{\sigma_d} = \tau$$

$$WE = \frac{1}{2} C V^2$$

B.V.P :-

$$\nabla^2 v = 0$$

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial v}{\partial r} \right) = 0$$



integrating  $\rightarrow \int \frac{dv}{dr} = \int \frac{A}{r^2}$

$$V = \frac{-A}{r} + B \rightarrow \text{general solution}$$

$$V(r=a) = V_0$$

$$V(r=b) = 0$$

$$V_0 = \frac{-A}{a} + \frac{A}{b}$$

$$-\frac{A}{b} = -B$$

$$V_0 = A \left( \frac{1}{b} - \frac{1}{a} \right)$$

$$B = \frac{A}{b}$$

$$A = \frac{V_0}{\frac{1}{b} - \frac{1}{a}}$$

$$V = V_0 \left( \frac{\frac{1}{r} - \frac{1}{b}}{\frac{1}{a} - \frac{1}{b}} \right)$$

$$\begin{aligned} \vec{E} &= -\nabla V = \frac{-dV}{dr} \hat{a}_r = \frac{-V_0}{\frac{1}{a} - \frac{1}{b}} \left( \frac{-1}{r^2} \right) \hat{a}_r \\ &= \frac{V_0}{\left( \frac{1}{a} - \frac{1}{b} \right) r^2} \hat{a}_r \frac{V}{m} \end{aligned}$$

$$\begin{aligned} \Phi &= \oint_S \vec{E} \cdot d\vec{s} = \int_0^{2\pi} \int_0^\pi \epsilon \frac{V_0}{\frac{1}{a} - \frac{1}{b}} \frac{1}{r^2} \hat{a}_r \cdot r^2 \sin\theta d\theta d\phi \hat{a}_r \\ &= \frac{\epsilon V_0}{\frac{1}{a} - \frac{1}{b}} (4\pi) C \end{aligned}$$

$$C = \frac{\Phi}{V_0} = \frac{4\pi\epsilon}{\frac{1}{a} - \frac{1}{b}} F$$