

EM I

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# CHI - vectors

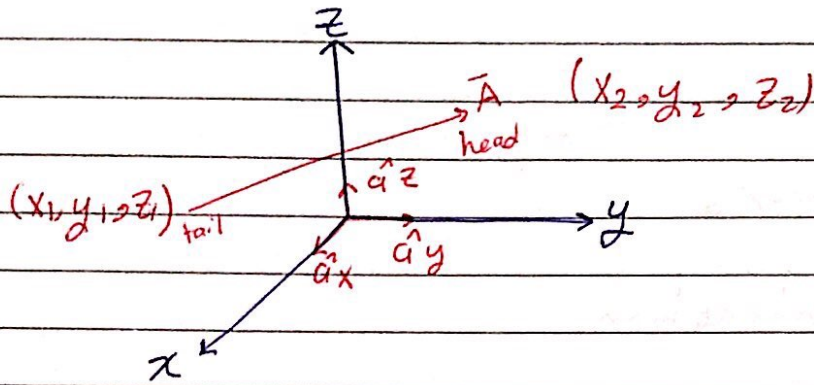
vector  $\rightarrow$  mag + dir

Vector  $A \rightarrow \bar{A} \rightarrow$  Bold in the book

scaler  $\rightarrow$  mag only

scaler  $A \rightarrow A$

\* in cartesian coordinate :-



\* unit vector :- only direction (mag = 1)

$\hat{a}_x \rightarrow$  unit vector in x-dir

$$\bar{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z \quad \text{--- [1] Long formal}$$

vector component (scaler)

$$\bar{A} = (A_x, A_y, A_z) \quad \text{--- [2] short formal}$$

Point  $\rightarrow P(x, y, z)$

ex:  $\bar{C} = 3 \hat{a}_x + 4 \hat{a}_z$

$\bar{C} = (3, 0, 4)$

\* magnitude of the vector

$$|\bar{A}| = A = \sqrt{(A_x)^2 + (A_y)^2 + (A_z)^2}$$

unit vector in  $\vec{A}$  dir

$$\hat{a}_A = \frac{\vec{A}}{A} = \frac{A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z}{\sqrt{(A_x)^2 + (A_y)^2 + (A_z)^2}}$$

$$\boxed{3} \quad \vec{A} = A \hat{a}_A$$

\* operation on vector :-

- Addition and subtraction

$$\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$$

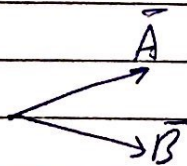
$$\vec{B} = B_x \hat{a}_x + B_y \hat{a}_y + B_z \hat{a}_z$$

$$\vec{C} = \vec{A} \oplus \vec{B}$$

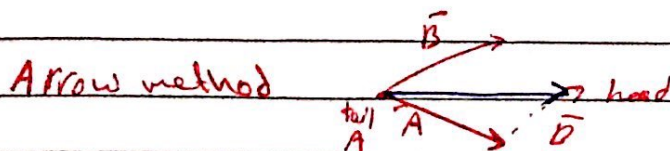
$$\vec{C} = (A_x + B_x) \hat{a}_x \oplus (A_y + B_y) \hat{a}_y \oplus (A_z + B_z) \hat{a}_z$$

$$\vec{C} = C_x \hat{a}_x + C_y \hat{a}_y + C_z \hat{a}_z$$

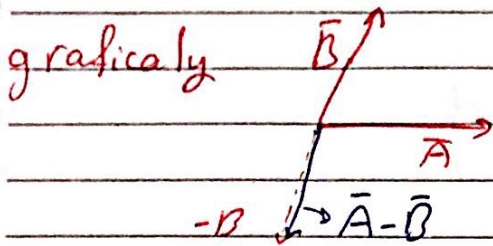
\* graphically :-



$$\vec{C} = \vec{A} + \vec{B}$$



$$\vec{D} = \vec{A} - \vec{B} \rightarrow \vec{D} = (A_x - B_x) \hat{a}_x + (A_y - B_y) \hat{a}_y + (A_z - B_z) \hat{a}_z$$



$$* \vec{A} + \vec{B} = \vec{B} + \vec{A}, \quad \vec{A} + (\vec{B} + \vec{C}) = (\vec{A} + \vec{B}) + \vec{C}, \quad k(\vec{A} + \vec{B}) = k\vec{A} + k\vec{B}$$

\* multiplication :

a) Dot product  $\rightarrow$  scalar

$$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta_{AB}$$

$$\vec{A} \cdot \vec{B} = A_x B_x + A_y B_y + A_z B_z$$

$$\hat{a}_x \cdot \hat{a}_x = (1)(1) \cos 0 = 1$$

$$\hat{a}_x \cdot \hat{a}_y = (1)(1) \cos 90 = \text{zero}$$

$$\hat{a}_n \cdot \hat{a}_m = 0 \quad \text{if } n \neq m$$

$$\hat{a}_n \cdot \hat{a}_m = 1 \quad \text{if } n = m$$

$$\cos \theta_{AB} = \frac{\vec{A} \cdot \vec{B}}{AB}, \quad \vec{A} \cdot \vec{A} = |\vec{A}|^2 = A^2 = A_x^2 + A_y^2 + A_z^2$$

$$\vec{A} \cdot \vec{B} = \vec{B} \cdot \vec{A}, \quad \vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$$

x

b) cross product : (answer = vector)

$$|\vec{A} \times \vec{B}| = AB \sin \theta$$

↳ magnitude for cross product

$$\sin \theta = \frac{|\vec{A} \times \vec{B}|}{AB}$$

$$\vec{A} \times \vec{B} = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$$

$$\vec{A} \times \vec{B} = -\vec{B} \times \vec{A}$$

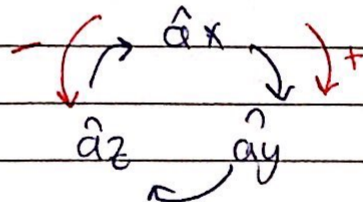
$$\vec{A} \times \vec{B} = (-1) (A_y B_z - A_z B_y) \hat{a}_x + (-1) (A_x B_z - A_z B_x) \hat{a}_y + (-1) (A_x B_y - A_y B_x) \hat{a}_z$$

$$\vec{A} \times \vec{B} \perp \vec{A} \text{ and } \perp \vec{B}$$

$$-\vec{A} \times (\vec{B} + \vec{C}) = \vec{A} \times \vec{B} + \vec{A} \times \vec{C}$$

$$-\vec{A} \times (\vec{B} \times \vec{C}) \neq (\vec{A} \times \vec{B}) \times \vec{C}$$

$$-\vec{A} \times \vec{B} \times \vec{C} = \text{eq. 11.6}$$



$$-\hat{a}_x \times \hat{a}_x = \text{zero}$$

$$|\hat{a}_x \times \hat{a}_y| = 1 \rightarrow \text{but } \hat{a}_x \times \hat{a}_y = \hat{a}_z$$
$$\hat{a}_z \times \hat{a}_y = -\hat{a}_x$$

\* Vector projection along another vector:-

$A_B$  : projection of A along B  
 ↳ scalar

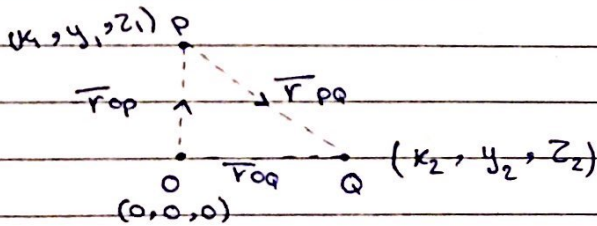
$\bar{A}_B$  : " " " " " "  
 ↳ vector

$$-\cos \theta_{AB} = \frac{A_B}{A} \rightarrow A_B = A \cos \theta_{AB}$$

$$-A_B = \bar{A} \cdot \hat{a}_B \rightarrow \hat{a}_B = \frac{\bar{B}}{B}, \cos \theta_{AB} = \frac{\bar{A} \cdot \bar{B}}{AB}$$

$$-\bar{A}_B = (A \cdot \hat{a}_B) \hat{a}_B$$

Distance: → vector



$$\begin{aligned} \bar{r}_{pq} &= \bar{r}_q - \bar{r}_p \\ &= (x_2, y_2, z_2) - (x_1, y_1, z_1) \\ &= (x_2 - x_1) \hat{a}_x + (y_2 - y_1) \hat{a}_y + (z_2 - z_1) \hat{a}_z \end{aligned}$$

$$|\bar{r}_{pq}| = r_{pq} = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$

$$\hat{a}_{r_{pq}} = \frac{\bar{r}_{pq}}{r_{pq}} = \hat{a}_{r_{qp}}$$

$$\boxed{\bar{r}_{qp} = -\bar{r}_{pq}}$$

Ex: Given  $\bar{A} = 3\hat{a}_x + 4\hat{a}_y + \hat{a}_z$   
 $\bar{B} = 2\hat{a}_y - 5\hat{a}_z$

Find: (a)  $\theta_{AB}$  (b)  $\bar{A}_B$

$$(a) \theta = \cos^{-1} \frac{\bar{A} \cdot \bar{B}}{AB} \quad \text{or} \quad \theta = \sin^{-1} \frac{|\bar{A} \times \bar{B}|}{AB} \quad A = \sqrt{6}, \quad B = \sqrt{29}$$

$$\bar{A} \cdot \bar{B} = 0 + 8 - 5 = 3, \quad \theta = \cos^{-1} \left( \frac{3}{\sqrt{29} \sqrt{6}} \right) = 83.73^\circ$$

$$b) \bar{AB} = (\bar{A} \cdot \hat{a}_B) \hat{a}_B$$

$$\hat{a}_B = \frac{\bar{B}}{B} = \frac{(0, 2, -5)}{\sqrt{29}}$$

$$= \frac{2}{\sqrt{29}} \hat{a}_y - \frac{5}{\sqrt{29}} \hat{a}_z$$

$$(\bar{A} \cdot \hat{a}_B) = \left( 0 + \frac{8}{\sqrt{29}} - \frac{5}{\sqrt{29}} \right) \cdot \left( 0, \frac{2}{\sqrt{29}}, \frac{-5}{\sqrt{29}} \right)$$

$$= \frac{3}{29} (0, 2, -5)$$

$$\Rightarrow \bar{AB} = \frac{6}{29} \hat{a}_y - \frac{15}{29} \hat{a}_z$$

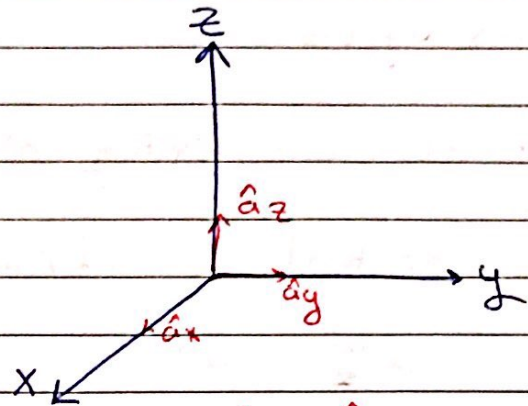
## CH-2 Coordinate systems-

### 1) Cartesian coordinate

$$-\infty < x < \infty$$

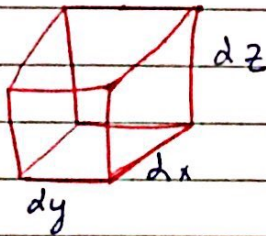
$$-\infty < y < \infty$$

$$-\infty < z < \infty$$



3D object  $\rightarrow$  infinite Box

$\hat{a}_x, \hat{a}_y, \hat{a}_z \rightarrow$  unit vector



$\rightarrow$  differential Box

\* Differential elements  $\rightarrow (dx, dy, dz)$

\* differential length ( $\vec{dl}$ )  $\rightarrow$  vector

$$\vec{dl} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

\* differential normal surface Area ( $\vec{ds}$ )  $\rightarrow$  vector

$$\vec{ds}_{\text{front}} = dy dz (\hat{a}_x)$$

$$\vec{ds}_{\text{back}} = dy dz (-\hat{a}_x)$$

$$\vec{ds}_{\text{left}} = dx dz (-\hat{a}_y)$$

$$\vec{ds}_{\text{right}} = dx dz (\hat{a}_y)$$

$$\vec{ds}_{\text{top}} = dx dy (\hat{a}_z)$$

$$\vec{ds}_{\text{bot}} = dx dy (-\hat{a}_z)$$



\* differential volume (dV)  $\rightarrow$  scalar

$$dV = dx dy dz$$

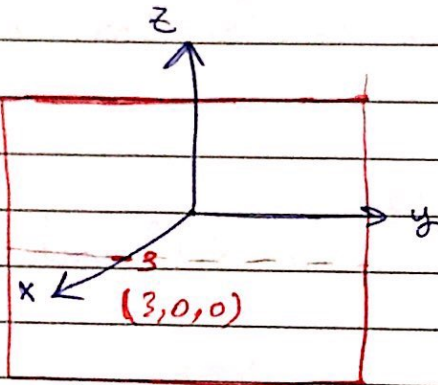
- 2D surface: by fixing one variable

• if  $x = \text{constant} \rightarrow$  inf plane //  $yz$  plane

ex:

$$x=3 \quad (-\infty < y < \infty)$$

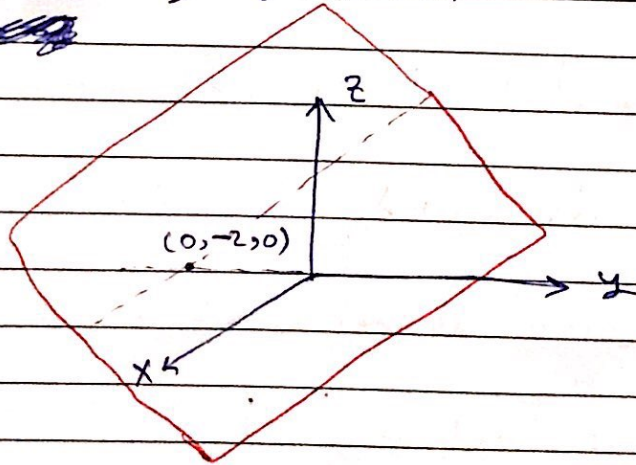
if  $x=0 \rightarrow$  inf plane along  $yz$  plane



• if  $y = \text{constant}$

$\rightarrow$  inf plane // or ~~along~~ along  $(y=0)$   $xz$  plane

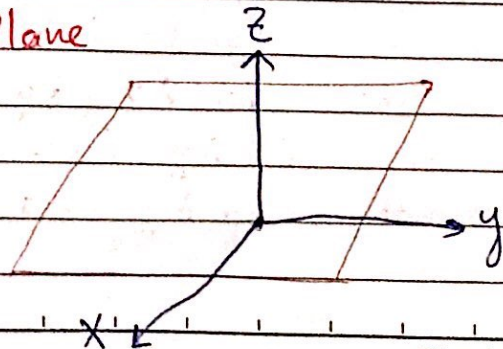
ex:  $y = -2$



• if  $z = \text{constant}$

$\rightarrow$  inf plane along  $xy$  plane

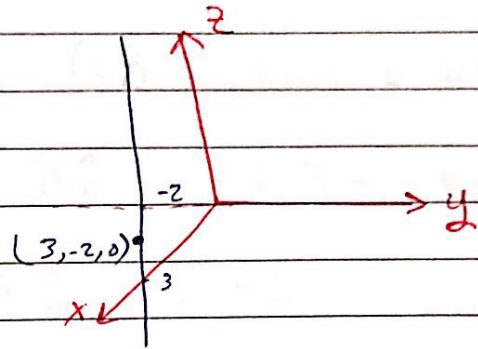
ex  $z=0$



\* 1D segment = by fixing two variables

• if  $x, y$  are constant

$x = -3, y = -2 \rightarrow$  inf line //  $z$ -axis



\* Same

-  $x, z$  are constant

$\rightarrow$  inf line // or along  $y$  axis

-  $y, z$  are constant

$\rightarrow$  inf line // or along  $x$ -axis

## \* 2) Cylindrical coordinate

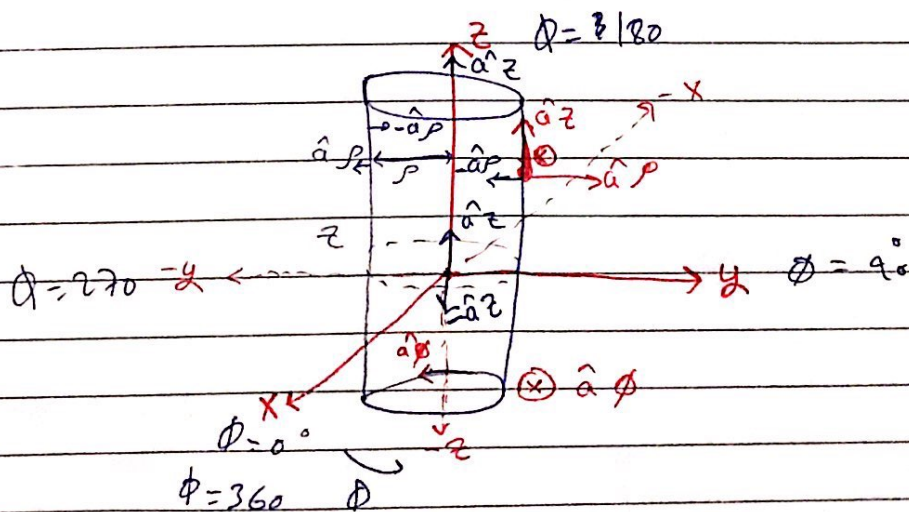
$$0 < \rho < \infty$$

$$0 \leq \phi \leq 2\pi$$

$$-\infty < z < \infty$$

} 3D object inf solid cylindrical

unit vector  $\rightarrow \hat{a}_\rho, \hat{a}_\phi, \hat{a}_z$



\* Differential elements :-

$$(dr, r d\phi, dz)$$

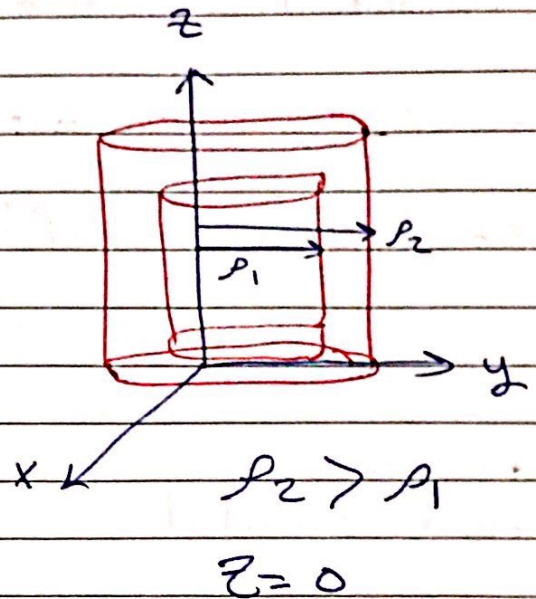
$$dL = dr \hat{r} + r d\phi \hat{\phi} + dz \hat{z}$$

$$ds_{top} = r dr d\phi (\hat{z})$$

$$ds_{bot} = -r dr d\phi (\hat{z})$$

$$ds_{side} = r d\phi dz (\hat{r})$$

$$ds_{\phi} = dr dz \hat{\phi}$$



$$\bullet dr = r dr d\phi dz$$

\* 2D surface

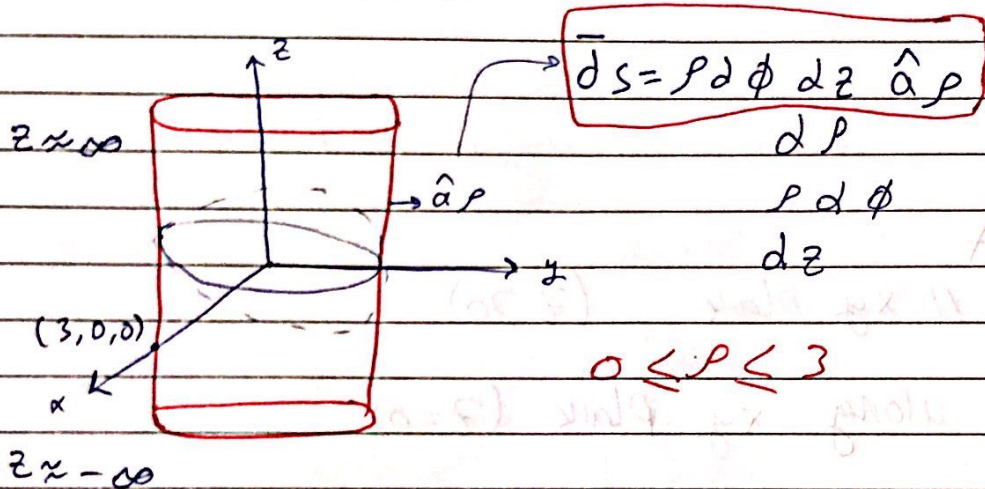
•  $\rho = \text{constant}$

↳ inf hollow cylinder

↳ inf line ( $\rho=0$ ) along z-axis

$\rho = 3$

$(3, \phi, 0)$

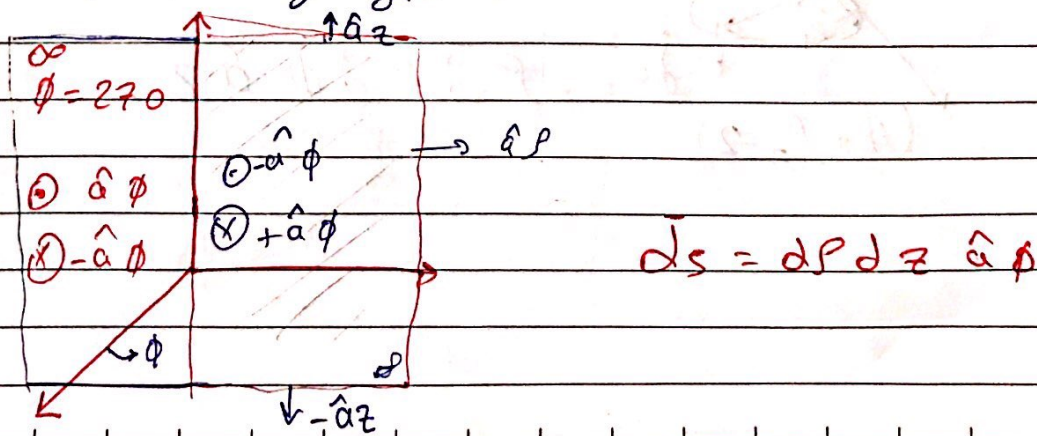


•  $\phi = \text{constant}$

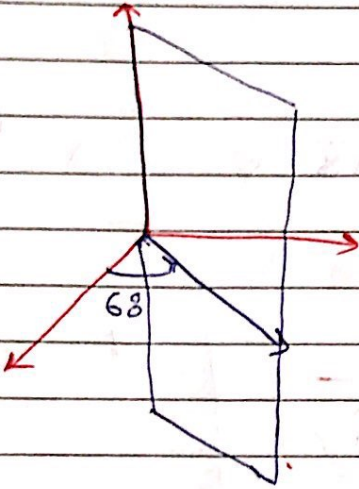
↳ inf plane

$\phi = 90$

↳ inf plane along yz-plane



$$\phi = 60$$

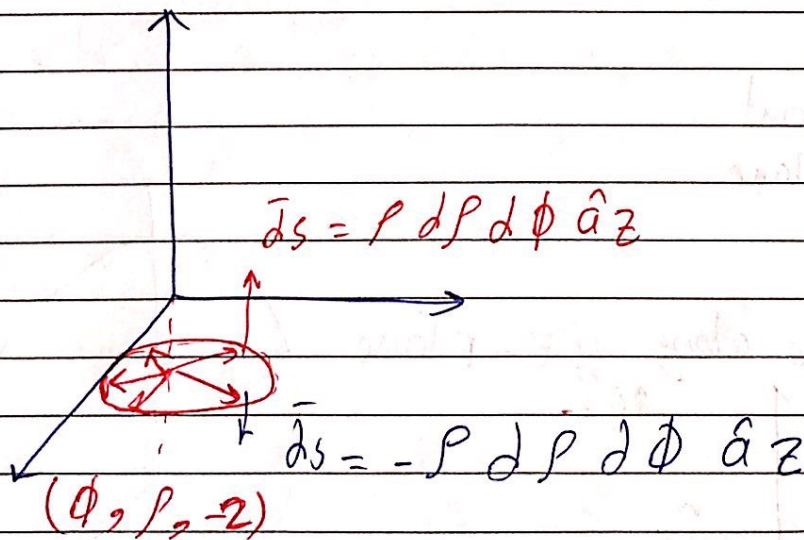


$z = \text{constant}$

thin disk //  $xy$  plane ( $z > 0$ )

along  $xy$  plane ( $z = 0$ )

$$z = -2$$



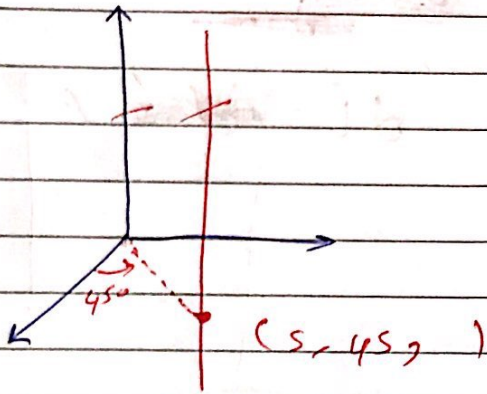
## \* 1D Segment

- $\rho, \phi$  are constant

↳ inf line // z axis ( $\rho > 0$ )

along z axis ( $z=0$ )

$$\rho = 5 \quad \phi = 45^\circ$$



$$\rho = 0 \quad \phi = 0^\circ$$

$$\rho = 0 \quad \phi = 90^\circ$$

$$dl = dz \hat{z} + \cancel{d\rho \hat{\rho}} + \cancel{\rho d\phi \hat{\phi}}$$

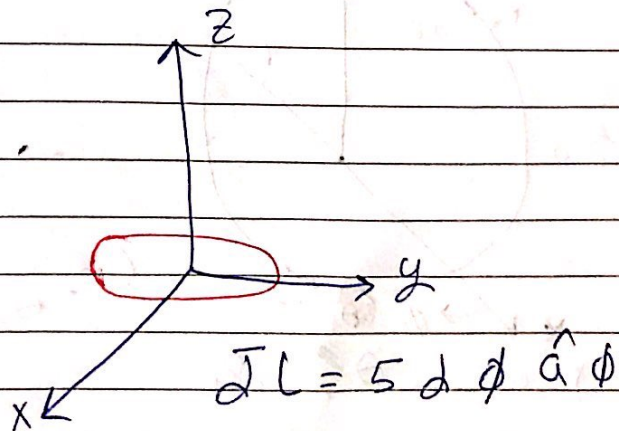
- $\rho, z$  are constant :-

↳ circle // xy plane ( $\rho \neq 0, z \neq 0$ )

↳ circle along xy plane ( $\rho \neq 0, z = 0$ )

↳ point  $\rightarrow (\rho = 0)$

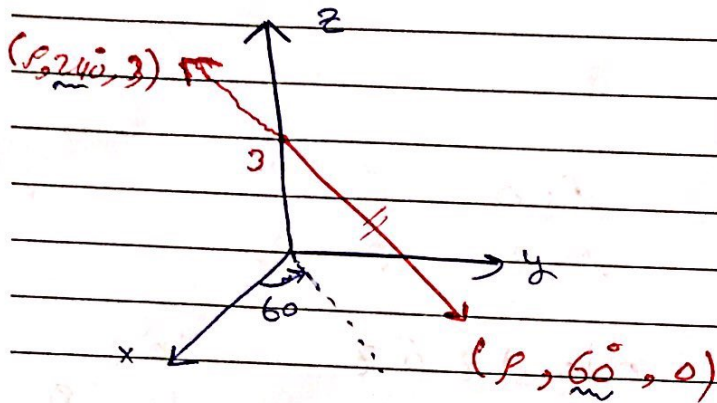
$$\rho = 5 \quad z = 0$$



•  $\phi, z$  are constant

↳ semi-inf-line (ray)

ex  $\phi = 60$   $z = 3$

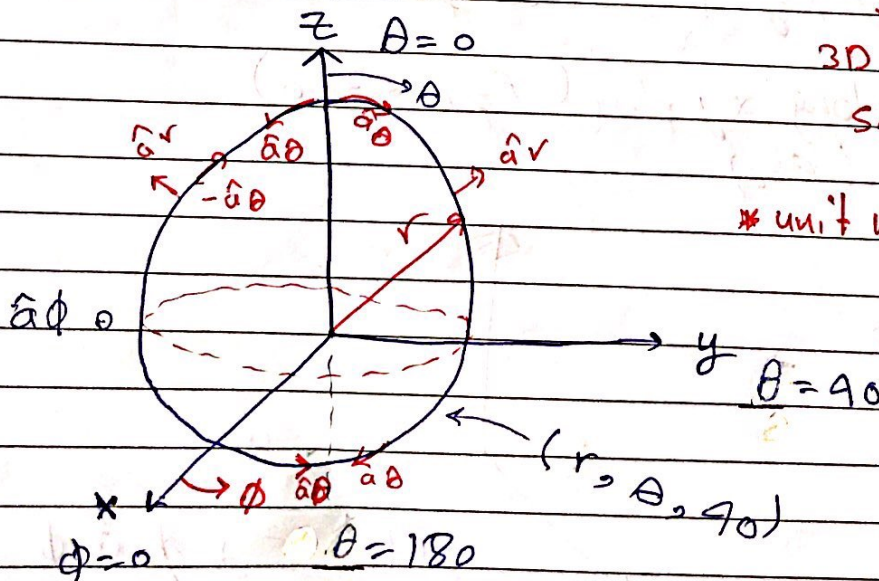


$$d\vec{l} = dr \hat{a}_r$$

\* 3) spherical coordinate.

$$0 \leq r < \infty, \quad 0 \leq \theta \leq \pi, \quad 0 \leq \phi \leq 2\pi$$

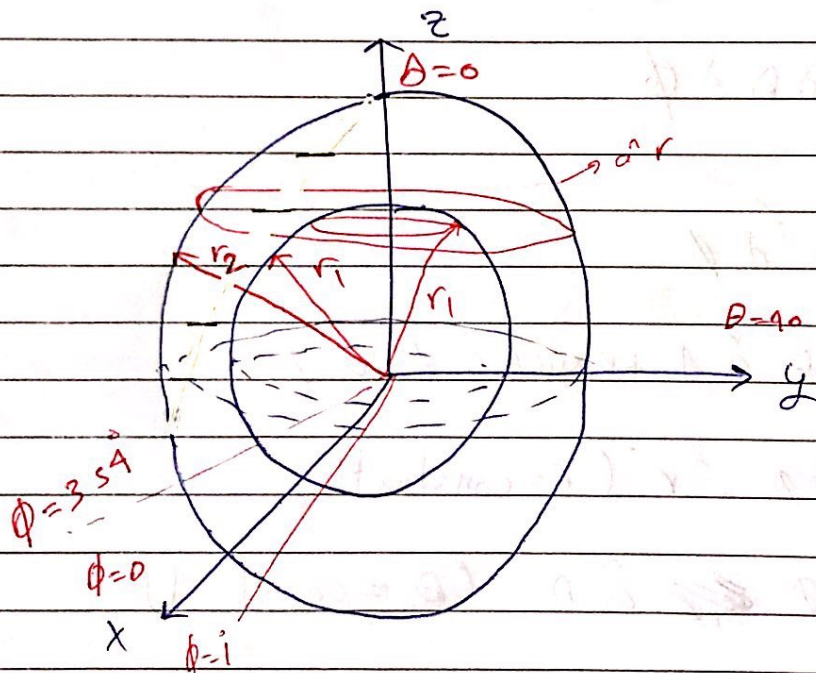
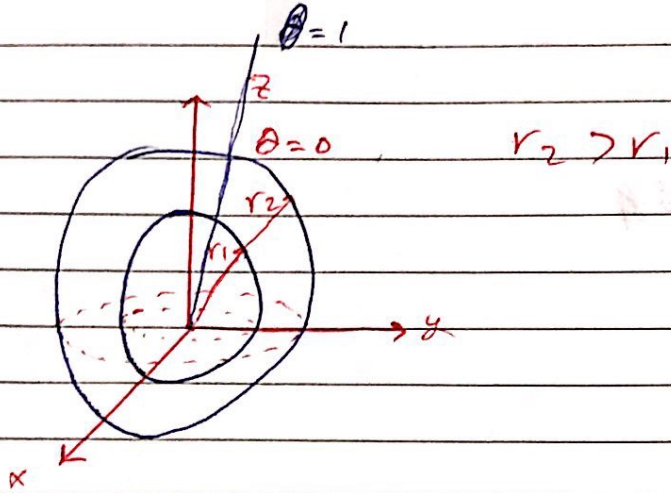
3D object in solid sphere.



\* unit vector  $\rightarrow \hat{a}_r, \hat{a}_\theta, \hat{a}_\phi$

Differential elements

$$dr, r d\theta, r \sin \theta d\phi$$





$$\begin{matrix} \rightarrow \theta, \phi \text{ const} & \rightarrow r, \phi \text{ const} & \rightarrow r, \theta \text{ const} \end{matrix}$$

$$dL = dr \hat{a}_r + r d\theta \hat{a}_\theta + r \sin \theta d\phi \hat{a}_\phi$$

$$\bar{d}s = r^2 \sin \theta d\theta d\phi \hat{a}_r$$

surface  
shell

$$ds_\theta = r \sin \theta dr d\phi \hat{a}_\theta$$

$\hookrightarrow \theta = \text{constant}$

$$ds_\phi = r dr d\theta \hat{a}_\phi$$

$\hookrightarrow \phi = \text{constant}$

$$dv = r^2 \sin \theta dr d\theta d\phi$$

$$dr, r d\theta, r \sin \theta d\phi$$

$$dL = dr \hat{a}_r + r d\theta \hat{a}_\theta + r \sin \theta d\phi \hat{a}_\phi$$

$$\bar{d}s = r^2 \sin \theta d\theta d\phi \hat{a}_r \quad (r = \text{constant})$$

$$\bar{d}s = r \sin \theta dr d\phi \hat{a}_\theta \quad (\theta = \text{constant})$$

$$\bar{d}s = r dr d\theta \hat{a}_\phi \quad (\phi = \text{constant})$$

$$dv = r^2 \sin \theta dr d\theta d\phi$$

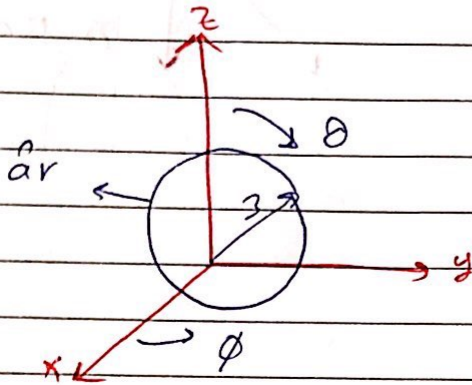
2D - surface

•  $r = \text{constant}$

↳ hollow sphere ( $r > 0$ )

↳ point ( $r = 0$ )

$r = 3$



$$\text{Area} = \int ds = \int_0^{2\pi} \int_0^{\pi} r^2 \sin \theta d\theta d\phi$$

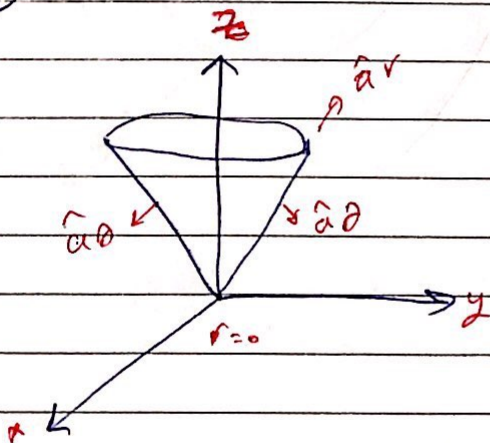
•  $\theta = \text{constant}$

↳ inf hollow cone  $\theta \in (0, 90)$  ↳ not include

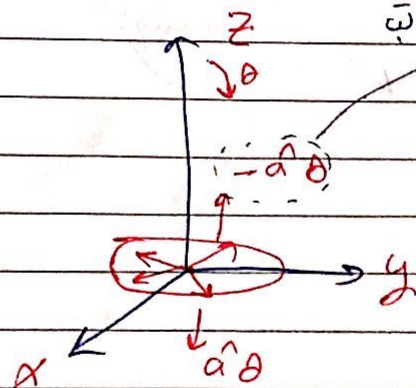
↳ inf Disk along xy plane ( $\theta = 90^\circ$ )

↳ semi-inf -line along (+ve z axis  $\theta = 0$ ) or (-ve z axis  $\theta = 180$ )

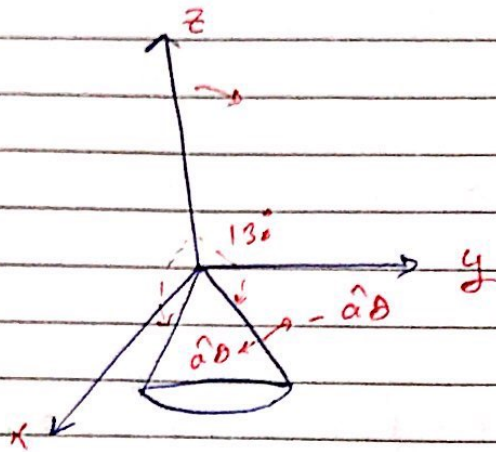
$\theta = 45^\circ$



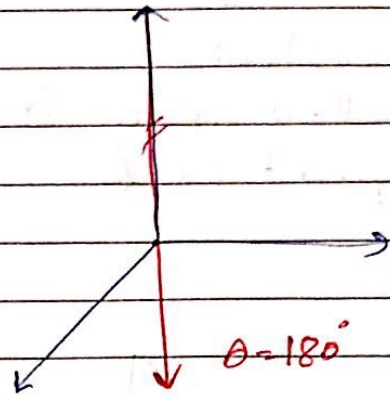
$\theta = 90^\circ$



$\theta = 130^\circ$



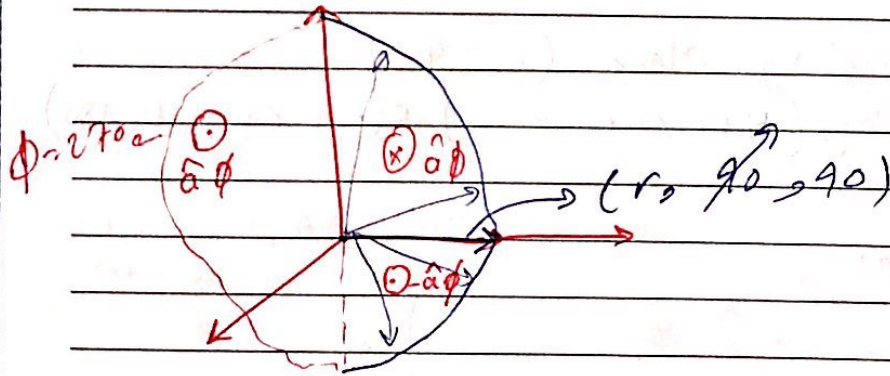
$\theta = 0$



•  $\phi = \text{constant}$

↳ semi inf Disk

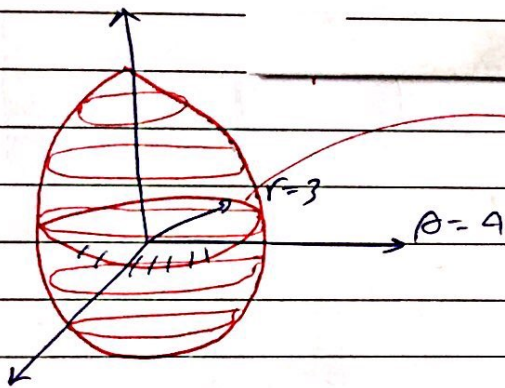
$\theta = 90$



\* 1D segment

$r, \theta$  are constant

- circle // xy plane ( $r \neq 0, \theta = 90^\circ$ )
- along xy plane ( $r \neq 0, \theta = 90^\circ$ )
- point ( $r = 0$ )



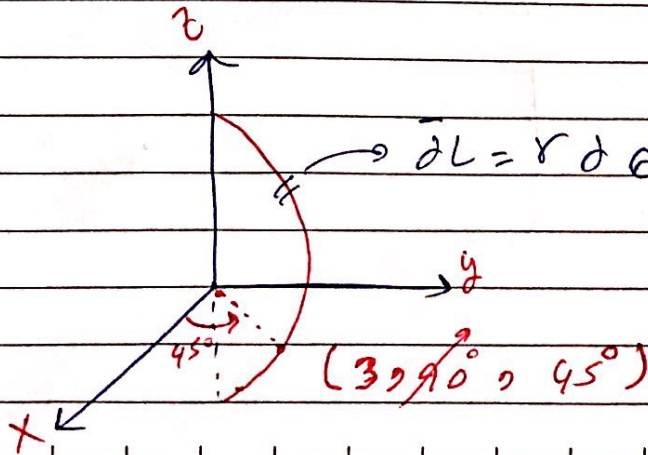
$$\vec{dL} = r \sin \theta \, d\phi \, \hat{a}_\phi$$

$$= 3 \sin 90^\circ \, d\phi \, \hat{a}_\phi$$

•  $r, \theta$  constant

- half circle ( $r \neq 0$ )
- point ( $r = 0$ )

$r = 3 \quad \theta = 45^\circ$



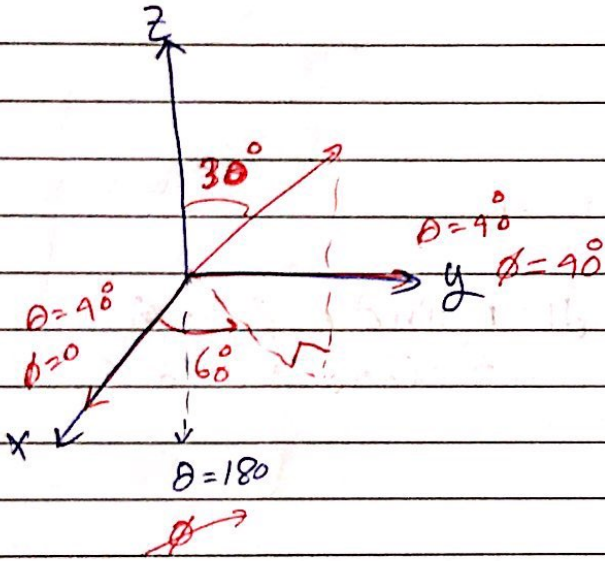
$$\vec{dL} = r \, d\theta \, \hat{a}_\theta$$

$(3, 90^\circ, 45^\circ)$

•  $\theta, \phi$  are constant

(semi-inf-Line (ray))

$$\theta = 30^\circ \quad \phi = 60^\circ$$



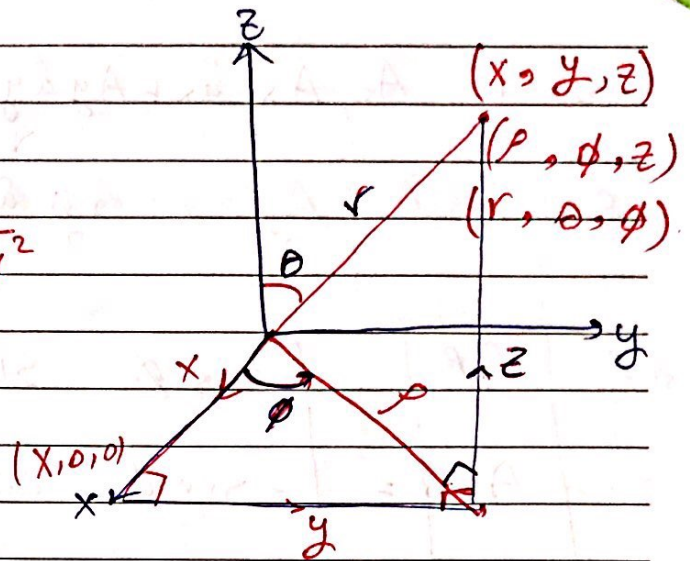
# \* point and vector transformation

↳ point conversion

$$\sin \phi = \frac{y}{\rho} = \frac{y}{\sqrt{x^2 + y^2}}$$

$$\cos \phi = \frac{x}{\rho}$$

$$\tan \phi = \frac{y}{x}$$



\* convert from:

• cart  $\rightarrow$  cyl

$$(x, y, z) \rightarrow (\rho, \phi, z) ?$$

$$\rho = \sqrt{x^2 + y^2}$$

$$\phi = \tan^{-1} \left( \frac{y}{x} \right)$$

$$z = z$$

• cyl  $\rightarrow$  cart

$$(\rho, \phi, z) \rightarrow (x, y, z)$$

$$x = \rho \cos \phi$$

$$y = \rho \sin \phi$$

$$z = z$$

• car  $\rightarrow$  sph

$$x, y, z \rightarrow (r, \theta, \phi)$$

$$r = \sqrt{x^2 + y^2 + z^2}$$

$$\theta = \tan^{-1} \left( \frac{\sqrt{x^2 + y^2}}{z} \right)$$

$$\phi = \tan^{-1} \frac{y}{x}$$

• cyl  $\rightarrow$  sph

$$(\rho, \phi, z) \rightarrow (r, \theta, \phi)$$

$$r = \sqrt{\rho^2 + z^2}$$

$$\theta = \tan^{-1} \left( \frac{\rho}{z} \right)$$

$$\phi = \phi$$

• sph  $\rightarrow$  cart

$$(r, \theta, \phi) \rightarrow (x, y, z)$$

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

$$z = r \cos \theta$$

• sph  $\rightarrow$  cyl

$$\rho = r \sin \theta$$

$$z = r \cos \theta$$

$$\phi = \phi$$

\* Vector conversion :-

Cart  $\rightarrow$  cyl

$$\text{cart: } \vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$$

$$\text{cyl: } \vec{A} = A_\rho \hat{a}_\rho + A_\phi \hat{a}_\phi + A_z \hat{a}_z$$

$$\begin{array}{l} \hat{a}_\rho \leftarrow \\ \hat{a}_\phi \leftarrow \\ \hat{a}_z \leftarrow \end{array} \begin{bmatrix} A_\rho \\ A_\phi \\ A_z \end{bmatrix} = \begin{bmatrix} \cos \phi & \sin \phi & 0 \\ -\sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} \begin{array}{l} \rightarrow \hat{a}_x \\ \rightarrow \hat{a}_y \\ \rightarrow \hat{a}_z \end{array}$$

Unit vector conversion

Given

Two step to use

$$\textcircled{1} A_\rho = \cos \phi \cdot A_x + \sin \phi \cdot A_y$$

$$A_\phi = -\sin \phi \cdot A_x + \cos \phi \cdot A_y$$

$$A_z = A_z$$

$$\textcircled{2} x = \rho \cos \phi$$

$$y = \rho \sin \phi$$

$$\text{ex } A_x = x^2 y \Rightarrow (\rho \cos \phi)^2 \rho \sin \phi$$

Cyl  $\rightarrow$  cart

$$(A\rho, A\phi, Az) \rightarrow (Ax, Ay, Az)$$

$$\begin{bmatrix} Ax \\ Ay \\ Az \end{bmatrix} = \begin{bmatrix} \cos\phi & -\sin\phi & 0 \\ \sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A\rho \\ A\phi \\ Az \end{bmatrix}$$

cart  $\rightarrow$  sph

$$\vec{B} = (B_x, B_y, B_z)$$

$$\vec{B} = (B_r, B_\theta, B_\phi)$$

$$\begin{bmatrix} B_r \\ B_\theta \\ B_\phi \end{bmatrix} = \begin{bmatrix} \sin\theta \cos\phi & \sin\theta \sin\phi & \cos\theta \\ \cos\theta \cos\phi & \cos\theta \sin\phi & -\sin\theta \\ -\sin\phi & \cos\phi & 0 \end{bmatrix} \begin{bmatrix} B_x \\ B_y \\ B_z \end{bmatrix}$$

unit vector basis

$$\begin{bmatrix} B_x \\ B_y \\ B_z \end{bmatrix} = \begin{bmatrix} \hat{e}_x \\ \hat{e}_y \\ \hat{e}_z \end{bmatrix} \begin{bmatrix} B_r \\ B_\theta \\ B_\phi \end{bmatrix}$$



• Cyl  $\rightarrow$  sph  
 $\leftarrow$

$$(A_r, A_\theta, A_z) \rightarrow (A_\rho, A_\theta, A_\phi)$$

$$\begin{bmatrix} A_r \\ A_\theta \\ A_\phi \end{bmatrix} = \begin{bmatrix} \sin \theta & 0 & \cos \theta \\ \cos \theta & 0 & -\sin \theta \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} A_\rho \\ A_\theta \\ A_z \end{bmatrix}$$

$$A_\phi = A_\phi$$

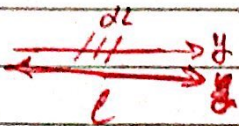


### CH3 Vector calculus

Integration:-

\* Line integral  $\rightarrow \vec{dl}$

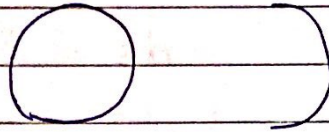
$$\int_C \frac{1}{L} dL \text{ scalar} \quad \text{or} \quad \int_C \vec{A} \cdot \vec{dl} \text{ vector}$$



$$dl = dy$$

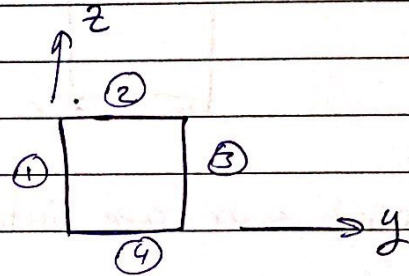
$$\vec{dl} = dy \hat{a}_y$$

1D segments



\* closed line integral

$$\oint_C \vec{A} \cdot \vec{dl}$$



$$\oint_C \vec{A} \cdot \vec{dl} = \int_{l_1} \vec{A} \cdot \vec{dl}_1 + \int_{l_2} \vec{A} \cdot \vec{dl}_2 \quad \#$$

$$+ \int_{l_3} \vec{A} \cdot \vec{dl}_3 + \int_{l_4} \vec{A} \cdot \vec{dl}_4$$

$$\vec{dl}_1 = dz \hat{a}_z$$

$$\vec{dl}_2 = dy \hat{a}_y$$

$$\vec{dl}_3 = dz \hat{a}_z$$

$$\vec{dl}_4 = dy \hat{a}_y$$

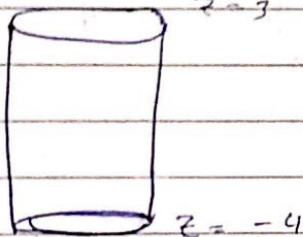
\* Surface integral

$$\int_S \rho_s ds \quad \text{or} \quad \int_S \vec{A} \cdot \vec{ds}$$

ex

$$\vec{A} = (A_\rho, 0, A_z)$$

$$\rho = 3$$



$$\vec{ds} = \rho d\phi dz \hat{a}_\rho$$

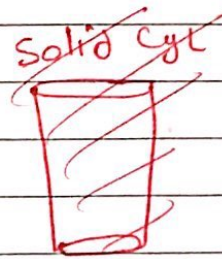
$$\int_{-4}^3 \int_0^{2\pi} \rho A_\rho d\phi dz$$

• closed surface integral:-

$$\oint_S \vec{A} \cdot \vec{ds}$$

ex  $\vec{A} = (A_x, A_y, A_z)$

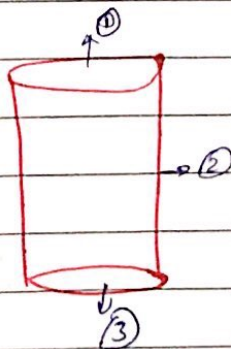
use matrix  $\rightarrow \vec{A} = (A_\rho, A_\phi, A_z)$  solid cyl



$$\vec{ds}_1 = \rho d\rho d\phi \hat{a}_z$$

$$\vec{ds}_2 = \rho d\phi dz \hat{a}_\rho$$

$$\vec{ds}_3 = -\rho d\rho d\phi \hat{a}_z$$



$$0 \leq \rho \leq 3$$

$$0 \leq \phi \leq 2\pi$$

$$-2 \leq z \leq 2$$

$$\oint_S \vec{A} \cdot \vec{ds} = \int_{S_1} \vec{A} \cdot \vec{ds}_1 + \int_{S_2} \vec{A} \cdot \vec{ds}_2$$

$$+ \int_{S_3} \vec{A} \cdot \vec{ds}_3$$

\* Volume integral

$$\int_V \rho v \, dv \quad dv = \rho \, d\rho \, d\phi \, dz$$

$$\int_{-2}^2 \int_0^{2\pi} \int_0^3 \rho v \, \rho \, d\rho \, d\phi \, dz$$

\* Del operator = (vector)  $(\nabla)$   $\vec{\nabla} \rightarrow x$

in cart.

$$\nabla = \frac{\partial}{\partial x} \hat{a}_x + \frac{\partial}{\partial y} \hat{a}_y + \frac{\partial}{\partial z} \hat{a}_z \quad \text{--- (1)}$$

in cyl.

$$\nabla = \frac{\partial}{\partial \rho} \hat{a}_\rho + \frac{1}{\rho} \frac{\partial}{\partial \phi} \hat{a}_\phi + \frac{\partial}{\partial z} \hat{a}_z \quad \text{--- (2)}$$

in sph.

$$\nabla = \frac{\partial}{\partial r} \hat{a}_r + \frac{1}{r} \frac{\partial}{\partial \theta} \hat{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} \hat{a}_\phi \quad \text{--- (3)}$$

- Del has 4 usage

1) Gradient  $\rightarrow$  vector

$\leftarrow$  scalar

$$\nabla V = \text{gradient of } V$$

$$\nabla V = \frac{\partial V}{\partial x} \hat{a}_x + \dots \hat{a}_z$$

2) Divergence  $\rightarrow$  scalar

$\nabla \cdot \vec{A}$  = Divergence of  $\vec{A}$

• in cart  $\nabla \cdot \vec{A} = \left( \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right) \cdot (A_x, A_y, A_z)$

$$\nabla \cdot \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

• in cyl. (given)

$$\nabla \cdot \vec{A} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho A_\rho) + \frac{1}{\rho} \frac{\partial A_\phi}{\partial \phi} + \frac{\partial A_z}{\partial z}$$

$$\vec{A} = \underbrace{\rho^2}_{A_\rho} \hat{a}_\rho + \underbrace{\cos \phi}_{A_\phi} \hat{a}_\phi, \quad A_z = 0$$

• in sph (given)

$$\nabla \cdot \vec{A} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta A_\theta) + \frac{1}{r \sin \theta} \frac{\partial A_\phi}{\partial \phi}$$

3) curl  $\rightarrow$  Vector

$$\nabla \times \bar{A} = \text{curl of } (A)$$

• in cart

$$\nabla \times \bar{A} = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix}$$

• in cyl (given)

$$\nabla \times \bar{A} = \frac{1}{\rho} \begin{vmatrix} \hat{a}_\rho & \rho \hat{a}_\phi & \hat{a}_z \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ A_\rho & \rho A_\phi & A_z \end{vmatrix}$$

• in sph (given)

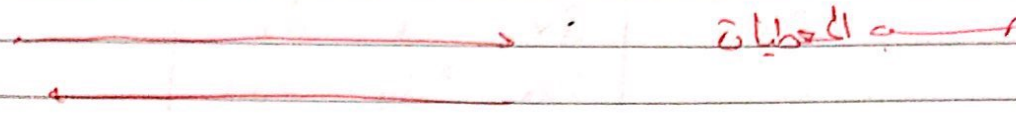
$$\nabla \times \bar{A} = \frac{1}{r^2 \sin \theta} \begin{vmatrix} \hat{a}_r & r \hat{a}_\theta & r \sin \theta \hat{a}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & r A_\theta & r \sin \theta A_\phi \end{vmatrix}$$

4) Laplacian  $\rightarrow$  scalar  $\rightarrow$  CH6

$$\nabla \cdot \nabla V = \nabla^2 V = \text{Laplacian of } (V)$$

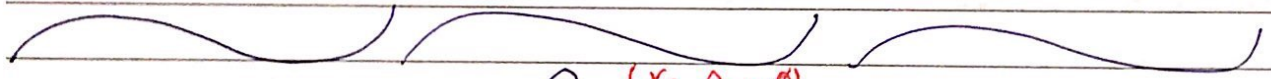
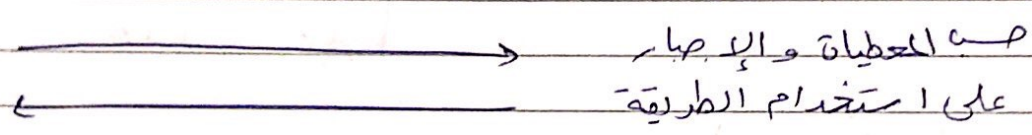
\* Divergence theorem -

$$\oint_S \vec{A} \cdot d\vec{s} = \int_{vol} \nabla \cdot \vec{A} \, dV$$



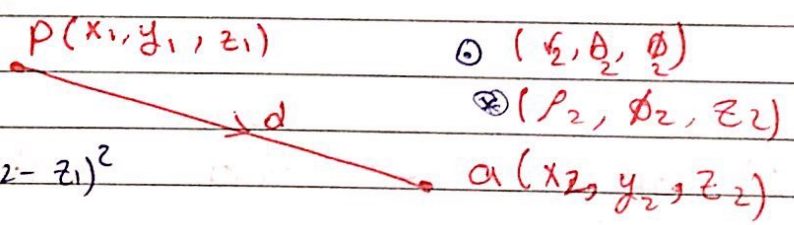
\* Stock's theorem -

$$\oint_C \vec{A} \cdot d\vec{l} = \int_S \nabla \times \vec{A} \cdot d\vec{s} \quad \text{curl}$$



- ⊙  $(r_1, \theta_1, \phi_1)$
- ⊗  $(\rho_1, \phi_1, z_1)$

\* Distance -



$$d^2 = (x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2$$

$$\textcircled{*} \quad d^2 = \rho_1^2 + \rho_2^2 - 2\rho_1\rho_2 \cos(\phi_2 - \phi_1) + (z_2 - z_1)^2$$

if  $\phi_1 = \phi_2 \rightarrow d^2 = (\rho_2 - \rho_1)^2 + (z_2 - z_1)^2$

⊙  $d^2 = (r_2 - r_1)^2$  if  $\theta_1 = \theta_2$   
 $\phi_1 = \phi_2$

أوعن طريقة التحويل بين cart, cyl, sph

**CH-4** Electrostatic fields:-

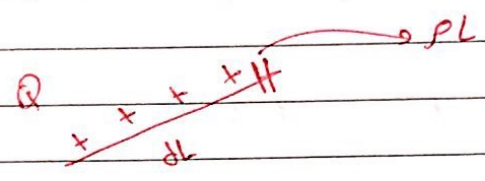
Sources:-

1) point charge ( $Q$ ) in (c) <sup>→ coulomb</sup>

2) continuous charge distribution

↳ a) line charge ( $\rho_L$ ) in (c/m)

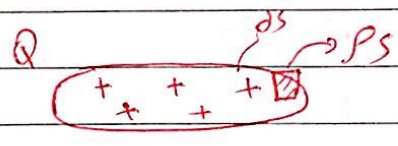
(1D segment)



$$Q = \int_L \rho_L dl$$

b) surface charge ( $\rho_S$ ) → (c/m<sup>2</sup>)

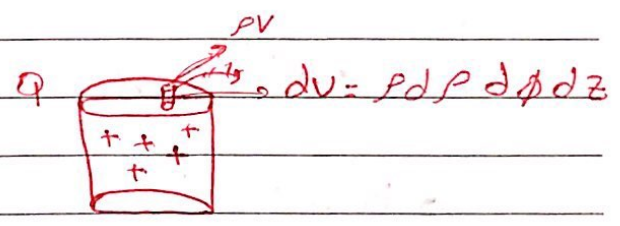
(2D surface)



$$Q = \int_S \rho_S ds$$

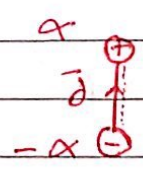
c) Volume charge dist ( $\rho_V$ ) → (c/m<sup>3</sup>)

(3D object)



$$Q = \int_V \rho_V dv$$

3) ~~Electric Dipole~~



4) ~~Polarized Dielectric~~

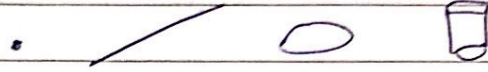
↳ CH5



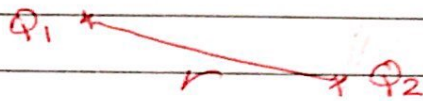
\*Major Laws :-

1) Coloumb's Law  
↳ general

2) Gauss's law (special case)



• Coloumb's Law (by Exp)



$F_e \equiv F \equiv$  electrical force (N)

$F \propto \frac{Q_1 Q_2}{r^2}$  relation

$F = \frac{K Q_1 Q_2}{r^2}$ , K = Proportionality constant

$K = \frac{1}{4\pi\epsilon_0}$  → CH<sub>4</sub> → Free space

↳ unit used  $\frac{1}{4\pi}$   
↳ media  $\epsilon$

$\epsilon =$  permittivity (F/m),  $\epsilon_0 =$  free space permittivity

$\epsilon_0 = \frac{10^{-9}}{36\pi} \text{ F/m} = 8.85 \times 10^{-12} \text{ F/m}$

$$F = \frac{Q_1 Q_2}{4 \pi \epsilon_0 r^2} \quad (N) \quad \rightarrow \text{magnitude only}$$

\* Force as a vector :-

• the force on ( $Q_2$ ) due to ( $Q_1$ )

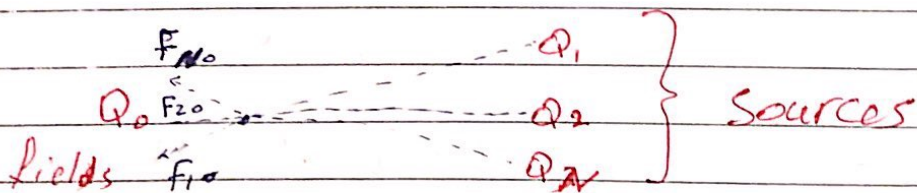
$$\textcircled{1} \quad \vec{F}_{12} = \frac{Q_1 Q_2}{4 \pi \epsilon_0 r_{12}^2} \hat{a}_{r_{12}} \quad \hat{a}_{r_{12}} \rightarrow \hat{a}_{r_{12}} = \frac{\vec{r}_{12}}{r_{12}}$$

$$\textcircled{2} \quad \vec{F}_{12} = \frac{Q_1 Q_2 \vec{r}_{12}}{4 \pi \epsilon_0 (r_{12})^3}$$

$$\textcircled{3} \quad \vec{F}_{12} = \frac{Q_1 Q_2 (\vec{r}_2 - \vec{r}_1)}{4 \pi \epsilon_0 |\vec{r}_2 - \vec{r}_1|^3} \quad (N) \quad \leftarrow \text{vector} \quad \text{الصورة النهائية للقانون}$$

distance = field - source

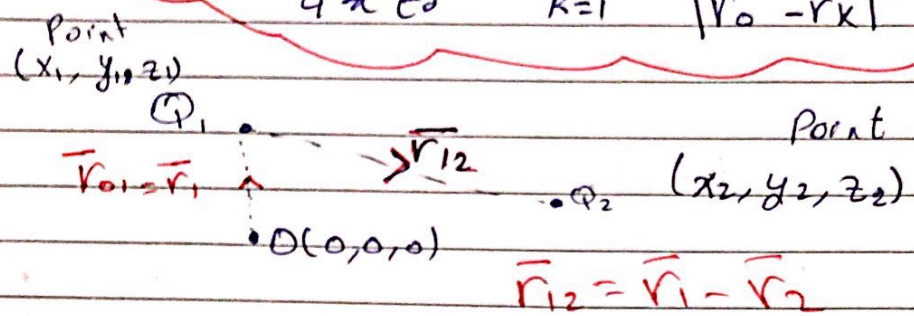
• the force due to N-Point charges



the force on  $Q_0$

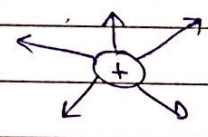
$$\vec{F} = \frac{Q_1 Q_0 (\vec{r}_0 - \vec{r}_1)}{4 \pi \epsilon_0 |\vec{r}_0 - \vec{r}_1|^3} + \frac{Q_2 Q_0 (\vec{r}_0 - \vec{r}_2)}{4 \pi \epsilon_0 |\vec{r}_0 - \vec{r}_2|^3} + \dots + \frac{Q_N Q_0 (\vec{r}_0 - \vec{r}_N)}{4 \pi \epsilon_0 |\vec{r}_0 - \vec{r}_N|^3}$$

$$\vec{F} = \frac{Q_0}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k (\vec{r}_0 - \vec{r}_k)}{|\vec{r}_0 - \vec{r}_k|^3} \quad (N)$$



\* Electric field intensity :-  $(\vec{E})$

$\vec{E} = \frac{\vec{F}}{Q_{field\ point}}$  in  $(N/C)$  or  $(V/m)$  "from coulomb law"



①  $\vec{E} = \frac{Q_{source}}{4\pi\epsilon_0 r^2} \hat{a}_r$

②  $\vec{E} = \frac{Q\vec{r}}{4\pi\epsilon_0 r^3} \quad V/m$

③  $\vec{E} = \frac{Q(\vec{r} - \vec{r}')}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|^3}$

convention

use dashes with the sources and without dashes with fields

$\vec{F}_{21} = -\vec{F}_{12}$   
 $\hat{a}_{r_{12}} \quad \hat{a}_{r_{21}}$

Ex: Two point charges  $1 \mu\text{C}$  and  $-3 \mu\text{C}$  are located  
 $(3, 2, -1)$  and  $(-1, -1, 4)$ . Find  $\vec{F}$  and  $\vec{E}$  at a  $10 \mu\text{C}$   
charge located  $(0, 3, 1)$ .

$$\vec{F} = \frac{1 \times 10^{-3} \times 10 \times 10^{-9}}{4\pi \times 10^{-7} \times 36\pi} \times (14)^{\frac{3}{2}} \hat{r}_1$$

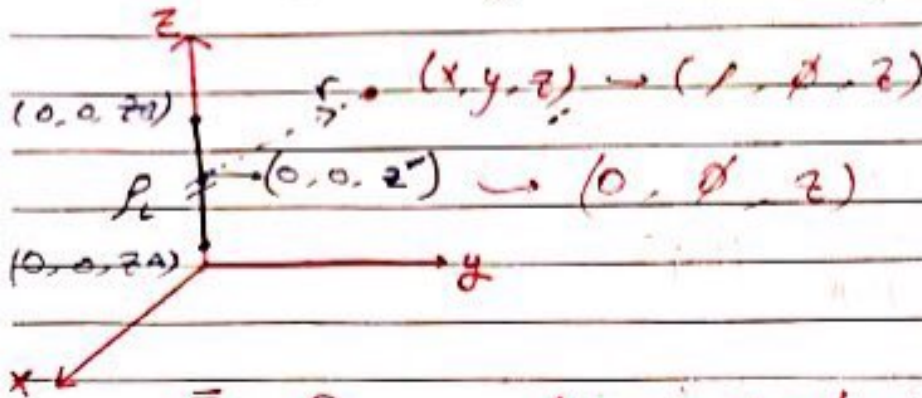
$$+ \frac{-3 \times 10^{-6} \times 10 \times 10^{-9}}{4\pi \times 10^{-7} \times 36\pi} \times (26)^{\frac{3}{2}} \hat{r}_2$$

$$\vec{F} = -6.507 \hat{a}_x - 3.817 \hat{a}_y + 7.506 \hat{a}_z \text{ mN}$$

$$\vec{E} = \frac{\vec{F}}{10 \times 10^{-9}} \rightarrow \vec{E} = -650.7 \hat{a}_x - 381.7 \hat{a}_y + 750.6 \hat{a}_z \text{ kV/m}$$

\*E-field due to line charge :-

Ex. consider a finite line along z-axis carry charge  $\rho_c$  C/m  
Find  $\vec{E}$  at  $(x, y, z)$ .



$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{r}$  → point charge

$Q = \int \rho_c dL$  →  $\vec{E} = \int \frac{\rho_c dL \vec{r}}{4\pi\epsilon_0 r^3}$

scalar

1 aap/b

$dL = dz'$        $\vec{r} = x\hat{a}_x + y\hat{a}_y + (z - z')\hat{a}_z$

$r = \sqrt{x^2 + y^2 + (z - z')^2}$

$\vec{E} = \frac{\rho_c}{4\pi\epsilon_0} \int_{z_A}^{z_B} \frac{(x, y, (z - z'))}{[x^2 + y^2 + (z - z')^2]^{3/2}} dz'$

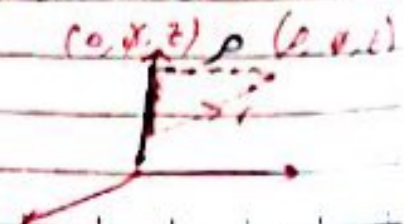
Table of integral

2 aap/b

convert to cylindrical:

$dL = dz'$        $\vec{r} = \rho\hat{a}_\rho + (z - z')\hat{a}_z$

$r = \sqrt{\rho^2 + (z - z')^2}$



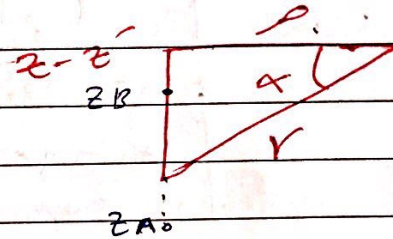
$$\vec{E} = \frac{\rho L}{4\pi\epsilon_0} \int_{z_A}^{z_B} \frac{\rho \hat{A} (z - z') \hat{z}}{[\rho^2 + (z - z')^2]^{\frac{3}{2}}} dz'$$

\* introduce angles  $\alpha, \alpha_1, \alpha_2$  and replace  $dz'$  by  $d\alpha$

$$\sin \alpha = \frac{z - z'}{r}$$

$$\cos \alpha = \frac{\rho}{r}$$

$$\tan \alpha = \frac{z - z'}{\rho}$$



$$z - z' = r \sin \alpha$$

$$(-1) dz' = (\rho \sec^2 \alpha) d\alpha$$

$$z - z' = \rho \tan \alpha$$

$$dz' = -\rho \sec^2 \alpha d\alpha$$

$$r^2 = \rho^2 + (z - z')^2 \rightarrow \rho^2 + \rho^2 \tan^2 \alpha$$

$$= \rho^2 (1 + \tan^2 \alpha) = \rho^2 \sec^2 \alpha$$

$$r = \rho \sec \alpha$$

$$r^3 = \rho^3 \sec^3 \alpha$$

$$z - z' = r \sin \alpha = \rho \sec \alpha \sin \alpha$$

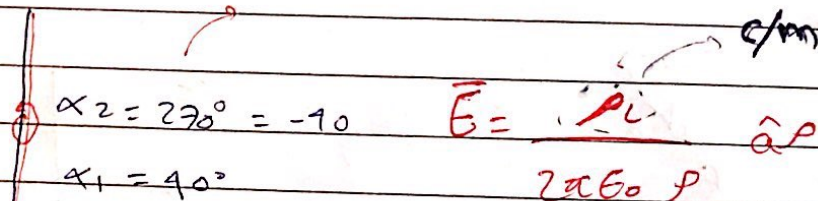
$$\rho = r \cos \alpha = \rho \sec \alpha \cos \alpha$$

$$\vec{E} = \frac{\rho L}{4\pi\epsilon_0} \int_{\alpha_1}^{\alpha_2} \frac{\rho \sec \alpha (\cos \alpha \hat{\rho} + \sin \alpha \hat{z})}{\rho^3 \sec^3 \alpha} - \rho \sec^2 \alpha d\alpha$$

$$\vec{E} = \frac{-\rho}{4\pi\epsilon_0 \rho} \left[ (\sin\alpha_2 - \sin\alpha_1) \hat{\rho} - (\cos\alpha_2 - \cos\alpha_1) \hat{z} \right] \quad \text{V/m}$$

For finite line along z-axis

• for inf. line

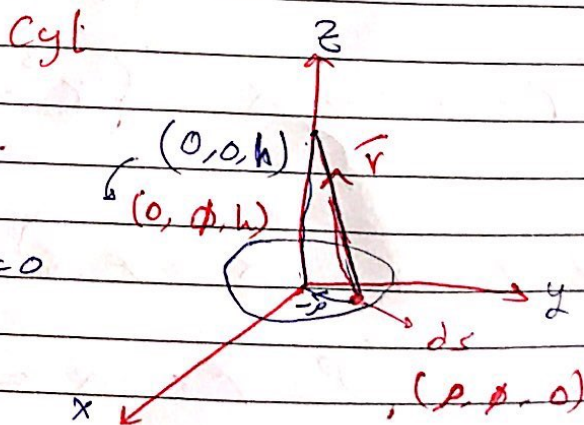
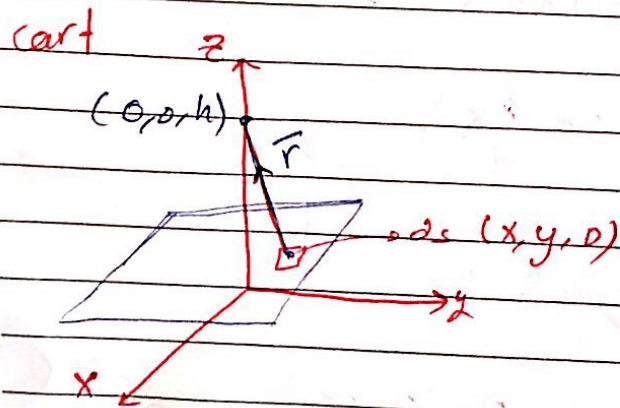


always for any line

$\rho$  is the shortest distance between the source and the field

### \* E. Field due to a surface charge

ex: consider a sheet on  $z=0$  carry charge  $\rho_s$  C/m<sup>2</sup>, find  $\vec{E}$  at  $(0,0,h)$ .



$$ds = dx dy$$

$$\vec{r} = -x\hat{x} - y\hat{y} + h\hat{z}$$

$$r = \sqrt{x^2 + y^2 + h^2}$$

$$ds = \rho d\rho d\phi$$

$$\vec{r} = -\rho\hat{\rho} + h\hat{z}$$

$$r = \sqrt{\rho^2 + h^2}$$

for point charge only

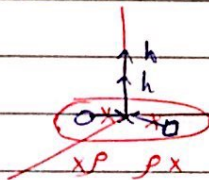
$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r, \quad Q = \int_S \rho_s ds$$

scalar

$$\vec{E} = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r^2} \hat{a}_r \rightarrow \vec{E} = \int_S \frac{\rho_s ds \vec{r}}{4\pi\epsilon_0 r^3}$$

$$\vec{E} = \frac{\rho_s}{4\pi\epsilon_0} \int_0^{2\pi} \int_0^\infty \frac{-\rho \hat{a}_\rho + h \hat{a}_z}{[\rho^2 + h^2]^{\frac{3}{2}}} \rho d\rho d\phi$$

• Due to symmetry, the  $\rho$ -component will be cancelled



$\hat{a}_\rho$  cancel

$$\vec{E} = \frac{\rho_s h}{4\pi\epsilon_0} \int_0^{2\pi} \int_0^\infty \frac{\rho}{[\rho^2 + h^2]^{\frac{3}{2}}} d\rho d\phi \hat{a}_z$$

$$\vec{E} = \frac{\rho_s h}{2\epsilon_0} \int_0^\infty \frac{\rho}{[\rho^2 + h^2]^{\frac{3}{2}}} d\rho \hat{a}_z$$

كاملة بالنسبة لـ  $\phi$  أول

let  $u = \rho^2 + h^2 \rightarrow du = 2\rho d\rho$

$$E = \frac{\rho_s h}{2\epsilon_0 (2)} \int \frac{du}{u^{\frac{3}{2}}} \rightarrow \vec{E} = \frac{\rho_s h}{4\epsilon_0 (-\frac{1}{2}) \sqrt{\rho^2 + h^2}} \Big|_0^\infty \hat{a}_z$$



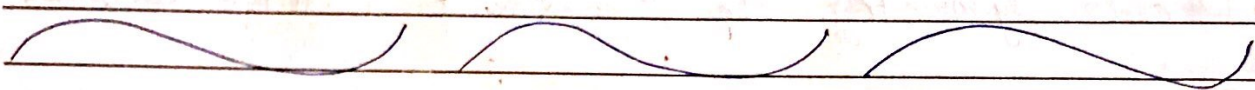
$$\vec{E} = -\frac{\rho_s h}{2\epsilon_0} \left(0 - \frac{1}{h}\right) \hat{a}_z \rightarrow \vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_z \quad \forall h$$

Note

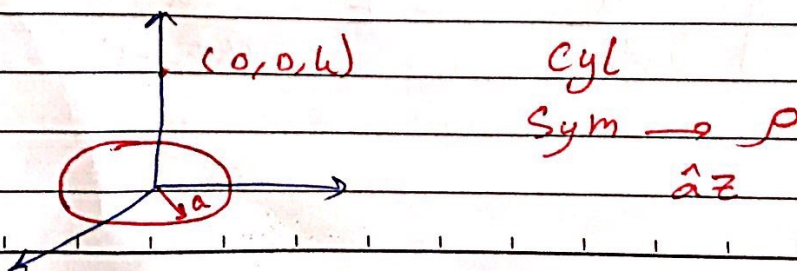
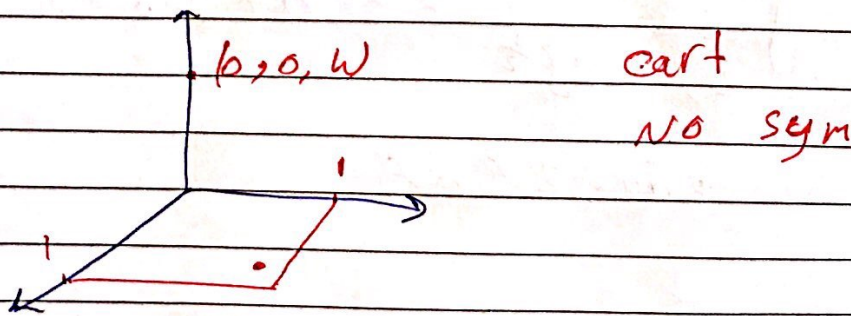
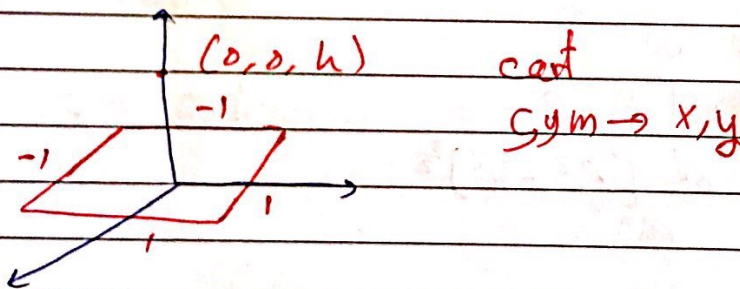
if  $(0, 0, -h) \rightarrow \vec{E} = \frac{\rho_s}{2\epsilon_0} (-\hat{a}_z)$  in cart

$(0, \phi, -h) \rightarrow \vec{r} = -\rho \hat{a}_\rho - h \hat{a}_z$  in cyl

in general  $\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_n \rightarrow$  always



Ex. for infite surface

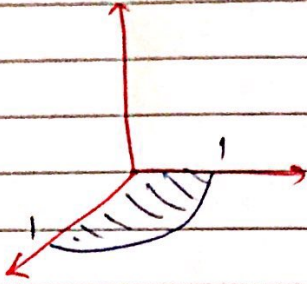


Ex.

Cyl No Sym

disk  $ds = \rho d\rho d\phi$

ring  $dl = \rho d\phi$



\* E. field for a volume charge disk.

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{r} \rightarrow \text{point}$$

$$Q = \int \rho dv \quad \vec{E} = \int \frac{\rho dv}{4\pi\epsilon_0 r^2} \hat{r}$$

So charge disk  $\rightarrow$  Gauss's law only

\* Electric field flux density ( $\vec{D}$ )

$$\vec{D} = \epsilon_0 \vec{E}$$

for point charge

$$\vec{D} = \frac{Q}{4\pi r^2} \hat{r}$$

$$F \cdot v = c$$

$$\vec{F} \downarrow \vec{E} \downarrow \vec{D}$$

for inf line

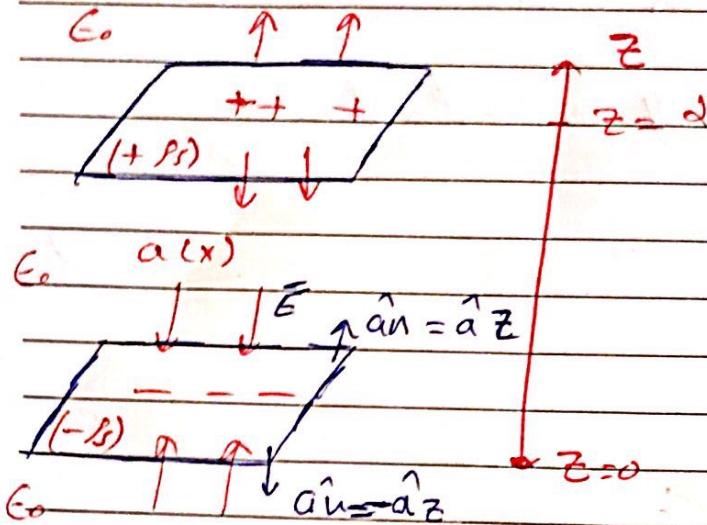
$$\vec{D} = \frac{\rho l}{2\pi r} \hat{r}$$

for inf sheet

$$\vec{D} = \frac{\rho s}{2} \hat{n}$$

Ex. for a parallel plate capacitor

(b) x



(c) x

$\vec{E}$  at point (a)

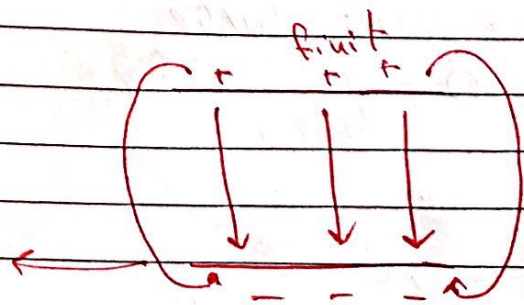
$$\vec{E} = \vec{E}_+ + \vec{E}_-$$

$$= \frac{\rho_s}{2\epsilon_0} (-\hat{a}_z) + \frac{-\rho_s}{2\epsilon_0} (\hat{a}_z) = \frac{\rho_s}{\epsilon_0} (-\hat{a}_z)$$

$$\vec{E}_b = \vec{E}_+ + \vec{E}_-$$

$$= \frac{\rho_s}{2\epsilon_0} \hat{a}_z + \frac{-\rho_s}{2\epsilon_0} \hat{a}_z = 0$$

fringing fields



field

Ex Find  $\vec{D}$  at  $(4, 0, 3)$  if there is a point charge

$-5 \pi \text{ mC}$  at  $(4, 0, 0)$  and a line charge  $3 \pi \text{ mC}$  along  $y$ -axis

$$\vec{D} = \vec{D}_Q + \vec{D}_L = \frac{Q\vec{r}}{4\pi r^3} + \frac{\rho_L \vec{\rho}}{2\pi \rho^2}$$

$$\vec{r} = 3\hat{z}, \quad r = 3 \text{ m}$$

$$\vec{\rho} = 4\hat{x} + 3\hat{z}, \quad \rho = 5 \text{ m}$$

field-source

$(0, 4, 0)$

$(0, 0, 0)$

z-axis

$$\vec{D} = 240\hat{x} + 42\hat{z} \quad \mu\text{C}/\text{m}^2 \quad \text{final answer}$$

Note:

capacitor

$$\text{at point } a) = \vec{E} = \frac{\rho_s}{\epsilon_0} (-a\hat{z})$$

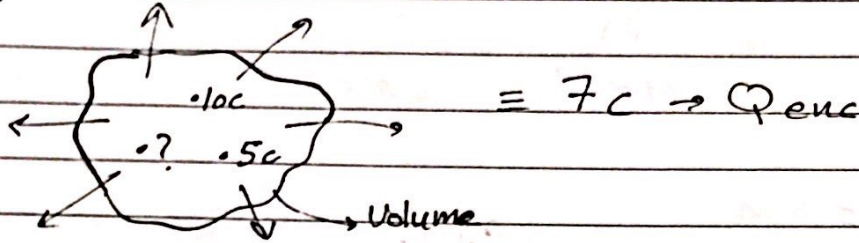
$$\vec{E} = \frac{\rho_s}{\epsilon_0} \hat{n}$$

$$\vec{D} = \rho_s \hat{n}$$

$$\boxed{\vec{D} \cdot \hat{n} = \rho_s} \text{ always}$$

\* Gauss's Law :-

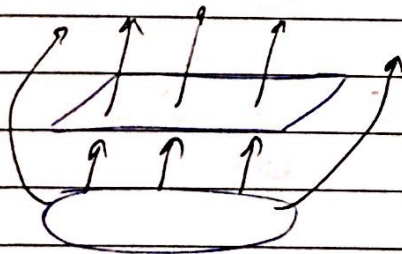
$$\oint_S \vec{D} \cdot d\vec{s} = Q_{\text{enclosed}}$$



$$\oint_S \vec{A} \cdot d\vec{s} = \int_V \nabla \cdot \vec{A} dv$$

$\Psi_e \equiv$  Electric Flux      Scaler in (c)

$$\Psi_e = \int_S \vec{D} \cdot d\vec{s} \longrightarrow \Psi_e = \oint_S \vec{D} \cdot d\vec{s} \rightarrow \text{Gauss's}$$



• Application of Gauss's law

$$\oint_S \vec{D} \cdot d\vec{s} = Q_{\text{enc}} = Q \rightarrow \text{point charge}$$

$$\int dl \rho_l dl \rightarrow \text{Line "}$$

$$\int_S \rho_s ds \rightarrow \text{surface "}$$

$\int_V \rho_V dv \rightarrow$  Volume charge

Gauss's law :

$$\oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_V dv$$

→ 1st Maxwell's eqn in integral form

- Apply Divergence theorem

$$\oint_S \vec{D} \cdot d\vec{s} = \int_V \nabla \cdot \vec{D} dv = \int_V \rho_V dv$$

$$\nabla \cdot \vec{D} = \rho_V$$

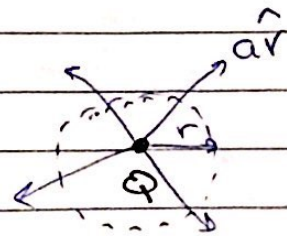
→ 1st Maxwell's eqn differential form

$$\rho_S = \vec{D} \cdot \hat{a}_n, \quad \vec{D} = \rho_S \hat{a}_n$$

$$\rho_V = \nabla \cdot \vec{D}, \quad \vec{D} = \epsilon_0 \vec{E}, \quad D \ll \ll E$$

1)  $\vec{E}$  or  $\vec{D}$  for a point charge

$$\oint_S \vec{D} \cdot d\vec{s} = Q_{enc} = Q$$



\*  $\vec{D} = D_r \hat{a}_r$

\* Gaussian surface

$$d\vec{s} = r^2 \sin \theta d\theta d\phi \hat{a}_r$$

$$\int_0^{2\pi} \int_0^{\pi} D_r r^2 \sin\theta \, d\theta \, d\phi \, \hat{a}_r = Q$$

$$\int_0^{\pi} \sin\theta \, d\theta = -\cos\theta \Big|_0^{\pi}$$

$$4\pi r^2 D_r = Q$$

$$D_r = \frac{Q}{4\pi r^2}$$

$$D = \frac{Q}{4\pi r^2} \hat{a}_r$$

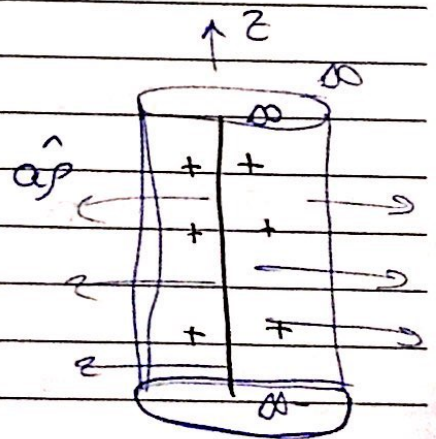
$$\vec{E} = \frac{D}{\epsilon_0} = \frac{Q}{4\pi \epsilon_0 r^2} \hat{a}_r \quad \rightarrow \text{same Coulomb law}$$

2)  $\vec{E}$  or  $D$  for an infinite line

$$\oint \vec{D} \cdot d\vec{s} = \int \rho_L \, dL$$

$$\vec{D} = D_\rho \hat{a}_\rho \quad (dL = dz)$$

$$d\vec{s} = \rho \, d\phi \, dz \, \hat{a}_\rho$$



$$-\frac{L}{2} \int_0^{2\pi} \int_0^{\rho} D_\rho \hat{a}_\rho \cdot \rho \, d\phi \, dz \, \hat{a}_\rho = \int_{-L/2}^{L/2} \rho_L \, dz$$

$L \rightarrow \infty$

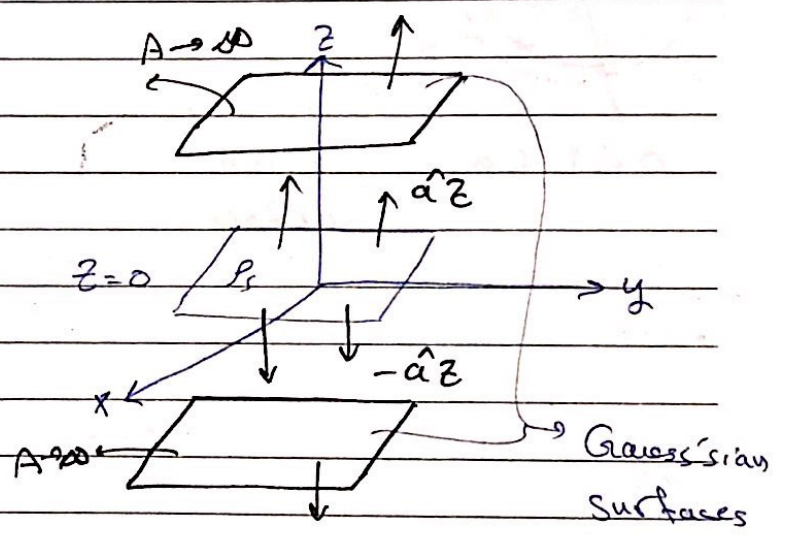
$$2\pi r \cdot k \cdot D_r = \rho_c \cdot t$$

$$D_r = \frac{\rho_c}{2\pi r} \rightarrow \bar{D} = \frac{\rho_c}{2\pi r} \hat{a}_r \rightarrow \bar{E} = \frac{\rho_c}{2\pi \epsilon_0 r} \hat{a}_r$$

3)  $\bar{E}$  or  $\bar{D}$  for an infinite sheet

$$\oint \bar{D} \cdot d\bar{s} = Q_{enc} = \int \rho_s dS$$

$$\bar{D} = \begin{cases} D_z \hat{a}_z, & z > 0 \\ D_z (-\hat{a}_z), & z < 0 \end{cases}$$



$$d\bar{s}_{top} = dx dy \hat{a}_z$$

$$d\bar{s}_{bot} = -dx dy \hat{a}_z$$

$$\int_{S_{top}} \bar{D} \cdot d\bar{s}_{top} + \int_{S_{bot}} \bar{D} \cdot d\bar{s}_{bot} = \int_S \rho_s dS$$

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} D_z dx dy + \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} D_z dx dy = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \rho_s dx dy$$

$$D_z A + D_z A = \rho_s A$$

$$D_z = \frac{\rho_s}{2} \rightarrow \bar{D} = \frac{\rho_s}{2} \hat{a}_n \begin{cases} \hat{a}_z & (z > 0) \\ -\hat{a}_z & (z < 0) \end{cases}$$

$$\bar{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_n \begin{cases} \hat{a}_z \\ -\hat{a}_z \end{cases} \quad * \text{ أيضا أنه كولوم نفس عاوس للبرقنة}$$

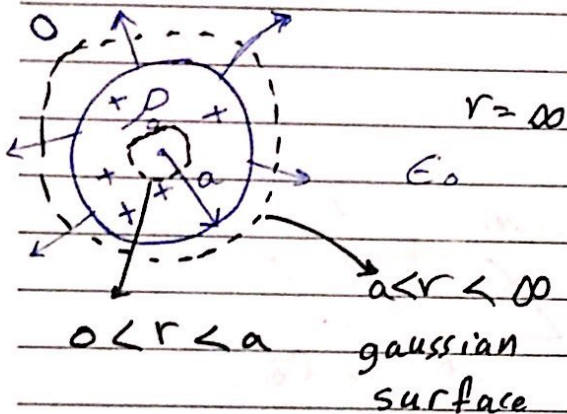
Five Apple



#### 4) $\vec{E}$ or $\vec{D}$ for volume charge dist

Ex: consider a sphere of radius ( $a$ ) has a

$$\rho_v = \begin{cases} \rho_0, & r \leq a \\ 0, & r > a \end{cases} \quad \text{C/m}^3, \text{ Find } \vec{E} \text{ and } \vec{D} \text{ every where}$$



• For  $r < a$ :

$$\oint_{S_0} \vec{D} \cdot \vec{d}s = Q_{enc} = \int \rho_v dV$$

$$\vec{D} = D r \hat{r} \quad \vec{d}s = r^2 \sin \theta d\theta d\phi \hat{r}$$

$$dV = r^2 \sin \theta dr d\theta d\phi$$

$$\int_0^{2\pi} \int_0^{\pi} \int_0^r D r \hat{r} \cdot r^2 \sin \theta d\theta d\phi \hat{r} = \int_0^{2\pi} \int_0^{\pi} \int_0^r \rho_0 r^2 \sin \theta dr d\theta d\phi$$

$$4\pi r^2 D r = \rho_0 \frac{4\pi r^3}{3}$$

$$\vec{D} = \frac{\rho_0 r}{3} \hat{r} \quad \vec{E} = \frac{\rho_0 r}{3\epsilon_0} \hat{r} \quad 0 < r < a$$

• For  $\infty > r > a$

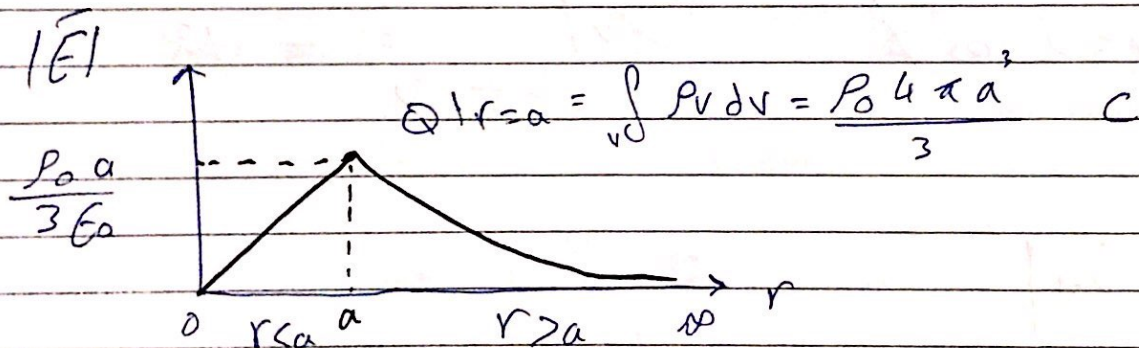
$$4\pi r^2 D r = \int_0^{2\pi} \int_0^{\pi} \int_0^a \rho_0 \sin\theta \, dr \, d\theta \, d\phi$$

$$+ \int \int \int_a^{\infty} 0 \, dr \, d\theta \, d\phi$$

$$4\pi r^2 D r = \rho_0 4\pi \frac{a^3}{3}$$

$$\vec{D} = \frac{\rho_0 a^3}{3r^2} \hat{a}_r \quad \vec{E} = \frac{\rho_0 a^3}{3\epsilon_0 r^2} \hat{a}_r$$

$$a \leq r < \infty$$



$$4\pi r^2 D r = Q = \frac{\rho_0 4\pi a^3}{3} + \int \int \int_a^r \rho_0 \, dv$$

$$\vec{D} = \frac{\rho_0 a^3}{3r^2} \hat{a}_r$$

Ex: Given  $\vec{D} = z\rho \cos^2 \phi \hat{a}_z$  C/m<sup>2</sup>

a) calculate the charge density at  $(1, \frac{\pi}{4}, 3)$

b) the total charge enclosed by the cylinder of radius 1 m with  $-2 \leq z \leq 2$

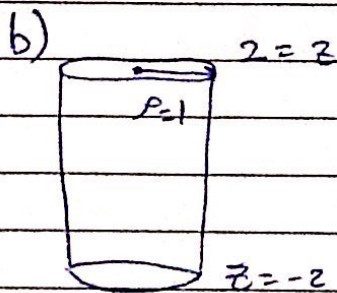
$\rho_s = \vec{D} \cdot \hat{a}_n \rightarrow$  what is the surface

$$\rho_v = \nabla \cdot \vec{D}$$

$$\begin{aligned} \rho_v = \nabla \cdot \vec{D} &= \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho D_\rho) + \frac{1}{\rho} \frac{\partial D_\phi}{\partial \phi} + \frac{\partial D_z}{\partial z} \\ &= \frac{\partial D_z}{\partial z} \end{aligned}$$

$$\rho_v = \rho \cos^2 \phi$$

$$\rho_v \Big|_{(1, \frac{\pi}{4}, 3)} = \frac{1}{2} \text{ C/m}^3$$



$$\begin{aligned} Q &= \int_V \rho_v dV \\ &= \int_{-2}^2 \int_0^{2\pi} \int_0^1 \rho \cos^2 \phi \rho d\rho d\phi dz \end{aligned}$$

$$Q = \frac{1}{3} \int_0^{2\pi} \frac{1}{2} (1 + \cos 2\phi) d\phi \cdot 4$$

$$= \frac{4}{3} \left( \pi + \frac{-\sin 2\phi}{2} \Big|_0^{2\pi} \right) = \frac{4\pi}{3} \text{ C}$$

Method (2) = Gauss

$$Q_{enc} = \oint_S \vec{D} \cdot \vec{ds} = Q = \int \rho_c dV$$

$$\rightarrow \int \rho_c dV$$

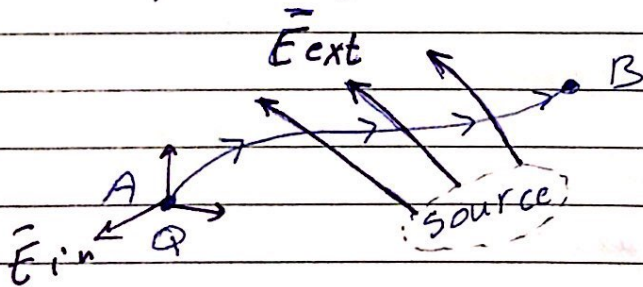
$$Q = \int_{s_{top}} \vec{D} \cdot \vec{ds}_{top} + \int_{s_{bot}} \vec{D} \cdot \vec{ds}_{bot} + \int_{side} \vec{D} \cdot \vec{ds}_{side}$$

$$Q = \int_0^{2\pi} \int_0^1 z \rho \cos^2 \phi \rho d\rho d\phi \Big|_{z=2} - \int_0^{2\pi} \int_0^1 z \rho \cos^2 \phi \rho d\rho d\phi \Big|_{z=-2}$$

$$Q = \frac{2\pi}{3} + \frac{2\pi}{3} = \frac{4\pi}{3} C$$

### \* Electric potential:

Scalar quantity  $\rightarrow$  in (V) volt



work (scalar)  $\rightarrow w = \vec{F} \cdot \vec{l}$  (N.m) or (J) Joule

$$w = Q \vec{E}_{ext} \cdot \vec{l}, \vec{F} = Q\vec{E} \rightarrow w = Q \vec{E} \cdot \vec{l}$$

$$w = -Q \vec{E} \cdot \vec{l} \rightarrow w = -\int Q \vec{E} \cdot d\vec{l} \rightarrow \text{general}$$

$\downarrow$   
for uniform length

$$V_{AB} = \frac{W}{Q} = \int_L \vec{E} \cdot d\vec{L}, \quad \frac{1J}{1C} = 1V$$

..... Coulomb's Gauss's

$$V_{AB} = V_B - V_A$$

• based on  $V_{AB} = - \int \vec{E} \cdot d\vec{L}$

↳ if the voltage is -ve:

- drop in potential (higher pot  $\rightarrow$  lower pot)

- the work is done by the field itself.

↳ if the voltage is +ve

- gain in potential (lower pot  $\rightarrow$  higher pot)

- the work is done by the ext field.

• for a point charge  $q$ :-

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \quad \begin{array}{l} \rightarrow \text{Coulombs} \\ \rightarrow \text{Gauss's} \end{array}$$

$$V = - \int_L \vec{E} \cdot d\vec{L} = - \int_{r_A}^{r_B} \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \cdot dr \hat{a}_r$$

$$= \frac{+Q}{4\pi\epsilon_0} \left( \frac{1}{r_B} - \frac{1}{r_A} \right) V = \frac{Q}{4\pi\epsilon_0 r_B} - \frac{Q}{4\pi\epsilon_0 r_A} = V_B - V_A$$

• if point A is at  $\infty \rightarrow r_A \approx \infty$

$$V_{AB} = V_B - V_A = V_B - 0 = V_B$$

$$= \frac{Q}{4\pi\epsilon_0 r_B} - \frac{Q}{4\pi\epsilon_0 r_A} \rightarrow V_B = \frac{Q}{4\pi\epsilon_0 r_B} \quad \text{if ref is at } \infty$$

$V_{\infty} = 0 \rightarrow \text{ref}$

$$V = \frac{Q}{4\pi\epsilon_0 r} \quad (\text{if ref is at } \infty)$$

• for  $N$ -point charges

$$V = \sum_{k=1}^N \frac{Q_k}{4\pi\epsilon_0 |r - r'_k|} \quad \text{if } V_{\infty} = 0$$

$r' \rightarrow \text{source}$

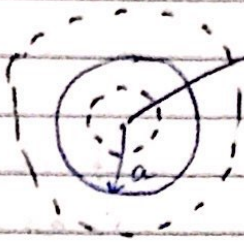
$$V = \int_L \frac{\rho_L dl}{4\pi\epsilon_0 r} \rightarrow \text{Line charge}$$

$$V = \int_s \frac{\rho_s ds}{4\pi\epsilon_0 r} \rightarrow \text{surface charge}$$

$$V = \int_v \frac{\rho_v dv}{4\pi\epsilon_0 r} \rightarrow \text{Volume charge}$$

$$V(\vec{r}) = \int_{v'} \frac{\rho_v(\vec{r}') dv'}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|}$$

from past example



$$\rho = \begin{cases} \rho_0, & r \leq a \\ 0, & r > a \end{cases}$$

$$\vec{E} = \begin{cases} \frac{\rho_0 r}{3\epsilon_0} \hat{a}_r, & 0 < r \leq a \\ \frac{\rho_0 a^3}{3\epsilon_0 r^2} \hat{a}_r, & a \leq r < \infty \end{cases}$$

+ find  $V$  everywhere:

for  $r > a$

$$V = -\int_{\infty}^r \vec{E} \cdot d\vec{l} \rightarrow V = -\int_{\infty}^r \frac{\rho_0 a^3}{3\epsilon_0 r^2} \hat{a}_r \cdot dr \hat{a}_r$$

$$= + \frac{\rho_0 a^3}{3\epsilon_0} \left( \frac{1}{r} - \frac{1}{\infty} \right) = \frac{\rho_0 a^3}{3\epsilon_0 r}, \quad a \leq r < \infty$$

for  $r < a$

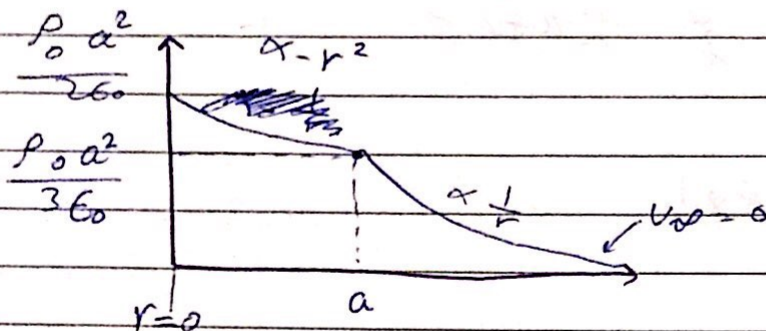
$$V = -\int_{\infty}^r \vec{E} \cdot d\vec{l} \rightarrow -\int_{\infty}^r \vec{E} \cdot d\vec{l}$$

$$= -\int_{\infty}^a \vec{E} \cdot d\vec{l} - \int_a^r \vec{E} \cdot d\vec{l}$$

$$= \frac{\rho_0 a^3}{3\epsilon_0 a} - \int_a^r \frac{\rho_0 r}{3\epsilon_0} \hat{a}_r \cdot dr \hat{a}_r = \frac{\rho_0 a^2}{3\epsilon_0} - \frac{\rho_0 (r^2 - a^2)}{6\epsilon_0} V$$

$$0 < r \leq a$$

$$V(r=0) = \frac{\rho_0 a^2}{3\epsilon_0} + \frac{\rho_0 a^2}{6\epsilon_0} = \frac{\rho_0 r^2}{2\epsilon_0}$$



Ex. A point charge of 5 nC located at  $(-3, 4, 0)$

and line  $y=1, z=1$  carries  $\rho_L = 2 \text{ nC/m}$   $\rightarrow (x, 1, 1)$

- a) ...      b) if  $V = 100 \text{ V}$  at  $B(2, 2, 1)$  find  $V$  at  $C(-2, 5, 3)$   
 c) ...

ref is point B

$V_C$ ?

$$V_{BC} = V_C - V_B \Rightarrow V_C = V_{BC} + 100 \quad (V_{BC} = V_{BCQ} + V_{BCL})$$

$$V_{BCQ} = - \int_L \vec{E} \cdot d\vec{L} = \int_{r_B}^{r_C} \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \cdot d\vec{r} \cdot \hat{a}_r$$

$$= \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_C} - \frac{1}{r_B} \right)$$



$$r_C = |(0, 1, 3)| = \sqrt{11} \quad , \quad r_B = |(4, 1, 3)| = \sqrt{26}$$

$$V_{BC} = - \int_C^B \vec{E} \cdot d\vec{L} = - \int_{r_C}^{r_B} \frac{P_C}{2\pi\epsilon_0 r} \hat{a}_r \cdot d\rho \hat{a}_r$$

$$= - \frac{P_C}{2\pi\epsilon_0} (\ln r_C - \ln r_B)$$

$$= \frac{P_C}{2\pi\epsilon_0} \ln \left( \frac{r_B}{r_C} \right)$$

$$r_B = |(0, 1, 0)| = 1$$

$$r_C = |(0, 4, 2)| = \sqrt{20}$$

$$V_{BC} = -50.175$$

$$V_C = 49.825 \text{ V}$$

• How to find  $\vec{E}$  from  $(V)$  :-

$$V = - \int_L \vec{E} \cdot d\vec{l}$$

Potential  $dV = -\vec{E} \cdot d\vec{l}$

in cartesian.

$$\vec{E} = E_x \hat{a}_x + E_y \hat{a}_y + E_z \hat{a}_z$$

$$d\vec{l} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

$$\vec{E} \cdot d\vec{l} = E_x dx + E_y dy + E_z dz$$

DIFF. partial.

$$dV = \frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz$$

by Equating similar terms :-

$$\frac{\partial V}{\partial x} dx = -E_x dx \quad \rightarrow \quad \boxed{E_x = -\frac{\partial V}{\partial x}}$$

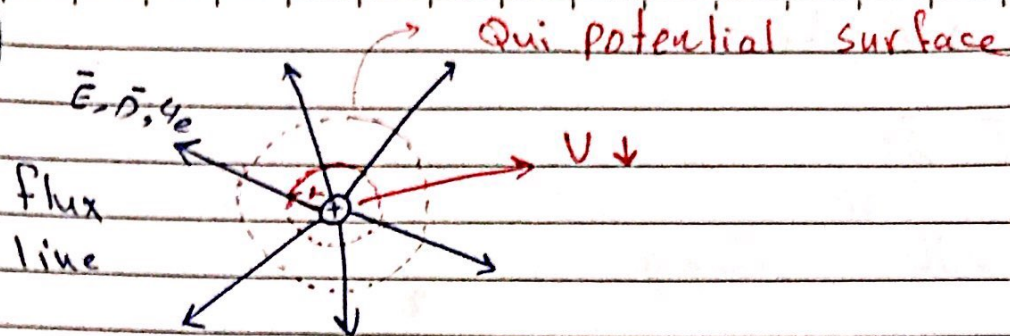
$$\boxed{E_y = -\frac{\partial V}{\partial y}}$$

$$\boxed{E_z = -\frac{\partial V}{\partial z}}$$

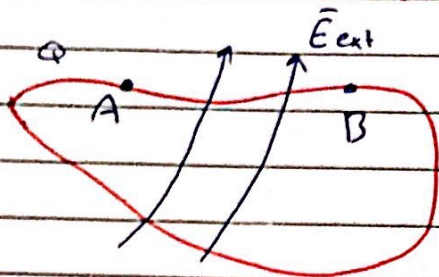
$$\vec{E} = - \left( \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z \right)$$

$$\boxed{\vec{E} = -\nabla V} \equiv \frac{V}{r}$$

→ 3<sup>rd</sup> way to find  $\vec{E}$  field (if  $(V)$  is given or easy to find)



\* potential over a closed path:-



Q:  $A \rightarrow B$  then  $B \rightarrow A$

$$V = - \int_{rA}^{rB} \vec{E} \cdot d\vec{l} + - \int_{rB}^{rA} \vec{E} \cdot d\vec{l} = 0$$

$$V_{AA} = V_A - V_A = \text{zero}$$

$$\oint \vec{E} \cdot d\vec{l} = 0 \quad \text{always}$$

2<sup>nd</sup> maxwell's equation in integral form.

\* by applying stoke's theorem:-

$$\oint \vec{E} \cdot d\vec{l} = \int_S \nabla \times \vec{E} \cdot d\vec{s} = \int_S 0 \cdot d\vec{s}$$

$$\boxed{\nabla \times \vec{E} = 0} \rightarrow \text{2nd maxwell's equation in Differential form}$$

Ex: Given  $V = \frac{10}{r^2} \sin \theta \cos \phi$

a) find  $\vec{D}$  at  $(2, \frac{\pi}{2}, 0)$

b) calculate the work done in moving  $10 \mu\text{C}$  charge from  $A(1, 30^\circ, 120^\circ)$  to  $B(4, 90^\circ, 60^\circ)$ .

$$\vec{E} = -\nabla V \quad , \quad \vec{D} = \epsilon_0 \vec{E}$$

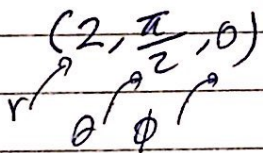
$$\vec{D} = -\epsilon_0 \nabla V$$

$$\vec{E} = - \left( \frac{dV}{dr} \hat{a}_r + \frac{dV}{r d\theta} \hat{a}_\theta + \frac{dV}{r \sin\theta d\phi} \hat{a}_\phi \right)$$

$$\vec{E} = \left( \frac{+20}{r^3} \sin\theta \cos\phi \hat{a}_r - \frac{10}{r^3} \cos\theta \cos\phi \hat{a}_\theta + \frac{10}{r^3} \cos\phi \hat{a}_\phi \right)$$

a)  $\vec{D} = \epsilon_0 \vec{E}$

$$|\vec{D}| = \epsilon_0 \left( \frac{20}{8} \hat{a}_r \right) \text{ C/m}^2$$



$$\vec{D} = 22.1 \hat{a}_r \text{ pC/m}^2$$

b) method (I)

$$W = Q V_{AB} \rightarrow Q (V_B - V_A)$$

$$10 \times 10^{-6} \left( \frac{10}{16} \cdot \frac{1}{2} - \frac{10}{2} \cdot \frac{1}{2} \cdot \frac{-1}{2} \right) = 10 \times 10^{-6} \left( \frac{5}{16} + \frac{10}{4} \right)$$

$$= 10 \times 10^{-6} \left( \frac{45}{16} \right) \xrightarrow{V_{AB}} = 28.125 \text{ mJ}$$

method (II)

$$W = -Q \int_C \vec{E} \cdot d\vec{l}$$

$$W = -10 \times 10^{-6} \int (E_r dr + E_\theta r d\theta + E_\phi r \sin\theta d\phi)$$

$$W = -10 \times 10^{-6} \left[ \int_1^4 E_r dr \right]_{\substack{\theta=30 \\ \phi=120}}$$

$$+ \int_{30^\circ}^{90^\circ} E_\theta r d\theta \Big|_{\substack{r=4 \\ \phi=120}}$$

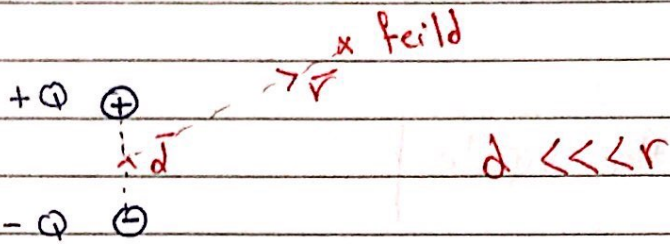
$$+ \int_{120^\circ}^{60^\circ} r \sin\theta E_\phi d\phi \Big|_{\substack{r=4 \\ \theta=90}}$$

$A(1, 30^\circ, 120^\circ)$

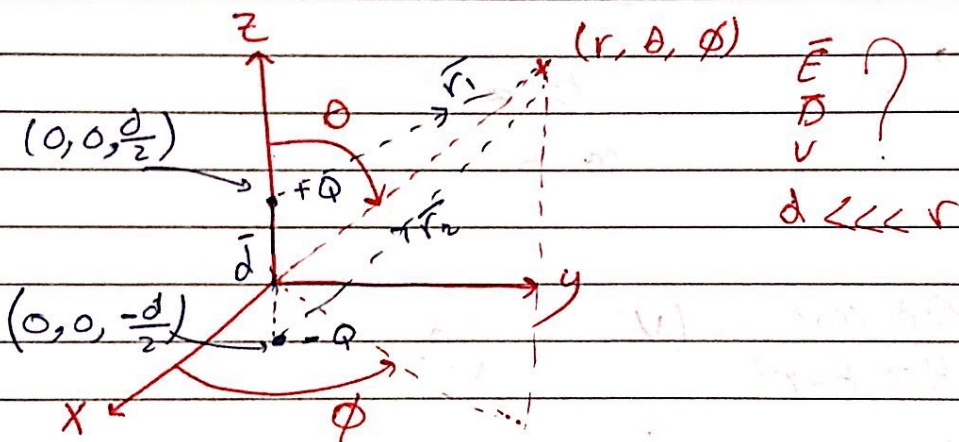
$B(4, 90^\circ, 60^\circ) \nearrow \phi$

$r \searrow (4, 30^\circ, 120^\circ) \xrightarrow{\theta} (4, 90^\circ, 120^\circ)$

\* Electric dipoles :-



Find  $\vec{E}, \vec{D}, V$  ?

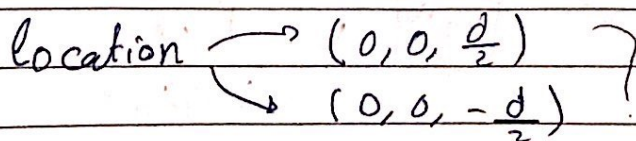


$$V = V_+ + V_- \quad (\text{ref is at } \infty)$$

$$= \frac{Q}{4\pi\epsilon_0 r_1} + \frac{-Q}{4\pi\epsilon_0 r_2} = \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_1} - \frac{1}{r_2} \right)$$

$$\boxed{1} \quad V = \frac{Q (r_2 - r_1)}{4\pi\epsilon_0 r_1 r_2}$$

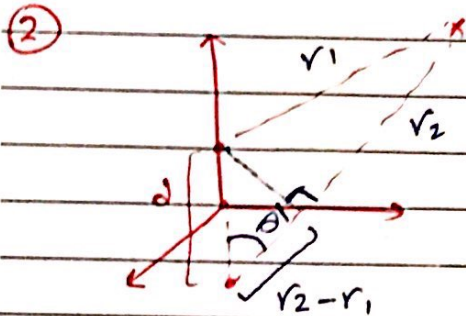
Q?



\* Approximations - (1), (2)

(1)  $r_1 r_2 \approx r^2$

$r =$  | field - center of the dipole |



$r_2 - r_1 = d \cos \theta$

$\theta' \approx \theta$

$\cos \theta = \frac{r_2 - r_1}{d}$

(2)  $V = \frac{Qd \cos \theta}{4\pi \epsilon_0 r^2}$  (V)  $\frac{Qd}{d^2}$

define: dipole moment

$P = Q \bar{d}$  in (C.m)

(3)  $V = \frac{P \cos \theta}{4\pi \epsilon_0 r^2}$  (V)  $\rightarrow P$  center of the dipole

$\theta$  is the angle between ( $\bar{P}$ ) and ( $\bar{r}$ )

(3')  $V = \frac{\bar{P} \cdot \hat{a}_r}{4\pi \epsilon_0 r^2}$   $\rightarrow P \cos \theta$

(3'')  $V = \frac{\bar{P} \cdot \bar{r}}{4\pi \epsilon_0 r^3}$

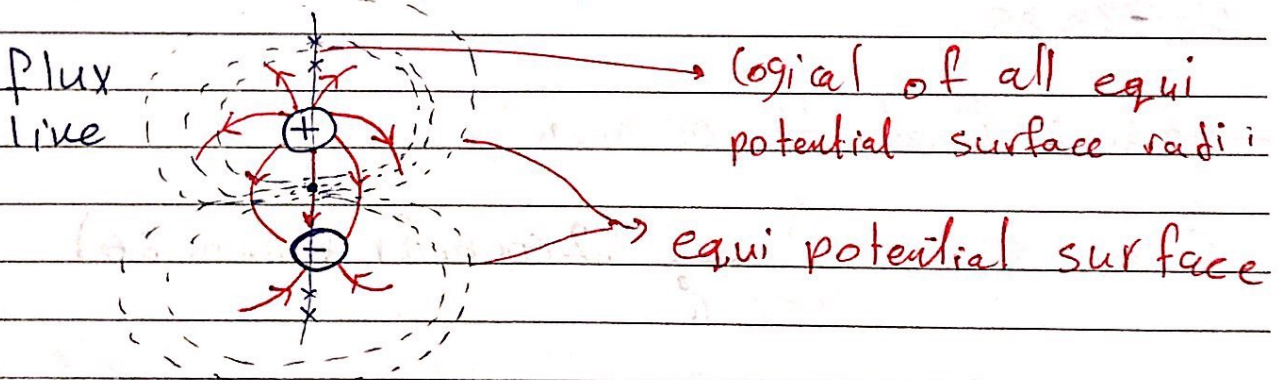
$$\vec{E} = -\nabla V$$

$$= \frac{-P}{4\pi\epsilon_0} \left( \frac{-2 \cos\theta}{r^3} \hat{a}_r - \frac{\sin\theta}{r^3} \hat{a}_\theta \right)$$

$$\vec{E} = \frac{P}{4\pi\epsilon_0 r^3} (2 \cos\theta \hat{a}_r + \sin\theta \hat{a}_\theta) \text{ V/m}$$

\* For N-dipoles

$$V = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^N \frac{\vec{p}_k \cdot (\vec{r} - \vec{r}'_k)}{|\vec{r} - \vec{r}'_k|^3} \text{ (V)}$$





Ex: two dipoles with dipole moments  $-5 \hat{a}_z \text{ nC}\cdot\text{m}$  and  $9 \hat{a}_z \text{ nC}\cdot\text{m}$  are located at  $(0, 0, -2)$  and  $(0, 0, 3)$

find the potential at the origin.

ref is at  $\infty$

$$V = \frac{\vec{p}_1 \cdot \vec{r}_1}{4\pi\epsilon_0 r_1^3} + \frac{\vec{p}_2 \cdot \vec{r}_2}{4\pi\epsilon_0 r_2^3} \quad \left| \quad \begin{array}{l} \vec{r}_1 = 2 \hat{a}_z \rightarrow r_1 = 2 \text{ m} \\ \vec{r}_2 = -3 \hat{a}_z \rightarrow r_2 = 3 \text{ m} \end{array} \right.$$

$$V = \frac{-5 \hat{a}_z \times 10^{-9} \cdot 2 \hat{a}_z}{4\pi \times 10^{-9} \cdot 8} + \frac{9 \hat{a}_z \times 10^{-9} \cdot (-3 \hat{a}_z)}{4\pi \times 10^{-9} \cdot 27}$$

$$V = -20.25 \text{ V}$$

→ find  $\vec{E}$  at the origin

$$\vec{E}_1 = -\nabla V = \frac{p_1}{4\pi\epsilon_0 r_1^3} (2 \cos \theta_1 \hat{a}_r + \sin \theta_1 \hat{a}_\theta)$$

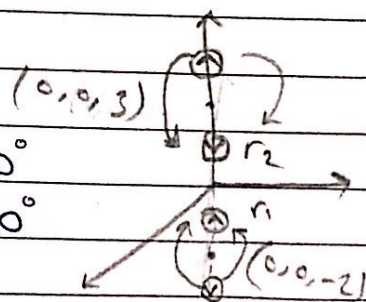
$$\vec{E}_2 = \dots$$

$$p_1 = -5 \times 10^{-9} \text{ C}\cdot\text{m}$$

$$\theta_1 = 180^\circ$$

$$p_2 = 9 \times 10^{-9} \text{ C}\cdot\text{m}$$

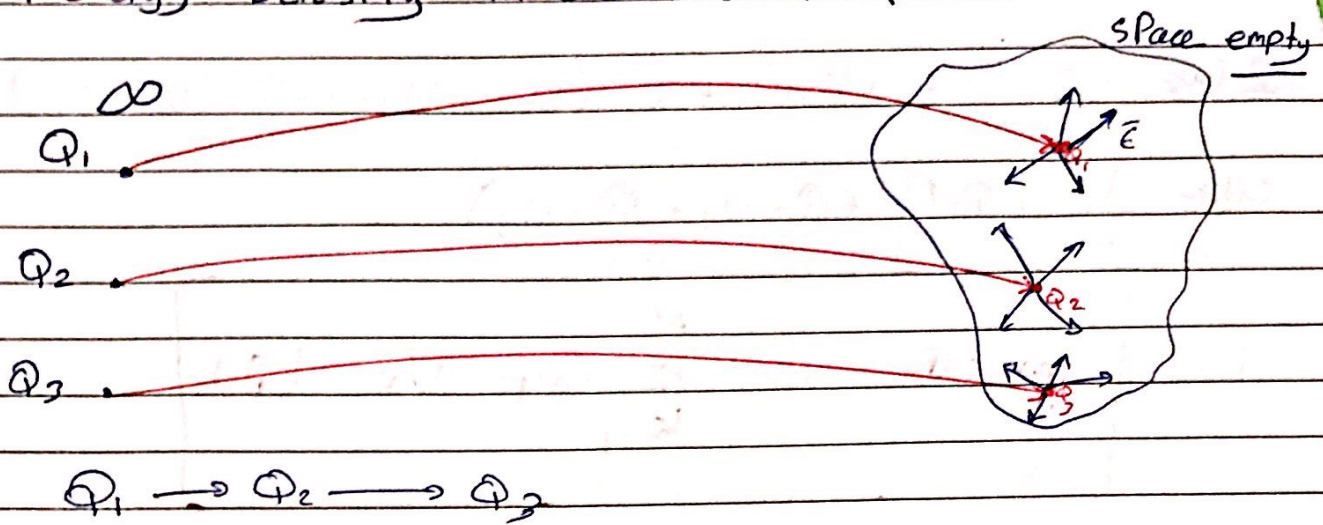
$$\theta_2 = 180^\circ$$



$$\vec{E} = \frac{10^{-9}}{4\pi \times 10^{-9} \cdot 36\pi} \left( \frac{+5}{8} (-2) \hat{a}_r + \frac{9}{27} (-2) \hat{a}_r \right)$$

$$\theta ( ) \hat{a}_r \text{ V/m}$$

\* Energy Density in electrostatic Fields :-



$W_E \equiv$  electrical energy

$$W_E = W_1 + W_2 + W_3$$

$$W_1 = Q_1 V_{\infty} = 0, \quad Q_1, Q_2, Q_3 \neq 0$$

$$V_{\infty} = 0, \quad V_{\text{space empty}} = 0$$

$$W_2 = Q_2 (V_{12}), \quad W_3 = Q_3 (V_{13} + V_{23})$$

$$W_E = 0 + Q_2 V_{12} + Q_3 (V_{13} + V_{23}) \quad \dots \quad \boxed{1}$$

$$Q_3 \rightarrow Q_2 \rightarrow Q_1 :$$

$$\begin{aligned} W_E &= W_1 + W_2 + W_3 \\ &= Q_1 (V_{21} + V_{31}) + Q_2 V_{32} + 0 \quad \dots \quad \boxed{2} \end{aligned}$$

① + ②

$$2W_E = Q_1 (V_{21} + V_{31}) + Q_2 (V_{12} + V_{32}) + Q_3 (V_{13} + V_{23})$$

$$W_E = \frac{1}{2} (Q_1 V_1 + Q_2 V_2 + Q_3 V_3)$$

$$* W_E = \frac{1}{2} \sum_{k=1}^N Q_k V_k \text{ (J)}$$

For  $N$ -point charges :-

$$W_E = \frac{1}{2} \int \rho_L V dL \longrightarrow \text{for line charge}$$

$$W_E = \frac{1}{2} \int \rho_S V dS \longrightarrow \text{for surface charge}$$

$$\odot W_E = \frac{1}{2} \int_{\text{Volume}} \rho_V V dV' \longrightarrow \text{for volume charge}$$

Volume  $\nearrow$  Potential

\* How to find  $W_E$  from  $\vec{E}$  ?

$$\vec{D} = \epsilon_0 \vec{E}$$

$$\rho_V = \nabla \cdot \vec{D}$$

$$\odot \quad W_E = \frac{1}{2} \int_V \rho \cdot \bar{D} \cdot \bar{V} \, dV = \frac{1}{2} \int_V \rho \cdot \bar{D} \cdot \bar{V} \, dV$$

• Scalar Identity :- (given) (general)

$$\nabla \cdot (V \bar{A}) = \bar{A} \cdot \nabla V + \underbrace{V (\nabla \cdot \bar{A})}_{\bar{D} \equiv \bar{A}}$$

$$W_E = \frac{1}{2} \left[ \int_V \rho \cdot (V \bar{D}) \, dV - \int_V \bar{D} \cdot \nabla V \, dV \right]$$

(1) (2)

Apply divergence theorem on integral (1) :

$$W_E = \frac{1}{2} \left[ \oint_S V \bar{D} \cdot \bar{dS} - \int_V \bar{D} \cdot \nabla V \, dV \right]$$

$$\left. \begin{array}{l} V \propto \frac{1}{r} \\ \bar{D} \propto \frac{1}{r^2} \\ dS \propto r^2 \end{array} \right\} \begin{array}{l} \downarrow \frac{1}{r} \\ \text{as } (r \rightarrow \infty) \rightarrow \oint_S V \bar{D} \cdot \bar{dS} \approx 0 \end{array}$$

$\downarrow -\bar{E} = +\nabla V$

$$W_E = \frac{1}{2} \int_V \bar{D} \cdot \bar{E} \, dV$$

$\downarrow \bar{D} = \epsilon_0 \bar{E}$

$$W_E = \frac{1}{2} \int_V \epsilon_0 E^2 \, dV \quad \text{or} \quad W_E = \frac{1}{2} \int_V \frac{\bar{D}^2}{\epsilon_0} \, dV$$

Energy density :- ( $w_E$ )

$$w_E = \frac{W_E}{\text{Volume}} \left( \frac{J}{m^3} \right)$$

$$w_E = \frac{1}{2} \vec{E} \cdot \vec{D} = \frac{1}{2} \epsilon_0 \vec{E}^2 = \frac{1}{2} \frac{D^2}{\epsilon_0}$$

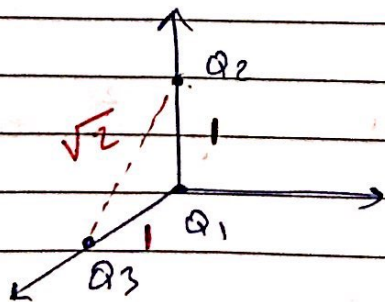
$$W_E = \int w_E dV$$

Ex:- The point charges  $-1 \mu c$ ,  $4 \mu c$  and  $3 \mu c$  are located at  $(0,0,0)$ ,  $(0,0,1)$  and  $(1,0,0)$  find the energy in the system.

$$W_E = \frac{1}{2} \sum_{k=1}^3 Q_k V_k$$

$$= \frac{1}{2} (Q_1 V_1 + Q_2 V_2 + Q_3 V_3)$$

$$= \frac{1}{2} [Q_1 (V_{21} + V_{31}) + Q_2 (V_{12} + V_{32}) + Q_3 (V_{13} + V_{23})]$$



$$W_C = \frac{1}{2} \left[ Q_1 \left( \frac{Q_2}{4\pi\epsilon_0(l)} + \frac{Q_3}{4\pi\epsilon_0(l)} \right) \right. \\ \left. + Q_2 \left( \frac{Q_1}{4\pi\epsilon_0(l)} + \frac{Q_3}{4\pi\epsilon_0\sqrt{2}} \right) \right. \\ \left. + Q_3 \left( \frac{Q_1}{4\pi\epsilon_0(l)} + \frac{Q_2}{4\pi\epsilon_0\sqrt{2}} \right) \right]$$

$$W_C = \frac{1}{8\epsilon_0\pi} \left[ 2Q_1Q_2 + 2Q_1Q_3 + \frac{2Q_2Q_3}{\sqrt{2}} \right] \\ = 13.37 \text{ nJ}$$

"END OF CHAPTER (4)"

# CH 5 :- Electrostatic in materials :-

classification of materials based on its elec. properties.

→ conductors (Metals)  $\sigma \gg \gg 1$   
(Cu, Al, lead, Au, Ag, brass, ...)

→ Semi-conductors  $\sigma > 1$   
Si, Ge, GaAs, InP, ...

→ Dielectrics (insulators)  $0 < \sigma \ll 1$   
 $\sigma = 0 \rightarrow$  free space

$\sigma =$  conductivity (S/m) or  $(\Omega \cdot m)^{-1}$

$\rho =$  Resistivity  $(\Omega \cdot m)$ ,  $\rho = \frac{1}{\sigma}$

$\sigma$  depends mainly on

→ Temperature (°K)

→ Frequency (Hz)  $\rightarrow$  CH. 10

i.e

lead

at 20°C  $\rightarrow$  293 K

$\sigma \approx 10^6$  S/m

at 4°K

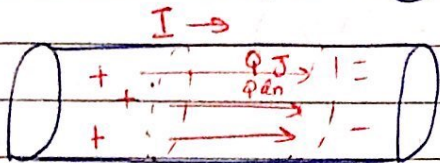
$\sigma \approx 10^{20}$  S/m

$\rightarrow$  super, perfect, good

\* Types of currents :-

- 1) conduction current (DC or AC)
- 2) convection current (DC)
- 3) Displacement current (AC)

$I = \frac{\Delta Q}{\Delta t}$  uniform sections  
 → C/s or (A)



$I = \frac{Q_2 - Q_1}{t_2 - t_1}$

$I = \frac{dq}{dt}$  in general

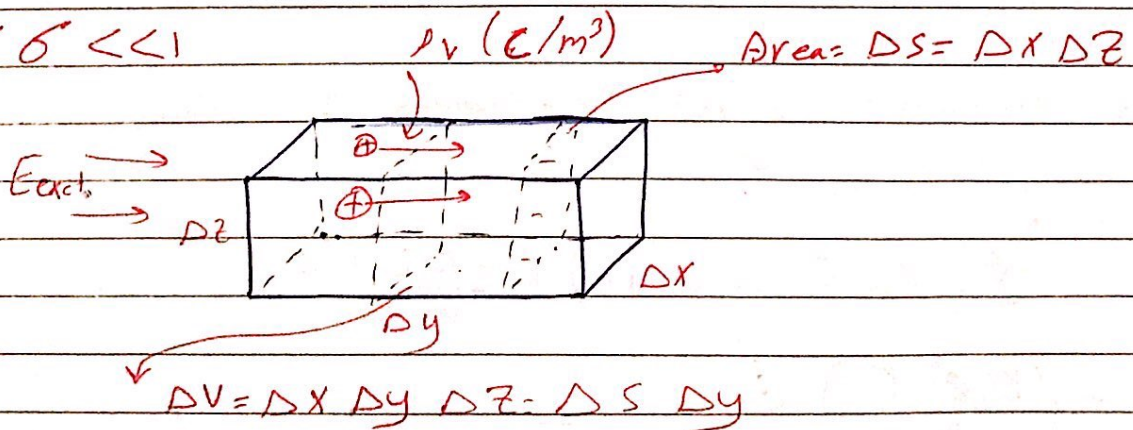
$I = \int \vec{J} \cdot \vec{ds}$

$\vec{J}$  = current density

$\vec{J} = \frac{I}{S}$

\* Portion of dielectric material :-

$0 < \sigma < \infty$



$I = \frac{\Delta Q}{\Delta t} = \frac{\rho_v \Delta V}{\Delta t} \rightarrow I = \frac{\rho_v \Delta S \Delta y}{\Delta t} \rightarrow \frac{\Delta y}{\Delta t} = u_y$



$$I = \rho v \Delta S u_y, \quad \bar{J} = \frac{I}{\Delta S} = \rho v u_y$$

$$\bar{J} = \rho \bar{u}$$

$$\bar{u} = u_y \hat{a}_y$$

$$\frac{C}{m^2} \frac{m}{s} = \frac{A}{m^2}$$

convection current density  $\left(\frac{A}{m^2}\right)$

$\bar{u} = \bar{v}_d \equiv$  drift velocity (m/s)

\* The force on one electron :-

$$Q = -e \rightarrow \bar{F} = Q \bar{E} = -e \bar{E} = m \bar{a} = \frac{m \bar{u}}{\tau}$$

$$\bar{v}_d = \bar{u} = \left(\frac{-e \tau}{m}\right) \bar{E} = \mu \bar{E}$$

$\tau =$  time between collisions (s) (depend on temperature)

$\mu \equiv$  mobility  $\left(\frac{C.s}{kg}\right)$

$$\bar{u} = \mu \bar{E}$$

+ For  $\rho v = -ne$ ,  $n \equiv$  # of charges for volume  $(1m^3)$

↓

$$\bar{J} = \rho v \bar{u} = (-ne) \left(\frac{-e \tau}{m}\right) \bar{E}$$

$$= \left(\frac{ne^2 \tau}{m}\right) \bar{E}$$

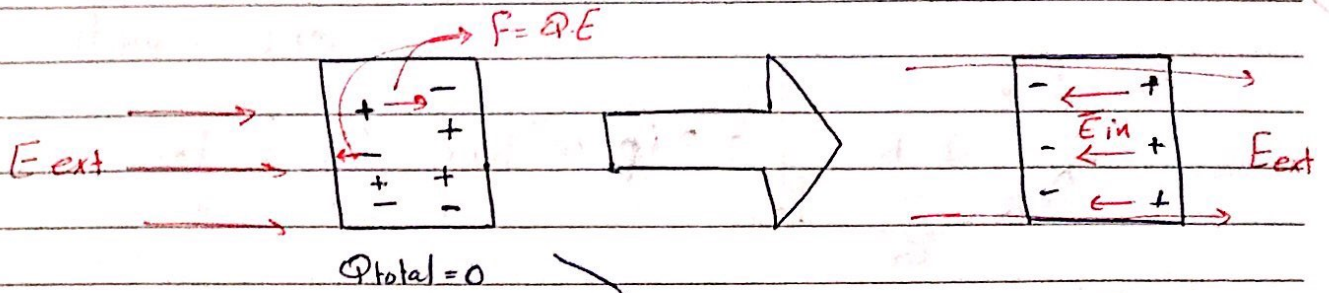
$$\bar{J} = \sigma \bar{E} \rightarrow \text{ohm's law in point form}$$

$$\frac{\sigma}{\mu} = \rho v$$

↳ conduction

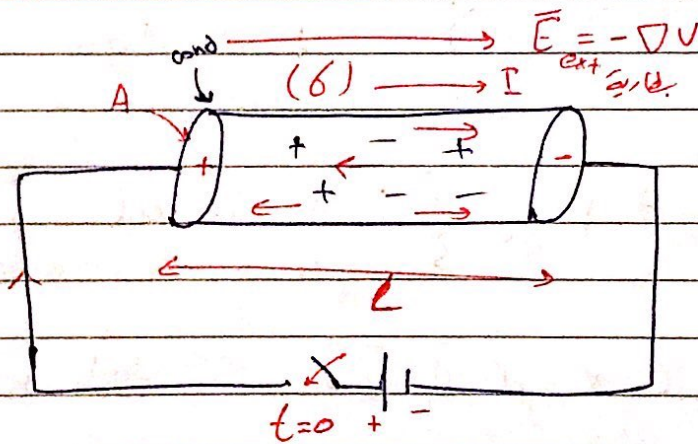
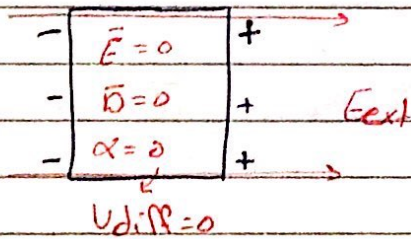
current density  $\frac{1}{\Omega \cdot m} \frac{V}{m} = \left(\frac{A}{m^2}\right)$

\* conductors :-



$\Phi_{total} = 0$

$10^{-19} \text{ s}$



$$R = \frac{V}{I} = \frac{-\int \vec{E} \cdot d\vec{l}}{\int \sigma \vec{E} \cdot d\vec{s}}$$

if uniform section  $l = \frac{l}{\sigma}, A$

$$R = \frac{E l}{\sigma E A} = \frac{l}{\sigma A} = \frac{\rho l}{A}$$

$$\text{Power} = \frac{\text{work}}{\text{time}} \Rightarrow P = \frac{W}{t} \text{ in } \left(\frac{J}{s}\right) \text{ or (W) watt}$$

$$\left. \begin{aligned} P &= I V \\ \frac{V^2}{R} &= I^2 R \\ Q V^2 &= \frac{I^2}{G} \end{aligned} \right\} \rightarrow \text{if uniform (Joules law)}$$

$$P = \frac{-F \cdot l}{t} = \frac{Q \bar{E}_{ext} \cdot l}{t}, \quad Q = \int_V \rho_v dv$$

$$P = \int_V \frac{\rho_v \bar{E} \cdot \bar{l}}{t} dv \rightarrow P = \int_V \rho_v \bar{E} \cdot \bar{l} dv$$

$$\boxed{P = \int_V \bar{E} \cdot \bar{J} dv} \rightarrow \text{Joules law}$$

$$\text{if uniform} \rightarrow P = \int_V \bar{E} \cdot \bar{J} ds dl$$

$$P = \int_V \bar{E} \cdot d\bar{l} \times \int_S \bar{J} \cdot d\bar{s} \rightarrow \text{جهد قوايين Joules}$$

$$P = \left\{ \begin{aligned} &= \int_V \bar{E} \cdot \bar{J} dv \\ &= \int_V \sigma \bar{E}^2 \cdot dv \\ &= \int_V \frac{\bar{J}^2}{\sigma} dv \end{aligned} \right.$$

$$\text{Power density (wp) in (W/m}^3\text{), } w_p = \left\{ \begin{aligned} &= \bar{E} \cdot \bar{J} \\ &= \sigma \bar{E}^2 \\ &= \frac{\bar{J}^2}{\sigma} \end{aligned} \right.$$

$$P = \int_V w_p dv$$

$$I = \oint_S \bar{J} \cdot \bar{J}_s = \int_V \nabla \cdot \bar{J} dv$$

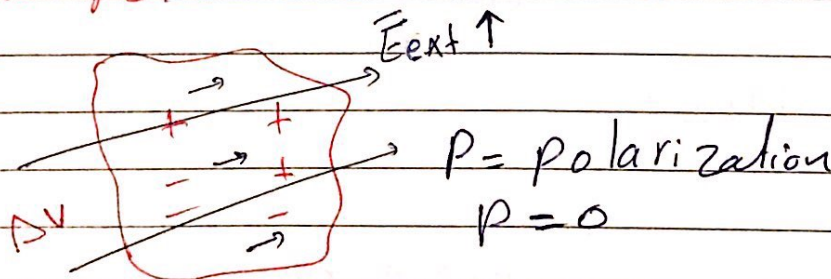
\* polarization in dielectrics:-

↳ Types of dielectrics :-

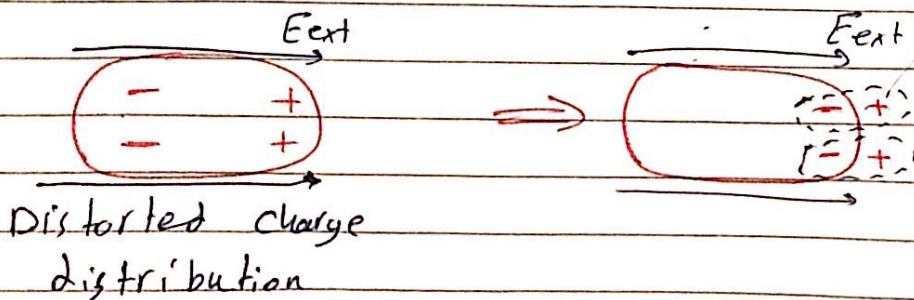
- ↳ non-polar  
O<sub>2</sub>, H<sub>2</sub>, N<sub>2</sub> + Rare gases  
(Kr, Ne, Xe)
- ↳ polar  
(permenant dipoles)  
Alloys H<sub>2</sub>O, NH<sub>3</sub>, HCl, ---



\* Non-polar

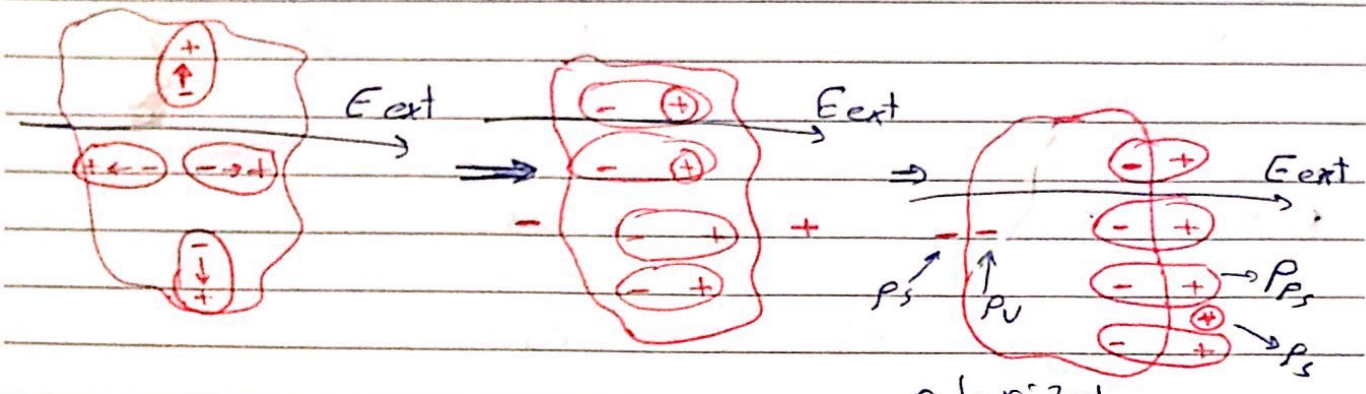


$E_{ext} \uparrow, f \uparrow \rightarrow \text{pressure} = \frac{F}{s} \quad N/m^2$



سختان غير متوازنة الحركة  
(حركة الحركة تلقائي)  
التي على السطح

\* for polar Dielectrics :-



$P_s$  = Free surface charge dist ( $C/m^2$ ) Polarized Dielectric

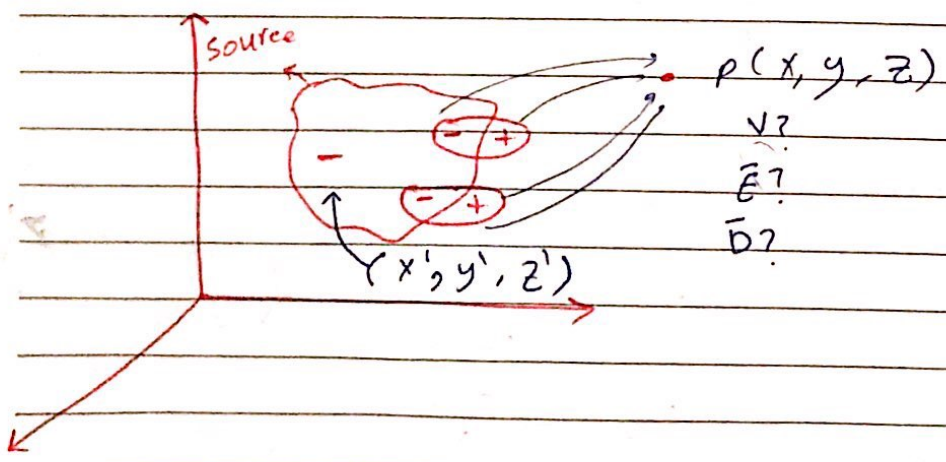
$P_s$  = Polarized (bound) Surface charge dist ( $C/m^2$ )

$P_v$  = Free Volume charge dist ( $C/m^3$ )

$P_v$  = polarized " " " ( $C/m^3$ )

$$\bar{P} = \lim_{\Delta V \rightarrow 0} \sum_{k=1}^N \frac{P_k}{\Delta V} = \frac{C \cdot m}{m^3} = \frac{C}{m^2}$$

\* for Polarized Dielectric :-



→ start  $V = \frac{\bar{P} \cdot \hat{a}_r}{4\pi\epsilon_0 r^2}$  \*  $r = \text{field-source}$ ,  $r' = \text{source-field}$

$$\frac{\hat{a}_r}{r^2} = \frac{\bar{r}}{r^3} = -\nabla\left(\frac{1}{r}\right) \hat{a}_r = -\left(-\frac{1}{r^2}\right) \hat{a}_r = \nabla\left(\frac{1}{r}\right)$$

derivation w.r.t  $(x', y', z')$

$$V = \frac{\bar{P} \cdot \nabla\left(\frac{1}{r}\right)}{4\pi\epsilon_0}$$

$$\int dV = \int \frac{\bar{P} \cdot \nabla\left(\frac{1}{r}\right)}{4\pi\epsilon_0} dV \rightarrow V = \int_{V'} \frac{\bar{P} \cdot \nabla\left(\frac{1}{r}\right)}{4\pi\epsilon_0} dV'$$

identity:  $\nabla \cdot (V\bar{A}) = \bar{A} \cdot \nabla V + V(\nabla \cdot \bar{A})$   
 (given)  $V = \frac{1}{R}$ ,  $\bar{A} = \bar{P}$ ,  $\nabla = \nabla'$

$$V = \frac{1}{4\pi\epsilon_0} \left[ \int_{V'} \frac{\nabla' \cdot \bar{P}}{R} dV' - \int_{V'} \frac{1}{R} \nabla' \cdot \bar{P} dV' \right]$$

\* by divergence theorem on integral (1)

$$V = \oint_{S'} \frac{\bar{P} \cdot d\bar{s}}{4\pi\epsilon_0 R} - \int_{V'} \frac{\nabla' \cdot \bar{P}}{4\pi\epsilon_0 R} dV'$$

$\downarrow \oplus$                        $\downarrow \ominus$                        $\oplus, \ominus$  charged dipole

\* from CH4  $V = \int_{S'} \frac{\rho_s ds'}{4\pi\epsilon_0 r}$   $\rightarrow \rho_s$ ,  $V = \int_{V'} \frac{\rho_v dV'}{4\pi\epsilon_0 r}$   $\rightarrow \rho_v$

$$\rho_s = \bar{E} \cdot \hat{a}_n \Rightarrow \rho_s = \bar{D} \cdot \hat{a}_n$$

$$\rho_v = -\nabla \cdot \bar{P} \Rightarrow \rho_v = \nabla \cdot \bar{P}$$

\*  $\vec{E} = -\nabla V \rightarrow (V \neq \text{number})$

or  $\vec{E} = \int_S \frac{\rho_s ds \hat{a}_r}{4\pi\epsilon_0 r^2} + \int_V \frac{\rho_v dv \hat{a}_r}{4\pi\epsilon_0 r^2} + \int_S \frac{\rho_s ds \hat{a}_r}{4\pi\epsilon_0 r^2} + \int_V \frac{\rho_v dv \hat{a}_r}{4\pi\epsilon_0 r^2}$   
*(V = number)*

\*  $\vec{D} = \epsilon_0 \vec{E}$  (without  $\epsilon_0$  term, same as  $\vec{E}$ )

\* For some dielectrics:  $\rightarrow$  linear  
 $\rightarrow$  isotropic

$\vec{P} = \chi_e \epsilon_0 \vec{E}$

$\hookrightarrow$  electrical susceptibility (constant)

free space  $\rightarrow \epsilon_r = 1$

air  $\rightarrow \epsilon_r = 1.00006 \approx 1$

conductor  $\rightarrow \epsilon_r = 0.9999 \approx 1$

$\rightarrow \chi_e = \text{zero}$

$P_v \text{ total} = P_v + P_v \rightarrow$  dipole charge  
 $\hookrightarrow$  charge free inside

$P_v = P_v \text{ total} - P_p v = \nabla \cdot \vec{D}$

$P_v = \nabla \cdot \vec{D} = \nabla \cdot (\epsilon_0 \vec{E} + \vec{P})$

$\nabla \cdot \vec{D} = \nabla \cdot (\epsilon_0 \vec{E} + \vec{P})$

$\vec{D} = \epsilon_0 \vec{E} + \chi_e \epsilon_0 \vec{E}$

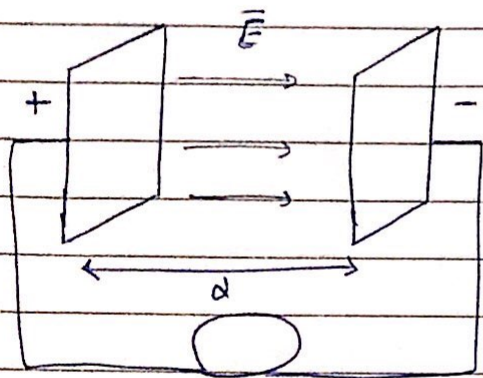
$= (1 + \chi_e) \epsilon_0 \vec{E}$

$\vec{D} = \epsilon_r \epsilon_0 \vec{E}$  ,  $\epsilon_r =$  relative permittivity (Dimensionless)

$\vec{D} = \epsilon \vec{E}$   $\hookrightarrow$  dielectric constant ( $D_k$ )

$\vec{D} |_{\text{dielectric}} \gg \vec{D} |_{\text{air or cond}}$

\*  $\epsilon_r = 1 + \chi_e \rightarrow \epsilon_r = \frac{\epsilon}{\epsilon_0}$  (by exp)



parallel plates capacitor  
+RLC meter  
+material sheet

fix  $d = 1 \text{ cm}$

$$C_0 = \frac{\epsilon_0 A}{d}$$

$$C_{\text{total (material)}} = \frac{\epsilon_0 \epsilon_r A}{d}$$

$$\epsilon_r = \frac{C}{C_0}$$

$$E = \epsilon_0 \epsilon_r$$

$\rightarrow \frac{F/m}{F/m} \rightarrow \text{unitless}$

total charge  $\rightarrow Q = \int P_s ds$   
 $\rightarrow Q = \int P_v dv$

\* total bound charge ( $Q_b$ )

$$Q_{b+} = \int P_s ds$$

$$Q_{b-} = \int P_v dv$$

$$Q_{b+} + Q_{b-} = Q_{\text{total}} = 0$$

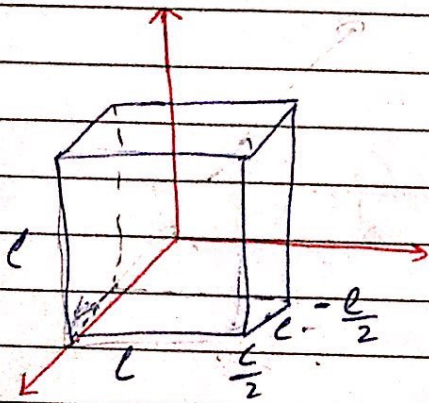
(electrically neutralized)



Ex a dielectric cube of length  $(l)$  centered at

the origin has  $\rho = a\vec{r}$  where  $\vec{r} = x\hat{a}_x + y\hat{a}_y + z\hat{a}_z$

and  $(a)$  is constant Find all bound charge densities and the total charge:-



$$P_s |_{\text{front}} = \vec{P} \cdot \hat{a}_n \Big|_{x = \frac{l}{2}} = a x \Big|_{x = \frac{l}{2}}$$

$$P_s |_{\text{front}} = \frac{al}{2} \text{ C/m}^2$$

$$P_s |_{\text{back}} = -a x \Big|_{x = -\frac{l}{2}} = \frac{al}{2} \text{ C/m}^2$$

$$x = -\frac{l}{2}$$

$$\hat{a}_n = -\hat{a}_x$$

$$P_s |_{\text{right}} \quad \text{All } P_s = \frac{al}{2} \text{ C/m}^2$$

$$P_v = -\nabla \cdot \vec{P} = -a(1+1+1) = -3a \text{ C/m}^3$$

$$Q_{b \text{ total}} = Q_{b+} + Q_{b-}$$

$$Q_{b+} = \int_S \rho_{ps} ds = \epsilon \int_S \rho_{ps} | ds$$

front

$$= \epsilon \frac{al}{2} \cdot l \cdot l = 3al^3 \epsilon$$

$$Q_{b-} = \int_V \rho_{pv} dv = -3al^3 \epsilon$$

$$Q_{b \text{ total}} = 0$$

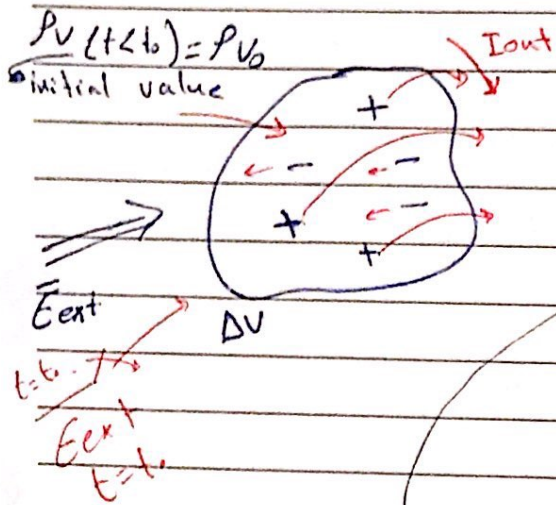
Dielectric Break down:  
depends mainly on:-

- 1) Nature of the material
- 2) temperature  $\downarrow$   $\epsilon \uparrow$
- 3) Humidity  $\uparrow$   $\epsilon \uparrow$
- 4) Applied E-field
- 5) time of the applied field.

Dielectric strength

the max value of  $\vec{E}_{ext}$  the

# \* continuity equation and relaxation time ( $-Tr$ )



$$KCL: I_{out} = I_{in}$$

$$\oint_S \vec{J} \cdot d\vec{s} = - \frac{dq}{dt}$$

$$q = \int_V \rho_V dv$$

$$\frac{dq}{dt} = \int_V \frac{d\rho_V}{dt} dv$$

$$\int_V \nabla \cdot \vec{J} dv = \int_V - \frac{d\rho_V}{dt} dv$$

$$\boxed{\nabla \cdot \vec{J} = - \frac{d\rho_V}{dt}} \rightarrow \text{in diff form}$$

$$\boxed{\int_V \nabla \cdot \vec{J} dv = \int_V - \frac{d\rho_V}{dt} dv} \rightarrow \text{in integral form}$$

Quality from CKT

$$P_V = P_{V_0} e^{-t/Tr}$$

$$\nabla \cdot \vec{J} = - \frac{d\rho}{dt} \quad *, \quad \nabla \cdot \vec{D} = \rho_V, \quad \vec{D} = \epsilon \vec{E}, \quad \vec{J} = \sigma \vec{E}$$

if  $\epsilon$  is homogeneous

$$\sigma \nabla \cdot \vec{E} = \frac{\sigma \rho_v}{\epsilon} \rightarrow \nabla \cdot \vec{J} = \frac{\sigma \rho_v}{\epsilon_0}$$

$$\frac{\sigma \rho_v}{\epsilon} = -\frac{\partial \rho_v}{\partial t} \rightarrow \int_{\rho_{v0}}^{\rho_v} \frac{d\rho_v}{\rho_v} = \int_{t_0}^t -\frac{\sigma}{\epsilon} dt$$

$$\ln \rho_v \Big|_{\rho_{v0}}^{\rho_v} = -\frac{\sigma}{\epsilon} (t - t_0)$$

$$\ln \left( \frac{\rho_v}{\rho_{v0}} \right) = -\frac{\sigma}{\epsilon} (t - t_0)$$

$$\frac{\rho_v}{\rho_{v0}} = e^{-\frac{\sigma}{\epsilon} (t - t_0)}$$

$$\rho_v = \rho_{v0} e^{-\frac{\sigma}{\epsilon} (t - t_0)}$$

if  $t_0 = 0$  and let  $\frac{\epsilon}{\sigma} = \tau$

$\tau$  = relaxation time in (s)

$$\rho_v = \rho_{v0} e^{-t/\tau}$$

$$V = V_0 e^{-t/\tau}$$

$$I = I_0 e^{-t/\tau}$$

$$\uparrow \tau = e^{-1} \text{ or } 36.8$$

$$t = \tau$$
$$V = V_0 e^{-1}$$

of charge are left inside the material

$$0.368$$

↳ 63.2% are on the surface

- For copper,  $\epsilon_r = 1$ ,  $\sigma = 5.8 \times 10^7 \text{ S/m}$

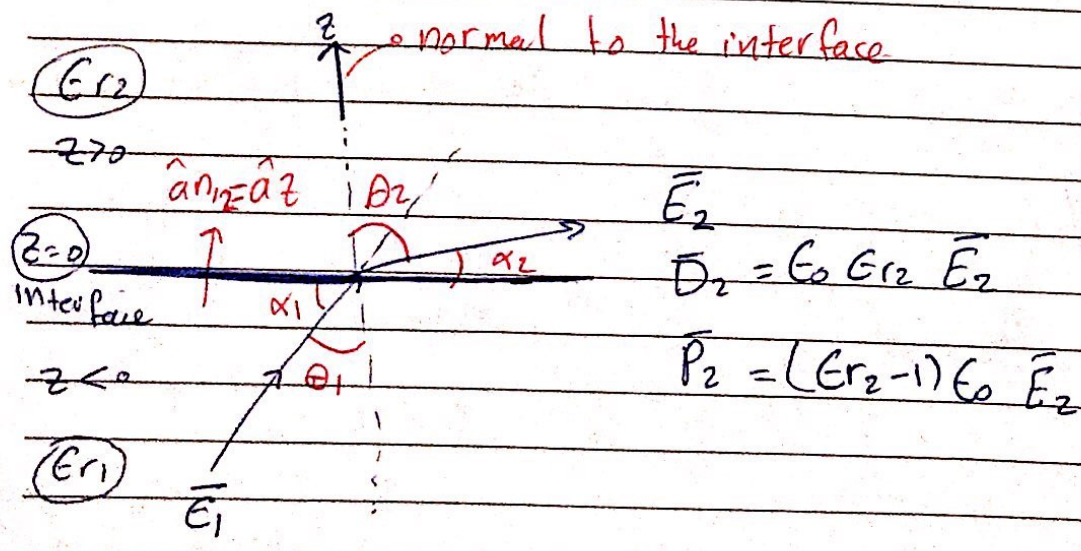
$$T_r = \frac{\epsilon}{\sigma} = \frac{\epsilon_0 \epsilon_r}{\sigma} = \frac{10^{-9}}{36\pi \times 5.8 \times 10^7} = 1.53 \times 10^{-19} \text{ s}$$

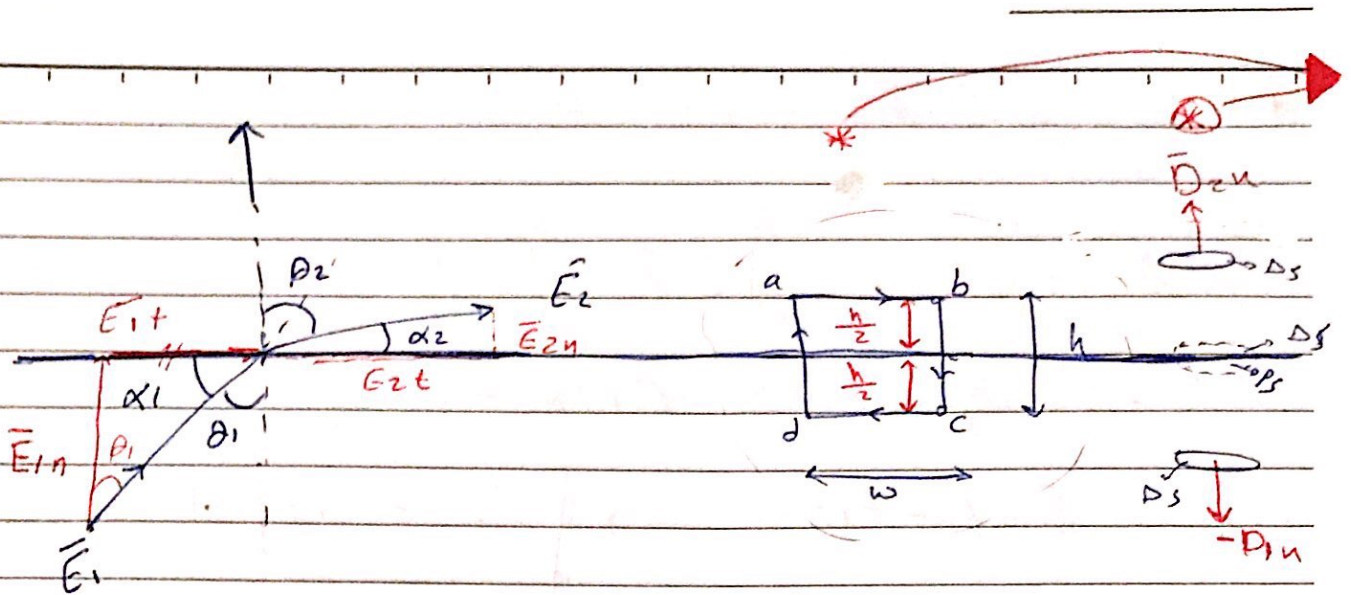
- for fused quartz,  $\epsilon_r = 5$ ,  $\sigma \approx 10^{-17} \text{ S/m}$

$$T_r = \frac{\epsilon}{\sigma} = \frac{10^{-9} \times 5}{\frac{36\pi}{10^{-17}}} = 51.2 \text{ days}$$

\* Boundary conditions -

A) Dielectric-to-Dielectric interface -





$$\vec{E}_1 = \vec{E}_{1n} + \vec{E}_{1t} \quad , \quad \boxed{\hat{a}_n = \hat{a}_z}$$

Gaussian surface

$$\vec{E}_{1n} = (\vec{E}_1 \cdot \hat{a}_n) \hat{a}_n \quad , \quad \vec{E}_{1t} = \vec{E}_1 - \vec{E}_{1n}$$

$$\theta_1 = \sin^{-1} \frac{E_{1t}}{E_1} = \cos^{-1} \frac{E_{1n}}{E_1} = \tan^{-1} \frac{E_{1t}}{E_{1n}}$$

$$\alpha_1 = 90^\circ - \theta_1$$

to find  $\vec{E}_2 \rightarrow \vec{E}_2 = E_{2n} + E_{2t}$

use Maxwell's

$$\textcircled{1} \oint_s \vec{D} \cdot d\vec{s} = Q_{\text{enc}} = \int_s \rho_s ds$$

$$\textcircled{2} \oint \vec{E} \cdot d\vec{l} = 0$$

Apply on the interface  $z=0$

\* Apply  $\oint \vec{E} \cdot d\vec{L} = 0$  at  $z=0$

$$\int_a^b \vec{E} \cdot d\vec{L} + \int_b^c \vec{E} \cdot d\vec{L} + \int_c^d \vec{E} \cdot d\vec{L} + \int_d^a \vec{E} \cdot d\vec{L} = 0$$

$$E_{zt} W - E_{zn} \frac{h}{2} - E_{in} \frac{h}{2} - E_{it} W + E_{in} \frac{h}{2} + E_{zn} \frac{h}{2} = 0$$

$$E_{zt} - E_{it} = 0 \rightarrow \boxed{E_{zt} = E_{it}} \text{ always}$$

\* Apply  $\oint \vec{D} \cdot d\vec{s} = \int \rho_s ds$

$$\int_{\text{stop}} \vec{D} \cdot d\vec{s}_{\text{top}} + \int_{\text{shot}} \vec{D} \cdot d\vec{s}_{\text{bot}} = \int \rho_s ds$$

$$D_{zn} \Delta s - D_{in} \Delta s = \rho_s \Delta s$$

$$\boxed{D_{zn} - D_{in} = \rho_s} \text{ Not always}$$

$$|\vec{D}_{in}| = \epsilon_0 \epsilon_r |\vec{E}_{in}|$$

$$D_{zn} = \epsilon_0 \epsilon_r E_{zn}$$

$$E_{zn} = \left( \frac{D_{zn}}{\epsilon_0 \epsilon_r} \right) \hat{a}_n$$

$$\vec{D}_2 = \epsilon_0 \epsilon_r \vec{E}_2$$

$$\vec{P}_2 = (\epsilon_r - 1) \epsilon_0 \vec{E}_2$$

$$\theta_2 = \sin^{-1} \frac{E_{zt}}{E_z}$$

$$\cos^{-1} \frac{E_{zn}}{E_z} = \tan^{-1} \frac{E_{zt}}{E_{zn}}$$

$$\boxed{\theta_2 = 90^\circ - \theta_2} \text{ } E_{zn}$$

if  $\rho_s = 0$   
 $\vec{D}_{zn} = \vec{D}_{in}$   
 $\vec{E}_{zn} = \frac{\epsilon_r}{\epsilon_r} \frac{\vec{E}_{in}}{\epsilon_r}$

$$E_{1t} = E_{2t}$$

$$E_1 \sin \theta_1 = E_2 \sin \theta_2 \quad \text{--- (1)}$$

$$\text{if } P_s = 0 \longrightarrow D_{1n} = D_{2n}$$

$$\epsilon_0 \epsilon_{r1} E_{1n} = \epsilon_0 \epsilon_{r2} E_{2n}$$

$$\epsilon_{r1} E_1 \cos \theta_1 = \epsilon_{r2} E_2 \cos \theta_2 \quad \text{--- (2)}$$

$$\text{(1)} \longrightarrow \frac{\tan \theta_1}{\epsilon_{r1}} = \frac{\tan \theta_2}{\epsilon_{r2}}$$

$$\text{(2)}$$

$$\boxed{\frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_{r1}}{\epsilon_{r2}}} \longrightarrow \text{if } P_s = 0$$

### B) conductor - to - Dielectric

$\epsilon_{r2} = 1$   
 $\sigma \approx \infty$   
 $z = 0$   
 $\hat{a}_n$   
 $-\hat{a}_n$   
 $\alpha_1$   
 $\alpha_2$   
 $\vec{E}_1 \rightarrow \theta_1 = 0^\circ$   
 $\alpha_1 = 90^\circ$   
 $\vec{E}_2 = 0 \rightarrow \begin{cases} E_{2t} = 0 \rightarrow E_{1t} = 0 \\ E_{2n} = 0 \end{cases}$   
 $\vec{D}_2 = 0 \rightarrow \begin{cases} D_{2t} = 0 \\ D_{2n} = 0 \end{cases}$   
 $\epsilon_{r1}$   
 $\vec{E}_1 = \vec{E}_{1t} + \vec{E}_{1n}$   
 $\vec{D}_2 \cdot \hat{n} - \vec{D}_1 \cdot \hat{n} = P_s \rightarrow D_{1n} = -P_s \rightarrow E_{1n} = \frac{-P_s}{\epsilon_0 \epsilon_{r1}} \hat{a}_n$   
 $\alpha_2$  } does not exist  
 exist



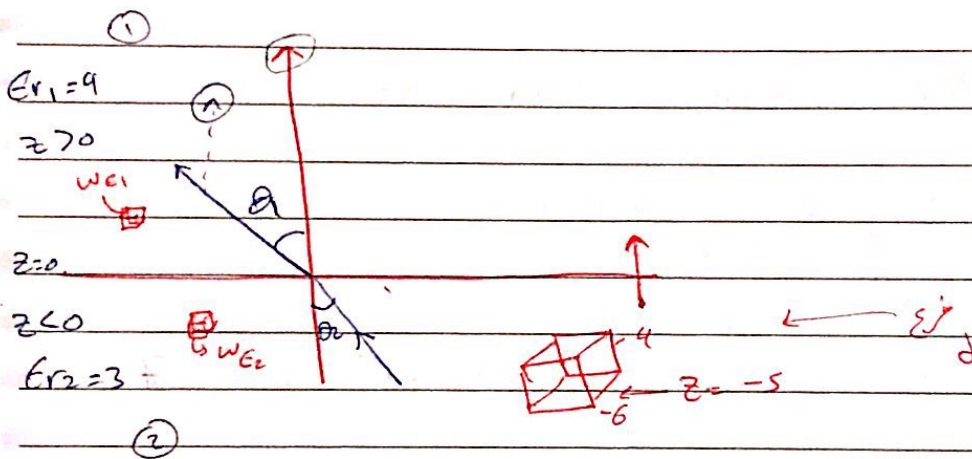
Ex: two homogeneous dielectrics meet on plane  $z=0$  for  $z < 0$   
~~and~~  $\rightarrow \epsilon_{r1} = 3$  and for  $z > 0 \rightarrow \epsilon_{r1} = 4$  and  $\vec{E}_1 = 5\hat{a}_x - 2\hat{a}_y + 3\hat{a}_z$   $\frac{KV}{m}$

Find: a)  $\vec{E}_2$  for  $z < 0$

b)  $\vec{D}_1, \vec{D}_2, \alpha_1, \alpha_2$

c) energy density in ~~each~~ both region

d) the energy in a cube of side (2m) centered at  $(3, 4, -5)$



a)  $\hat{a}_n = +\hat{a}_z$

$\vec{E}_{1n} = 3\hat{a}_z$   $KV/m$

$\vec{E}_{1t} = 5\hat{a}_x - 2\hat{a}_y$   $KV/m = \vec{E}_{2t}$

$D_{1n} - D_{2n} = \rho_s$

$\vec{D}_{2n} = \vec{D}_{1n}$

$\epsilon_{r2} \vec{E}_{2n} = \epsilon_{r1} \vec{E}_{1n}$

$\vec{E}_{2n} = \frac{4}{3} 3 \times 10^3 \hat{a}_z$

$\vec{E}_{2n} = 4\hat{a}_z$   $KV/m$

$\vec{E}_2 = 5\hat{a}_x - 2\hat{a}_y + 4\hat{a}_z$   $KV/m$

$\vec{D}_2 \rightarrow \rho_{v2}$   
 $\vec{P}_2$

$$b) \theta_1 = \sin^{-1} \frac{E_{1t}}{E_1} = \sin^{-1} \left( \frac{\sqrt{29}}{\sqrt{38}} \right) = \cos^{-1} \left( \frac{3}{\sqrt{35}} \right)$$

$$= 60.9^\circ \rightarrow \alpha_1 = 90 - \theta_1 = 29.1^\circ$$

$\theta_2 = ?$  since  $p_s = 0$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{E_{r1}}{E_{r2}} = \frac{4}{3} \rightarrow \theta_2 = 53.4^\circ$$

$$\alpha_2 = 36.6^\circ$$

$\theta_1 > \theta_2$  since  $E_{r1} > E_{r2}$

$$c) W_{E1} = \frac{1}{2} \epsilon_1 E_1^2 = \frac{1}{2} * \frac{10^{-9}}{36\pi} * 4 * 38 * 10^6 = 672 \text{ MJ/m}^3$$

$$W_{E2} = \frac{1}{2} \epsilon_0 E_2^2 = \frac{1}{2} * \frac{10^{-9}}{36\pi} * 9 * 45 * 10^6 = 597 \text{ MJ/m}^3$$

d) the cube is in region (2) (3, 4, -5)

$$W_E = \frac{1}{2} \int_V \epsilon_2 E_2^2 = \int_V W_{E2} dV$$

$$= 597 * 10^6 \int_{-6}^{-4} \int_3^5 \int_2^4 dx dy dz$$

$$2 * 2 * 2 = 8 \text{ m}^3$$

$$= 4.776 \text{ MJ}$$

END OF CH 5

## CH6: Boundary value problems

↳ if the charge or potential is known for some part of object

$$\nabla \cdot \vec{D} = \rho_v \quad , \quad \vec{E} = -\nabla V \quad , \quad \vec{D} = \epsilon \vec{E}$$

$$\bullet \nabla \cdot \epsilon (-\nabla V) = \rho_v \rightarrow \boxed{-\nabla \cdot \epsilon \nabla V = \rho_v}$$

↳ Poisson's eq for non-homogeneous media;  $\epsilon_r$  is function

• if  $\rho_v = 0$  (source free region)

$$\rho_v = 0, \quad \vec{J} = 0$$

$$\boxed{\nabla \cdot \epsilon \nabla V = 0}$$

↳ Laplace's eq for non homogeneous media

• if  $\epsilon$  is homogeneous

$$\nabla \cdot \nabla = \nabla^2$$

$$\boxed{\nabla^2 V = -\frac{\rho_v}{\epsilon}}$$

↳ Poisson's eq for homo media

• if  $\epsilon_r$  is homo  $\rho_v = 0$

$$\boxed{\nabla^2 V = 0}$$

↳ Laplace's eq for homo media

# CH 6 - Boundary value problems

$$\nabla \cdot -E \nabla V = \rho_v$$

$$\nabla \cdot E \nabla V = 0$$

$$\left. \begin{array}{l} \nabla^2 V = -\frac{\rho_v}{E} \\ \nabla^2 V = 0 \end{array} \right\} \text{Er is homogeneous}$$

$$\nabla^2 = \nabla \cdot \nabla = \text{laplacian operator}$$

$$\nabla = \frac{\partial}{\partial x} \hat{a}_x + \frac{\partial}{\partial y} \hat{a}_y + \frac{\partial}{\partial z} \hat{a}_z \rightarrow \text{cart}$$

cart

$$\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}$$

laplacian of (V)  $\rightarrow$  scalar

in cyl

↓

(given)

↑

$$\nabla^2 V = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial V}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 V}{\partial \phi^2} + \frac{\partial^2 V}{\partial z^2}$$

in sph

$$\nabla^2 V = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial V}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial V}{\partial \theta} \right)$$

$$+ \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2}$$

\* procedure to solve B.V.P :-

1) chose a suitable coordinates then chose the equation to solve (poisson or laplace).

2) solve laplace or poisson's equation either:

a) by direct integration if  $(V)$  is function of one var.

b) by separation of variables if  $(V)$  is function of two or three var.

3) Apply the four initial conditions to find the unique potential.

4) Find  $\vec{E}$  using  $\vec{E} = -\nabla V$

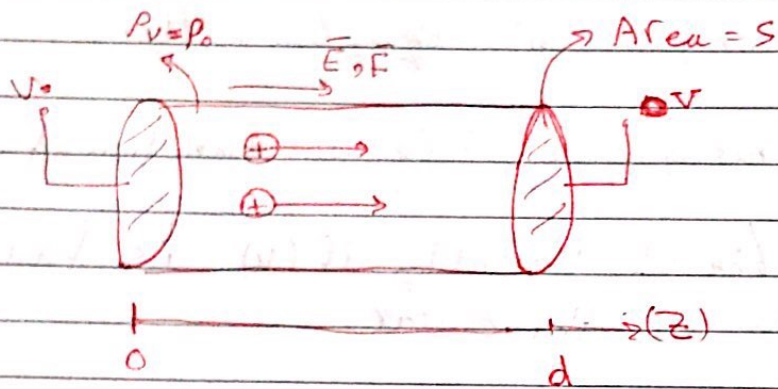
5) Find what ever is required

$$Q = \int_S \epsilon \vec{E} \cdot \vec{ds}$$

$$I = \int_S \sigma \vec{E} \cdot \vec{ds}$$

$$\text{pressure} = \frac{\text{Force}}{\text{Area}}, \quad F = Q \vec{E}$$

Ex: an electrohydrodynamic pumping has a uniform  $\rho_0$  exists between the two electrode calculate the pressure of the pump if  $\rho_0 = 25 \text{ mcl/m}^3$  and  $V_0 = 22 \text{ KV}$



$$\nabla^2 V = \frac{-\rho_v}{\epsilon} = \frac{-\rho_0}{\epsilon} \quad \begin{matrix} \rightarrow \rho_v \neq 0 \\ \rightarrow E_r \text{ is homo (not mention in ques)} \end{matrix}$$

$$\frac{d^2 V}{dz^2} = \frac{-\rho_0}{\epsilon} \quad \rightarrow \int \frac{d^2 V}{dz^2} = \int \frac{-\rho_0}{\epsilon}$$

$$\int \frac{dV}{dz} = \int \left( -\frac{\rho_0}{\epsilon} z + A \right)$$

$$V = \frac{-\rho_0 z^2}{2\epsilon} + Az + B \quad \text{general}$$

I.C.S

$$V(z=0) = V_0 = \beta$$

$$V(z=d) = 0$$

$$V(z=0) = V_0 = \beta$$

$$V(z=d) = 0 = -\frac{\rho_0 d^2}{2\epsilon} + Ad + V_0 \rightarrow A = \frac{1}{d} \left( \frac{\rho_0 d^2}{2\epsilon} - V_0 \right)$$

$$V = -\frac{\rho_0 z^2}{2\epsilon} + \frac{z}{d} \left( \frac{\rho_0 d^2}{2\epsilon} - V_0 \right) + V_0 \rightarrow \text{unique potential}$$

$$\vec{E} = -\nabla V = -\frac{dV}{dz} \hat{a}_z$$

$$\vec{E} = \left[ +\frac{\rho_0 z}{\epsilon} - \frac{1}{d} \left( \frac{\rho_0 d^2}{2\epsilon} - V_0 \right) \right] \hat{a}_z \quad \text{V/m}$$

$$\vec{F} = Q\vec{E}, \quad Q = \int_V \rho_v dv$$

$$\vec{F} = \int_V \rho_0 \vec{E} dv = \rho_0 S \int \vec{E} dz$$

$$\vec{F} = \rho_0 S \int_0^d \left[ \frac{\rho_0 z}{\epsilon} - \frac{1}{d} \left( \frac{\rho_0 d^2}{2\epsilon} - V_0 \right) \right] dz \hat{a}_z$$

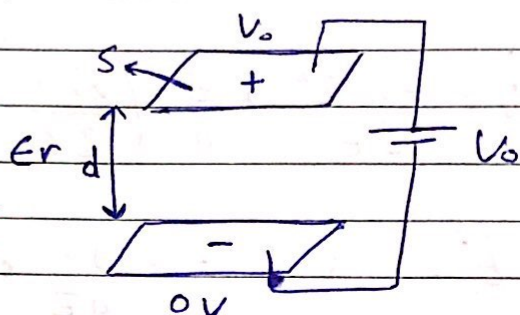
$$= \rho_0 S \left( \frac{\rho_0 d^2}{2\epsilon} - \frac{\rho_0 d^2}{2\epsilon} + V_0 \right) \hat{a}_z \rightarrow \vec{F} = \rho_0 S V_0 \hat{a}_z \quad \text{N}$$

$$\text{Pressure} = \frac{|\vec{F}|}{S} = \rho_0 V_0 \quad (\text{N/m}^2) = 550 \text{ N/m}^2$$

\* Resistance and capacitance :-

$$R = \frac{V}{I} = \frac{-\int \vec{E} \cdot d\vec{l}}{\int \sigma \vec{E} \cdot d\vec{s}} \quad , \quad C = \frac{Q}{V} = \frac{\int \epsilon \vec{E} \cdot d\vec{s}}{-\int \vec{E} \cdot d\vec{l}}$$

• procedure to find (R) and (C) :-



1) choose a suitable coordinates :-

↓ B.V.P

2) Assume  $V_0$  difference on the two plates.

3) solve Laplace equation and substitute the two initial condition to find the unique potential

4)  $\vec{E} = -\nabla V$

5) Find  $Q = ?$  using Gauss's law

$$Q = \oint \epsilon \vec{E} \cdot d\vec{s} \quad \text{and find} \quad I = \int \sigma \vec{E} \cdot d\vec{s}$$

6)  $\left[ C = \frac{Q}{V} \quad , \quad R = \frac{V}{I} \right]$  where (V) is assumed ( $V_0$ ) in step (2)



→ Gauss

2) assume  $\pm Q$

3) find  $\vec{E}$  using Gauss

$$Q = \oint_S \vec{E} \cdot \vec{dS} \rightarrow \text{CH 4}$$

4) Find  $V = -\int_L \vec{E} \cdot \vec{dL}$ ,  $I = \int_S \sigma \vec{E} \cdot \vec{dS}$

5)  $C = \frac{Q}{V} \rightarrow \text{step (3)}$   
 $\quad \quad \quad \quad \quad \rightarrow \text{step (4)}$

$$R = \frac{V}{I} \rightarrow \text{step (4)}$$

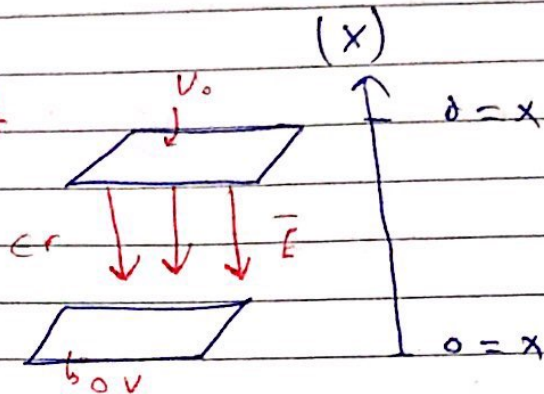
\* Types of capacitor :-

1) parallel plate capacitor

method (1)  $\rightarrow$  B.V.P cart

$$\nabla^2 V = 0$$

$$\int \frac{d^2 V}{dx^2} = \int 0$$



$$\int \frac{dV}{dx} = \int A \rightarrow V = Ax + B$$

$\rightarrow$  I.C  
 $V(x=0) = 0$   
 $V(x=d) = V_0$

$$B = 0, Ad = V_0 \rightarrow A = \frac{V_0}{d}$$

$$V = \frac{V_0}{d} x$$

$$\vec{E} = -\nabla V = -\frac{dV}{dx} \hat{a}_x = -\frac{V_0}{d} \hat{a}_x \text{ V/m}$$

نفسا اتجاه  $\vec{E}$  اي فرقتهم

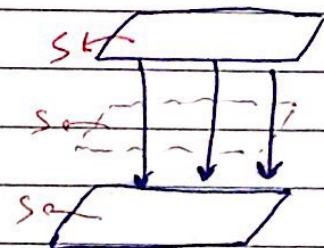
$$Q = \int_S \epsilon \vec{E} \cdot d\vec{S} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \epsilon \left( \frac{+V_0}{d} \hat{a}_x \right) \cdot dy dz \hat{a}_x$$

$$Q = \frac{\epsilon V_0 S}{d} \rightarrow C = \frac{Q}{V}$$

$$= \frac{\epsilon V_0 S}{V_0}$$

$$\rightarrow C = \frac{\epsilon S}{d} \text{ (F)}$$

Farad

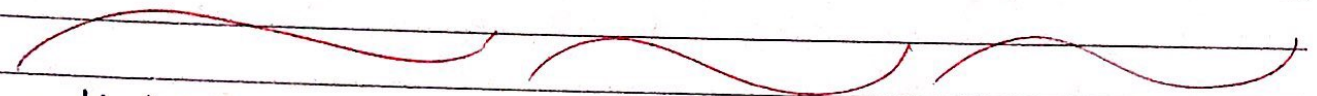


$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} dy dz = S$$

$$R_d = \frac{V}{I} \rightarrow I = \int_S \sigma_d \vec{E} \cdot d\vec{s}$$

$$I = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \left( \frac{-V_0}{d} \hat{a}_x \cdot dy dz (-\hat{a}_z) \right) \rightarrow \boxed{I = \frac{\sigma_d V_0 S}{d} \text{ (A)}}$$

$$\underline{R_d} = \frac{V_0}{\frac{\sigma_d V_0 S}{d}} = \frac{d}{\sigma_d S} = \boxed{\frac{d}{\sigma_d A}} \text{ (}\Omega\text{)}$$



method (2)  $\rightarrow$  Gauss:

$$Q = \int_S \epsilon \vec{E} \cdot d\vec{s}$$

$$\vec{E} = E_x (-\hat{a}_x) \quad d\vec{s} = dy dz (-\hat{a}_x)$$

$$Q = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \epsilon E_x (-\hat{a}_x) dy dz (-\hat{a}_x) \rightarrow \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} dy dz = S$$

$$Q = \epsilon E_x S \text{ (C)}$$

$$\vec{E} = \left( \frac{Q}{\epsilon S} \right) (-\hat{a}_x)$$

$$E = \frac{\rho_s}{\epsilon} (-\hat{a}_x)$$

نفسی CH4

$$V = -\int_{-ve}^{+ve} \vec{E} \cdot d\vec{l} = -\int_0^d \frac{Q}{\epsilon S} (-\hat{a}_x) \cdot dx \hat{a}_x$$

$$V = \frac{Qd}{\epsilon S} \text{ (V) constant}$$

$$C = \frac{Q}{V} = \frac{Q}{\frac{Qd}{\epsilon S}}$$

$$\rightarrow \boxed{C = \frac{\epsilon S}{d} \text{ (F)}}$$

$$I = \int_S \sigma_d \vec{E} \cdot \vec{ds} = \int_{-\infty}^{\infty} \int \sigma_d \frac{Q}{\epsilon_s} (-\hat{a}_x) dy dz (-\hat{a}_x)$$

$$\boxed{I = \frac{\sigma_d Q}{\epsilon} (A)} \Rightarrow \frac{C}{n \cdot w \cdot \frac{\epsilon}{x}} = \frac{C}{n \cdot F} = A$$

$$R_d = \frac{V}{I} = \frac{\frac{Qd}{\epsilon_s}}{\frac{\sigma_d Q}{\epsilon}} = \frac{d}{\sigma_d s} (-\Omega) = R_d$$

$$\rightarrow \boxed{G = \frac{1}{R_d} = \frac{\sigma_d s}{d} (S)}$$

\* always  $R_{dc} = \tau_r = \left(\frac{d}{\sigma_d s}\right) \cdot \left(\frac{\epsilon s}{d}\right) = \frac{\epsilon}{\sigma_d}$

$$W_E = \frac{1}{2} \int_V \vec{E} \cdot \vec{E} \cdot (dV) \rightarrow s dx$$

$\swarrow \quad \searrow$   
 $s d \quad m^3$

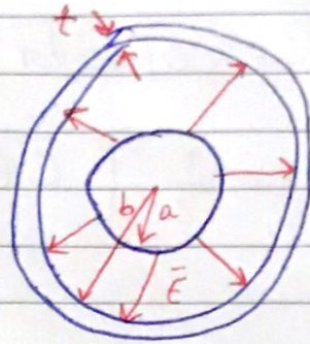
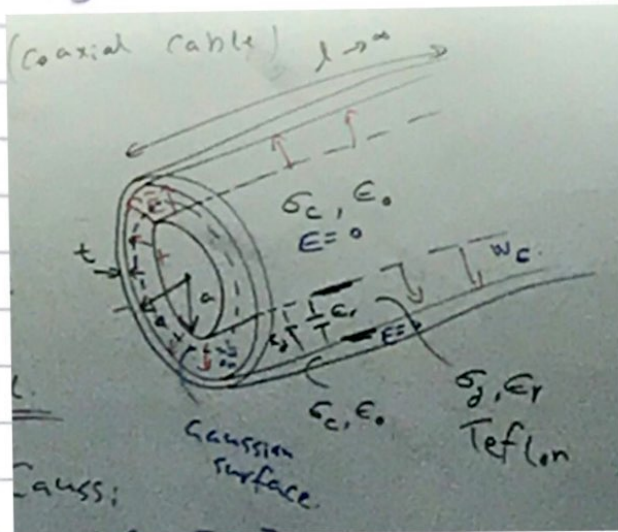
$$= \frac{\epsilon}{2} s \int_0^d \frac{Q^2}{\epsilon^2 s^2} dx = \frac{Q^2 d}{2 \epsilon s}$$

$$= \frac{Q^2}{2C} \quad \rightarrow Q = CV$$

$$= \frac{C^2 V^2}{2C} = \frac{1}{2} C V^2$$

$$\boxed{W_E = \frac{1}{2} C V^2}$$

## 2) Cylindrical capacitor



Gauss

$$Q = \oint_S \epsilon \vec{E} \cdot d\vec{s}$$

$$\vec{E} = E_\rho \hat{a}_\rho$$

$$d\vec{s} = \rho d\phi dz \hat{a}_\rho$$

$$Q = \int_0^L \int_0^{2\pi} \epsilon E_\rho \hat{a}_\rho \cdot \rho d\phi dz \hat{a}_\rho$$

in CHU  $Q = \epsilon E_\rho \rho 2\pi l \Rightarrow \boxed{\vec{E} = \frac{Q}{2\pi \rho \epsilon l} \hat{a}_\rho}$

$$\vec{E} = \frac{\rho l}{2\pi \epsilon \rho} \hat{a}_\rho, \rho l = \frac{Q}{l}$$

$$V = - \int_l \vec{E} \cdot d\vec{l} = - \int_b^a \frac{Q}{2\pi \epsilon \rho l} \hat{a}_\rho \cdot d\rho \hat{a}_\rho$$

$$V = \frac{+Q}{2\pi \epsilon l} \ln\left(\frac{b}{a}\right) (V)$$

$$C = \frac{Q}{V} = \frac{Q}{\frac{Q \ln(b/a)}{2\pi \epsilon l}} \rightarrow \boxed{C = \frac{2\pi \epsilon l}{\ln(b/a)} (F)}$$

$$\frac{C}{l} = \frac{2\pi\epsilon}{\ln(b/a)} \quad (\text{F/m})$$

↳ capacitor per unit length

$$W_E = \frac{1}{2} \int_{vol} \epsilon E^2 dV \rightarrow \frac{1}{2} C V^2$$

$$R_d = \frac{V}{I} \quad \bullet \quad I = \int_S \sigma_d \vec{E} \cdot d\vec{s}$$

$$= \int_0^l \int_0^{2\pi} \sigma_d \frac{Q}{2\pi\epsilon r l} \hat{r} \cdot \hat{r} \cdot r d\theta dz \hat{r} \rightarrow \boxed{I = \frac{\sigma_d Q (A)}{\epsilon}}$$

$$R_d = \frac{\frac{Q}{2\pi\epsilon l} \ln\left(\frac{b}{a}\right)}{\frac{\sigma_d Q}{\epsilon}} \rightarrow \boxed{R_d = \frac{\ln(b/a)}{2\pi\epsilon_0 l} \quad (\Omega)}$$

$$G = \frac{2\pi\sigma_d l}{\ln(b/a)} \quad (S)$$

$$G/l = \frac{2\pi\sigma_d}{\ln(b/a)} \quad (S/m)$$

$$CR_d = \frac{\epsilon}{\sigma_d} = \tau$$

using B.V.P

$$\nabla^2 V = 0, \quad \rho V = 0 \quad \text{Er is homo}$$

$$\frac{1}{\rho} \int \frac{\partial}{\partial \rho} \left( \rho \frac{dV}{d\rho} \right) = \int 0$$

$$\rho \int \frac{dV}{d\rho} = \int \frac{A}{\rho}$$

general

$$V = A \ln \rho + B$$

I.C

$$V(\rho = a) = V_0$$
$$V(\rho = b) = 0$$

$$A \ln a + B = V_0 \quad \dots (1)$$

$$A \ln b + B = 0 \quad \dots (2)$$

$$B = -A \ln b$$

$$A \ln a - A \ln b = V_0 \quad \rightarrow \quad A \ln \frac{a}{b} = V_0$$

$$A = \frac{V_0}{\ln \left( \frac{a}{b} \right)}$$

$$B = \frac{-V_0 \ln(b)}{\ln \left( \frac{a}{b} \right)}$$

$$V = \frac{V_0}{\ln \left( \frac{a}{b} \right)} \left( \ln \rho - \ln b \right)$$

$$V = V_0 \frac{\ln \frac{\rho}{b}}{\ln \frac{a}{b}} \rightarrow \text{unique}$$

continue

$$\vec{E} = -\nabla V$$

$$= -\frac{\partial V}{\partial \rho} \hat{a}_\rho \rightarrow \vec{E} = -\frac{V_0}{\ln\left(\frac{a}{b}\right)} \hat{a}_\rho$$

$$Q = \oint_S \epsilon \vec{E} \cdot \vec{d}s = \int_0^{2\pi} \int_0^{2a} \epsilon \frac{-V_0}{\ln\left(\frac{a}{b}\right)} \hat{a}_\rho \cdot \rho d\phi dz \hat{a}_\rho$$

$$= \frac{V_0 \epsilon}{\ln\left(\frac{b}{a}\right)} 2\pi L (\epsilon)$$

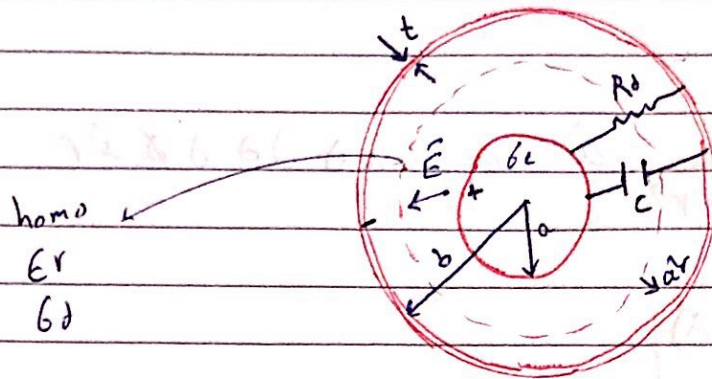
$$C = \frac{Q}{V} = \frac{V_0 \epsilon 2\pi L}{V \ln(b/a)}$$

$$C/l = \frac{2\pi \epsilon}{\ln\left(\frac{b}{a}\right)} \text{ F/m}$$

$$T = \frac{G_1 Q}{\epsilon}, \quad R_1 = \frac{\ln(b/a)}{2\pi \epsilon_0 l} (\Omega)$$



### 3) spherical capacitor



Gauss

$$Q = \oint_s \vec{E} \cdot \vec{ds} \quad , \quad \vec{E} = E_r \hat{a}_r$$

$$\vec{ds} = r^2 \sin \theta d\theta d\phi \hat{a}_r$$

$$Q = \int_0^{2\pi} \int_0^{\pi} E_r E_r r^2 \sin \theta d\theta d\phi$$

$$Q = E_r E_r 4\pi r^2 \quad , \quad \boxed{\vec{E} = \frac{Q}{4\pi \epsilon r^2} \hat{a}_r}$$

$$V = - \int_a^b \vec{E} \cdot \vec{dl} = - \int_a^b \frac{Q}{4\pi \epsilon r^2} \hat{a}_r \cdot dr \hat{a}_r$$

$$V = \frac{Q}{4\pi \epsilon} \left( \frac{1}{a} - \frac{1}{b} \right) (V)$$

$$C = \frac{Q}{V} = \frac{Q}{\frac{Q}{4\pi \epsilon} \left( \frac{1}{a} - \frac{1}{b} \right)} \quad \rightarrow \quad \boxed{C = \frac{4\pi \epsilon}{\frac{1}{a} - \frac{1}{b}} (F)}$$

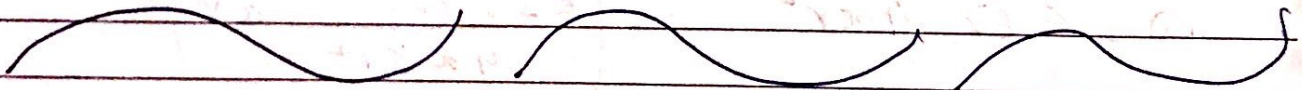
$$I = \int_S \epsilon_0 \vec{E} \cdot \vec{dS}$$

$$= \int \int \epsilon_0 \frac{Q}{4\pi\epsilon r^2} \hat{a}_r r^2 \sin\theta d\theta d\phi \hat{a}_r$$

$$I = \frac{\epsilon_0 Q}{\epsilon} \quad (A)$$

$$R_d = \frac{V}{I} = \frac{Q}{4\pi\epsilon} \left( \frac{1}{a} - \frac{1}{b} \right) \rightarrow R_d = \frac{1}{4\pi\epsilon_0} \left( \frac{1}{a} - \frac{1}{b} \right) \quad (\Omega)$$

$$W_E = \frac{1}{2} \int_V \epsilon E^2 dV \rightarrow W_E = \frac{1}{2} CV^2 \quad G = \frac{4\pi\epsilon_0}{\frac{1}{a} - \frac{1}{b}} \quad (S)$$



4) Isolated capacitor  
Isolated sphere

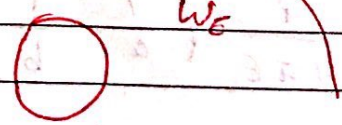
if  $b \rightarrow \infty$

$$C = 4\pi\epsilon_0 a \quad (F)$$

$$R_d = \frac{1}{4\pi\epsilon_0 a} \quad (\Omega)$$

$$G = 4\pi\epsilon_0 a \quad (S)$$

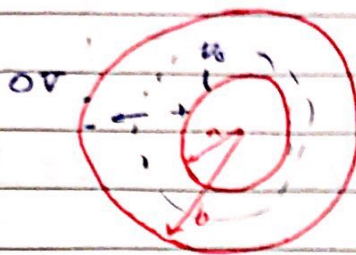
$$R_{dc} = \frac{\epsilon}{\sigma}$$



## Spherical capacitor:

Gauss

$$C = \frac{4\pi\epsilon}{\frac{1}{a} - \frac{1}{b}} \quad (F)$$



using B.V.P

$$\nabla^2 V = 0$$

$$\frac{1}{r^2} \int \frac{d}{dr} (r^2 \frac{dV}{dr}) = \int 0$$

$$r^2 \int \frac{dV}{dr} = \int \frac{A}{r^2} \rightarrow V = -\frac{A}{r} + B$$

I.C.S

$$V(r=a) = V_0 \rightarrow V_0 = -\frac{A}{a} + B \quad \dots \textcircled{1}$$

$$V(r=b) = 0$$

$$0 = -\frac{A}{b} + B \quad \dots \textcircled{2}$$

$$\hookrightarrow B = \frac{A}{b} \rightarrow \text{sub in 1}$$

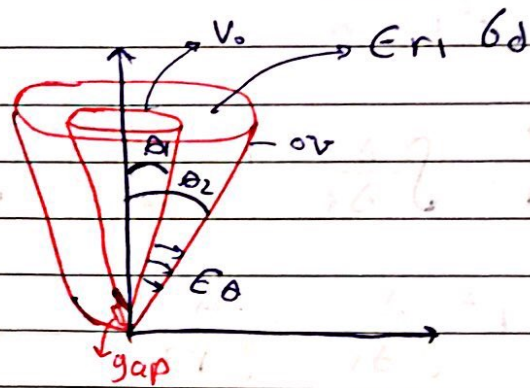
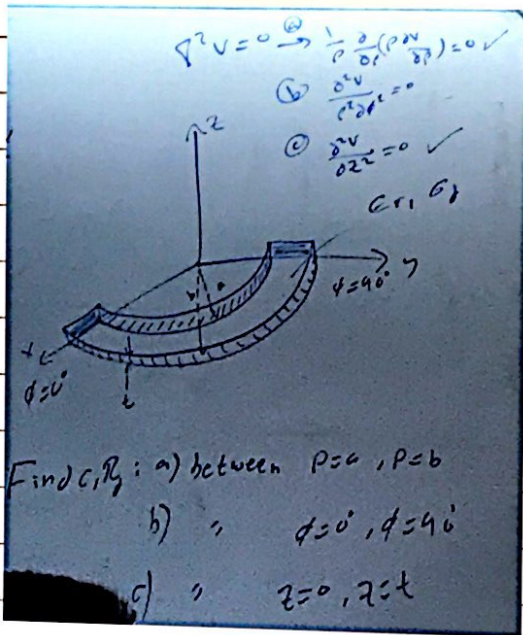
$$V_0 = -\frac{A}{a} + \frac{A}{b} \rightarrow V_0 = -A \left( \frac{1}{a} - \frac{1}{b} \right) \rightarrow \boxed{A = \frac{-V_0}{\frac{1}{a} - \frac{1}{b}}}$$

$$V = \frac{V_0}{\left(\frac{1}{a} - \frac{1}{b}\right)} \left[ \frac{1}{r} - \frac{1}{b} \right] \rightarrow \text{unique}$$

$$\boxed{\vec{E}} = -\nabla V = -\frac{dV}{dr} \hat{r} = \boxed{\frac{+V_0}{\left(\frac{1}{a} - \frac{1}{b}\right) r^2} \hat{r} \quad V/m}$$

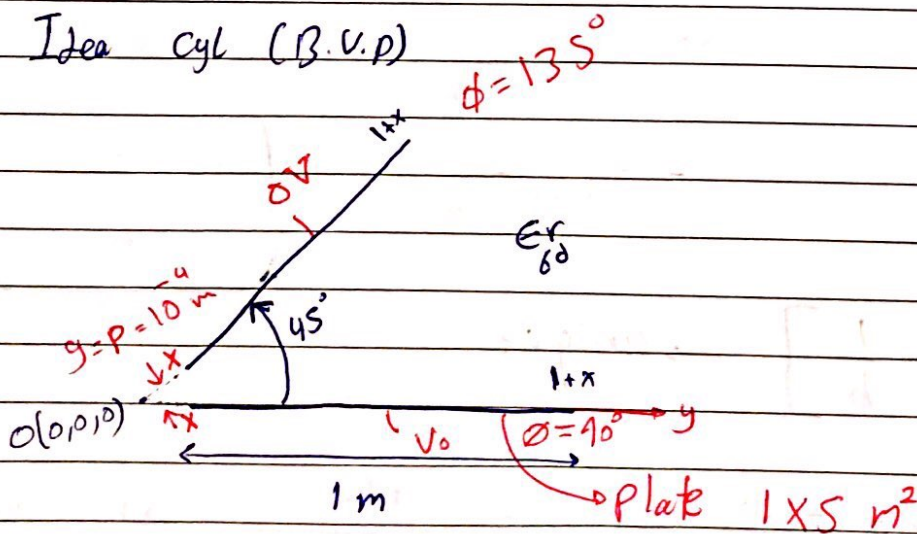
$$Q = \oint_S \epsilon \vec{E} \cdot d\vec{s} = \int_0^{2\pi} \int_0^\pi \frac{\epsilon V_0}{\frac{1}{a} - \frac{1}{b}} \frac{1}{r^2} \hat{a}_r \sin\theta \, d\theta \, d\phi \, \hat{a}_r$$

$$Q = \frac{4\pi\epsilon V_0}{\frac{1}{a} - \frac{1}{b}} (C) \rightarrow C = \frac{Q}{V_0} = \frac{4\pi\epsilon}{\frac{1}{a} - \frac{1}{b}} (F)$$



$$\frac{1}{r^2 \sin\theta} \frac{\partial}{\partial \theta} (\sin\theta \frac{\partial V}{\partial \theta}) = 0$$

Ex Idea cyl (B.V.P)



$$\nabla^2 V = 0$$

$$\int \frac{\partial^2 V}{\rho^2 \partial \phi^2} = \int 0$$

$$\int \frac{dV}{d\phi} = \int A \longrightarrow V = A\phi + B$$

$$V(\phi = \frac{\pi}{2}) = V_0$$

$$V(\phi = \frac{3\pi}{4}) = 0$$

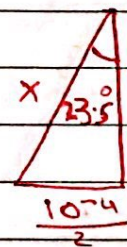
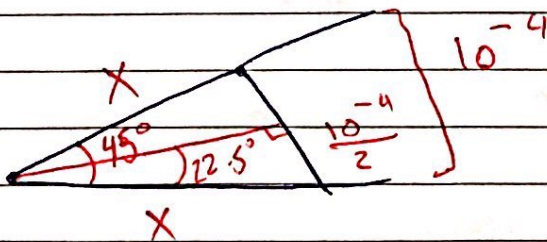
$$V_0 = A \frac{\pi}{2} + B \quad \text{--- (1) Solve for A, B}$$

$$0 = A \frac{3\pi}{4} + B \quad \text{--- (2)}$$

$$\vec{E} = -\nabla V = -\frac{1}{\rho} \frac{\partial V}{\partial \phi} \hat{a}_\phi$$

$$Q = \oint_S \vec{E} \cdot d\vec{s}$$

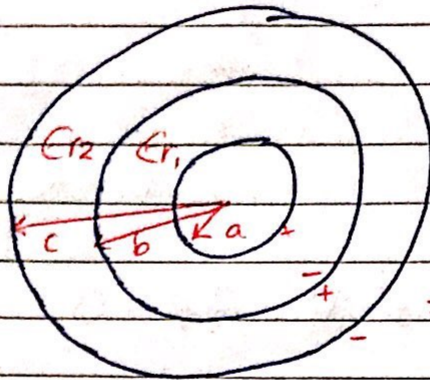
$$Q = \int_{\phi_1}^{\phi_2} \int_{\rho_1}^{\rho_2} \int_{z_1}^{z_2} \vec{E} \cdot \hat{a}_\phi \cdot \rho d\rho dz \hat{a}_\phi$$



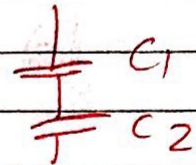
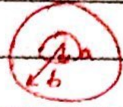
$$\sin 22.5 = \frac{10^{-4}}{\frac{X}{2}}$$

Ex spherical

$C_{eq}?$



$$C = 4\pi\epsilon \left( \frac{1}{a} - \frac{1}{b} \right)$$

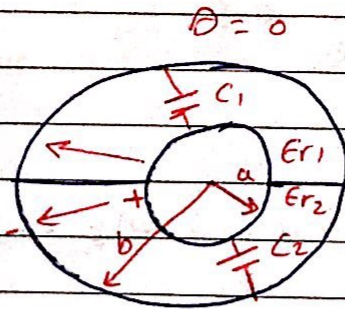


$$C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$$

$$C_1 = \frac{4\pi\epsilon_0 \epsilon_{r1}}{\frac{1}{a} - \frac{1}{b}}$$

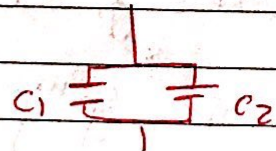
$$C_2 = \frac{4\pi\epsilon_0 \epsilon_{r2}}{\frac{1}{b} - \frac{1}{c}}$$

Ex spherical



$\theta = 90$

$\theta = 90$



$$C_1 = \frac{4\pi\epsilon_0 \epsilon_{r1}}{\frac{1}{a} - \frac{1}{b}} \cdot \frac{1}{2}$$

$$C_2 = \frac{4\pi\epsilon_0 \epsilon_{r2}}{\frac{1}{a} - \frac{1}{b}} \cdot \frac{1}{2}$$

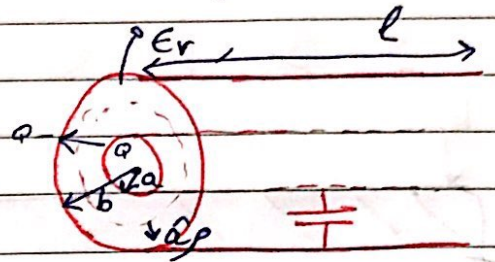
Ex: a coaxial cable has  $a = 1 \text{ cm}$   $b = 2.5 \text{ cm}$  is filled with a dielectric material has  $\epsilon_r = \frac{10 + \rho}{\rho}$  where  $\rho$  is in cm find  $C/l$ ?

Gauss

$$Q = \oint_S \vec{E} \cdot d\vec{s}$$

$$Q = \int_0^l \int_0^{2\pi} \epsilon \epsilon_r \hat{\rho} \cdot \rho d\phi dz \hat{\rho}$$

$\epsilon \epsilon_r$



$$Q = \epsilon \epsilon_r \rho 2\pi l$$

$$\vec{E} = \frac{Q}{2\pi \epsilon_r l} \hat{\rho}$$

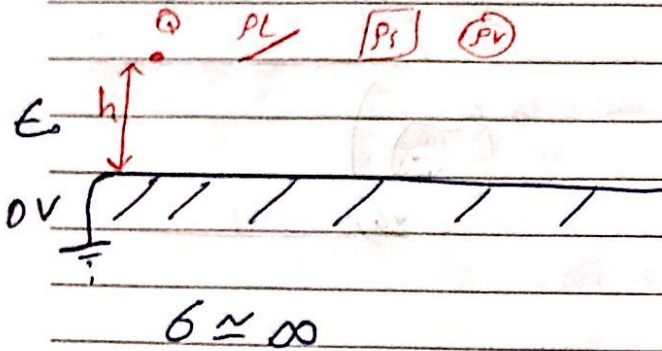
$$V = - \int_b^a \vec{E} \cdot d\vec{l} = - \int_b^a \frac{Q}{2\pi \epsilon_0 \left( \frac{10 + \rho}{\rho} \right) l} \hat{\rho} \cdot d\rho \hat{\rho}$$

$$V = \frac{+Q}{2\pi \epsilon_0 l} \ln \left( \frac{10 + b}{10 + a} \right)$$

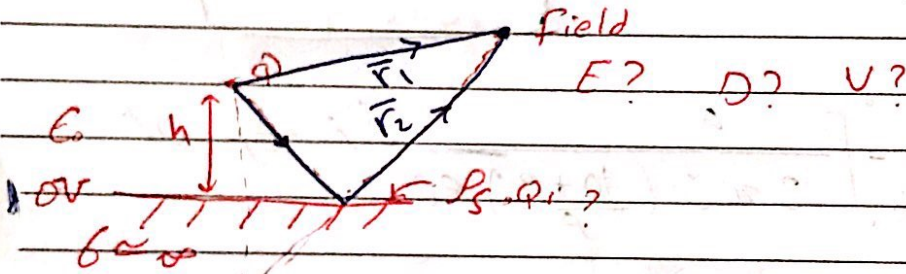
$$\frac{C}{l} = \frac{Q}{V} = \frac{2\pi \epsilon_0 l}{\ln \left( \frac{10 + b}{10 + a} \right)}$$

$$\frac{C}{l} = \frac{2\pi \frac{10^{-9}}{36\pi}}{\ln \left( \frac{12.5}{11} \right)} = 434.6 \text{ pF/m}$$

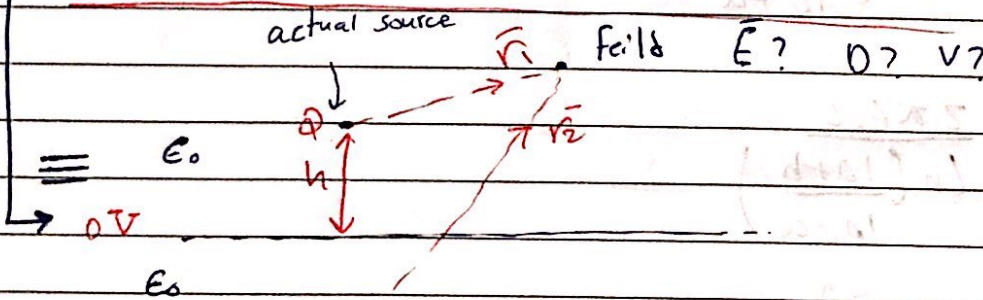
# \* method of Images



A) point charge above a perfect ground conducting plane



## \* original problem



$-Q$  Image (virtual source)

## \* equivalent problem

$\therefore \text{proof } Q_i = -Q$

هنا الخطوة عبارة عن وجود  $\vec{E}$  فوق السطح بعد ما أصبح  $\vec{E} = 0, \vec{D} = 0, \vec{V} = 0$  ←  $\vec{E} = 0$



eq Problem

$$\vec{E} = \vec{E}_+ + \vec{E}_- = \frac{Q \vec{r}_1}{4\pi\epsilon_0 r_1^3} + \frac{Q \vec{r}_2}{4\pi\epsilon_0 r_2^3}$$

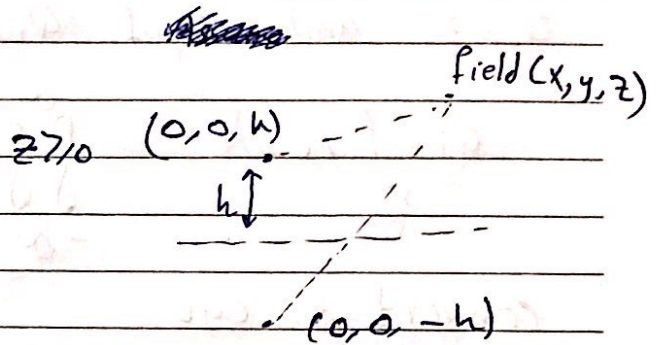
$$\vec{E} = \frac{Q}{4\pi\epsilon_0} \left[ \frac{\vec{r}_1}{r_1^3} - \frac{\vec{r}_2}{r_2^3} \right] \quad V/h$$

$$\vec{r}_1 = x\hat{x} + y\hat{y} + (z-h)\hat{z}$$

$$r_1 = \sqrt{x^2 + y^2 + (z-h)^2}$$

$$\vec{r}_2 = x\hat{x} + y\hat{y} + (z+h)\hat{z}$$

$$r_2 = \sqrt{x^2 + y^2 + (z+h)^2}$$



$$\vec{E}_{\text{original}} = \begin{cases} \frac{Q}{4\pi\epsilon_0} \left( \frac{\vec{r}_1}{r_1^3} - \frac{\vec{r}_2}{r_2^3} \right), & z > 0 \\ \frac{-Q 2h \hat{z}}{4\pi\epsilon_0 [x^2 + y^2 + h^2]^{3/2}}, & z = 0 \Rightarrow \vec{D} = \epsilon_0 \vec{E} \\ 0, & z < 0 \end{cases}$$

$$V = -\int \vec{E} \cdot d\vec{l} \quad \underline{\text{or}} \quad V = V_+ + V_-$$

$$V = \frac{Q}{4\pi\epsilon_0 r_1} - \frac{Q}{4\pi\epsilon_0 r_2}$$

$$V_{\text{original}} = \begin{cases} \frac{Q}{4\pi\epsilon_0} \left[ \frac{1}{r_1} - \frac{1}{r_2} \right], & z > 0 \\ 0, & z \leq 0 \end{cases}$$

$$P_s = \bar{D} \cdot \hat{a}_n \quad , \hat{a}_n = \hat{a}_z$$

$z=0$

$$P_s = \frac{-\phi h}{2\pi [x^2 + y^2 + h^2]^{3/2}} \quad C/m^2$$

$Q_i = ?$  and proof  $Q_i = -\phi$

$$Q_i = \int_s P_s ds = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{-\phi h dx dy}{2\pi [x^2 + y^2 + h^2]^{3/2}}$$

convert to cyl

$$Q_i = \int_s P_s ds \quad , ds = \rho d\rho d\phi$$

$$Q_i = \frac{-\phi h}{2\pi} \int_0^{2\pi} \int_0^{\infty} \frac{\rho d\rho d\phi}{[\rho^2 + h^2]^{3/2}}$$

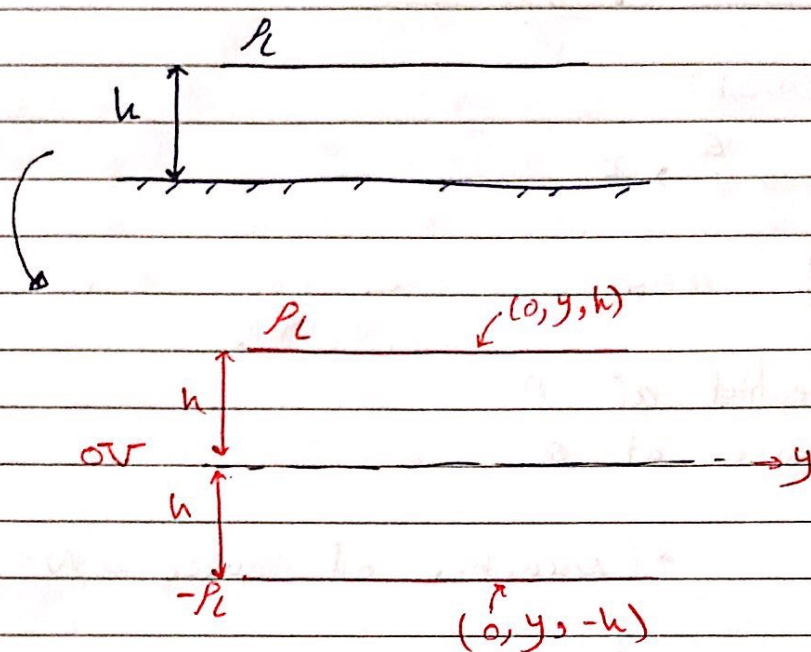
let  $u = \rho^2 + h^2$

$$du = 2\rho d\rho \rightarrow \rho d\rho = \frac{du}{2}$$

$$Q_i = +\phi h \cdot \frac{1}{\frac{1}{2} u^{1/2}}$$

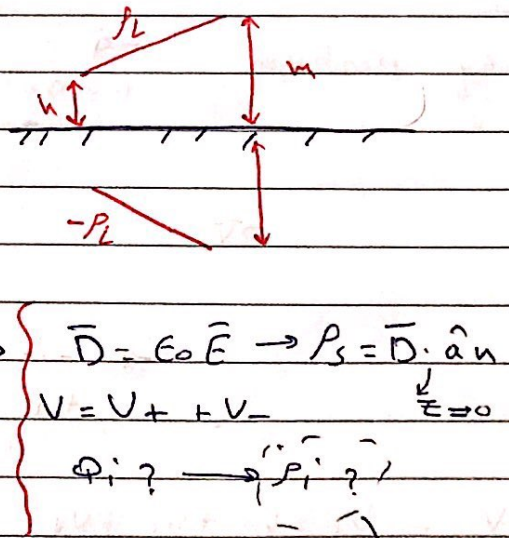
$$Q_i = \phi h \frac{1}{\sqrt{\rho^2 + h^2}} \Big|_0^{\infty} = \phi h \left( 0 - \frac{1}{h} \right) = -\phi \quad \#$$

B) Line charge above a perfect ground conducting plane



$$\vec{E} = \vec{E}_+ + \vec{E}_-$$

$$= \begin{cases} \frac{\rho_L \vec{r}_1}{2\pi\epsilon_0 r_1^2} - \frac{\rho_L \vec{r}_2}{2\pi\epsilon_0 r_2^2}, & z > 0 \\ -\frac{2h \rho_L}{2\pi\epsilon_0 (x^2 + h^2)} \hat{z}, & z = 0 \\ 0, & z < 0 \end{cases}$$



$$\vec{r}_1 = x\hat{x} + (z-h)\hat{z}$$

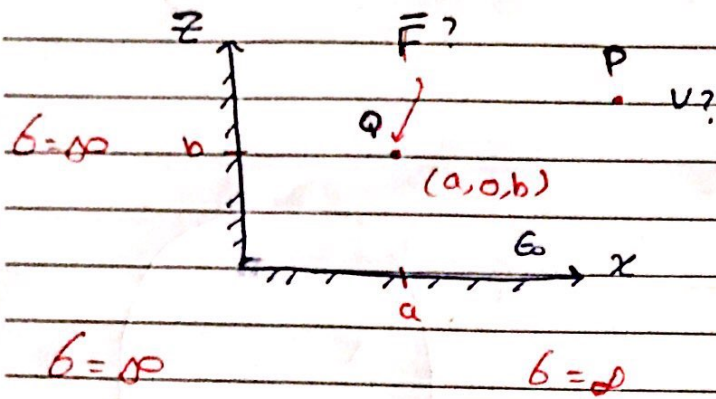
$$r_1 = \sqrt{x^2 + (z-h)^2}$$

$$\vec{r}_2 = x\hat{x} + (z+h)\hat{z}$$

$$r_2 = \sqrt{x^2 + (z+h)^2}$$

$$Q_i = \int_L \rho_L dl = \int_S \rho_S ds \rightarrow (dx dy) \Rightarrow P_i = \int_L \rho_S dx$$

$\epsilon_x$

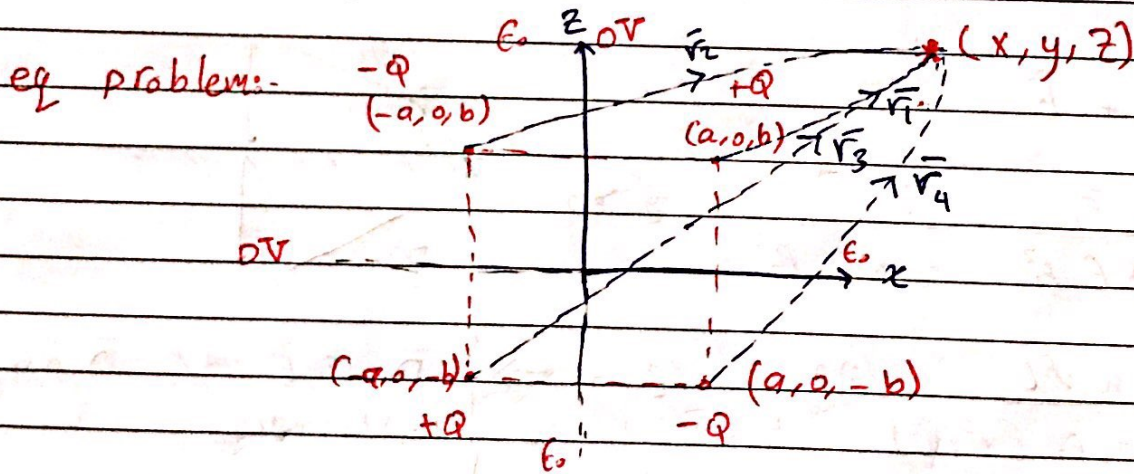


- a) find the potential at  $P$
- b) " " force at  $q$

a)

$$N = \frac{360}{\theta} - 1 \quad * (\text{Number of source} \rightarrow N = \frac{360}{\theta})$$

number of Images



$$V|_P = V_1 + V_2 + V_3 + V_4$$

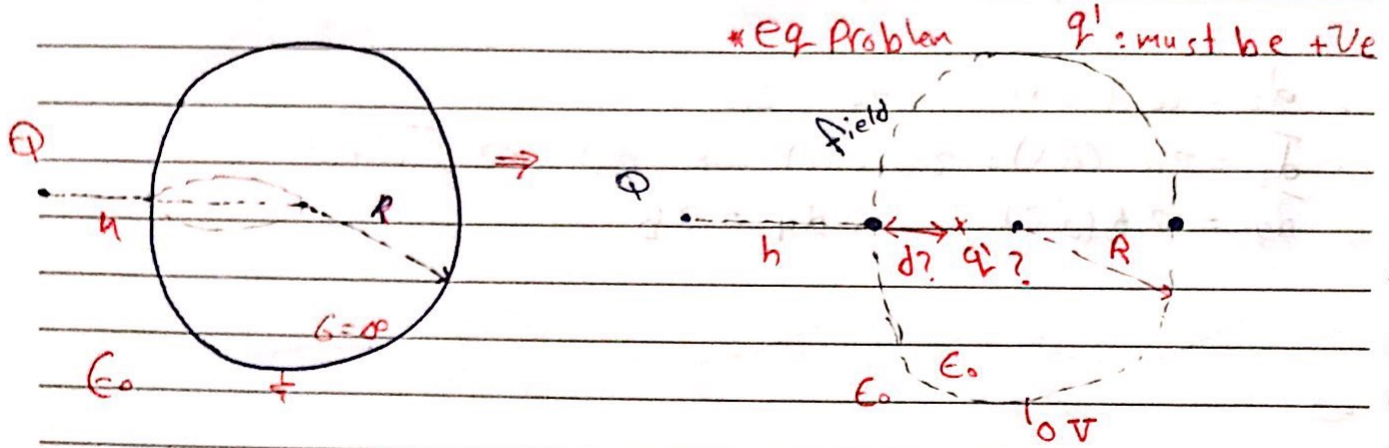
$$= \begin{cases} \frac{q}{4\pi\epsilon_0} \left[ \frac{1}{r_1} - \frac{1}{r_2} + \frac{1}{r_3} - \frac{1}{r_4} \right], & x > 0 \\ 0, & \text{otherwise} \end{cases}$$

$$\begin{cases} \vec{r}_1 = (x-a)\hat{x} + y\hat{y} + (z-b)\hat{z} \\ \vec{r}_2 = (x+a)\hat{x} + y\hat{y} + (z-b)\hat{z} \\ \vec{r}_3 = (x+a)\hat{x} + y\hat{y} + (z+b)\hat{z} \\ \vec{r}_4 = (x-a)\hat{x} + y\hat{y} + (z+b)\hat{z} \end{cases}$$



Ex. - a point charge near a perfect ground conducting sphere :-

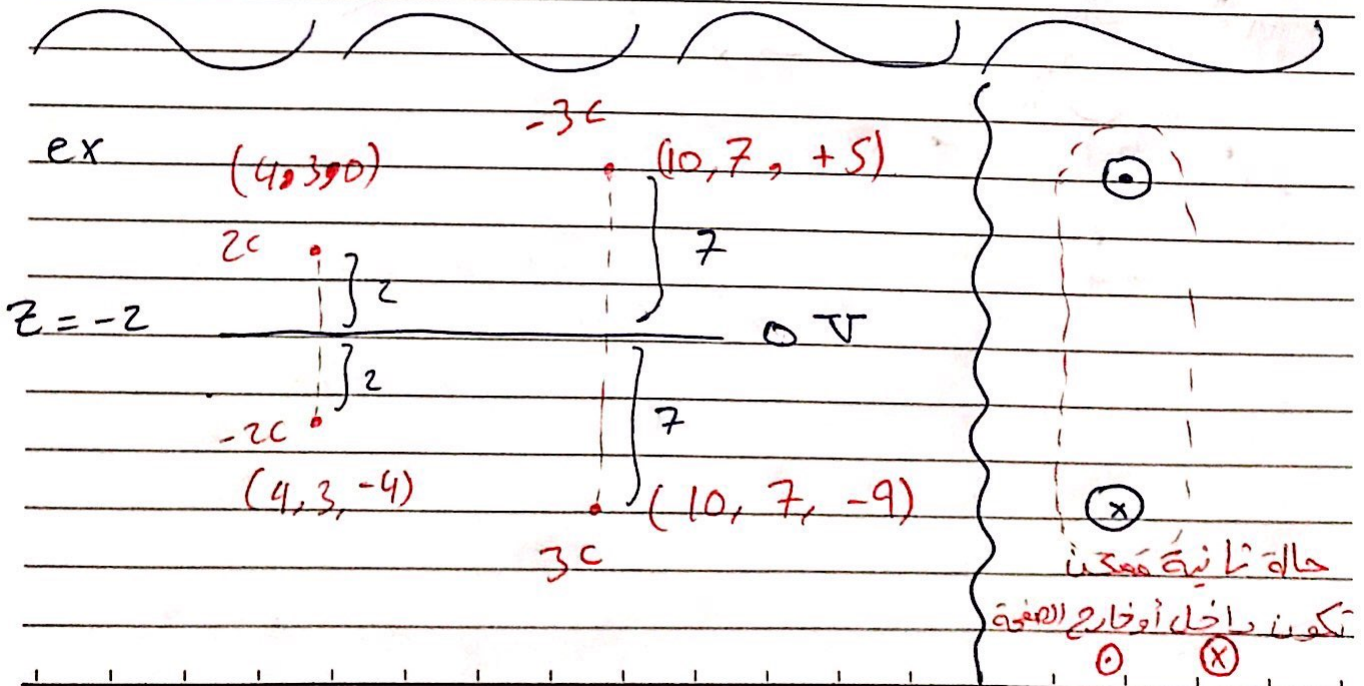
- Find location and value of the image.



$$V|_{r=h} = 0 \rightarrow \frac{Q}{4\pi\epsilon_0 \cdot h} - \frac{q'}{4\pi\epsilon_0 \cdot d} = 0 \quad \text{--- (1)}$$

$$q' = \frac{dQ}{h}$$

$$V|_{r=h+2R} = 0 \rightarrow \frac{Q}{4\pi\epsilon_0 (h+2R)} - \frac{q'}{4\pi\epsilon_0 (2R-d)} = 0 \quad \text{--- (2)}$$



## CH 7: Magnetostatic Fields

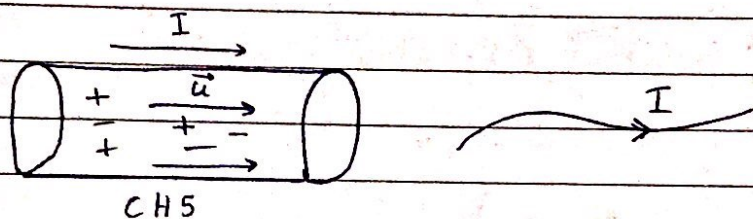
\* Source for magnetostatics:-

1) permanent magnet

(constant)

2) charge moving with uniform velocity  $\rightarrow$  Zero acceleration

3) Dc current flowing in the wire

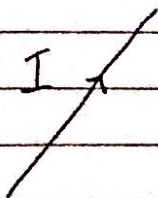


\* Major laws:-

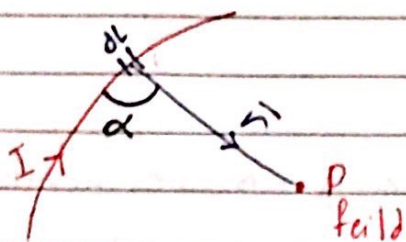
1) Biot-savart's law (general)

2) Ampere's law (special case)

or instead (Motor principle)



\* Biot savart's Law  
by exp



$\vec{H} \equiv$  Magnetic field intensity: (A/m)

$$dH \propto \frac{I dl \sin \alpha}{r^2} \text{ (relation)} \quad (\times \rightarrow \text{cross product})$$

$$dH = \frac{K I dl \sin \alpha}{r^2}$$

$$K = \frac{1}{4\pi}$$

↳ proportionality constant

$$\int dH = \int \frac{I dl \sin \alpha}{4\pi r^2}$$

$$H = \int \frac{I dl \sin \alpha}{4\pi r^2} \Rightarrow \text{magnitude only}$$

$\vec{H}?$

$$\vec{H} = \int \frac{I d\vec{L} \times \hat{r}}{4\pi r^2}$$

$$|\vec{A} \times \vec{B}| = AB \sin \theta_{AB}$$

$$|d\vec{L} \times \hat{r}| = dl (l) \sin \alpha$$

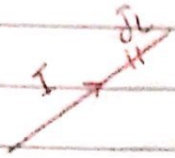
$$\perp d\vec{L} \perp \vec{r} \quad \Rightarrow d\vec{L} = dl \hat{a}_L$$

$$\vec{H} = \int \frac{I d\vec{L} \times \vec{r}}{4\pi r^3} = \int \frac{I \hat{a}_L \times \vec{r}}{4\pi r^3} dl \quad \text{For line current (1D segment)}$$



## Types of current distribution

1) line current  $\rightarrow$  1D segment

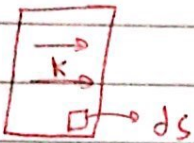


$$I \, dl \equiv A \cdot m$$

A/m

$$\vec{H} = \int_L \frac{I \, d\vec{l} \times \vec{r}}{4\pi r^3}$$

2) Surface current  $\rightarrow$  2D surfaces

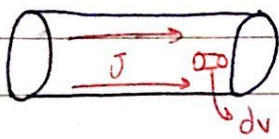


$$\vec{k} \, ds \equiv A \cdot m$$

$\vec{k}$  = surface current density (A/m)

$$\vec{H} = \int_S \frac{\vec{k} \, ds \times \vec{r}}{4\pi r^3} \Rightarrow \vec{H} = \int_S \frac{\vec{k} \times \vec{r}}{4\pi r^3} \, ds$$

3) Volume current  $\rightarrow$  3D object



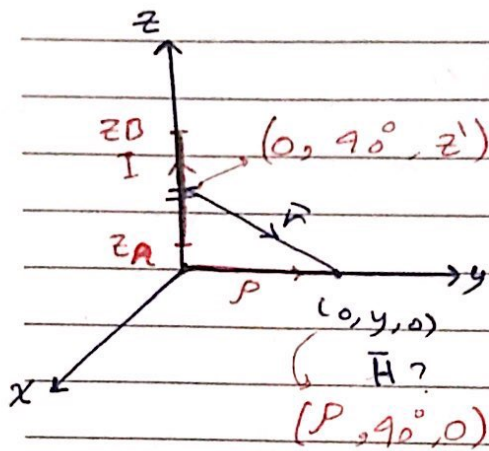
$$\vec{J} \, dv = A \cdot m$$

$\vec{J}$  = volume current density (A/m<sup>2</sup>)

$$\vec{H} = \int_V \frac{\vec{J} \, dv \times \vec{r}}{4\pi r^3}$$

X Volume  $\rightarrow$  Amperes Law

Ex: find  $\vec{H}$  at  $(0, y, 0)$  due to a finite straight wire along z-axis carry current (I)



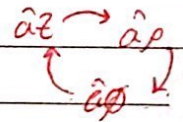
$$\vec{H} = \int_L \frac{I \, d\vec{L} \times \vec{r}}{4\pi r^3}$$

$$d\vec{L} = dz' \hat{a}_z$$

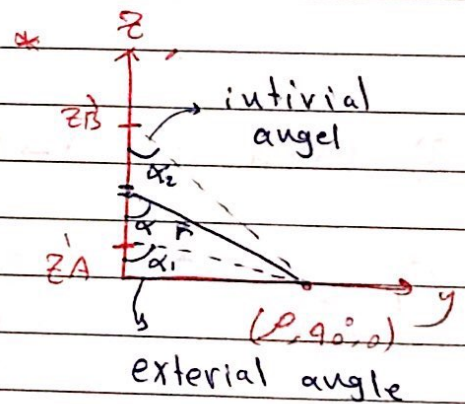
$$\vec{r} = p\hat{a}_p - z'\hat{a}_z$$

$$r = \sqrt{p^2 + z'^2}$$

$$\vec{H} = \frac{I}{4\pi} \int_{z'_A}^{z'_B} \frac{dz' \hat{a}_z \times (p\hat{a}_p - z'\hat{a}_z)}{[p^2 + z'^2]^{3/2}}$$



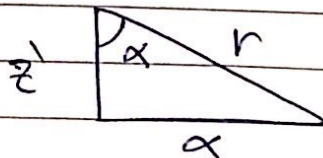
$$\vec{H} = \frac{I}{4\pi} \int_{z'_A}^{z'_B} \frac{dz' \hat{a}_\phi}{[p^2 + z'^2]^{3/2}}$$



introduce angle  $\alpha$ ,  $\alpha_1$ ,  $\alpha_2$   
relate  $z'$  with  $\alpha$ .

$$\sin \alpha = \frac{p}{r}$$

$$\cos \alpha = \frac{z'}{r}$$



$$\tan \alpha = \frac{p}{z'} \rightarrow z' = p \cot \alpha$$

$$z' = \rho \cot \alpha \rightarrow dz' = -\rho \csc^2 \alpha d\alpha$$

$$\rho^2 + z'^2 = \rho^2 + \rho^2 \cot^2 \alpha = \rho^2 (1 + \cot^2 \alpha)$$

$$r^2 = \rho^2 \csc^2 \alpha, \quad r^3 = \rho^3 \csc^3 \alpha$$

$$\vec{H} = \frac{I\rho}{4\pi} \int_{\alpha_1}^{\alpha_2} \frac{-\rho \csc^2 \alpha}{\rho^3 \csc^3 \alpha} d\alpha \hat{a}_\phi$$

$$\vec{H} = \frac{I}{4\pi\rho} \int_{\alpha_1}^{\alpha_2} \sin \alpha d\alpha \hat{a}_\phi$$

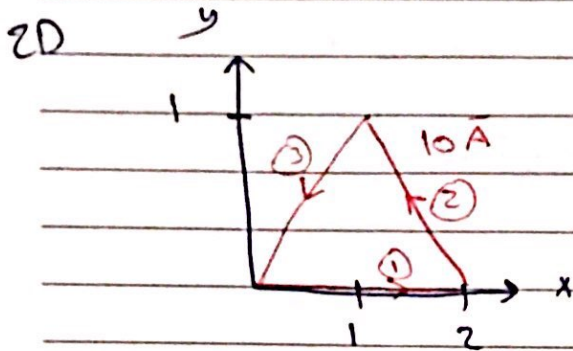
$$\vec{H} = \frac{I}{4\pi\rho} (\cos \alpha_2 - \cos \alpha_1) \hat{a}_\phi$$

(interior - exterior) angle

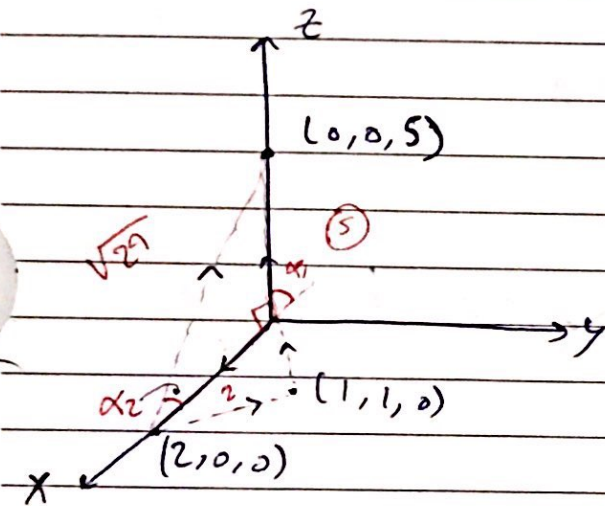
always for finite wire  
straight

$$\hat{a}_\phi = \hat{a}_l \times \hat{a}_\rho$$

Ex. for a triangular loop



Find  $\vec{H}$  at  $(0,0,5)$  due to side (1) of the loop :-



$$\vec{H} = \frac{I}{4\pi r} (\cos\alpha_2 - \cos\alpha_1) \hat{n}$$

$$\alpha_1 = 90^\circ \rightarrow \cos\alpha_1 = 0$$

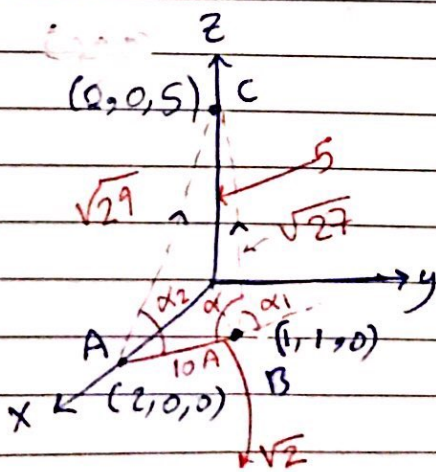
$$\cos\alpha_2 = \frac{2}{\sqrt{29}}$$

$$\vec{P} = 5 \hat{a}_z \rightarrow P = 5 \text{ m}$$

$$\hat{a}_n = \hat{a}_l \times \hat{a}_p \\ = \hat{a}_x \times \hat{a}_z = -\hat{a}_y$$

$$\vec{H} = -5 \cdot 1 \hat{a}_y \text{ mA/m}$$

Side (2)



$$\vec{AB} \cdot \vec{AC} = |\vec{AB}| |\vec{AC}| \cos\alpha_2$$

$$\vec{BA} \cdot \vec{BC} = |\vec{BA}| |\vec{BC}| \cos\theta_1$$

$$\cos\alpha_1 = -\cos\theta_1$$

$$\alpha_1 = 90^\circ \rightarrow P = \sqrt{27}$$

$$(1, -1, 0) \cdot (-1, -1, 5) = \sqrt{2} \sqrt{27} \cos\theta_1$$

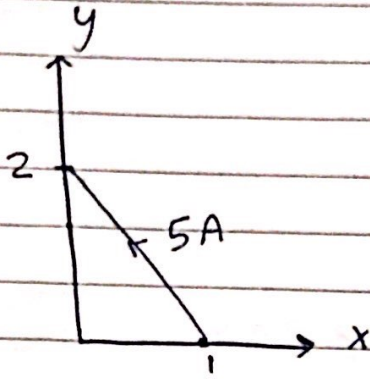
$$-1 + 1 + 0$$

$$\cos\theta_1 = 0$$

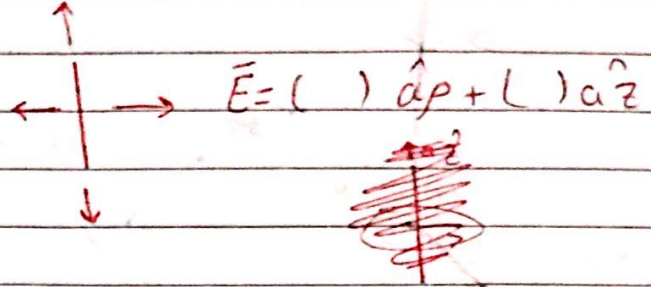
$$\vec{AB} = (-1, 1, 0) \rightarrow AB = \sqrt{2}$$

Five Apple

ex:



Find  $\vec{H}$  at  $(0,0,5)$ ?

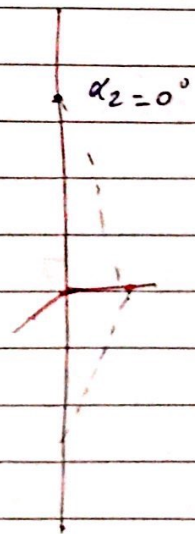
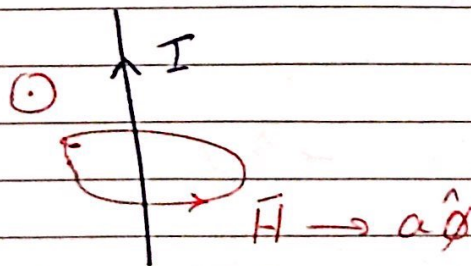


$$\vec{H} = \frac{I}{4\pi r} (\cos \alpha_2 - \cos \alpha_1) \hat{a}_\phi$$

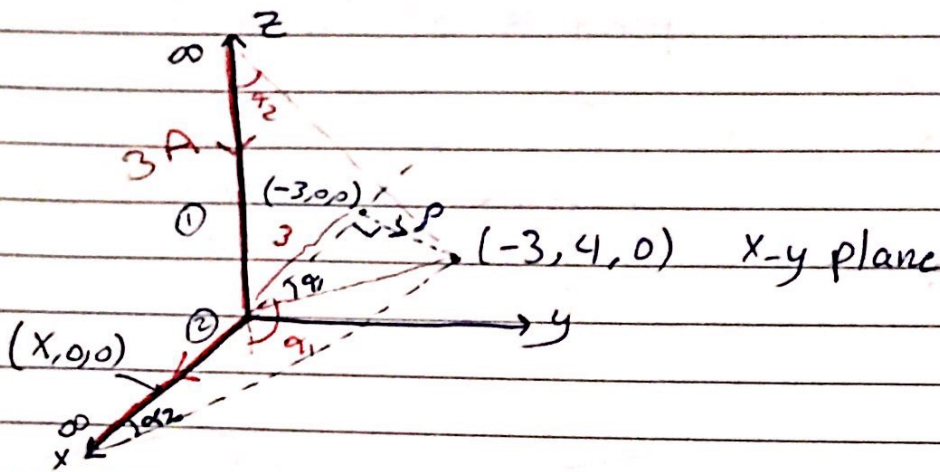
For an infinite line

$$\vec{H} = \frac{I}{2\pi r} \hat{a}_\phi$$

always for any inf line



Ex: Find  $\vec{H}$  at  $(-3, 4, 0)$



$$\vec{H} = \vec{H}_1 + \vec{H}_2$$

$$H_1 = \frac{I}{4\pi\rho} (\cos\alpha_2 - \cos\alpha_1) a_{\hat{\phi}}$$

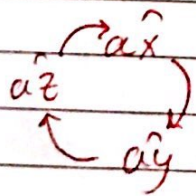
$$\alpha_1 = 90^\circ$$

$$\alpha_2 = 0^\circ$$

$$\vec{P} = (-3, 4, 0), \rho = 5 \text{ m}$$

$$a_{\hat{\phi}} = a_{\hat{t}} \times a_{\hat{p}}$$

$$= -a_{\hat{z}} \times \frac{(-3, 4, 0)}{5} = \frac{4}{5} a_{\hat{x}} + \frac{3}{5} a_{\hat{y}}$$



$$\vec{H}_1 = \frac{I}{4\pi\rho} a_{\hat{\phi}}$$

$$\vec{H}_1 = -47.75 a_{\hat{\phi}} \text{ mA/m} \rightarrow \text{cyl}$$

$$\vec{H}_1 = 38.2 a_{\hat{x}} + 28.65 a_{\hat{y}} \text{ mA/m} \rightarrow \text{cart}$$

$$\vec{H}_2 = \frac{I}{4\pi\rho} \left(1 + \frac{3}{5}\right) a \hat{\phi}$$

$$\cos \alpha_1 = -\frac{3}{5}$$

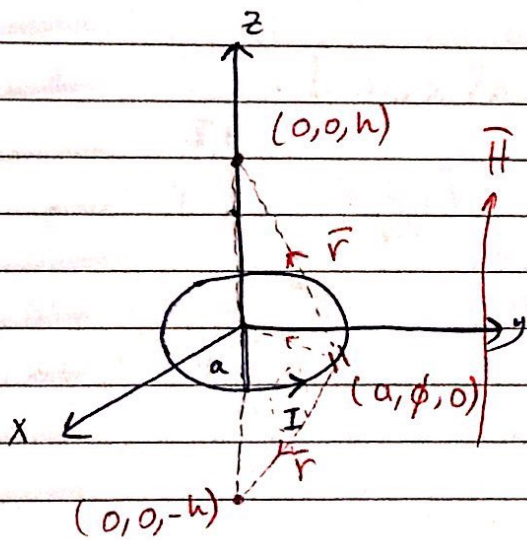
$$\alpha_2 = 0^\circ$$

$$\vec{P} = 4a\hat{y}, \rho = 4m$$

$$\begin{aligned} a\hat{\phi} &= a\hat{l} \times a\hat{p} \\ &= a\hat{x} \times a\hat{y} \\ &= a\hat{z} \end{aligned}$$

$$\vec{H}_2 = 23.88a\hat{z} \text{ m A/m}$$

ex: find  $\vec{H}$  at  $(0,0,h)$  and  $(0,0,-h)$



$$\vec{H} = \int \frac{I d\vec{l} \times \vec{r}}{4\pi r^3} \text{ at } (0,0,h)$$

$$d\vec{l} = a d\phi a\hat{\phi}$$

$$\vec{r} = -a a\hat{\phi} + h a\hat{z}$$

$$r = \sqrt{a^2 + h^2}$$

$$\vec{H} = \frac{I}{4\pi} \int_0^{2\pi} a d\phi a\hat{\phi} \times (-a\hat{\phi} + h a\hat{z})$$

due to symmetry

$$\vec{H} = \frac{I a^2}{2(a^2 + h^2)^{3/2}} a\hat{z} \text{ A/m}$$

at  $(0,0,-h)$   
Same Answer

\* Ampere's law :-

$$\oint_C \vec{H} \cdot d\vec{L} = I_{enc} \rightarrow 3^{rd} \text{ maxwell's eq in integral form}$$

Apply Stokes's theorem

$$\oint_C \vec{H} \cdot d\vec{L} = \int_S \nabla \times \vec{H} \cdot d\vec{s} = I_{enc} = \int_S \vec{J} \cdot d\vec{s}$$

$$\nabla \times \vec{H} = \vec{J} \rightarrow 3^{rd} \text{ maxwell's eq in diff form}$$

\* applications on Ampere's law :-

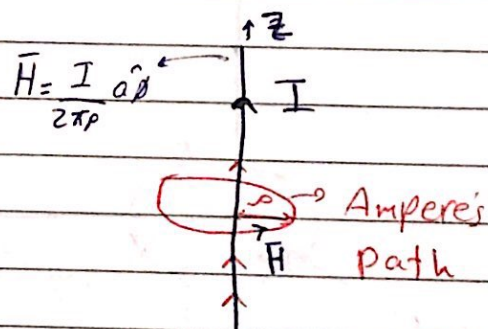
1) find  $\vec{H}$  for an infinite line of current.

$$\oint_C \vec{H} \cdot d\vec{L} = I_{enc} = I$$

From R.H.R

$$\vec{H} = H\phi \hat{a}_\phi$$

$$d\vec{L} = \rho d\phi \hat{a}_\phi$$



$$\int_0^{2\pi} H\phi \hat{a}_\phi \rho d\phi \hat{a}_\phi = I$$

$$2\pi\rho H\phi = I$$

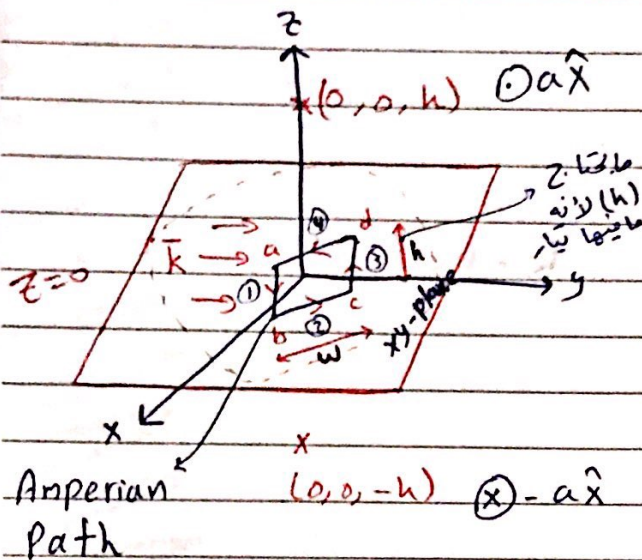
$$\vec{H} = \frac{I}{2\pi\rho} \hat{a}_\phi$$



2) find  $\vec{H}$  for an infinite sheet of current

i.e for  $z=0$  plane carry current  $\vec{K} = K_y \hat{a}_y$ .

find  $\vec{H}$  every where.  $\rightarrow z > 0$   
 $\rightarrow z < 0$



$$\oint \vec{H} \cdot d\vec{l} = I_{enc} = K_y w$$

$$\vec{H} = \begin{cases} H_0 \hat{a}_x, & z > 0 \\ H_0 (-\hat{a}_x), & z < 0 \end{cases}$$

$$\oint \vec{H} \cdot d\vec{l} = \int_a^b \vec{H} \cdot d\vec{l}_1 + \int_b^c \vec{H} \cdot d\vec{l}_2 + \int_c^d \vec{H} \cdot d\vec{l}_3 + \int_d^a \vec{H} \cdot d\vec{l}_4 = K_y w$$

$$\int_b^c H_0 (-\hat{a}_x) \cdot dx (-\hat{a}_x) + \int_d^a H_0 \hat{a}_x \cdot dx \hat{a}_x = K_y w$$

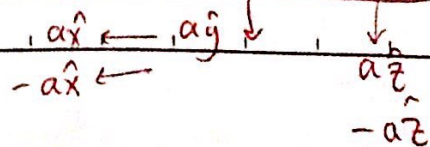
$$H_0 w + H_0 w = K_y w \quad * \text{Recall CH 4}$$

$$H_0 = \frac{K_y}{2}$$

$$E = \frac{\rho_s}{2\epsilon_0}$$

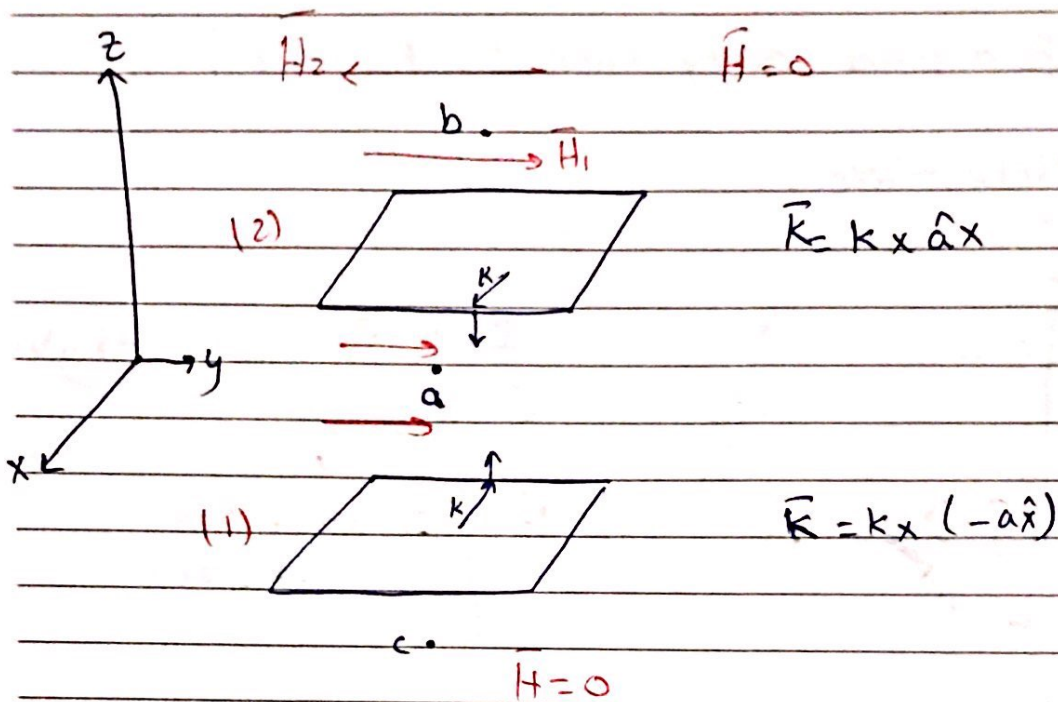
$$\vec{H} = \begin{cases} \frac{K_y}{2} \hat{a}_x, & z > 0 \\ \frac{K_y}{2} (-\hat{a}_x), & z < 0 \end{cases}$$

$$\Rightarrow \boxed{\vec{H} = \frac{1}{2} \vec{K} \times \hat{a}_n} \text{ always for any inf sheet}$$



( $\hat{a}_n$ )  
Five Apple

i.e for a parallel plate capacitor, find  $\vec{H}$  every where

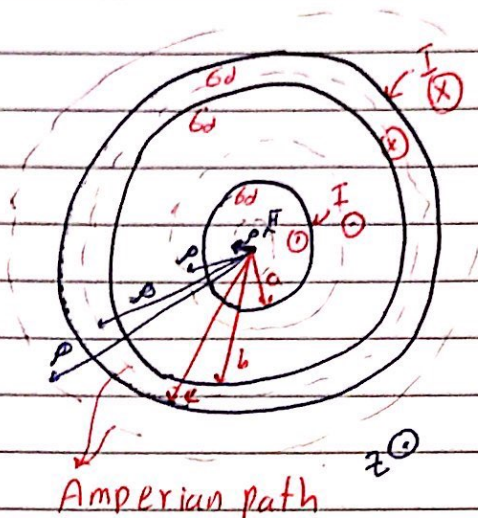


$$H \Big|_a = \vec{H}_1 + \vec{H}_2$$

$$= \frac{1}{2} K_x (-\hat{a}_x) \times a \hat{z} + \frac{1}{2} K_x \hat{a}_x \times (-a \hat{z})$$

$$= \frac{K_x}{2} a \hat{y} + \frac{K_x}{2} a \hat{y} = K_x a \hat{y}$$

3) Find  $\vec{H}$  for an infinite coaxial cable :-



$$\oint \vec{H} \cdot d\vec{L} = I_{enc}$$

for  $0 < \rho < a$

$$\vec{H} = H_\phi \hat{a}_\phi$$

$$d\vec{L} = \rho d\phi \hat{a}_\phi$$

$$\int_0^{2\pi} H_\phi \hat{a}_\phi \rho d\phi \hat{a}_\phi = I_{enc} = \int_s \vec{J} \cdot d\vec{s}$$

$$H_\phi 2\pi\rho = \int_s \vec{J} \cdot d\vec{s} \quad \text{--- (1)}$$

at  $\rho = a \rightarrow I_{enc} = I \Rightarrow I = \int_s \vec{J} \cdot d\vec{s}$

$$I = \int_0^{2\pi} \int_0^a J_z \hat{a}_z \cdot \rho d\rho d\phi \hat{a}_z$$

$$I = J_z \frac{a^2 2\pi}{2} \Rightarrow \boxed{\vec{J} = \frac{I}{\pi a^2} a \hat{z}}$$

$$H_\phi 2\pi\rho = \int_0^{2\pi} \int_0^\rho \frac{I}{\pi a^2} a \hat{z} \cdot \rho d\rho d\phi \hat{a}_z \Rightarrow H_\phi 2\pi\rho = \frac{I}{\pi a^2} \frac{\rho^2 2\pi}{2}$$

$$2\pi\rho H_\phi = \frac{I \pi \rho^2}{\pi a^2} \Rightarrow \boxed{\vec{H} = \frac{I \rho}{2\pi a^2} \hat{a}_\phi} \quad 0 < \rho < a$$

• For  $a < \rho < b$

نفس الكحل

$$\rightarrow 2\pi \rho H \phi = I_{enc} = I$$

$$*1 \quad \boxed{\bar{H} = \frac{I}{2\pi \rho} a \hat{\phi}} \quad a < \rho < b$$

• For  $b < \rho < c$

الكحل

$$\rightarrow 2\pi \rho H \phi = I_{enc} = I = \int_S \bar{J} \cdot d\vec{s} \quad \text{--- (2)}$$

at  $\rho = c \rightarrow I_{enc} = I \quad b < \rho < c$

$$I = \int_0^{2\pi} \int_b^c J_z (-a \hat{z}) \cdot \rho d\rho d\phi (-a \hat{z})$$

$$I = \frac{J_z (c^2 - b^2)}{2} 2\pi$$

$$\boxed{\bar{J} = \frac{I}{\pi (c^2 - b^2)} a \hat{z}} \quad \text{sub in (2)}$$

$$2\pi \rho H \phi = I = \int_0^{2\pi} \int_b^c \frac{I}{\pi (c^2 - b^2)} a \hat{z} \cdot \rho d\rho d\phi a \hat{z}$$

$$2\pi \rho H \phi = I = \frac{I}{\pi (c^2 - b^2)} \frac{\rho^2 - b^2}{2} 2\pi$$

$$2\pi\rho H\phi = I \left( \frac{1 - \pi(\rho^2 - b^2)}{\pi(c^2 - b^2)} \right)$$

$$*2 \quad \bar{H} = \frac{I}{2\pi\rho} \left( 1 - \frac{\rho^2 - b^2}{c^2 - b^2} \right) a\hat{\phi} \quad b \leq \rho \leq c$$

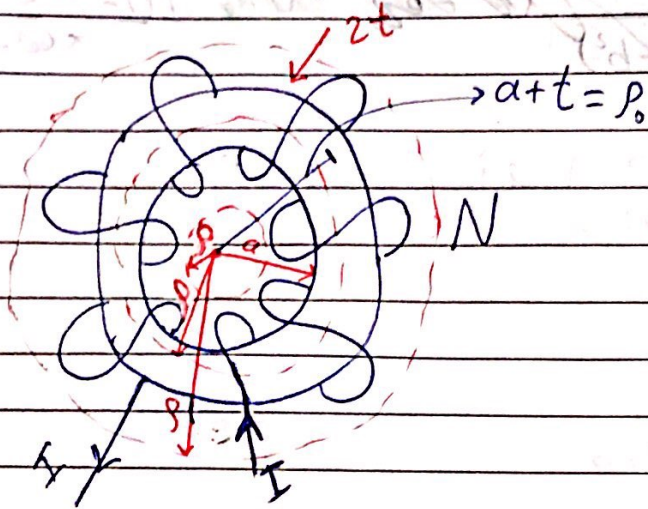
• for  $\rho > c$

$$2\pi\rho H\phi = I_{enc} = I - I = 0$$

$$*3 \quad \bar{H} = 0 \quad \rho > c$$

$$\bar{H} = \begin{cases} *1 \quad \frac{I}{2\pi\rho} a\hat{\phi}, & a \leq \rho < b \\ *2 \quad \frac{I}{2\pi\rho} \left( 1 - \frac{\rho^2 - b^2}{c^2 - b^2} \right) a\hat{\phi}, & b \leq \rho \leq c \\ *3 \quad 0, & \rho > c \end{cases}$$

4) Toroid  $\rightarrow$  Find  $H$  every where



$$0 < \rho < a \rightarrow I_{enc} = 0 \rightarrow \bar{H} = 0$$

$$\rho > a+t \rightarrow I_{enc} = I - I = 0 \rightarrow \bar{H} = 0$$

$$\text{or } \rho > \rho_0 + t$$

$$\rho_0 = a + t \quad \rho - t < \rho < \rho_0 + t$$

$$\oint_C \bar{H} \cdot d\bar{l} = I_{enc}$$

$$\bar{H} = H \hat{\phi} a \hat{\rho} \quad d\bar{l} = \rho d\phi a \hat{\phi}$$

$$2\pi \rho H a = I_{enc} = NI$$

$$\bar{H} = \frac{NI}{2\pi \rho} a \hat{\phi}$$

$$\bar{H} = \frac{NI}{\ell} a \hat{\phi}$$

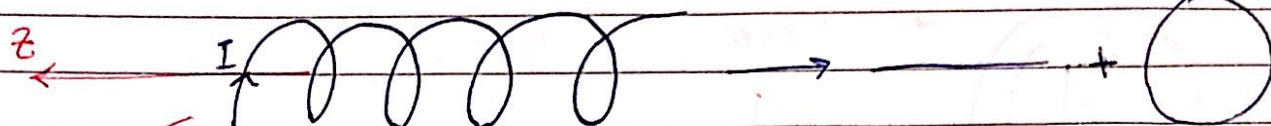
$$\bar{H} = \frac{NI}{\ell} \rightarrow \bar{H} \cdot \bar{l} = NI$$

$$\oint_C \bar{H} \cdot d\bar{l} = NI \rightarrow \text{Ampere's Law for } N\text{-turn}$$

$$\bar{H} = \frac{NI}{\ell} a \hat{\phi} = n I a \hat{\phi} \quad , \quad \frac{N}{\ell} = n \equiv \text{turns density}$$

Ex in your book (solenoid)

finite line ring



finite solenoid  $\rightarrow$  Biot-Savart's

Infinite solenoid  $\rightarrow$  Biot-Savart's  
 $\rightarrow$  Ampere's

$$\vec{H} = nI a \hat{z}$$

\* Magnetic flux density :-

$$\vec{B} = \mu_0 \vec{H} \quad , \quad \mu_0 \equiv \text{Free space permeability (H/m)} \\ = 4\pi * 10^{-7} \text{ (H/m)}$$

$$\text{unit of } \vec{B} \rightarrow \frac{\text{H}}{\text{m}} \frac{\text{A}}{\text{m}} = \frac{\text{H} \cdot \text{A}}{\text{m}^2} = \frac{\text{Wb}}{\text{m}^2} \quad , \quad \text{Wb} = \text{Weber}$$

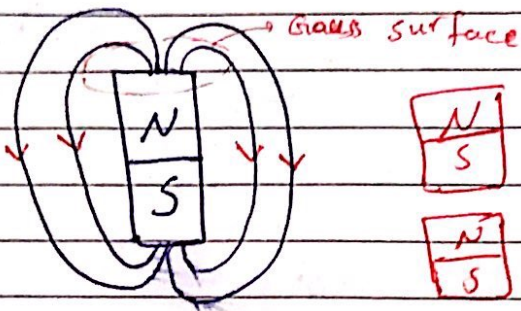
$$\text{old : } G \equiv \text{Gauss} \quad 1G = 10^{-5} \text{ T} \quad \text{T} = \text{Tesla}$$

magnetic flux :-

$$\Psi_m = \int_{SV} \vec{B} \cdot d\vec{s} \quad \text{in Wb}$$

$$\Psi_m = \oint_{SV} \vec{B} \cdot d\vec{s} \rightarrow \text{magnetic Gauss law}$$

Flux line :-



$$\Rightarrow \Psi_m = \oint_S \vec{B} \cdot d\vec{s} = 0 \text{ always}$$

Since there is no single pole magnet

4th Maxwell's eq in integral form

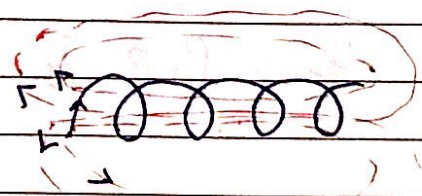
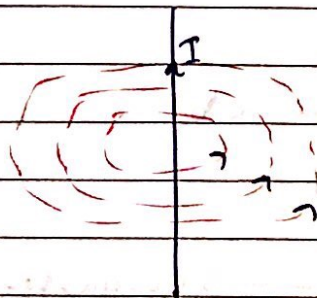
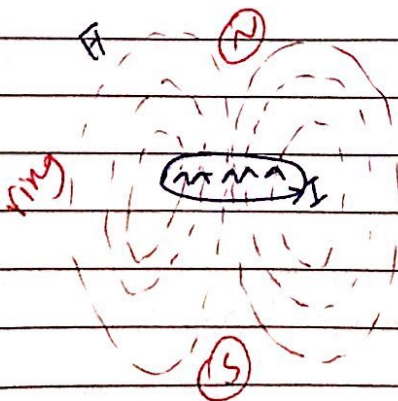
in diff form

Apply divergence theorem

$$\oint_S \vec{B} \cdot d\vec{s} = \int_{VU} \nabla \cdot \vec{B} \, dV = 0$$

$$\nabla \cdot \vec{B} = 0$$

4th Maxwell's eq in diff form





# maxwell's eq for static <sup>DC</sup> fields

integral	diff
----------	------

$\oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_v dv$	$\nabla \cdot \vec{D} = \rho_v$
---	---------------------------------

$\oint_L \vec{E} \cdot d\vec{l} = 0$	$\nabla \times \vec{E} = 0$ *
--------------------------------------	-------------------------------

$\oint_L \vec{H} \cdot d\vec{l} = I_{enc} = \int_S \vec{J} \cdot d\vec{l}$	$\nabla \times \vec{H} = \vec{J}$ *
--	-------------------------------------

$\oint_S \vec{B} \cdot d\vec{s} = 0$	$\nabla \cdot \vec{B} = 0$
--------------------------------------	----------------------------

\* Magnetic potential :-

Scalar mag potential ( $V_m$ )

Vector mag potential ( $\vec{A}$ )

maxwell

using

$$\begin{cases} \textcircled{3} \{ \nabla \times \vec{H} = \vec{J} \dots \textcircled{1} \\ \textcircled{4} \{ \nabla \cdot \vec{B} = 0 \dots \textcircled{2} \end{cases}$$

and

math identities

$$\begin{cases} \nabla \cdot (\nabla \times \vec{A}) = 0 \dots \textcircled{a} \\ \nabla \times (-\nabla V) = 0 \dots \textcircled{b} \end{cases}$$

from (1) and (b)

if  $\vec{J} = 0 \Rightarrow \boxed{\vec{H} = -\nabla V_m}$  by duality  $\vec{E} = -\nabla V$

From (2) and (a)

$$\vec{B} = \nabla \times \vec{A} \quad , \quad \vec{H} = \frac{\vec{B}}{\mu_0} \implies \vec{B} = \mu_0 \vec{H}$$

How to find  $\vec{A} = ?$   
by duality:

Line charge  $\longrightarrow$  Line current

$$V = \int_L \frac{\rho_L dl}{4\pi\epsilon_0 r}$$

$$\vec{A} = \int_L \frac{\mu_0 I dl \vec{r}}{4\pi r}$$

Surface charge  $\longrightarrow$  Surface current

$$V = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r}$$

$$\vec{A} = \int_S \frac{\mu_0 \vec{K} ds \vec{r}}{4\pi r}$$

Volume charge  $\longrightarrow$   $V = \int_V \frac{\rho_V dv}{4\pi\epsilon_0 r}$

Volume current  $\longrightarrow$   $\vec{A} = \int_V \frac{\mu_0 \vec{J} dv}{4\pi r}$  ,  $\vec{B} = \int_V \frac{\mu_0 I dl \times \vec{r}}{4\pi r^3}$

$$\vec{r} \cdot \frac{\vec{r}}{r^3} = -\nabla \left( \frac{1}{r} \right)$$

magnetic flux

$$\textcircled{1} \Psi_m = \int_S (\vec{B} \cdot \vec{ds})$$

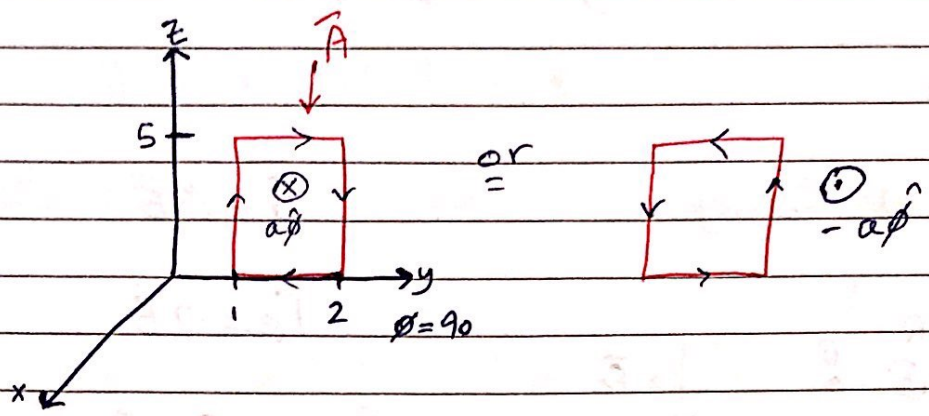
$$\Psi_m = \int_S \nabla \times \vec{A} \cdot \vec{ds}$$

Applying Stokes's Theorem:

$$\textcircled{2} \Psi_m = \int_L \vec{A} \cdot d\vec{l}$$

Ex Given  $\vec{A} = \frac{-\rho^2}{4} a_z \hat{z}$  wbm calculate the magnetic

flux crossing the surface  $\phi = \frac{\pi}{2}$   $1 \leq \rho \leq 2$ ,  $0 \leq z \leq 5$



$$\Psi_m = \oint \vec{A} \cdot d\vec{l} = \int_{L_1} \vec{A} \cdot d\vec{l}_1 + \int_{L_2} \vec{A} \cdot d\vec{l}_2 + \int_{L_3} \vec{A} \cdot d\vec{l}_3 + \int_{L_4} \vec{A} \cdot d\vec{l}_4$$

$$d\vec{l}_1 = dz a_z \hat{z} \quad d\vec{l}_2 = d\rho a_\rho \hat{\rho}$$

$$d\vec{l}_3 = (-) dz a_z \hat{z} \quad d\vec{l}_4 = (-) d\rho a_\rho \hat{\rho}$$

$$\Psi_m = \int_{z=0}^5 \int_{\rho=1}^2 \frac{-\rho^2}{4} a_z \hat{z} \cdot dz a_z \hat{z} + \int_{z=0}^5 \int_{\rho=1}^2 \frac{-\rho^2}{4} a_z \hat{z} \cdot dz a_z \hat{z}$$

$$= -\frac{1}{4} (5) - 1 (-5) = -\frac{5}{4} + 5 = \frac{15}{4} \text{ wb}$$

method (2)

$$\Psi_m = \int_S \vec{B} \cdot d\vec{s} \quad \vec{B} = \nabla \times \vec{A} = \frac{1}{\rho} \begin{vmatrix} a_\rho & \rho a_\phi & a_z \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ \frac{A_\rho}{\rho} & \rho A_\phi & A_z \end{vmatrix}$$

$$\vec{B} = \frac{1}{\rho} \left[ \frac{\rho}{2} \rho a_\phi \hat{\phi} \right] \Rightarrow \Psi_m = \int_0^5 \int_1^2 \frac{\rho}{2} a_\phi \hat{\phi} \cdot d\rho dz a_\phi \hat{\phi}$$

$$\Rightarrow = \frac{4-1}{4} (5) = \frac{15}{4} \text{ wb}$$

\*CH8: magnetic force and magnetic materials :-

There are 3 cases for magnetic forces,

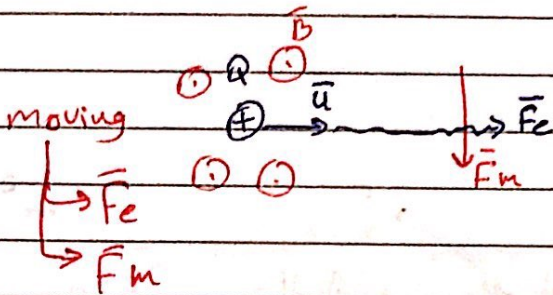
1) The force in a moving charged particle

charge

static  $\oplus$   $\vec{F}_e$  only

$$\vec{u} = M\vec{E}$$

$$\vec{F}_e = q\vec{E}$$



$$\vec{F}_m = q\vec{u} \times \vec{B} \quad \begin{matrix} u \neq 0 \\ B \neq 0 \end{matrix}$$

R.H.R

$$\vec{F} = \vec{F}_e + \vec{F}_m \quad \text{if } \vec{E} \neq 0, B \neq 0, u \neq 0$$

$$\boxed{\vec{F} = q(\vec{E} + \vec{u} \times \vec{B}) = m\vec{a}}$$
 Lorentz's force of law

special case if  $\vec{E} \neq 0$   $B \neq 0$  but  $u$ 's uniform  $a=0$

$$\vec{F}_e + \vec{F}_m = 0$$

$$\vec{F}_e = -\vec{F}_m$$

$$q\vec{E} = -q\vec{u} \times \vec{B}$$

$$E = Bv$$

$$\vec{E} = B \times \vec{u}$$

$$\boxed{u = \frac{E}{B}} \quad \text{if } a=0$$

$$K.E = \frac{1}{2} m |\bar{u}|^2 \text{ (J)}$$

$\bar{F}_e$  will affect K.E

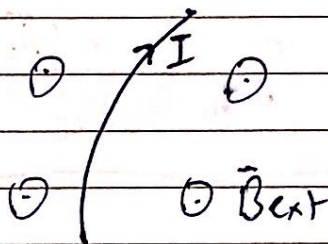
$\bar{F}_m$  will not affect K.E

$\bar{F}_e \gg \bar{F}_m$  unless  $\bar{u}$  is very large

2) the force on a current element  $\left( \begin{array}{l} 1D \text{ segment} \\ 2D \text{ surface} \\ 3D \text{ object} \end{array} \right)$

assume  $\bar{E}_{ext} = 0$

$\bar{F}_m = ?$



\*  $\bar{F}_m = q \bar{u} \times \bar{B}$   $\rightarrow$  moving point charge

\*  $I d\bar{l} = \bar{K} ds = \bar{J} dv$

\*  $\bar{J} = \rho v \bar{u}$     \*  $q = \int \rho v dv$

$$d\bar{F}_m = (dq) \bar{u} \times \bar{B}$$

$$dq = \rho v dv$$

$$d\bar{F}_m = (\rho v) dv \bar{u} \times \bar{B}$$

$$d\bar{F}_m = (\bar{J} / v) \times \bar{B} dv$$

$$d\bar{F}_m = I d\bar{l} \times \bar{B} = \bar{K} ds \times \bar{B}$$

$$\bar{F}_m = \oint I d\bar{l} \times \bar{B}$$

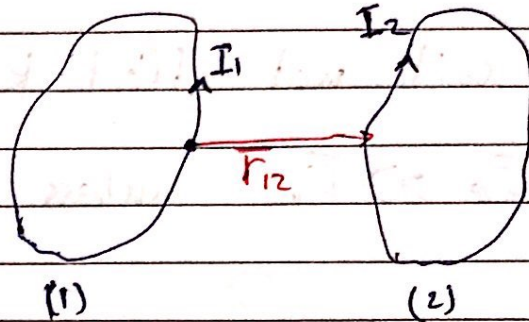
$$\bar{F}_m = \oint \bar{K} ds \times \bar{B}$$

$$\bar{F}_m = \int \bar{J} dv \times \bar{B}$$

3) The force between two current elements :-

$\vec{F}_{12}$  = The force on (2) due to (1)

$$\vec{F}_{12} = \int_{L_2} I_2 d\vec{L}_2 \times \vec{B}_1$$



$$\vec{B}_1 = \int_{L_1} \frac{\mu_0 I_1 d\vec{L}_1 \times \vec{r}_{12}}{4\pi r_{12}^3}$$

,  $\vec{r}_{12} = (2) - (1)$   
coordinates

$$\vec{F}_{12} = \frac{\mu_0 I_1 I_2}{4\pi} \oint_{L_2} \oint_{L_1} \frac{d\vec{L}_2 \times (d\vec{L}_1 \times \vec{r}_{12})}{r_{12}^3} \quad (N)$$

for force between two surface currents :-

$$\vec{F}_{12} = \int_{S_2} \int_{S_1} \frac{\mu_0 \vec{K}_2 \times (\vec{K}_1 \times \vec{r}_{12})}{4\pi r_{12}^3} ds_1 ds_2$$

$$\vec{B}_1 = \int_{S_1} \frac{\mu_0 \vec{K}_1 \times \vec{r}_{12}}{4\pi r_{12}^3} ds_1$$

$$\vec{F}_{12} = \int_{S_2} \vec{K}_2 ds_2 \times \vec{B}_1$$

Ex A charged particle of mass  $2\text{ kg}$  and charge  $3\text{ C}$  starts at point  $(1, -2, 0)$  with the velocity  $(4\hat{a}_x + 3\hat{a}_z \text{ m/s})$  in  $\vec{E} = 12\hat{a}_x + 10\hat{a}_y \text{ V/m}$ . At time  $t = 1\text{ s}$ , find:-

a)  $\vec{a}$ , b)  $\vec{u}$ , c) K.E, d) position

$$\vec{F} = Q\vec{E}_{\text{ext}} + Q\vec{u} \times \vec{B}_{\text{ext}} = m\vec{a}$$

$$Q\vec{E} = m\vec{a} \rightarrow \vec{a} = \frac{Q}{m}\vec{E} = \frac{3}{2}(12, 10, 0)$$

$$\vec{a} = 18\hat{a}_x + 15\hat{a}_y \text{ m/s}^2$$

$$\vec{a} = \frac{d\vec{u}}{dt} \quad \text{vector diff equ}$$

$$a_x = \frac{du_x}{dt} \rightarrow \int du_x = \int a_x dt$$

$$u_x = 18t + c_1$$

$$a_y = \frac{du_y}{dt} \rightarrow u_y = 15t + c_2$$

$$a_z = \frac{du_z}{dt} \rightarrow u_z = c_3$$

Find  $c_1, c_2, c_3$

$$\text{I.C } \vec{u}(t=0) = (4, 0, 3)$$

$$u_x(t=0) = \boxed{4 = c_1} \quad \boxed{c_2 = 0} \quad \boxed{c_3 = 3}$$

$$\vec{u}(t) = (18t + 4, 15t, 3) \text{ m/s}$$

$$u(15) = 22a\hat{x} + 15a\hat{y} + 3a\hat{z} \text{ m/s}$$

$$c) K.E \Big|_{t=1} = \frac{1}{2}(2)(22^2 + 15^2 + 3^2) \text{ J} = 7.16 \text{ J}$$

$$K.E \Big|_{t=0} = \frac{1}{2}(2)(25) = 25 \text{ J}, \quad \therefore \vec{F}_c \text{ affect } K.E$$

d)  $\vec{L}$ ?

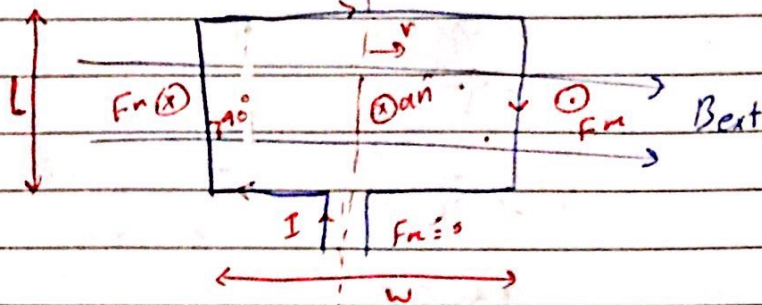
$$\vec{u} = \frac{d\vec{L}}{dt} \quad \text{or} \quad \vec{a} = \frac{d^2\vec{L}}{dt^2}$$



\* Magnetic Torque ( $\vec{T}$ ) and moment ( $\vec{m}$ ) :-

$$\vec{T} = \vec{r} \times \vec{F} \quad \text{in (N.m)}$$

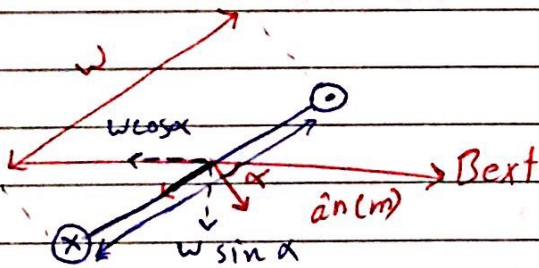
✓ Ax for rotation:  $F_m = 0 \Rightarrow \vec{r} \parallel \vec{B}$



$$\vec{F}_m = \oint I d\vec{l} \times \vec{B}$$

if uniform  $\vec{F} = I \vec{L} \times \vec{B}$

$$\vec{F}_{\text{total (net)}} = 0$$



$$\vec{T} = \vec{r} \times \vec{F}$$

$$T = rF$$

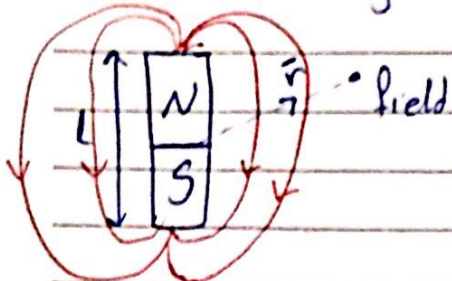
$$= w I L B \sin \alpha \Rightarrow T = I B S \sin \alpha$$

$$\boxed{\vec{T} = \vec{m} \times \vec{B}} = m B \sin \alpha$$

define  $\vec{m} \equiv$  <sup>mag</sup> dipole moment (duality  $\underline{p} \rightarrow$  <sup>elec</sup> dipole moment)  
 $\vec{m} = I S \hat{n}$

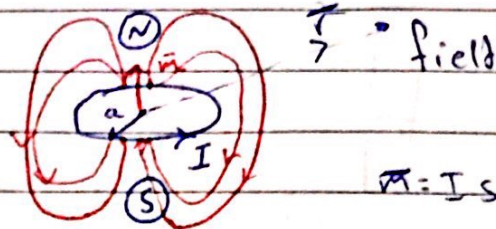
\* magnetic dipoles

Small bar magnet



$L \ll r$

Small loop carrying current



$a \ll r$

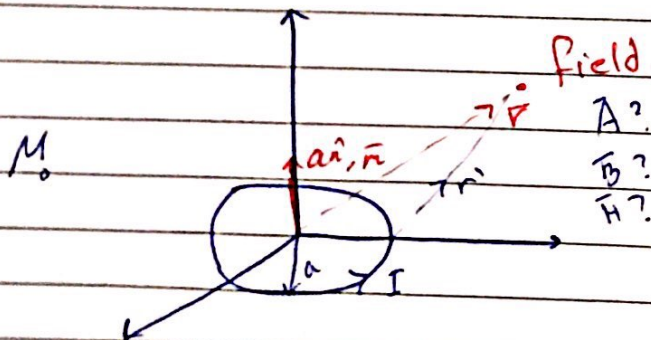
$\vec{m} = I S \hat{n}$   
 $S = \pi a^2$

$\vec{T} = \vec{m} \cdot \vec{B}$

$\vec{m} = \frac{I \vec{m} \times \vec{B}}{|\vec{B}|}$

$\vec{T} = \vec{m} \times \vec{B}_{ext}$

• for a small loop of current where  $a \ll r$

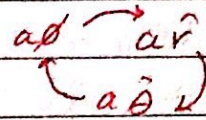


$\vec{A} = \int \frac{\mu_0 I d\vec{l}}{4\pi r}$   $\Rightarrow$  Binomial expansion

$r \rightarrow r'$

Duality from electric dipole

$$\vec{A} = \frac{\mu_0 \vec{m} \times \hat{a}_r}{4\pi r^2} \quad (\text{V in elec dipole})$$



$$\vec{A} = \frac{\mu_0 I \pi a^2 \sin\theta}{4\pi r^2} a_\theta$$

$$\vec{m} = I S a \hat{a}_z$$

$$= I \pi a^2 a \hat{a}_z \quad ; \quad \hat{a}_z = \cos\theta \hat{a}_r - \sin\theta \hat{a}_\theta + 0 \hat{a}_\phi$$

$$\vec{B} = \nabla \times \vec{A} = \frac{1}{r^2 \sin\theta} \begin{vmatrix} \hat{a}_r & r \hat{a}_\theta & r \sin\theta \hat{a}_\phi \\ \partial/\partial r & \partial/\partial \theta & \partial/\partial \phi \\ A_r & r A_\theta & r \sin\theta A_\phi \end{vmatrix}$$

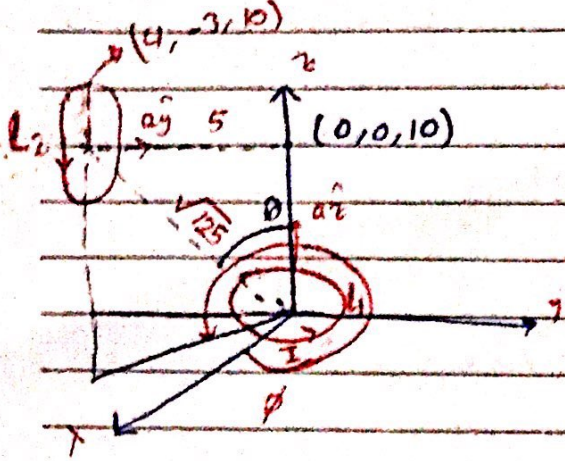
$$\vec{B} = \frac{1}{r^2 \sin\theta} \cdot \frac{\mu_0 I a^2}{4\pi} \left( \frac{2 \sin\theta \cos\theta}{r^2} \hat{a}_r - \frac{(-1) \sin^2\theta}{r^2} r \hat{a}_\theta \right)$$

$$\vec{B} = \frac{\mu_0 I \pi a^2}{4\pi r^3} [ 2 \cos\theta \hat{a}_r + \sin\theta \hat{a}_\theta ]$$

$$\vec{B} = \frac{\mu_0 m}{4\pi r^3} ( 2 \cos\theta \hat{a}_r + \sin\theta \hat{a}_\theta ) \quad \text{wb/m}^2$$

$$\vec{H} = \frac{\vec{B}}{\mu_0}$$

Ex: a small loop ( $L_1$ ) with  $\vec{m} = 5a\hat{z}$  A.m<sup>2</sup> located at the origin while another small loop ( $L_2$ ) located at  $(4, -3, 10)$  with  $\vec{m} = 3a\hat{y}$  A.m<sup>2</sup> find the Torque on  $L_2$ ?



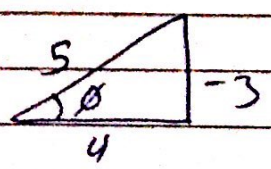
$$\vec{T}_2 = \vec{m}_2 \times \vec{B}_1$$

$$\vec{B}_1 = \frac{\mu_0 (5)}{4\pi (\sqrt{125})^3} \left( \frac{2 \cdot 10 a\hat{r}}{\sqrt{125}} + \frac{5}{\sqrt{125}} a\hat{z} \right)$$

$$\vec{m}_2 = 3a\hat{y} = 3 \left( \sin\theta \sin\phi a\hat{r} + \cos\theta \sin\phi a\hat{\theta} + \cos\phi a\hat{\phi} \right)$$

$$\frac{5}{\sqrt{125}} \quad \frac{10}{\sqrt{125}}$$

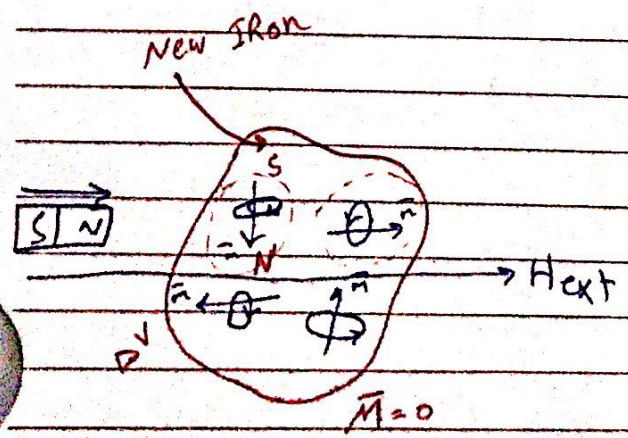
$$\tan\phi = \frac{y}{x} = \frac{-3}{4}$$



$$\sin\phi = \frac{-3}{5}$$

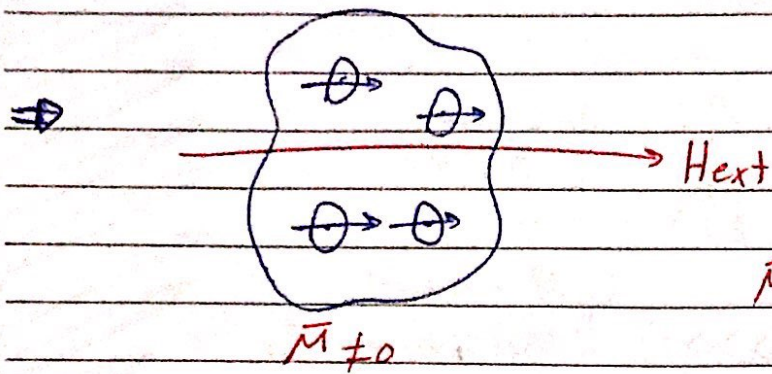
$$\cos\phi = \frac{4}{5}$$

\* magnetization in materials



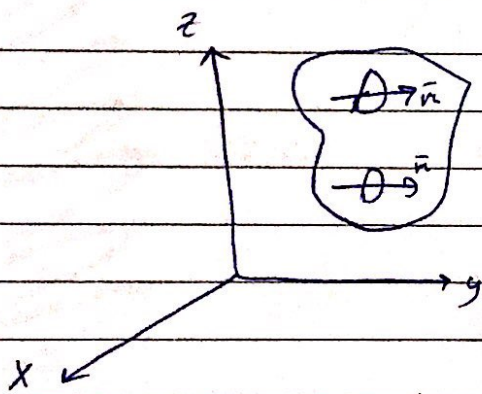
$$\vec{M} = \lim_{\Delta V \rightarrow 0} \sum_{k=1}^N \vec{m}_k$$

$\vec{F}$  will affect K.E



$\vec{M}_s \equiv$  saturation magnetization

• for a magnetized material, -



• field

$\vec{A}?$

B?  $\vec{B} = \nabla \times \vec{A}$

H?  $\vec{H} = \frac{\vec{J}}{m_0}$

duality

$$\begin{aligned} \rho_{ps} &= \nabla \cdot \vec{a} \hat{u} \\ \rho_{pv} &= -\nabla \cdot \vec{P} \end{aligned}$$

$$\begin{aligned} \vec{K}_b &= \vec{M} \times \hat{a} \hat{u} \\ \vec{J}_b &= \nabla \times \vec{M} \end{aligned}$$

Free  $(\rho_s, \rho_v), (\rho_{ps}, \rho_{pv})$   
bound  $(\vec{K}, \vec{J}), (\vec{K}_b, \vec{J}_b)$

$\vec{K}_b =$  bound (magnetized) surface current density (A/m)

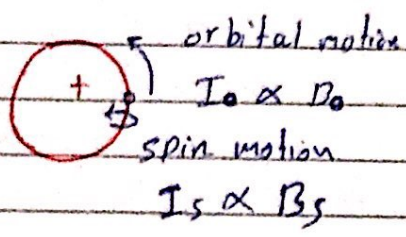
$\vec{J}_b =$  " " volume " " (A/m<sup>2</sup>)

for some material  $\left[ \begin{array}{l} \text{linear} \\ \text{isotropic} \end{array} \right.$

$$\vec{M} = \chi_m \vec{H}, \quad \vec{P} = \chi_e \epsilon_0 \vec{E}$$

## Types of magnetic materials:-

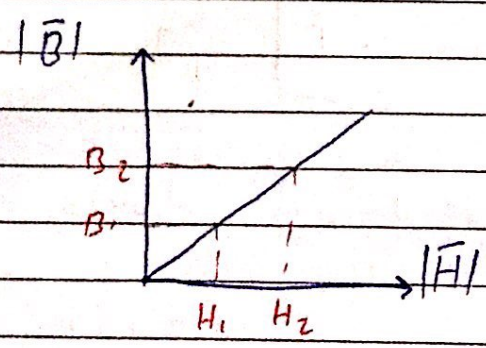
→ Dia magnetic ( $M_r \approx 1$ )	} Linear	$\vec{B} = \mu_0 \mu_r \vec{H}$
Cu, Al, Au, ...		
→ Para magnetic ( $M_r \approx 1$ )	} Non linear	$\vec{B} = \mu_0 \mu_r \vec{H}$
Air, ...		
→ Ferro magnetic ( $M_r \gg \gg 1$ )		$\vec{B} = \mu_0 \mu_r \vec{H}$
Iron, Nickel, Cobalt, ...		only at point



Diamagnetic  
 ↪  $B_o$  cancel  $B_s$

Ferromagnetic  
 ↪  $B_o$  in-phase with  $B_s$

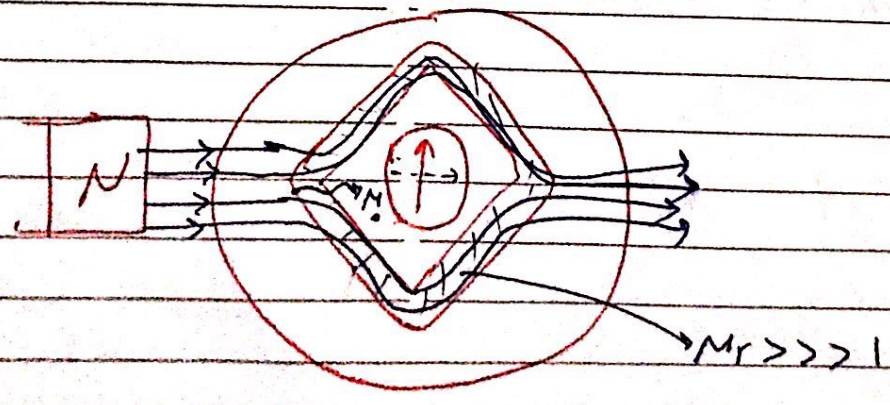
## • B/H curve (For linear material)

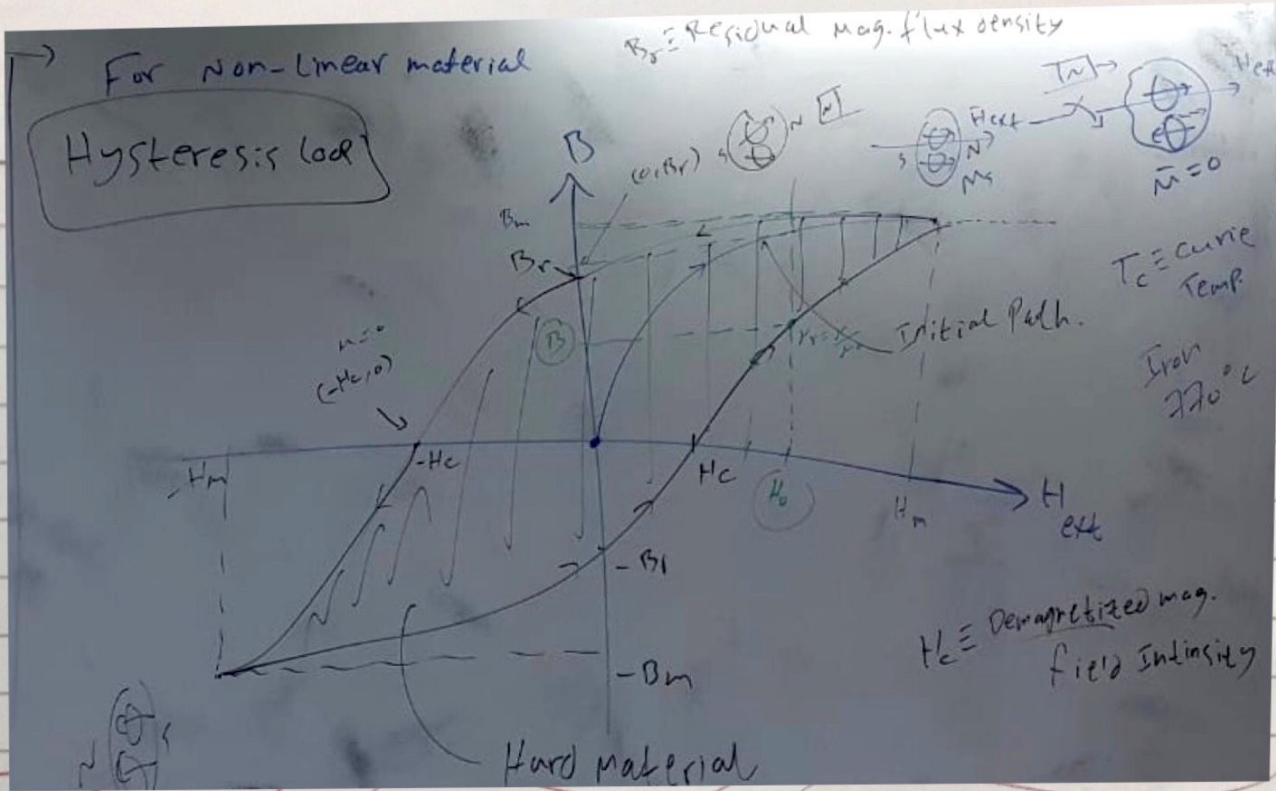


$$\mu = \frac{B_2 - B_1}{H_2 - H_1} = \mu_0 \mu_r$$

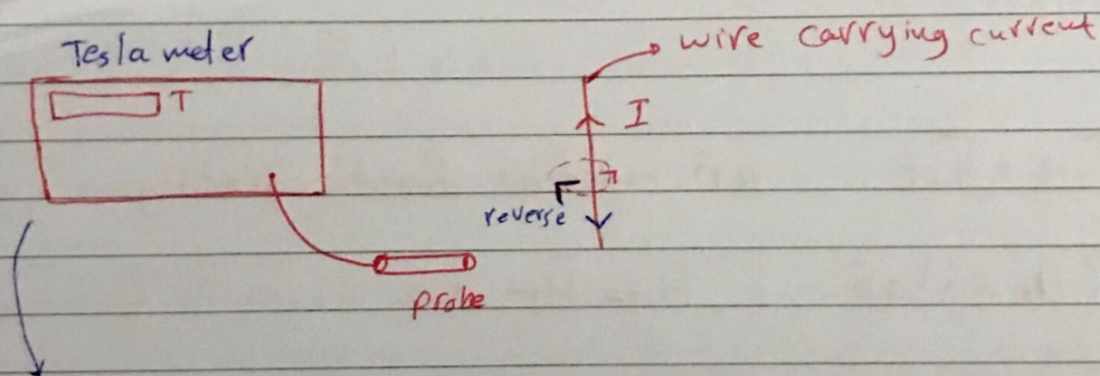
$$\mu_0 = 4\pi \times 10^{-7}$$

(For non-linear material) → Next Page





To measure B earth?



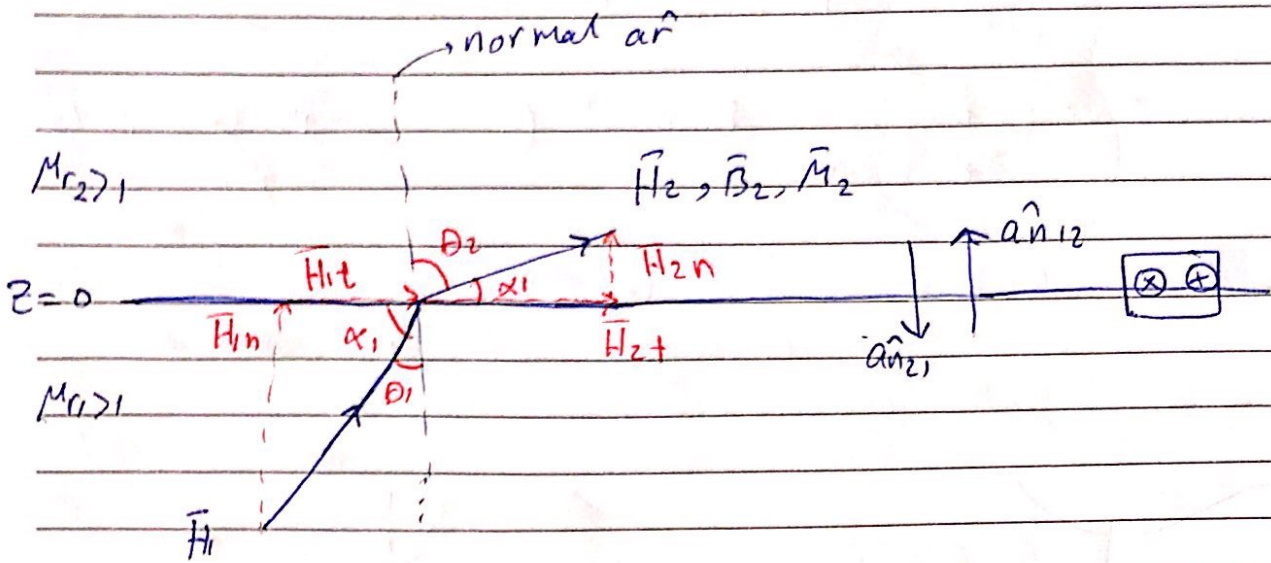
$$B_1 = B_{\text{wire}} + B_{\text{earth}}$$

reverse the current

$$B_2 = (-) B_{\text{wire}} + B_{\text{earth}}$$

$$\frac{B_1 + B_2}{2} = B_{\text{earth}}$$

\* mag Boundary condition =



$$\vec{B}_1 = \mu_0 M_1 \vec{H}_1$$

$$\vec{M}_1 = (M_1 - 1) \vec{H}_1$$

$\vec{H}_1 = \vec{H}_{1n} + \vec{H}_{1t}$       $\hat{a}_n$  must be found correctly

$\vec{H}_{1n} = (\vec{H}_1 \cdot \hat{a}_n) \hat{a}_n$  ,  $\vec{H}_{1t} = \vec{H}_1 - \vec{H}_{1n}$

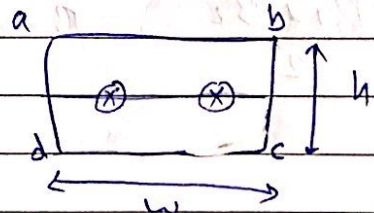
or  $\vec{H}_{2t} = H_1 \sin \theta_1 \hat{a}_{n2}$       $H_{1n} = H_1 \cos \theta_1$

$\theta_1 = \sin^{-1} \frac{H_{1t}}{H_1}$       $\alpha_1 = 90^\circ - \theta_1$

to find  $\vec{H}_2 \rightarrow$  B.C

$\vec{H}_2 = \vec{H}_{2n} + \vec{H}_{2t} \rightarrow$  2 B.C

$\oint \vec{H} \cdot d\vec{l} = I_{enc}$  ,  $\oint \vec{B} \cdot d\vec{s} = 0$





$$\int_a^b \vec{H} \cdot d\vec{l}_1 + \int_b^c \vec{H} \cdot d\vec{l}_2 + \int_c^d \vec{H} \cdot d\vec{l}_3 + \int_d^a \vec{H} \cdot d\vec{l}_4 = Kw$$

$$H_{2t} w - H_{2n} \frac{w}{2} - H_{1n} \frac{w}{2} - H_{1t} w + H_{1n} \frac{w}{2} + H_{2n} \frac{w}{2} = Kw$$

$$H_{2t} - H_{1t} = K \rightarrow \text{scaler}$$

↓  
given

$$\text{if } K=0$$

$$H_{2t} = H_{1t}$$

$$H_{2t} - H_{1t} = K$$

$$*(\vec{H}_2 - \vec{H}_1) \times \hat{n}_2 = \vec{K}$$

$$\text{or } *(\vec{H}_1 - \vec{H}_2) \times \hat{n}_{12} = \vec{K}$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{M_{r1}}{M_{r2}}$$

if  $\vec{K} = 0$

to find  $H_{2n}$  ?

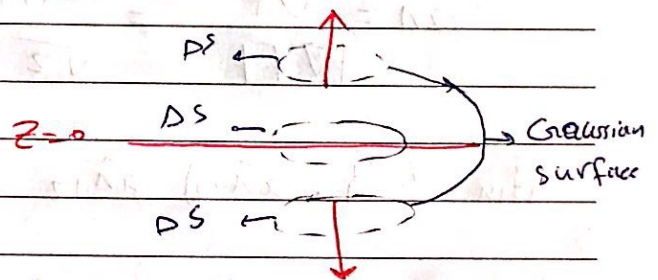
Use  $\oint \vec{B} \cdot d\vec{s} = 0$

$$\int_{s_{top}} \vec{B} \cdot d\vec{s} + \int_{s_{bot}} \vec{B} \cdot d\vec{s} = 0$$

$$B_{2n} \Delta s - B_{1n} \Delta s = 0$$

$$B_{2n} = B_{1n} \text{ always}$$

$$H_{2n} = \frac{M_{r1}}{M_{r2}} H_{1n}$$

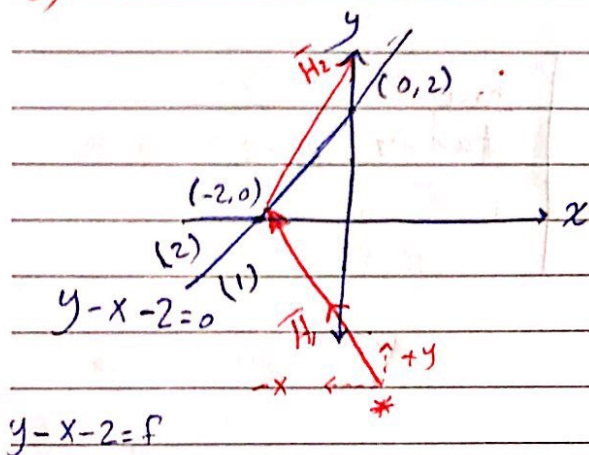


Given that  $\vec{H}_1 = -2ax\hat{x} + 6ay\hat{y} + 4az\hat{z}$  A/m in region  $y-x-2 \leq 0$  where  $\mu_1 = 5\mu_0$  calculate:

a)  $\vec{B}_1$  and  $\vec{M}_1$       b)  $\vec{H}_2$  and  $\vec{B}_2$  in region  $y-x-2 \geq 0$   
if  $\mu_2 = 2\mu_0$

a)  $\vec{B}_1 = \mu_0 \mu_{r1} \vec{H}_1 = (-10, 30, 20) \text{ mT}$   
 $\vec{M}_1 = (\mu_{r1} - 1)\vec{H}_1 = 4\vec{H}_1 = (-8, 24, 16) \text{ A/m}$

b)



$$a\hat{n} = \frac{\nabla f}{|\nabla f|} = \frac{(-1, 1, 0)}{\sqrt{2}} \Rightarrow a\hat{n}_{12} = \frac{-1}{\sqrt{2}} a\hat{x} + \frac{1}{\sqrt{2}} a\hat{y}$$

$$\vec{H}_{1n} = (\vec{H}_1 \cdot a\hat{n}_{12}) a\hat{n}_{12} = (-4, 4, 0) \text{ A/m}$$

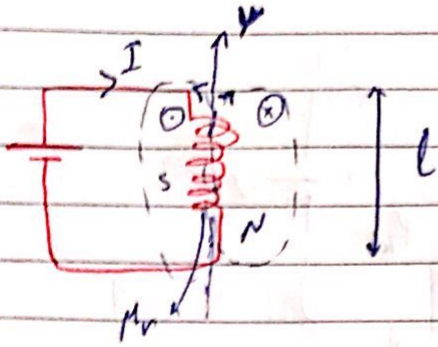
$$\vec{H}_{1t} = \vec{H}_1 - \vec{H}_{1n} = (2, 2, 4) \text{ A/m} \Rightarrow H_{2t} \quad (\text{since } \vec{K} = 0)$$

$$\vec{H}_{2n} = \frac{\mu_{r1}}{\mu_{r2}} \vec{H}_{1n} \quad (\vec{B}_{1n} = \vec{B}_{2n}) = \frac{5}{2} (-4, 4, 0) = (-10, 10, 0)$$

$$\vec{H}_2 = \vec{H}_{2n} + \vec{H}_{2t} = -8a\hat{x} + 12a\hat{y} + 4a\hat{z} \text{ A/m}$$

$$\vec{B}_2 = 2\mu_0 \vec{H}_2, \quad \vec{M}_2 = \vec{H}_2$$

## \* Inductors (L)



$$I \propto B \propto \Psi \propto \lambda, \quad \lambda = \text{flux linkage} \quad \lambda = N \Psi \text{ in (wb)}$$

$\lambda \propto I$  = relation

$$\lambda = L I$$

→ proportionality constant

(Inductance)

$$\textcircled{1} \quad L = \frac{\lambda}{I} = \frac{N \Psi}{I} \quad (\text{H}) \text{ henry}$$

• magnetic energy ( $W_m$ ) in (J)

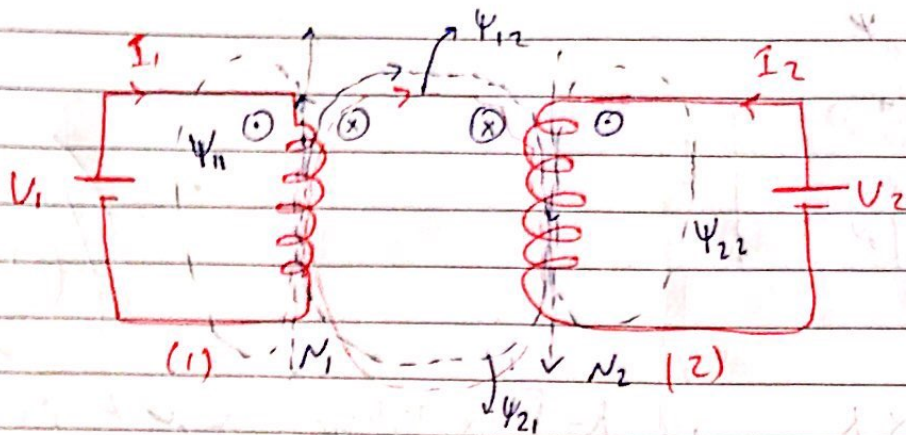
$$W_m = \frac{1}{2} \int_V \vec{H} \cdot \vec{B} \, dV = \frac{1}{2} \int_V \mu H^2 \, dV = \frac{1}{2} \int_V \frac{B^2}{\mu} \, dV$$

$$\boxed{W_m = \frac{1}{2} L I^2} \quad \text{in uniform} \quad \textcircled{2} \quad L = \frac{2 W_m}{I^2}$$

$$w_m = \frac{W_m}{\text{Vol}} \quad (\text{J/m}^3)$$

↓  
mass energy density

## \* Self Inductance and mutual Inductance



$\Psi_{11}$ ,  $\Psi_{22} \equiv$  self flux  
(kt)  $\rightarrow$   $\frac{N_1}{N_2}$  current  $\rightarrow$

$\Psi_{12}$ ,  $\Psi_{21} \equiv$  mutual flux

### Self Inductance

$$L_{11} = \frac{k_{11}}{I_1} = \frac{N_1 \Psi_{11}}{I_1}$$

$$L_{22} = \frac{k_{22}}{I_2} = \frac{N_2 \Psi_{22}}{I_2}$$

### mutual Inductance

$$M_{12} = \frac{k_{12}}{I_2} = \frac{N_1 \Psi_{12}}{I_2}$$

$$M_{21} = \frac{k_{21}}{I_1} = \frac{N_2 \Psi_{21}}{I_1}$$

total Inductance

$$L_1 = L_{11} + M_{12} \Rightarrow L_1 = \frac{N_1 \Psi_1}{I_1}$$

total flux

$$\Psi_1 = \Psi_{11} \oplus \Psi_{12}$$

same  
opposit

CKT  
NO

$$W_m = \frac{1}{2} L_{11} I_1^2 + \frac{1}{2} L_{22} I_2^2$$

$$\pm \frac{1}{2} (M_{12} I_2^2 + M_{21} I_1^2) \text{ (J)}$$

$$\text{if } M_{12} = M_{21} \Rightarrow \frac{I_1}{I_2} = \frac{N_2}{N_1}$$

procedure to find (L) or (M)

1) choose a suitable coordinates

2) Assume currents  $\rightarrow \vec{I}$

3) find  $\vec{B}$  (Biot savart's law, Amperes law, mag Pot) CH7

$$4) \Psi = \int_S \vec{B} \cdot \vec{dS}$$

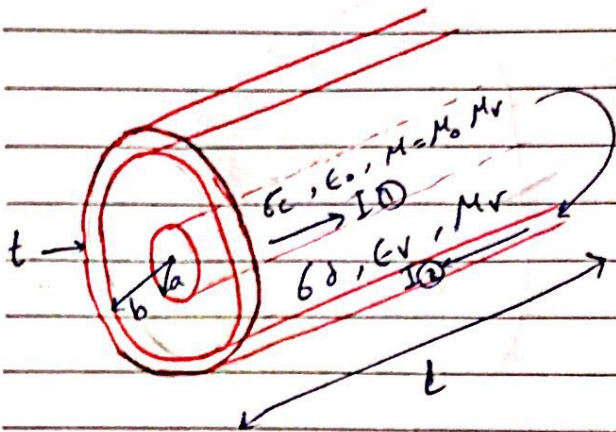
$$W_m = \frac{1}{2} \int_V \frac{B^2}{\mu} dv$$

$$5) \Phi = N \Psi$$

$$6) L = \frac{N \Psi}{I}$$

$$L = \frac{2 W_m}{I^2}$$

Ex 8 Find the self Inductance for a coaxial cable shown?



$$\vec{B} = \begin{cases} \frac{\mu I \rho \hat{\phi}}{2\pi a^2}, & 0 \leq \rho \leq a \\ \frac{\mu I \hat{\phi}}{2\pi \rho}, & a \leq \rho \leq b \\ \times \frac{I}{2\pi \rho} (-\hat{\phi}), & b \leq \rho \leq c \\ \times 0, & \rho > c \end{cases}$$

self Inductance

$$L = L_{int} + L_{ext} \quad \text{for } L_{int} \text{ (use } L = \frac{2W}{I^2} \text{)}$$

$$W_{int} = \frac{1}{2} \int_0^L \int_0^{2\pi} \int_0^a \frac{\mu^2 I^2 \rho^2}{4\pi^2 a^4} \rho d\rho d\phi dz$$

$$\frac{\mu I^2}{48\pi^2 a^4} \left(\frac{a^4}{4}\right) (2\pi)(L) = \frac{\mu I^2 L}{16\pi}$$

$$L_{int} = \frac{\mu L}{8\pi} \text{ H} \Rightarrow L_{int}/L = \frac{\mu}{8\pi} \text{ (H/m)}$$

$L_{ext}$  (use  $L = \frac{N\psi}{I}$ )  
 $a \leq \rho \leq b$

$$\psi = \int_s \vec{B} \cdot d\vec{s} \Rightarrow \psi = \int_0^L \int_a^b \frac{\mu I}{2\pi \rho} a \hat{\phi} d\rho dz a \hat{\phi}$$

$$= \frac{\mu I L}{2\pi} \ln\left(\frac{b}{a}\right) \quad \text{w/o } (N=1 \text{ turn}) \Rightarrow L_{ext}/L = \frac{\mu \ln\left(\frac{b}{a}\right)}{2\pi} \text{ (H/m)}$$

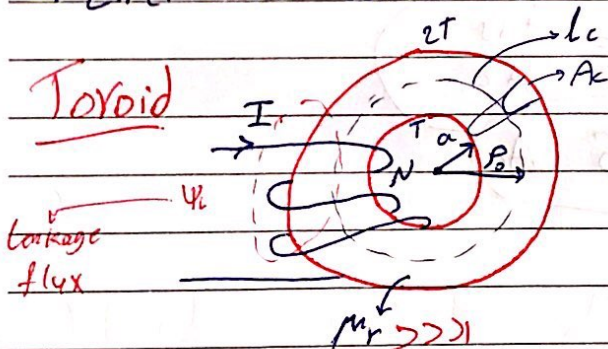
$$L = \frac{\mu}{2\pi} \left[ \frac{1}{4} + \ln\left(\frac{b}{a}\right) \right] \text{ H/m}$$

\* Magnetic Circuits :-

elec ckt	mag ckt
$V_{emf} \equiv V \left(\frac{1}{I}\right)$	$V_{mmf} \equiv F \left(\frac{1}{\Psi}\right)$
$I$	$\Psi$
$R = \frac{V}{I} = \frac{L}{\sigma A}$ (ohm's)	$R_m = \frac{F}{\Psi} = \frac{l}{\mu A_c}$ (ohm's)
$G$	$M$
$G = \frac{1}{R}$	$P = \frac{1}{R_m}$ $\rightarrow$ Permeance

\* magnetic structure :- (Gapless circuit)

- ↳ mag core ( $l_c, A_r, \mu_s$ )
- ↳ Excitation coil ( $I, N$ )



$l_c =$  Average length of the core

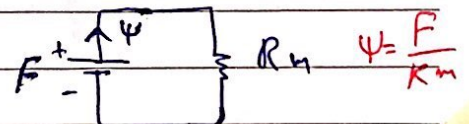
$$l_c = 2\pi r_0 \rightarrow a+t$$

$A_c =$  cross section Area of the core

$$R_m = \frac{l_c}{\mu_0 \mu_r A_c} = \frac{l}{\mu} = H^{-1}$$

$$A_c = \pi r^2$$

(mag resistance) Reluctance

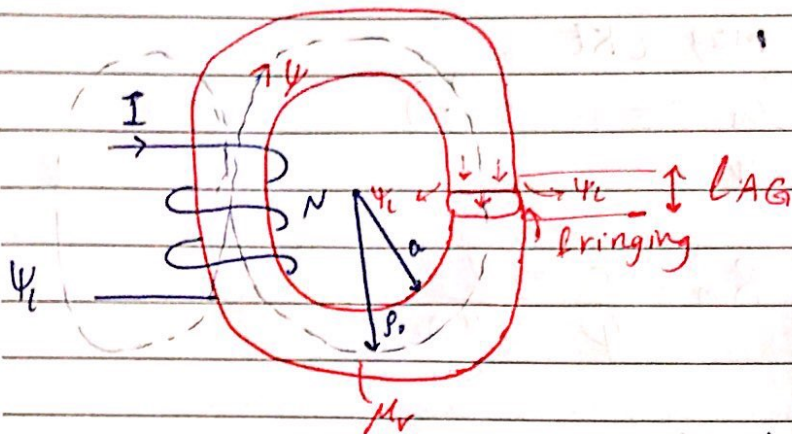


$$V_{mmf} = F = NI \equiv A \cdot t$$

$$= \Psi R_m \rightarrow \oint \vec{H} \cdot d\vec{l} = NI = Hl \text{ if uniform}$$

$$= Hl$$

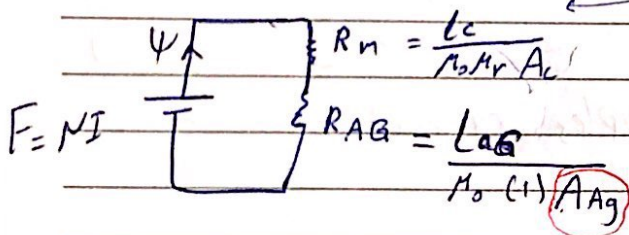
\* magnetic structure with Air gap



$L_{AG} = 0.5 \text{ cm} \rightarrow 1.5 \text{ cm}$

$L = 2\pi r_0$

$L_c = 2\pi r_0 - L_{AG}$



$R_m = \frac{L_c}{\mu_0 \mu_r A_c}$

$R_{AG} = \frac{L_{AG}}{\mu_0 (1) A_{Ag}}$

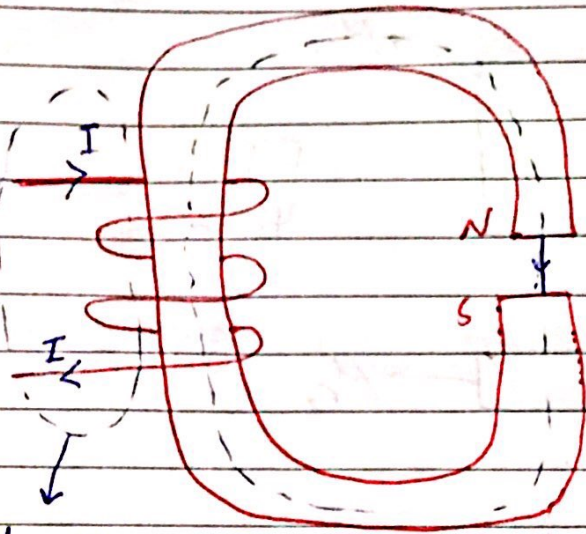
$R_{eq} = R_m + R_{AG}$

$\Phi = \frac{F}{R_{eq}}$

$FF = \text{Fringing Factor} \geq 1 \quad FF = \frac{A_{Ag}}{A_c}$

$FF = 1.5 \quad A_{Ag} = 1.5 A_c$





Leakage flux

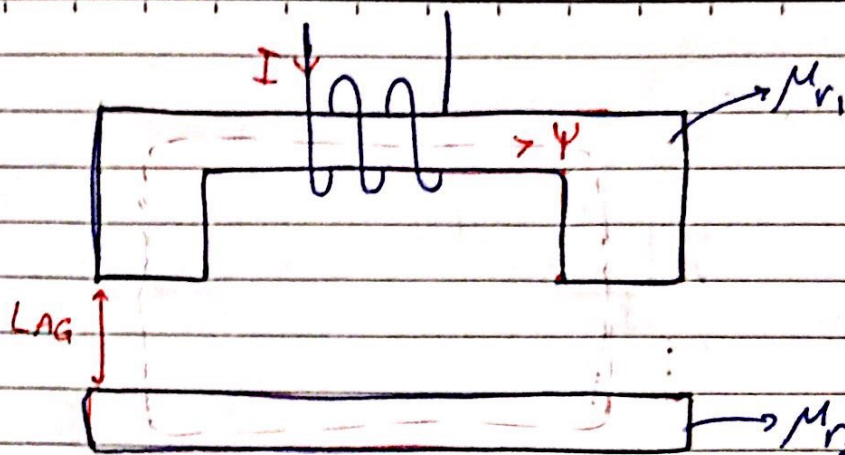
From  $I \rightarrow B \rightarrow \psi$    
 —————   
 → leakage   
 ↘ core

Force in the airgap

$F_{MT} \equiv$  magnetic fraction force

$$\text{air} \leftarrow = \frac{(-) B^2 A_c}{2 \mu_0} \quad \text{in one airgap}$$

$$\text{pressure} = \frac{F_{MT}}{A_c}$$

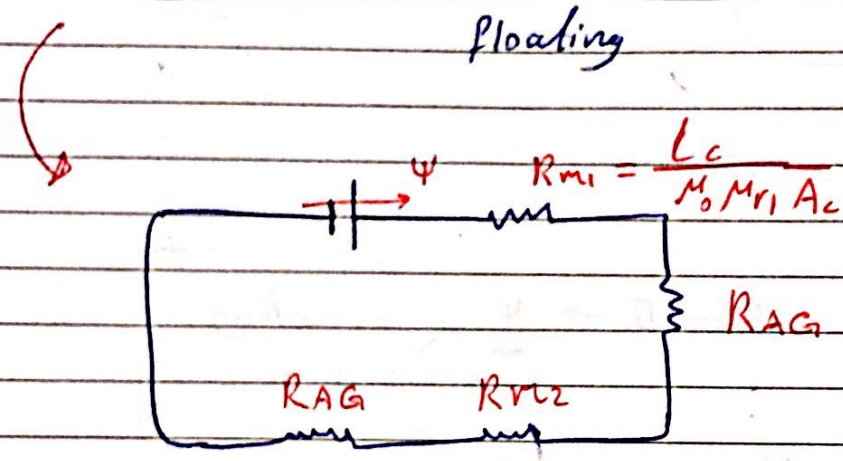


$$FF=1$$

$$\psi_c=0$$

$$g=9.8 \text{ m/s}^2$$

floating

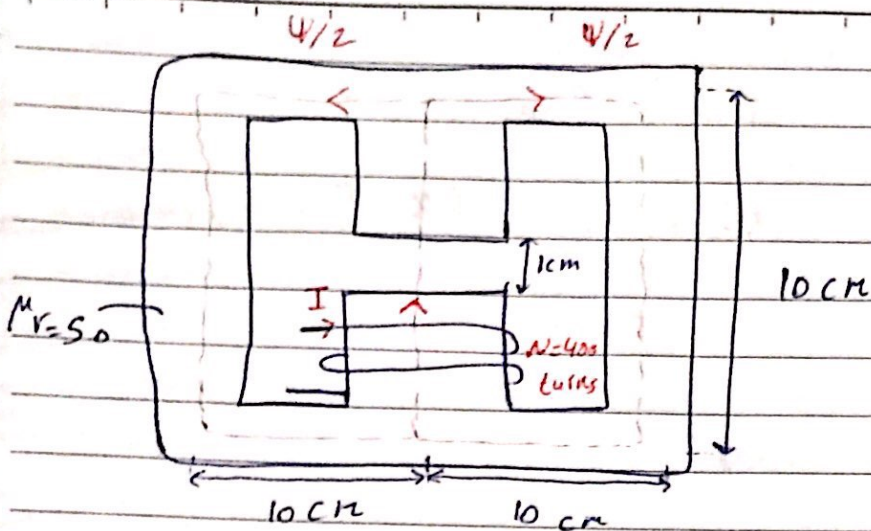


$$\text{Weight} = mg = F_{ut}$$

$$F_{ut} = \frac{B^2 A_c}{\mu_0} \quad \text{for low air gap}$$

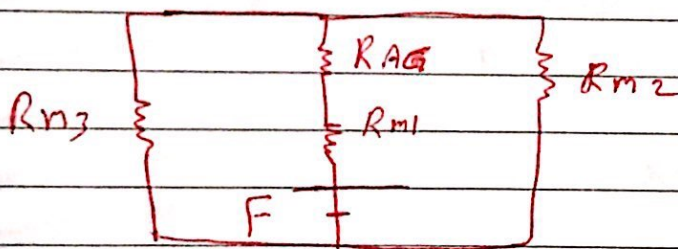
$$B = \frac{\psi}{A_c} \rightarrow \psi = \frac{F}{R_{eq}}$$

$$F = NI$$



all  $A_c = 10 \text{ cm}^2$ , find  $I$  to produce  $1.5 \text{ T}$  in the airgap

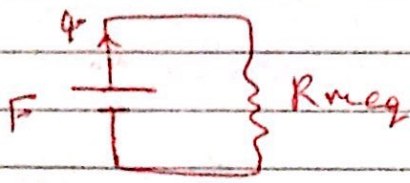
$FF=1$ ,  $\psi_c=0$ ,  $\mu_r$  is given area the same



$$R_{m1} = \frac{9 \times 10^{-12}}{(4\pi \times 10^{-7})(50)(10 \times 10^{-4})}, \quad R_{AG} = \frac{1 \times 10^{-2}}{4\pi \times 10^{-7} \times 10 \times 10^{-4}}$$

$$R_{m2} = \frac{30 \times 10^{-2}}{(4\pi \times 10^{-7})(50)(10 \times 10^{-4})} = R_{m3}$$

$$R_{m_{eq}} = (R_{m2} \parallel R_{m3}) + R_{m1} + R_{AG}$$



$$F = \Psi R_{meq} = NI$$

$$\Psi = B A_c \quad (\Psi = \int \vec{B} \cdot d\vec{s})$$

$$F_{MT} = \frac{B^2 A_c}{2\mu} \rightarrow A_{ag}$$

$$I = 44.16 \text{ A}$$

$$L = \frac{NI^2}{I}$$

$$B_c < B_{AG} \text{ if } \psi_c > 0$$

$$W_m = \frac{1}{2} LI^2$$

$$A_{AG} = FF (A_c)$$

$$M = (M_r - 1) H \rightarrow H_c = \frac{B_c}{\mu_0 \mu_r} \quad H_{AG} = \frac{B_{AG}}{\mu_0 (1)}$$

\* if  $M_r$  is not given

B	H	
0.5	--	
0.75	--	$M = \frac{B}{H}$
1	--	
1.25	--	

$FF = 1$   
 $\psi_c = 0$

more application duality to CH 6

$$\nabla^2 V = 0$$

scalar Laplace

$$\nabla^2 V = -\frac{\rho V}{\epsilon}$$

$\epsilon$

scalar Poisson

↪ duality

$$\nabla^2 \vec{A} = 0$$

vector Laplace

if  $\vec{J} = 0$

$$\nabla^2 \vec{A} = -\mu \vec{J}$$

vector Poisson

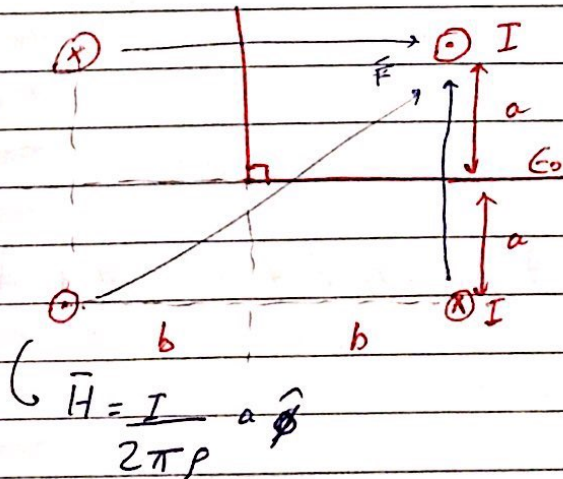
if  $\vec{J} \neq 0$

↪  $\nabla^2 A_x = 0$

$$\nabla^2 A_y = 0$$

$$\nabla^2 A_z = 0$$

\* method of images



# CH 9: maxwell's eq (time varying field)

Ac Source  $\longrightarrow$  Ac fields

$$\rho_v, \mathbf{J} \longrightarrow \mathbf{E}, \mathbf{D}, \mathbf{H}, \mathbf{B}$$

$$(x, y, z; t) \longrightarrow (x, y, z; t)$$

• Review:-

$$\textcircled{1} \nabla \cdot \mathbf{D} = \rho_v \longrightarrow \oint \mathbf{D} \cdot \mathbf{d}\mathbf{s} = \nu \int \rho_v d\nu$$

$$\textcircled{2} \nabla \times \mathbf{E} = 0 \longrightarrow \oint \mathbf{E} \cdot \mathbf{d}\mathbf{l} = 0$$

$$\textcircled{3} \nabla \times \mathbf{H} = \mathbf{J} \longrightarrow \oint \mathbf{H} \cdot \mathbf{d}\mathbf{l} = I_{enc} = \int \mathbf{J} \cdot \mathbf{d}\mathbf{s}$$

$$\textcircled{4} \nabla \cdot \mathbf{B} = 0 \longrightarrow \oint \mathbf{B} \cdot \mathbf{d}\mathbf{s} = 0$$

Sources for Ac source

1) charge moving with acceleration

2) Ac current flowing in the wire

\* Faraday's Law  
(generator principle)

$$V_{emp} = - \frac{d\psi}{dt} = - \frac{d \int \mathbf{B} \cdot \mathbf{d}\mathbf{s}}{dt} = - \int \frac{d\mathbf{B}}{dt} \cdot \mathbf{d}\mathbf{s} = - \int \mathbf{E} \cdot \mathbf{d}\mathbf{l} \quad N=1$$

↳ Lenz's Law,  $\psi = \int \mathbf{B} \cdot \mathbf{d}\mathbf{s}$

in CH 4

$$V_{emp} = \oint \mathbf{E} \cdot \mathbf{d}\mathbf{l}$$

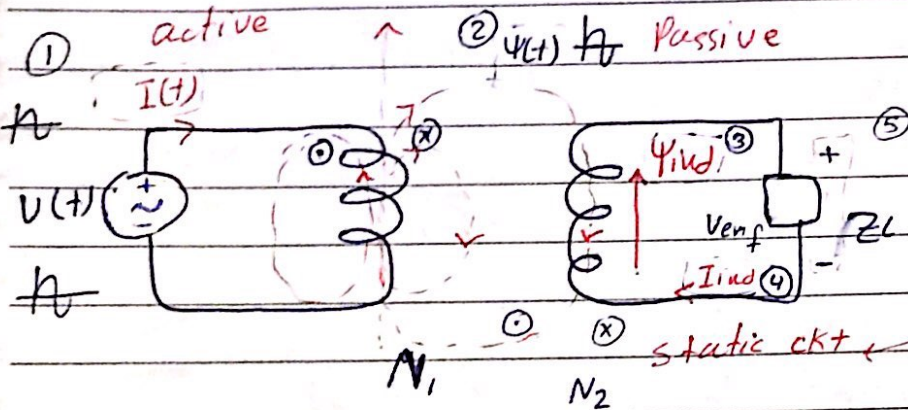
$$V_{emp} = - \frac{d\psi}{dt} = - \frac{d}{dt} \int \mathbf{B} \cdot \mathbf{d}\mathbf{s} = \oint \mathbf{E} \cdot \mathbf{d}\mathbf{l}$$

$$\oint \mathbf{E} \cdot \mathbf{d}\mathbf{l} = - \frac{d}{dt} \int \mathbf{B} \cdot \mathbf{d}\mathbf{s}$$

↳ Faraday's Law  
↳ 2nd maxwell eq  
in time varying fields

There are 3 cases for Faraday's Law:

1) time varying fields on a stationary loop



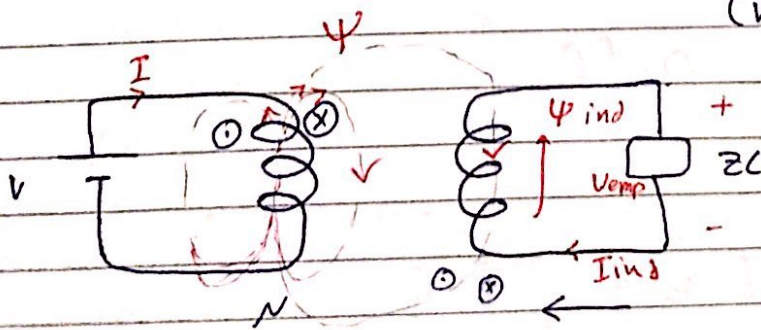
(Transformer EMF)

$$V_{emp} = \oint_L \vec{E} \cdot d\vec{l} = \int_S -\frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

$$\Rightarrow \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\int_S \nabla \times \vec{E} \cdot d\vec{s} = \int_S -\frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$$

2) static field on a moving loop (DC generator) (motional EMF)



$$V_{emp} = \oint_L \vec{E} \cdot d\vec{l} = \int_L \vec{u} \times \vec{B} \cdot d\vec{l} \quad \vec{F}_m = q \vec{u} \times \vec{B}$$

$$\nabla \times \vec{E} = \nabla \times (\vec{u} \times \vec{B})$$

$$\frac{\vec{F}_m}{q} = \vec{E}_m = \vec{u} \times \vec{B}$$

3) time varying field on a moving loop  
 (induction and synchronous generator)  
 (+ transformer + motional) EMF

$$V_{emf} = \oint_C \vec{E} \cdot d\vec{l} = - \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} + \oint_C \vec{u} \times \vec{B} \cdot d\vec{l}$$

$$\nabla \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}, \quad \nabla \times (\vec{u} \times \vec{B})$$

\* Displacement current Ac current ( $I_d$ )

$$I_d = \int_S \vec{J}_d \cdot d\vec{s}, \quad \vec{J}_d \equiv \text{displacement current Density} \quad (A/m^2)$$

$$\vec{J}_d = \epsilon_0 \frac{\partial \vec{E}}{\partial t} \quad \vec{J} = \rho \vec{v}$$

From continuity eq

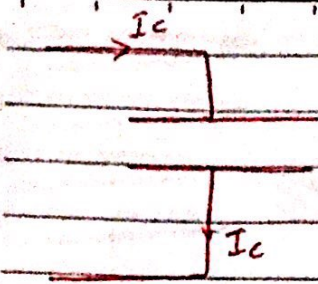
$$\oint_S \vec{J} \cdot d\vec{s} = - \int_V \frac{\partial \rho}{\partial t} dV$$

$$\nabla \cdot \vec{J} = - \frac{\partial \rho}{\partial t} \quad \text{Diff}$$

$$\oint_C \vec{H} \cdot d\vec{l} = I_{enc} = \int_S \vec{J} \cdot d\vec{s} \quad \text{Amperes Law}$$

→ conduction





$$\oint \vec{H} \cdot d\vec{l} = I_{enc} = I_c + I_b = \int \vec{J} \cdot d\vec{s} + \int \vec{J}_d \cdot d\vec{s}$$

↳ modified Ampere's Law  
(3rd Maxwell eq)

$$\int \vec{J} + \vec{J}_d \cdot d\vec{s}$$

$$\nabla \times \vec{H} = \vec{J} + \vec{J}_d$$

$$\nabla \times \vec{H} = \vec{J} + \vec{J}_d$$

$$\nabla \cdot (\nabla \times \vec{H}) = \nabla \cdot \vec{J} + \nabla \cdot \vec{J}_d$$

$$\nabla \cdot \vec{J}_d = -\nabla \cdot \vec{J} \Rightarrow \nabla \cdot \vec{J}_d = + \frac{d\rho_v}{dt}, \rho_v = \nabla \cdot \vec{D}$$

$$\nabla \cdot \vec{J}_d = + \frac{d}{dt} \nabla \cdot \vec{D} \quad \text{xyz}$$

$$\nabla \cdot \vec{J}_d = + \nabla \cdot \frac{d\vec{D}}{dt}$$

$$\vec{J}_d = \frac{d\vec{D}}{dt}$$

Maxwell's eq in time varying fields (in time domain)

$$\nabla \cdot \vec{D} = \rho_v \quad (\nabla \cdot \vec{D}(x, y, z; t) = \rho_v(x, y, z; t))$$

$$\nabla \times \vec{E} = -\frac{d\vec{B}}{dt} = -\mu \frac{d\vec{H}}{dt} \Rightarrow \nabla \times \vec{H} = \sigma \vec{E} + \epsilon \frac{d\vec{E}}{dt}$$

$$\nabla \cdot \vec{B} = 0$$

\* time harmonic fields :- 9.7 9.6 x  
Periodic (sinusoidal)

$j = \sqrt{-1} \rightarrow$  imaginary operator

$$z = r \angle \theta$$
$$\sqrt{z} = \sqrt{r} \angle \theta/2$$

Euler's Identity :-

$$e^{j\theta} = \cos \theta + j \sin \theta$$

$$e^{-j\theta} = \cos \theta - j \sin \theta$$

$$(e^{j\theta})^* = e^{-j\theta} = \cos \theta - j \sin \theta$$

$$\cos \theta = \frac{e^{j\theta} + e^{-j\theta}}{2}, \quad \sin \theta = \frac{e^{j\theta} - e^{-j\theta}}{2j}$$

i.e.  $I = I_0 \cos(\omega t + \phi) A$   
(instantaneous form)

$$I(t) = \text{Re} [ I_0 e^{j(\omega t + \phi)} ]$$

$$I(t) = \text{Re} [ I_0 e^{j\phi} e^{j\omega t} ]$$

$\Downarrow$

$$I_s = I_0 e^{j\phi} = I_0 \cos \phi + j I_0 \sin \phi$$

phase  $\nearrow$

$$= I_0 \angle \phi = I_0 \cos \phi + j I_0 \sin \phi$$

$$\frac{d}{dt} e^{j\omega t} = j\omega e^{j\omega t} \quad / \quad \int e^{j\omega t} dt = \frac{1}{j\omega} e^{j\omega t}$$

maxwell's equation in phasor form

$$\nabla \cdot \bar{D}(x, y, z; t) = \rho_v(x, y, z; t)$$

$$\text{Re} \{ \nabla \cdot \bar{D}_s(x, y, z) e^{j\omega t} \} = \text{Re} \{ \rho_{vs}(x, y, z) e^{j\omega t} \}$$

$$\nabla \cdot \bar{D}_s = \rho_{vs} \quad (1)$$

$$\nabla \times \bar{E}(x, y, z; t) = -\frac{\partial \bar{B}}{\partial t}(x, y, z; t)$$

$$\nabla \times \text{Re} \{ \bar{E}_s e^{j\omega t} \} = -\text{Re} \left\{ \frac{\partial \bar{B}_s}{\partial t} e^{j\omega t} \right\}$$

$$\nabla \times \text{Re} \{ \bar{E}_s e^{j\omega t} \} = -\text{Re} \{ j\omega \bar{B}_s e^{j\omega t} \}$$

$$\nabla \times \bar{E}_s = j\omega \bar{B}_s \quad (2) \Rightarrow \nabla \times \bar{E}_s = -j\omega \mu \bar{H}_s$$

$$\nabla \times \bar{H}_s = \sigma \bar{E}_s + j\omega \epsilon \bar{E}_s \quad (3)$$

$$\nabla \cdot \bar{B}_s = 0 \quad (4)$$

Ex: given

$\omega \rightarrow$  rad/s) phase const  $\rightarrow$  (rad/m)

$$\vec{E} = \frac{50}{\rho} \cos(10^6 t + \beta z) a_{\phi} \text{ V/m}$$

$$\vec{H} = \frac{H_0}{\rho} \cos(10^6 t + \beta z) a_{\hat{\rho}} \text{ A/m}$$

in free space and source free region find  $H_0$  and  $\beta$

$\rightarrow \sigma = 0, \epsilon = 3 \times 10^8 \text{ m/s} \rightarrow \rho_v = 0, \vec{J} = 0$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}, \quad \nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t} \quad \text{**} \quad \text{**} \quad \text{**} \quad \text{**} \quad \text{**} \quad \text{**}$$

$$\vec{E}_s = \frac{50}{\rho} e^{j\beta z} a_{\phi} \text{ V/m}$$

$$\vec{H}_s = \frac{H_0}{\rho} e^{j\beta z} a_{\hat{\rho}} \text{ A/m}$$

$$\nabla \times \vec{E}_s = -j\omega \mu \vec{H}_s, \quad \nabla \times \vec{H}_s = j\omega \epsilon \vec{E}_s$$

$$\vec{H}_s = \frac{-1}{j\omega \mu} \nabla \times \vec{E}_s$$

$$\begin{bmatrix} H_{\rho s} \\ H_{\phi s} \\ H_{z s} \end{bmatrix} = \frac{-1}{j\omega \mu} \frac{1}{\rho} \begin{vmatrix} a_{\hat{\rho}} & \rho a_{\hat{\phi}} & a_z \\ \partial/\partial z & \partial/\partial \phi & \partial/\partial z \\ E_{\rho s} & \rho E_{\phi s} & E_{z s} \end{vmatrix}$$

$$H_{\rho s} = \frac{1}{j\omega \mu \rho} \left( -\rho \frac{50}{\rho} (j\beta) e^{j\beta z} \right) a_{\hat{\rho}}$$

$$\frac{H_0}{\rho} e^{j\beta z} a_{\hat{\rho}} = \frac{50}{\omega \mu \rho} e^{j\beta z} a_{\hat{\rho}}$$

$$H_0 = \frac{S_0 \beta}{\omega \mu} \quad \text{--- ①}$$

$$\vec{E}_s = \frac{1}{j\omega \epsilon} \nabla \times \vec{H}_s$$

$$E_{\phi s} = \frac{1}{j\omega \epsilon \rho} \left( 0 + \frac{H_0}{\rho} j\beta e^{j\beta z} \right) \rho a \hat{\phi}$$

$$\frac{S_0}{\rho} e^{j\beta z} a \hat{\phi} = \frac{H_0 \beta}{\omega \epsilon \rho} e^{j\beta z} a \hat{\phi}$$

$$S_0 = \frac{H_0 \beta}{\omega \epsilon} \quad \text{--- ②}$$

$$S_0 = \frac{S_0 \beta^2}{\omega^2 \mu \epsilon} \Rightarrow \beta = \omega \sqrt{\mu \epsilon} = \frac{\omega}{c}$$

$$= 10^6 \sqrt{4\pi \times 10^{-7}} \times \frac{10^{-4}}{36\pi} = \frac{1}{3}$$

$$H_0 = \frac{1}{3} \times 0.1326 \text{ A/m}$$

# The END

بالتواضع