

* CH #1

* How to write a vector :-

↳ Cartesian :- $\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$ OR (A_x, A_y, A_z)

Unit vector $\hat{a}_x, \hat{a}_y, \hat{a}_z$
 قسماً 1 سے بدلو کے لیے $\hat{a}_x, \hat{a}_y, \hat{a}_z$
 Vector کی طرف $\hat{a}_x, \hat{a}_y, \hat{a}_z$
 Cartesian coordinate موجود ہے

↳ Cylindrical :- $\vec{A} = A_\rho \hat{a}_\rho + A_\phi \hat{a}_\phi + A_z \hat{a}_z$ OR (A_ρ, A_ϕ, A_z)

↳ Spherical :- $\vec{A} = A_r \hat{a}_r + A_\theta \hat{a}_\theta + A_\phi \hat{a}_\phi$ OR (A_r, A_θ, A_ϕ)

Note

don't mix between points & vectors!
 $P(x, y, z) \rightarrow$ point
 $\vec{A} = (A_x, A_y, A_z) \rightarrow$ vector

* Vector Magnitude :- (Scalar)

$$|\vec{A}| = A = \sqrt{A_x^2 + A_y^2 + A_z^2}$$

Scalar Quantities :-
 time / mass / distance / temperature / entropy
 electric potential / population
 کچھ ایسے ہیں جن کی مقدار
 $\vec{A} = A \hat{a}$

* Unit vector along a vector :-

$$\hat{a}_A = \frac{\vec{A}}{A} = \frac{A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z}{\sqrt{A_x^2 + A_y^2 + A_z^2}}$$

Vector کی magnitude (1)
 magnitude of vector (r)

Vector Quantities :-
 Velocity / force / displacement
 Electric field
 کچھ ایسے ہیں جن کی مقدار



* Operations on vectors :-

(1) Addition

$$\vec{C} = \vec{A} + \vec{B}$$

$$= (A_x + B_x) \hat{a}_x + (A_y + B_y) \hat{a}_y + (A_z + B_z) \hat{a}_z$$

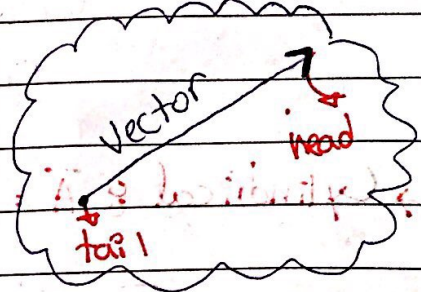
الجزء الذي يساوي
الجزء الذي يساوي

from vector definition.

- Graphically :-

كيفية الرسم مع 2 vectors

↳ Arrow method.

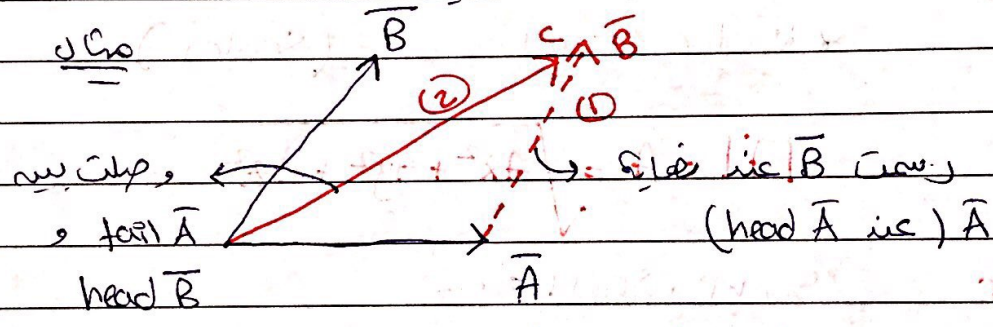


(head) (الذي هو الرأس) vector الأول

يجيب ان vector الثاني و يرسو به

تواصل بين tail الاول

head الثاني



(2) Subtraction

$$\vec{C} = \vec{A} - \vec{B}$$

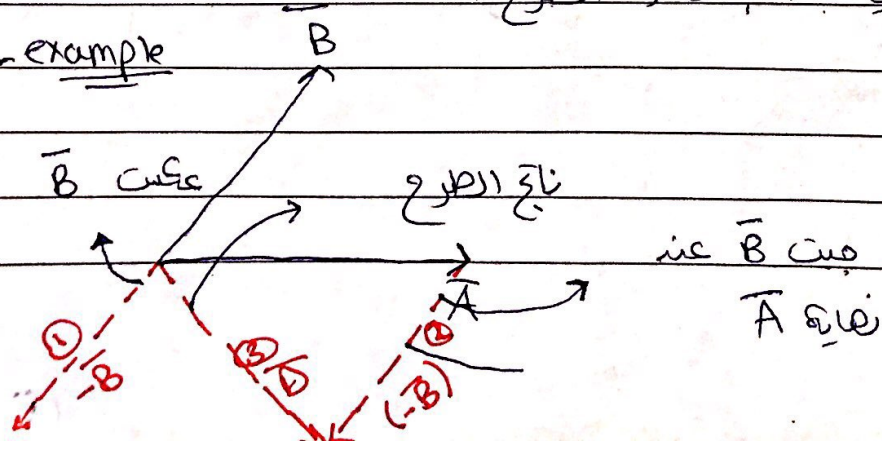
$$= (A_x - B_x) \hat{a}_x + (A_y - B_y) \hat{a}_y + (A_z - B_z) \hat{a}_z$$

- Graphically :-

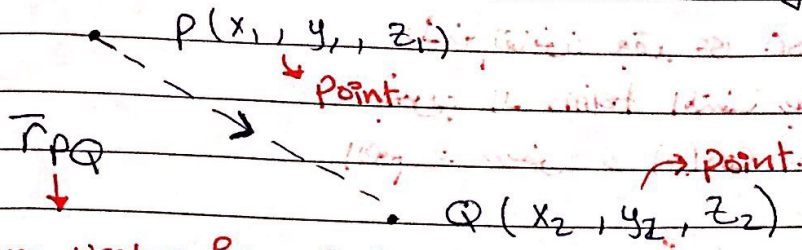
نفس طريقة الرسم ولكن كزخم عكس

ان vector الذي نريد ان نطرحه

- example



- Application on Subtraction is Distance (vector)



المسافة بين نقطتين
المسافة بين نقطتين
المسافة بين نقطتين

Distance vector from P to Q

$$\vec{r}_{PQ} = \vec{r}_Q - \vec{r}_P$$

$$= (x_2 - x_1)\hat{a}_x + (y_2 - y_1)\hat{a}_y + (z_2 - z_1)\hat{a}_z$$

→ distance vector

المقدار distance لاجل
magnitude $|\vec{r}_{PQ}| = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$

direction ال

$$\hat{a}_{\vec{r}_{PQ}} = \frac{\vec{r}_{PQ}}{|\vec{r}_{PQ}|}$$

[3] Multiplication

(a) Dot product

$$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta_{(AB)}$$

هنا لقانون يستخدمه لما يكون يعرف الزاوية بين ال Vectors

dot product

$$\vec{A} \cdot \vec{B} = A_x B_x + A_y B_y + A_z B_z$$

إذا ما يعرف الزاوية بينهم نستخدم هذا لقانون

Scalar (معنى الجوانب رقم)

$$\theta_{AB} = \cos^{-1} \left(\frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|} \right)$$

لو طلب مني الزاوية نستخدم هذا لقانون

* ليس (dot product) بطرح قيمته scalar

لأنه لقانون بقدر على $\cos A$ ولما آتينا ضرب vectors

بضرب الـ terms المتشابهة و الزاوية بينه (unit vector)

الهم = صفر و $\cos(0) = 1$

توضيح $\rightarrow A \cdot \hat{a}_x \cdot B \cdot \hat{a}_x$

$= A \cdot B \cdot (\hat{a}_x \cdot \hat{a}_x)$ (أحيانا نكتبها به على شكل مشترك)

$= A \cdot B \cdot (1)$

لأنه الزاوية بينهم صفر

$\hat{a}_n \cdot \hat{a}_m = \begin{cases} 1, & n=m \\ 0, & n \neq m \end{cases}$

properties of dot product -

1) $\vec{A} \cdot \vec{B} = \vec{B} \cdot \vec{A}$

2) $\vec{A} \cdot \vec{A} = A^2 = A_x^2 + A_y^2 + A_z^2$

3) $\vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$

\rightarrow b) Cross product (it has magnitude + direction).

$|\vec{A} \times \vec{B}| = AB \sin \theta_{AB}$

لأنه لقانون يستخدمه لما أعرف لزاوية بين \vec{A} و \vec{B}

$\vec{A} \times \vec{B} =$	\hat{a}_x	\hat{a}_y	\hat{a}_z
\rightarrow	A_x	A_y	A_z
\rightarrow	B_x	B_y	B_z

إذا ما عرف لزاوية بينهم بعد

cross product بينهم باستخدام Matrix

Unit Vector أول صنف

تاني صنف بعد أول vector
و ثالث صنف بعد تاني vector

$\vec{A} \times \vec{B} = (-1)^{1+1} (A_y B_z - A_z B_y) \hat{a}_x$
 $+ (-1)^{1+2} (A_x B_z - A_z B_x) \hat{a}_y$
 $+ (-1)^{1+3} (A_x B_y - A_y B_x) \hat{a}_z$

أول مرة رجعنا أول عامود و ضرب
الثاني والثالث ببعض (تاني مرة رجعنا تاني عامود
و ضرب الأول والثالث و آخر اثنين رجعنا ثالث
عامود و ضرب الأول والثاني

$$\theta = \sin^{-1} \left(\frac{|\vec{A} \times \vec{B}|}{|\vec{A}| |\vec{B}|} \right)$$

→ إذا طلب مني الزاوية
 بطرح $\vec{A} \times \vec{B}$ باستخدام ال matrix حسب
 القانون ، نجد من مخرج magnitude لـ vector
 التي طرح من ال matrix ، و مخرج
 ال magnitude لـ \vec{A} و \vec{B} و يقسم $\frac{|\vec{A} \times \vec{B}|}{|\vec{A}| |\vec{B}|}$

و بعد ال \sin^{-1} (Sin inverse) و ال $\vec{A} \times \vec{B}$ (cross product)

Properties of cross product

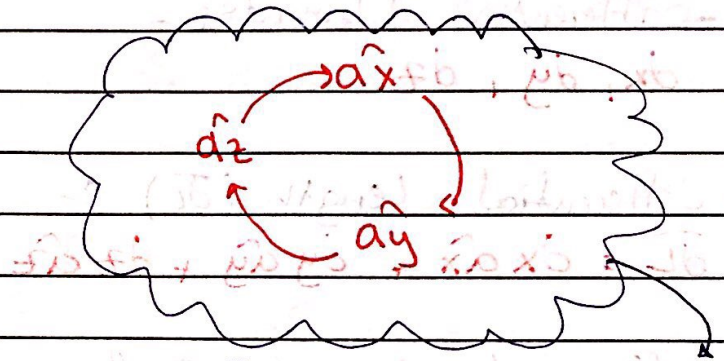
1) $\vec{A} \times \vec{B} = -\vec{B} \times \vec{A}$

2) $\vec{A} \times (\vec{B} \times \vec{C}) \neq (\vec{A} \times \vec{B}) \times \vec{C}$

3) $|\vec{a} \times \vec{a}| = 0$

لأن الزاوية بين ال \vec{a} مع ال \vec{a}
 هو $0 \Rightarrow \sin(0) = 0$

السالب للزاوية
 الأولوية للأقواس



إذا أصبحت مع عقارب الساعة يكون ال \vec{a} ، إذا عكس عقارب الساعة سالب

* Vector projection along another vectors —

↳ 1) Scalar projection —

$$AB = \vec{A} \cdot \hat{a}_B$$

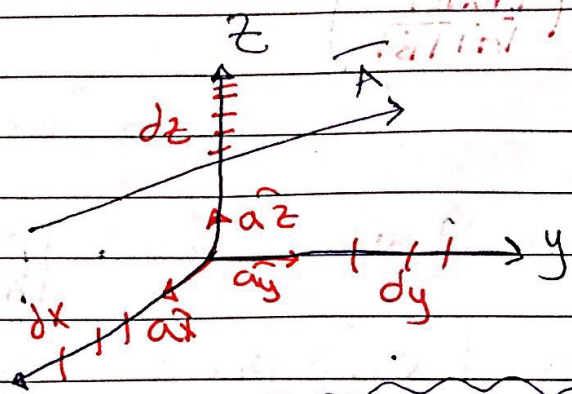
2) Vector projection —

$$\vec{AB} = (\vec{A} \cdot \hat{a}_B) \hat{a}_B, \quad \hat{a}_B = \frac{\vec{B}}{B}$$

لما طلب ال vector projection أول شيء يكون ال $\hat{a}_B = \frac{\vec{B}}{B}$ ال $\vec{A} \cdot \hat{a}_B$ ال \hat{a}_B ال scalar projection ال \vec{A} ال dot product ال $\vec{A} \cdot \hat{a}_B$ ال \vec{A} ال \hat{a}_B ال \vec{A} ال \hat{a}_B ال

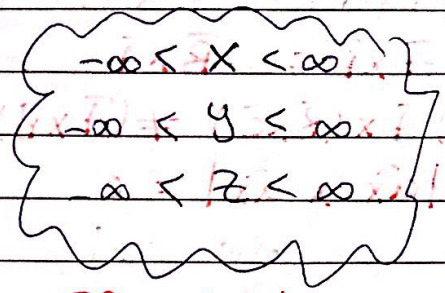
* CH #2

1) Cartesian Coordinates



$$\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$$

- Differential Elements -
 dx, dy, dz



3D object
 Infinite Box

* Differential Length (dL) :-

$$dL = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

* Differential Normal Surface Area (dS)

$$dS_{front} = dy dz \hat{a}_x$$

بالوجه الأمامي يكون عندنا هذا المساحة في الـ x direction
 وهو \hat{a}_x

$$dS_{back} = -dy dz \hat{a}_x$$

السالب لأننا في الـ x direction

$$dS_{right} = dx dz \hat{a}_y$$

لأننا في الـ y direction

$$dS_{left} = -dx dz \hat{a}_y$$

$$dS_{top} = dx dy \hat{a}_z$$

$$dS_{bottom} = -dx dy \hat{a}_z$$

Differential Volume (dV)

$$dV = dx dy dz$$

vector \cdot scalar

* 2D Surface (we fix one variable only).

- if $x = \text{constant}$ (not zero).

↳ infinite plane parallel to yz plane.

لو سألني سؤالي ما هو الجواب على ذلك هو yz plane
التي هي في الواقع $(-ax)$ و (ax) في yz Plane

- if $x = 0$

↳ infinite plane along yz plane.

- if $y = \text{constant}$ (not zero)

↳ infinite plane parallel to xz plane.

- if $y = 0$

↳ infinite plane along xz plane.

- if $z = \text{constant}$ (not zero)

↳ infinite plane parallel to xy plane.

- if $z = 0$

↳ infinite plane along xy plane.

** 1D Segment (we fix two variables).

- if x, z are constants (not zero) ($x \neq 0, z \neq 0$).

↳ infinite line parallel to y -axis.

- if $x = 0, z = 0$

↳ infinite line along y -axis.

- if y, z constants ($y \neq 0, z \neq 0$).

↳ infinite line parallel to x -axis.

-if $y=0, z=0$.

↳ infinite line along x-axis.

-if x, y are constants ($x \neq 0, y \neq 0$)

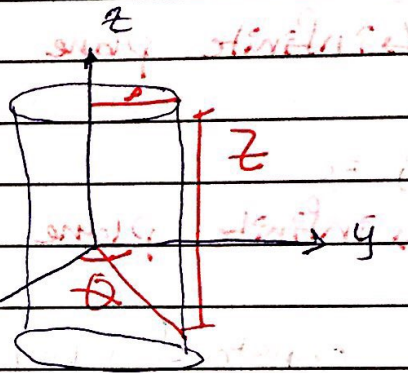
↳ infinite line parallel to z-axis.

-if $x=0, y=0$.

↳ infinite line along z-axis.

* Cylindrical coordinates:

$$\begin{aligned} 0 < \rho < \infty \\ 0 < \phi < 2\pi \\ -\infty < z < \infty \end{aligned}$$



Infinite solid cylinder.

$$\vec{A} = A_\rho \hat{a}_\rho + A_\phi \hat{a}_\phi + A_z \hat{a}_z$$

* Differential Elements -

$d\rho, \rho d\phi, dz$

$$dL = d\rho \hat{a}_\rho + \rho d\phi \hat{a}_\phi + dz \hat{a}_z$$

$$dS_{top} = \rho d\rho d\phi \hat{a}_z$$

$$dS_{bottom} = -\rho d\rho d\phi \hat{a}_z$$

$$dS_{side} = \rho d\phi dz \hat{a}_\rho$$

$$dS_{cut} (\phi = \text{constant}) = d\rho dz \hat{a}_\phi$$

$$dV = \rho d\rho d\phi dz$$

عنه عرفه ρ و $d\rho$ و $d\phi$ و dz و dS_{top} و dS_{bottom} و dS_{side} و dS_{cut} و dV

Const انهي هو

بكون عامه

* 2D Surface (we fix one variable)

- $\rho = \text{constant} \rightarrow$ infinite hollow cylinder

$\rho = 0 \rightarrow$ inf line along z-axis

- $\phi = \text{constant} \rightarrow$ semi-infinite plane

$\phi = 90^\circ \rightarrow$ semi-inf plane along yz plane.

- $z = \text{constant} \rightarrow$ inf. Disk // xy plane

$z = 0 \rightarrow$ inf. Disk along xy plane.

* 1D Surface (we fix 2 variables)

- ρ, ϕ constants & $\rho \neq 0$
 \hookrightarrow inf. Line parallel to z-axis

- ρ, ϕ constants & $\rho = 0$
 \hookrightarrow inf. Line along z-axis

- ρ, z constants ($z \neq 0, \rho > 0$)
 \hookrightarrow Circle // xy plane

- ρ, z constants ($z = 0, \rho > 0$)
 \hookrightarrow Circle along xy plane

- ρ, z constants ($\rho = 0$)
 \hookrightarrow point

- ϕ, z constants
 \hookrightarrow semi-inf line (Ray)

* Spherical coordinates -

$$\begin{aligned} 0 < r < \infty \\ 0 \leq \theta \leq \pi \\ 0 \leq \phi \leq 2\pi \end{aligned}$$

3D object
Infinite solid

Sphere

$$\vec{A} = A_r \hat{r} + A_\theta \hat{\theta} + A_\phi \hat{\phi}$$

* Differential Elements -

$$dr, r d\theta, r \sin\theta d\phi$$

$$d\vec{l} = dr \hat{r} + r d\theta \hat{\theta} + r \sin\theta d\phi \hat{\phi}$$

$$d\vec{s}_{\text{surface}} = r^2 \sin\theta d\theta d\phi \hat{r}$$

$$d\vec{s}_\theta = r \sin\theta dr d\phi \hat{\theta}$$

$$d\vec{s}_\phi = r dr d\theta \hat{\phi}$$

$$dV = r^2 \sin\theta dr d\theta d\phi$$

* 2D Surface (we fix one variable) -

- if $r = \text{constant}$ ($r \neq 0$) \rightarrow hollow sphere

- if $r = 0 \rightarrow$ point

- if $\theta = \text{constant}$

$\hookrightarrow \theta \in (0, 90)$ and $(90, 180) \rightarrow$ inf. hollow cone

$\hookrightarrow \theta = 90^\circ \rightarrow$ inf. disk along xy plane

$\hookrightarrow \theta = 0^\circ \rightarrow$ semi-inf. line in the +ve z-axis

$\hookrightarrow \theta = 180^\circ \rightarrow$ semi-inf. line in the -ve z-axis

- if $\phi = \text{constant} \rightarrow$ semi-inf. Disk

$\hookrightarrow \phi = 90^\circ \rightarrow$ semi-inf. Disk along yz plane

* 1D Segment (we fix 2 variables).

- if r, θ constants

$\hookrightarrow (r > 0), (\theta \neq 90^\circ) \rightarrow$ Circle // xy plane

$\hookrightarrow (r > 0), (\theta = 90^\circ) \rightarrow$ Circle along xy plane

$\hookrightarrow r = 0 \rightarrow$ point

- if r, ϕ constants

$\hookrightarrow (r > 0) \rightarrow$ half circle in $\theta = \phi$ plane

$\hookrightarrow (r = 0) \rightarrow$ point

- if θ, ϕ are constants

\hookrightarrow semi-inf. Line (\neq Ray).

* Transformation between ~~Cartesian~~ coordinates -

$(x, y, z) \rightarrow (\rho, \phi, z)$

$$\rho = \sqrt{x^2 + y^2}, \quad \phi = \tan^{-1}\left(\frac{y}{x}\right), \quad z = z.$$

$(\rho, \phi, z) \rightarrow (x, y, z)$

$$x = \rho \cos \phi, \quad y = \rho \sin \phi, \quad z = z$$

$(x, y, z) \rightarrow (r, \theta, \phi)$

$$r = \sqrt{x^2 + y^2 + z^2}, \quad \theta = \tan^{-1}\left(\frac{\sqrt{x^2 + y^2}}{z}\right), \quad \phi = \tan^{-1}\left(\frac{y}{x}\right)$$

~~Cartesian coordinates~~

* $(r, \theta, \phi) \rightarrow (x, y, z)$

$x = r \sin \theta \cos \phi$, $y = r \sin \theta \sin \phi$, $z = r \cos \theta$

~~* $(r, \theta, \phi) \rightarrow (x, y, z)$~~

* $(\rho, \phi, z) \rightarrow (r, \theta, \phi)$

$r = \sqrt{\rho^2 + z^2}$, $\theta = \tan^{-1}(\frac{\rho}{z})$, $\phi = \phi$

* $(r, \theta, \phi) \rightarrow (\rho, \phi, z)$

$\rho = r \sin \theta$, $\phi = \phi$, $z = r \cos \theta$

القواسم التي قبلها تكون لتحويل نقاط من Vectors

* Vectors Transformation

$$\begin{bmatrix} A\rho \\ A\phi \\ Az \end{bmatrix} = \begin{bmatrix} \cos\phi & \sin\phi & 0 \\ -\sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} Ax \\ Ay \\ Az \end{bmatrix}$$

هذا هو matrix يكون
مصفوفة بالتحويلات

للطلب

للطلب

$A\rho = \cos\phi Ax + \sin\phi Ay$

$\therefore \dots \dots \dots$

لو طلب من ان Cartesian و من المطلوب ان cylindrical كيف انزلنا

بالحذف ان transpose للماتريكس يعني ان كل عامود يصبح صف في نفس الطريقة

$(\frac{\rho}{z}) \tan^{-1} = \phi$, $(\frac{\sqrt{\rho^2 + z^2}}{z}) \tan^{-1} = \theta$

* CH # 3

* Line Integrals -

$$\int_C \vec{A} \cdot d\vec{L}$$

ہر ایک ٹکڑوں کی ایک مجموعہ سے لائنیں
کی (خاندان)

* Surface Integrals -

$$\int_S \vec{A} \cdot d\vec{s}$$

* Volume Integrals -

$$\int_V |\vec{A}| dV$$

* Del operator (∇)

- in Cartesian

$$\nabla v = \frac{\partial v}{\partial x} \hat{a}_x + \frac{\partial v}{\partial y} \hat{a}_y + \frac{\partial v}{\partial z} \hat{a}_z$$

Partial

اس طرح

Gradient

$\nabla * V = \text{vector}$

vector

↓
Scalar

- in cylindrical

$$\nabla u = \frac{\partial u}{\partial \rho} \hat{a}_\rho + \frac{1}{\rho} \frac{\partial u}{\partial \phi} \hat{a}_\phi + \frac{\partial u}{\partial z} \hat{a}_z$$

- in spherical

$$\nabla T = \frac{\partial T}{\partial r} \hat{a}_r + \frac{1}{r} \frac{\partial T}{\partial \theta} \hat{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial T}{\partial \phi} \hat{a}_\phi$$

*CH 4

- Coulomb's Law

↳ the force between two point charges is along the line joining them, directly proportional to Q_1, Q_2 and inversely proportional to the square of the distance between them.

$$F = k \frac{Q_1 Q_2}{R^2} \text{ (N)}, \quad k = \frac{1}{4\pi\epsilon_0}, \quad \epsilon_0 = \frac{10^{-9}}{36\pi} \text{ (F/m)}$$

magnitude only, \downarrow
only

* F as a vector quantity -

↳ ① $\vec{F}_{12} = \frac{Q_1 Q_2}{4\pi\epsilon_0 R^2} \hat{a}_{R_{12}}$
Force on Q_2 due to Q_1

$$\hat{a}_{R_{12}} = \frac{\vec{R}_{12}}{|\vec{R}_{12}|}$$

↳ ② $\vec{F}_{12} = \frac{Q_1 Q_2 \cdot \vec{R}_{12}}{4\pi\epsilon_0 R^3}$

↳ ③ $\vec{F}_{12} = \frac{Q_1 Q_2 (\vec{r}_2 - \vec{r}_1)}{4\pi\epsilon_0 |\vec{r}_2 - \vec{r}_1|^3}$

قانون كولوم (1) و (2) و (3) نفس الشيء ولكن بأشكال مختلفة

* Force due to N-Point charges -

$$\vec{F} = \frac{Q}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k (\vec{r} - \vec{r}_k)}{|\vec{r} - \vec{r}_k|^3}$$

$\vec{F}_{12} = -\vec{F}_{21}$
نفس المقدار، نفس الشيء

↳ Using Superposition Principle

Field \rightarrow التي بيها أحسب
عن اللى بيأثروا على

1. the distance between Q_1 & Q_2 must be large compared to their bodies (point charges)

2. Q_1 & Q_2 must be static (at rest)

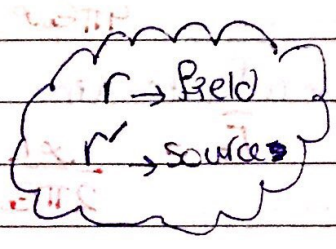
Source \rightarrow التي بيأثروا على
اللى بيأثر على

+ve

* Electric Field intensity is the force that a + charge experiences when placed in an Electric Field.

$$\vec{E} = \frac{\vec{F}}{Q} \quad (\text{N/C}) \text{ or } (\text{V/m})$$

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{r} = \frac{Q(\vec{r}-\vec{r}')}{4\pi\epsilon_0 |\vec{r}-\vec{r}'|^3}$$



For N-point charges-

$$\vec{E} = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k (\vec{r}-\vec{r}_k)}{|\vec{r}-\vec{r}_k|^3}$$

Electric Fields due to continuous charge distributions -

$\rho_L \rightarrow$ Line charge density (C/m)

$\rho_s \rightarrow$ Surface charge density (C/m²)

$\rho_v \rightarrow$ Volume charge density (C/m³)

don't mix between ρ for cylindrical radial and ρ for surface.

Total charges -

1) Line charge.

$$dQ = \rho_L dL \rightarrow Q = \int_L \rho_L dL$$

- Electric Field intensity

1) Line charge.

$$\vec{E} = \int_L \frac{\rho_L dL}{4\pi\epsilon_0 R^2} \hat{a}_r$$

Surface charge

$$dQ = \rho_s ds \rightarrow Q = \int_s \rho_s ds$$

2) Surface charge

$$\vec{E} = \int_s \frac{\rho_s ds}{4\pi\epsilon_0 R^2} \hat{a}_r$$

Volume charge

$$dQ = \rho_v dv \rightarrow Q = \int_v \rho_v dv$$

3) Volume charge

$$\vec{E} = \int_v \frac{\rho_v dv}{4\pi\epsilon_0 R^2} \hat{a}_r$$

* Line Charge

- Finite line charge

$$\vec{E} = \frac{\rho L}{4\pi\epsilon_0} \left[-(\sin\alpha_2 - \sin\alpha_1) \hat{a}_\rho + (\cos\alpha_2 - \cos\alpha_1) \hat{a}_z \right] \text{ (V/m)}$$

- infinite line charge

$$\vec{E} = \frac{\rho L}{2\pi\epsilon_0} \hat{a}_\rho \text{ (V/m)}$$

* Surface Charge

- infinite sheet of charge

$$\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_n \text{ (V/m)}, \text{ } \hat{a}_n \text{ is unit vector normal to the sheet.}$$

- For parallel plate capacitor:

$$\vec{E} = \frac{\rho_s}{\epsilon_0} \hat{a}_n \text{ (V/m)}$$

Volume Charge

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \text{ (V/m)}$$

Electric Flux Density & -

$$\vec{D} = \epsilon_0 \vec{E} \text{ (C/m}^2\text{)}$$

infinite sheet of ~~charge~~ charge

$$\vec{D} = \rho_s \hat{a}_n \text{ (C/m}^2\text{)}$$

infinite line charge

$$\vec{D} = \rho L \hat{a}_\rho \text{ (C/m}^2\text{)}$$

Volume charge distribution

$$\vec{D} = \int \frac{\rho_v}{4\pi R^2} \hat{a}_r$$

The flux (\vec{D}) is independent of the medium
القوة (\vec{D}) مستقلة عن الوسط

* Gauss's Law -

↳ total electric flux through closed surface is equal to the total charge enclosed by that surface.

$$Q = \oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_v dV$$

↳ enclosed surface

- First Maxwell's equation in integral form

$$\oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_v dV$$

- First Maxwell's equation in point form

$$\rho_v = \nabla \cdot \vec{D}$$

+ Electric Potentials -

$$W = -Q \int_A^B \vec{E} \cdot d\vec{L} \quad (\text{J})$$

↳ work (potential energy) required to move Q from point A to point B.

negative sign means the work is done by an external agent.

$$V_{AB} = \frac{W}{Q} = - \int_A^B \vec{E} \cdot d\vec{L} \quad (\text{J/C}) \quad (\text{V})$$

V_{AB} is potential difference between A & B
A is the initial point
B is the final point

if V_{AB} is positive

↳ gain in potential
↳ external agent performs the work

if V_{AB} is negative

↳ loss in potential
↳ work is being done by the field.

$$V_{AB} = V_B - V_A$$

* For a point charge:-

$$V_{AB} = \frac{Q}{4\pi\epsilon_0} \left[\frac{1}{r_B} - \frac{1}{r_A} \right]$$

$$V(r) = \frac{Q}{4\pi\epsilon_0 |r-r'|}$$

* Line charge

$$V(r) = \frac{1}{4\pi\epsilon_0} \int \frac{\rho_L dl'}{|r-r'|}$$

- Surface charge

$$V(r) = \frac{1}{4\pi\epsilon_0} \int \frac{\rho_s ds'}{|r-r'|}$$

- Volume charge

$$V(r) = \frac{1}{4\pi\epsilon_0} \int \frac{\rho_v dv'}{|r-r'|}$$

$$E = -\nabla V$$

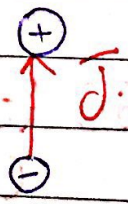
\vec{E} is opposite to the direction in which V increases

Electric dipole:-

$$V = \frac{Q}{4\pi\epsilon_0} \left(\frac{1}{r_2} - \frac{1}{r_1} \right) \text{ when locations are given.}$$

or

$$V = \frac{Qd \cos\theta}{4\pi\epsilon_0 r^2}$$



- define dipole moment $\vec{P} = Q\vec{d}$

$$V = \frac{P \cos\theta}{4\pi\epsilon_0 r^2} = \frac{P \cdot (\vec{r} - \vec{r}')}{4\pi\epsilon_0 |r-r'|^3}$$

or

$$V = \frac{P \cdot \hat{a}_r}{4\pi\epsilon_0 r^2}$$

$$\vec{E} = \frac{P}{4\pi\epsilon_0 r^3} (2 \cos\theta \hat{a}_r + \sin\theta \hat{a}_\theta)$$

ref. point is taken as 1 if the question is asked by the questioner
 $V_{\infty} = 0$

* Energy Density of Electrostatic Fields -

$$W_E = \frac{1}{2} \sum_{k=1}^N Q_k V_k \quad (\text{J}) \quad \text{For point charges}$$

- For line charge

$$W_E = \frac{1}{2} \int_L \rho_L V dL \quad (\text{J})$$

- For surface charge

$$W_E = \frac{1}{2} \int_S \rho_S V dS \quad (\text{J})$$

- For volume charge

$$W_E = \frac{1}{2} \int_V \rho_V V dV \quad (\text{J})$$

* To find energy from \bar{E}

$$W_E = \frac{1}{2} \int_V \bar{D} \cdot \bar{E} dV \quad (\text{J})$$

or

$$W_E = \frac{1}{2} \int_V \epsilon_0 E^2 dV \quad (\text{J})$$

$$\bar{D} = \bar{E} \epsilon_0$$

or

$$W_E = \frac{1}{2} \int_V \frac{D^2}{\epsilon_0} dV \quad (\text{J})$$

$$\bar{E} = \frac{\bar{D}}{\epsilon_0}$$

* Energy density (w_E)

$$w_E = \frac{dW_E}{dV} = \frac{1}{2} \bar{E} \cdot \bar{D} = \frac{1}{2} \epsilon_0 E^2 = \frac{1}{2} \frac{D^2}{\epsilon_0} \quad (\text{J/m}^3)$$

$$W_E = \int_V w_E dV \quad (\text{J/m}^3)$$

CH5 - Materials based on its electrical properties

↳ Conductors ($\sigma \gg \gg 1$)

i.e. (Cu, Al, Ag, Lead)

↳ Semi-conductors ($\sigma \approx 1$)

i.e. (Si, GaAs, Ge)

↳ Dielectrics (Insulators) ($\sigma \ll \ll 1$)

i.e. (Li, Mica, Polythelene, Polystyrene)

σ Conductivity (S/m)

↳ depends on -

1) Temperature ($T \uparrow, \sigma \downarrow$)

2) Frequency.

$$I = \frac{\Delta Q}{\Delta t} \quad (A)$$

Current is the electric charge passing through an area per unit time.

- Current Density (\vec{J})

$$\vec{J} = \frac{\Delta I}{\Delta S} \quad (A/m^2)$$

- Types of current -

1] Convection Current

$$I = \rho_v \vec{u} \cdot \Delta S \quad (A)$$

$$\vec{J} = \rho_v \vec{u} \quad (A/m^2)$$

2] Conduction Current

$$\vec{J} = \sigma \vec{E}$$

$$\sigma = n^2 \frac{e \tau}{m}$$

$$\rho_v = n e$$

* Conductors

↳ if the conductor is isolated.

↳ $\vec{E}_{\text{inside}} = 0$

$\vec{D}_{\text{inside}} = 0$

$\rho_v_{\text{inside}} = 0$

$V_{ab \text{ inside}} = 0$

- The conductor is called equipotential body.

↳ if the conductor is not isolated

$R = \frac{V}{I} = \frac{L}{\sigma S} = \frac{\rho L}{S} \quad (\rho = \frac{1}{\sigma}) \Rightarrow$ cross section uniform conductor

$R = \frac{V}{I} = \frac{\int \vec{E} \cdot d\vec{l}}{\int \vec{J} \cdot d\vec{s}}$ in general.

* Power

$P = \int_V \vec{J} \cdot \vec{E} dV$

or $P = \int_V \sigma E^2 dV \text{ (W)}$ ($\vec{J} = \sigma \vec{E}$)

or $P = \int_V \frac{J^2}{\sigma} dV \text{ (W)}$ ($\vec{E} = \frac{\vec{J}}{\sigma}$)

* Power Density

$w_p = \frac{dP}{dV} = \vec{J} \cdot \vec{E} = \sigma E^2 = \frac{J^2}{\sigma} \text{ (W/m}^3\text{)}$

$P = \int_V w_p dV$

- Non-polarized dielectrics -

$$\bar{P} = \lim_{\Delta V \rightarrow 0} \frac{\sum_{k=1}^N Q_k \bar{r}_k}{\Delta V}$$

- Polarized dielectrics -

$$V = \int_S \rho_p ds$$

$$V = \int_V \rho_p dv$$

الشحنات الحرة
dielectrics

ρ_p is polarized (bound) surface charge density

ρ_p is polarized (bound) volume charge density

$$V = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r}$$

$$V = \int_V \frac{\rho_v dv}{4\pi\epsilon_0 r}$$

Free charge

$$\rho_p = \bar{P} \cdot \hat{n}$$

$$\rho_s = \bar{D} \cdot \hat{n}$$

$$\bar{D} = \epsilon_0 \bar{E} + \bar{P}$$

$$\bar{P} = \chi_e \epsilon_0 \bar{E}$$

$$\bar{D} = \epsilon \bar{E}$$

$$\epsilon = \epsilon_r \epsilon_0$$

$$\epsilon_r = 1 + \chi_e$$

Relative permittivity

$$\bar{P} = (\epsilon_r - 1) \epsilon_0 \bar{E}$$

الشحنات الحرة

$$Q_{b+} = \int_S \rho_p ds$$

$$Q_{b-} = \int_V \rho_p dv$$

$Q_{b\text{tot}} = 0 \rightarrow$ material is electrically neutralized.

* Continuity Equation

$$\oint_S \vec{J} \cdot d\vec{s} = - \int_V \frac{d\rho_V}{dt} dV$$

* Relaxation (Time)

$$T_r = \frac{\epsilon_0 \epsilon_r}{\sigma} \quad (s)$$

$$\rho_V = \rho_{V_0} e^{-t/T_r} \quad (C/m^3)$$

ρ_{V_0} is initial charge density

* Boundary conditions -

A) Dielectric - to - dielectric

$$\vec{E}_1 = \vec{E}_{1t} + \vec{E}_{1n}$$

$$\vec{E}_{1n} = (\vec{E}_1 \cdot \hat{a}_n) \cdot \hat{a}_n$$

$$\vec{E}_{1t} = \vec{E}_1 - \vec{E}_{1n}$$

$$\vec{E}_{2t} = \vec{E}_{1t}$$

$$\vec{D}_{2n} - \vec{D}_{1n} = \rho_s \quad (\text{if } \rho_s = 0 \rightarrow \vec{D}_{1n} = \vec{D}_{2n})$$

$$\vec{D}_{2n} = \epsilon_0 \epsilon_r \vec{E}_{2n}$$

$$\vec{E}_{2n} = \frac{\epsilon_r}{\epsilon_0} \vec{E}_{1n}$$

$$\theta_2 = \sin^{-1} \left(\frac{E_{1t}}{E_2} \right) = \cos^{-1} \left(\frac{E_{2n}}{E_2} \right) = \tan^{-1} \left(\frac{E_{1t}}{E_{2n}} \right)$$

$$\alpha_2 = 90 - \theta_2$$

(B) Dielectric - to - Conductor

$$\vec{D}_{1n} = \rho_s \hat{a}_n$$

$$\vec{E}_{1n} = \frac{\rho_s}{\epsilon_0 \epsilon_r} (-\hat{a}_z)$$

CH6 Resistance and Capacitance -

$$R = \frac{V}{I} = \frac{-\int_L \vec{E} \cdot d\vec{L}}{\int_S \sigma \vec{E} \cdot d\vec{s}}$$

- Steps to find R & C -

1) Choose suitable coordinates

2) Assume (+Q) and (-Q)

3) $Q = \int_S \epsilon \vec{E} \cdot d\vec{s}$ (Find \vec{E})

$$C = \frac{Q}{V} = \frac{\int_S \epsilon \vec{E} \cdot d\vec{s}}{-\int_L \vec{E} \cdot d\vec{L}}$$

4) Find $V = -\int_L \vec{E} \cdot d\vec{L}$ / $I = \int_S \sigma \vec{E} \cdot d\vec{s}$

Notes R & C must be +ve values

~~Resistivity~~

CH7 Magnetostatic Fields -

- Biot-Savart's Law!

$$d\vec{H} \propto \frac{I \sin(\alpha) d\vec{L}}{r^2}, \quad \alpha \text{ is angle between } d\vec{L} \text{ \& } \vec{r}$$

- For line current

$$\vec{H} = \int_L \frac{I d\vec{L} \times \vec{r}}{4\pi r^3}, \quad I \text{ is Line Current (A/m)}$$

- For surface current

$$\vec{H} = \int_S \frac{\vec{K} \times \vec{r}}{4\pi r^3} d\vec{s}, \quad \vec{K} \text{ is Surface Current (A/m)}$$

- For volume current

$$\vec{H} = \int_V \frac{\vec{J} \times \vec{r}}{4\pi r^3} dV, \quad \vec{J} \text{ is Volume Current (A/m)}$$

- \vec{H} For Straight Finite lines

$$\vec{H} = \frac{I}{4\pi r} (\cos\alpha_2 - \cos\alpha_1) \hat{a}_\phi$$

$$\hat{a}_\phi = \hat{a}_1 \times \hat{a}_2$$

- \vec{H} For Semi-infinite lines -

$$\vec{H} = \frac{I}{4\pi r} \hat{a}_\phi$$

- \vec{H} For infinite lines -

$$\vec{H} = \frac{I}{2\pi r} \hat{a}_\phi$$

* Ampere's Law -

$$\oint_L \vec{H} \cdot d\vec{L} = I_{enc}$$

* \vec{H} For infinite Sheets - ($K = \vec{K}$)

$$\vec{H} = \frac{1}{2} \vec{K} \times \hat{a}_n$$

\hat{a}_n is unit vector directed from the sheet to the point.

* Magnetic Flux density (\vec{B}) :-

$$\vec{B} = \mu_0 \vec{H}$$

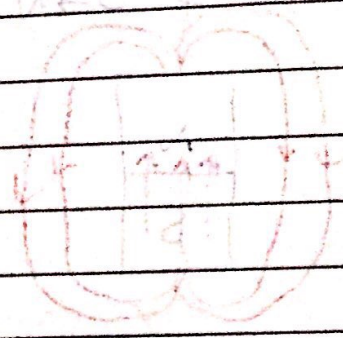
μ_0 is Free space permeability ($4\pi \times 10^{-7}$)

\vec{B} For infinite line

$$\vec{B} = \frac{\mu_0 I}{4\pi r} (\cos\alpha_2 - \cos\alpha_1) \hat{a}_\phi$$

\vec{B} For infinite sheet

$$\vec{B} = \frac{\mu_0 \vec{K} \times \hat{a}_n}{2}$$



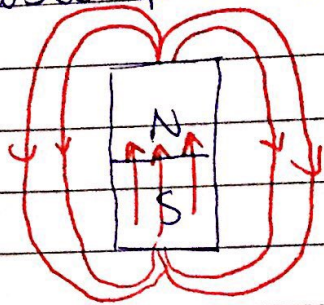
* Magnetic Flux (Ψ_m)

$$\Psi_m = \int_S \vec{B} \cdot d\vec{s} \quad (\text{wb})$$

* Flux Lines -

① Continuous

② From N \rightarrow S outside & S \rightarrow N inside



* Magnetic Gauss Law -

$$\Psi_m = \int_S \vec{B} \cdot d\vec{s} = 0$$

* Magnetic Potentials -

$$\vec{H} = -\nabla V_m$$

(V_m is Scalar potential)

(\vec{A} is Vector potential)

- Vector Potential for line currents

$$\vec{A} = \int \frac{\mu_0 I}{4\pi r} d\vec{L}$$

- Vector Potential for Surface currents

$$\vec{A} = \int_S \frac{\vec{K} \mu_0}{4\pi r} ds$$

- Vector Potential for Volume currents

$$\vec{A} = \int_V \frac{\vec{J} \mu_0}{4\pi r} dv$$

$$\Psi_m = \int_L \vec{A} \cdot d\vec{L}$$

$$\Psi_m = \int_S \vec{B} \cdot d\vec{s}$$

Ch 8 Magnetization -

$$\bar{M} = \lim_{\Delta V \rightarrow 0} \sum_{k=1}^N \bar{m}_k \quad , \quad \bar{m}_k \text{ magnetic moment}$$

- Free current

$$\bar{K} = \bar{H} \cdot \hat{a}_n$$

- Bound current

$$\bar{K}_b = \bar{M} \times \hat{a}_n$$

$$\bar{M} = \chi_m \bar{H} \quad , \quad \chi_m = \mu_r - 1 \quad (\text{Magnetization})$$

* Classification of magnetic materials -

- L Diamagnetic ($\mu_r < 1$) (i.e. Cu, lead, Al)
 - L Paramagnetic ($\mu_r > 1$) (i.e. Air)
 - L Ferromagnetic ($\mu_r \gg 1$) (i.e. iron, Nickel, rebar) \rightarrow Nonlinear
- } Linear

* Curie temperatures The temperature that if a ferromagnetic is heated above it loses its nonlinear properties and becomes a linear paramagnetic material. Thus if a permanent magnet is heated above the Curie temp. it loses its magnetization.

* Magnetic Boundary Conditions -

$$\mu = \mu_0 \mu_r \quad (\text{if free space, } \mu_r = 1)$$

$$\bar{H}_{in} = (\bar{H}_1 \cdot \hat{a}_n) \cdot \hat{a}_n$$

$$\bar{H}_{1t} = \bar{H}_1 - \bar{H}_{in}$$

$$\bar{B}_{in} = (\bar{B}_1 \cdot \hat{a}_n) \cdot \hat{a}_n$$

$$\bar{B}_{1t} = \bar{B}_1 - \bar{B}_{in}$$

$$\bar{B}_{in} = \bar{B}_{2n}$$

$$(\bar{H}_1 - \bar{H}_2) \times \hat{a}_n = \bar{K} \quad (\text{if } \bar{K} = 0 \rightarrow \bar{H}_{1t} = \bar{H}_{2t}) \quad \tan \theta_1 = \frac{H_{1t}}{H_{1n}}$$

$$\alpha_1 = 90 - \theta_1$$

(27)

* Inductors:

$$L = \frac{\lambda}{I} \text{ (H)}, \quad \lambda = N \cdot \Psi, \quad \Psi = \int_S \vec{B} \cdot d\vec{s}$$

* Magnetic energy:-

$$W_m = \frac{1}{2} \int_V \vec{H} \cdot \vec{B} \, dV \text{ (J)}$$

$$= \frac{1}{2} \int_V \mu H^2 \, dV \text{ (J)}$$

$$= \frac{1}{2} \int_V \frac{B^2}{\mu} \, dV \text{ (J)}$$

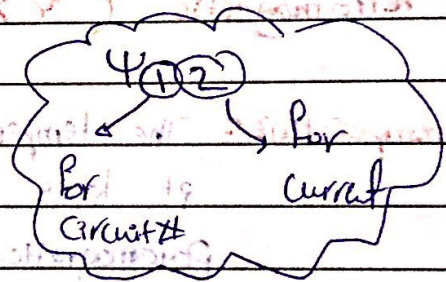
- If uniform:-

$$W_m = \frac{1}{2} L I^2 \Rightarrow L = \frac{2W_m}{I^2}$$

* Self inductance:-

$$L_{11} = \frac{\lambda_{11}}{I_1} = \frac{N_1 \Psi_{11}}{I_1}$$

$$L_{22} = \frac{\lambda_{22}}{I_2} = \frac{N_2 \Psi_{22}}{I_2}$$

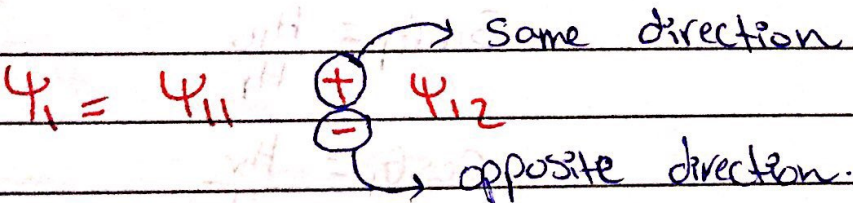


* Mutual inductance:-

$$M_{(1)2} = \frac{\lambda_{12}}{I_2} = \frac{N_1 \Psi_{12}}{I_2}$$

$$M_{(2)1} = \frac{\lambda_{21}}{I_1} = \frac{N_2 \Psi_{21}}{I_1}$$

- total flux in circuit 1:- (Ψ_1)



$$\Psi_1 = \Psi_{11} + \Psi_{12}$$

* Total inductance of circuit is

$$L = L_{11} + M_{12} + M_{21} + L_{22}$$

$\begin{matrix} \nearrow \text{iP Flux +} \\ \ominus \\ \ominus \\ \searrow \text{iP Flux -} \end{matrix}$

* Total energy is -

$$W_m = \frac{1}{2} L_{11} I_1^2 + \frac{1}{2} L_{22} I_2^2 + \left(\frac{1}{2} M_{12} I_2^2 + \frac{1}{2} M_{21} I_1^2 \right)$$

$$\frac{I_2}{I_1} = \frac{N_1}{N_2}$$

* Procedure to find (L) :-

- 1) Choose suitable coordinates
- 2) Assume current
- 3) Find B
- 4) $\Psi = \int \vec{B} \cdot \vec{ds} \rightarrow L = \frac{N\Psi}{I}$

or

$$W_m = \frac{1}{2} \int_V \vec{B}^2 dV \rightarrow L = \frac{2W_m}{I^2}$$

* Magnetic Circuits -

Electrical Circuit	Magnetic circuit
V_{emf}	$V_{emf} = F$
I	Ψ
$R = \frac{V}{I} = \frac{L}{G}$	$R_m = \frac{F}{\Psi} = \frac{l}{\mu_0 \mu_r N^2 A}$
$G = 1/R$	$P = 1/R_m$
$I = \int_S \vec{J} \cdot \vec{ds}$	$\Psi = \int_S \vec{R}_B \cdot \vec{ds}$
$W_E = \frac{1}{2} \int_V \epsilon E^2 dV$	$W_m = \frac{1}{2} \int_V \mu H^2 dV$
ϵ	μ

Principle of duality

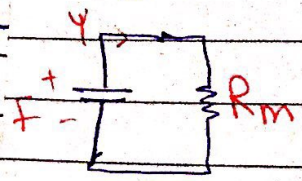
* Magnetic Resistance (Reluctance) $(\frac{1}{\mu})$

$$R_m = \frac{L_c}{\mu_0 \mu_r A_c}$$

$$L_c = 2\pi r_0 \quad (\text{toroid})$$

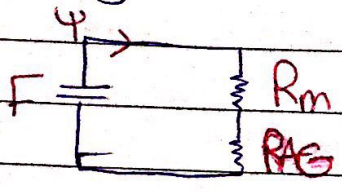
$$A_c = \pi t^2 \quad (\text{toroid})$$

* Magnetic Circuits



$$\Psi = \frac{F}{R_m} = \frac{NI}{\frac{L_c}{\mu_0 \mu_r A_c}}$$

* Magnetic circuit with air gaps-



$$R_m = \frac{L_c}{\mu_0 \mu_r A_c}$$

$$R_{AG} = \frac{L_{GA}}{\mu_0 A_c} \quad (\mu_r = 1)$$

$$R_{eq} = R_m + R_{AG}$$

$$\Psi = \frac{F}{R_{eq}}$$

Force in the air gaps-

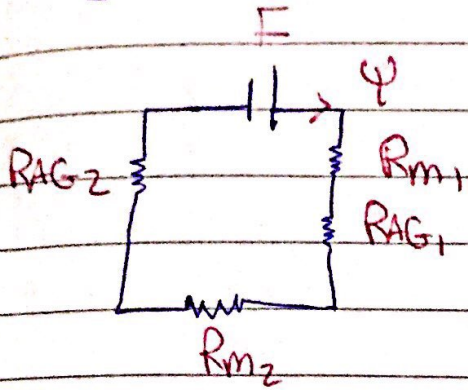
(Magnetic Tractive Force) (F_{MT})

$$F_{MT} = \frac{B^2 A_c}{2\mu_0}$$

$$B = \frac{\Psi}{A_c}$$

$$\text{Pressure} = \frac{F_{MT}}{A_c}$$

* Magnetic Limitations :-



$$R_{m1} = \frac{Lc_1}{\mu_0 \mu_{r1} A_c}$$

$$R_{m2} = \frac{Lc_2}{\mu_0 \mu_{r2} A_c}$$

$$R_{AG1} = \frac{L A_c}{\mu_0 A_c}$$

$$R_{AG2} = R_{AG1}$$

$$R_{eq} = 2R_{AG} + R_{m1} + R_{m2}$$

$$F_{MT} = mg = \frac{B^2 A_c}{2\mu_0}$$

* CH 9 Time Varying Fields

- Sources for time varying fields :-

- 1) Charge moving with acceleration
- 2) AC current flowing in wire.

* Faraday's Law :-

$$V_{emf} = - \frac{d\psi}{dt} \quad (\text{if } N=1)$$

$$(\psi = \int_S \vec{B} \cdot d\vec{s})$$

$$V_{emf} = \oint \vec{E} \cdot d\vec{L} = - \frac{d}{dt} \int_S \vec{B} \cdot d\vec{s}$$

1) Stationary loop in time-varying \vec{B} field (Transformer emf)

$$V_{emf} = \oint_L \vec{E} \cdot d\vec{L} = - \int_S \frac{d\vec{B}}{dt} \cdot d\vec{s}$$

2) Moving loop in static \vec{B} field (Motional emf)

$$V_{emf} = \oint_L \vec{E} \cdot d\vec{L} = \oint_L (\vec{u} \times \vec{B}) \cdot d\vec{L}$$

u : velocity

3) Time varying field with moving loop

$$V_{emf} = \int_L \vec{E} \cdot d\vec{l} = - \int_S \frac{d\vec{B}}{dt} \cdot d\vec{s} + \int (\vec{u} \times \vec{B}) \cdot d\vec{l}$$

* Displacement current - (\vec{J}_d)

$$\int_L \vec{H} \cdot d\vec{l} = \int_S (\vec{J} + \vec{J}_d) \cdot d\vec{s}$$

\vec{J}_d : Displacement current density (A/m^2)

* Continuity equation -

$$\int_L \vec{H} \cdot d\vec{l} = \int_S (\vec{J} + \frac{d\vec{D}}{dt}) \cdot d\vec{s}$$

$$\vec{J}_d = \frac{d\vec{D}}{dt}, \quad \vec{D} = \epsilon \vec{E}$$

$\vec{J}_{conduction} = \sigma \vec{E}$
 $\vec{J}_{convection} = \rho_v \vec{u}$
 $\vec{J}_{displacement} = \frac{d\vec{D}}{dt}$

* Time harmonic fields -

- Complex Numbers

↳ Euler identity: $e^{j\theta} = \cos\theta + j\sin\theta$

- Rectangular form of complex numbers -

$$Z = x + jy$$

Real \downarrow \downarrow imaginary

- Polar form

$$Z = r \angle \theta$$

$$r = \sqrt{x^2 + y^2} \quad \theta = \tan^{-1} \left(\frac{\text{imaginary}}{\text{real}} \right)$$

Complex conjugate (*)

$$Z = x + jy = r \angle \theta = r e^{j\theta}$$

$$Z^* = x - jy = r \angle -\theta = r e^{-j\theta}$$

- Exponential form

$$r e^{j\theta}$$

* Phasor domains -

$$I_0 e^{j\omega t} = I_s \text{ (phasor)}$$

$\frac{d}{dt} (e^{j\omega t}) = (j\omega) e^{j\omega t}$
 $\int_t e^{j\omega t} dt = \frac{1}{j\omega} e^{j\omega t}$

CH 10 Electromagnetic wave Propagation

- λ : wave length
- u : speed
- T : period
- ω : radian frequency

$$\lambda = uT \quad (m)$$

$$u = f\lambda \quad (T = \frac{1}{f})$$

$$\omega = 2\pi f \quad (rad/s)$$

$$\beta = \frac{\omega}{u} \quad (rad/m)$$

$$T = \frac{2\pi}{\omega} \quad (s)$$

$$\beta = \frac{2\pi}{\lambda}$$

$\beta = |\beta| \cos \theta \hat{a}_z$

$$\vec{E} = 50 \cos(10^8 t + \beta z) \hat{a}_z$$

$$\hat{a}_k = -\hat{a}_x$$

$$\sin(\psi + \frac{\pi}{2}) = \pm \cos \psi$$

$$\sin(\psi \pm \pi) = -\sin \psi$$

$$\cos(\psi \pm \frac{\pi}{2}) = \mp \sin \psi$$

$$\cos(\psi \pm \pi) = -\cos \psi$$

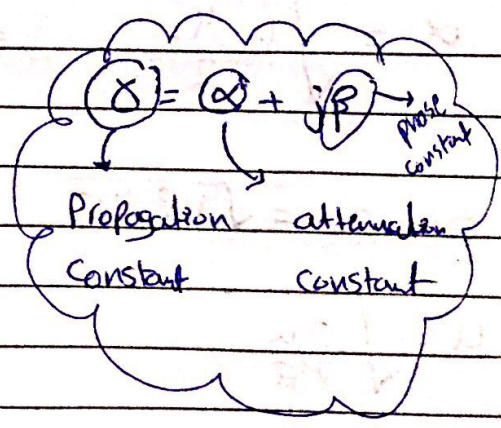
*Wave propagation in lossless media:-

$$(E = E_0 E_r, \quad \mu = \mu_0 \mu_r, \quad \sigma = 0)$$

$$\alpha = 0 \quad (\text{since } \sigma = 0)$$

$$\beta = \omega \sqrt{\mu \epsilon}$$

$$u = \frac{1}{\sqrt{\mu \epsilon}} = \frac{c}{\sqrt{\mu_r \epsilon_r}}$$



$$\lambda = \frac{2\pi}{\beta}$$

$$c = \frac{1}{\sqrt{\mu_0 \epsilon_0}}$$

speed of light

$\mu = \sqrt{\frac{\mu}{\epsilon}} \quad (90^\circ)$

$\vec{E} \neq \vec{H}$ are in phase

intrinsic impedance

$$\vec{E} = E_0 \cos(\omega t - \beta z) \hat{a}_x$$

$$\vec{H} = \frac{E_0}{\mu} \cos(\omega t - \beta z) \hat{a}_y$$

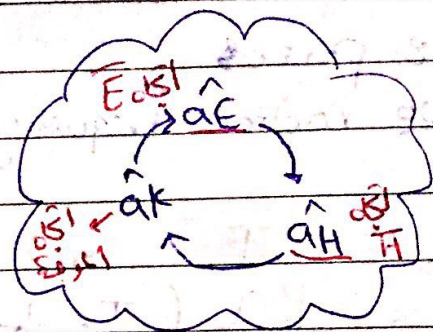
$$\hat{a}_z \times \hat{a}_x = \hat{a}_y \quad (33)$$

*Wave propagation in free space:-
 $(\epsilon = \epsilon_0, \mu = \mu_0, \sigma = 0)$

$$\alpha = 0 \text{ (since } \sigma = 0)$$

$$\beta = \omega \sqrt{\mu_0 \epsilon_0} = \frac{\omega}{c}$$

$$u = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = c \text{ Speed of light}$$



$$\eta = \sqrt{\frac{\mu_0}{\epsilon_0}} = 120\pi \Omega$$

\vec{E} & \vec{H} are in phase

$$\lambda = \frac{2\pi}{\beta}$$

*Skindepth (δ)

$$\delta = \frac{1}{\alpha} = \infty$$

1 NP = $20 \log e$
 1 NP = 8.686 dB

*Wave propagation in a good conductor:-
 $(\epsilon = \epsilon_0, \mu = \mu_0 \mu_r, \sigma \approx \infty)$

$$\alpha = \sqrt{\frac{\omega \mu \sigma}{2}} = \sqrt{\pi f \mu \sigma}$$

$$\beta = \alpha = \sqrt{\pi f \mu \sigma}$$

$$\eta = \sqrt{\frac{j\omega\mu}{\sigma}} = \sqrt{\frac{\omega\mu}{\sigma}} \angle 45^\circ$$

$$u = \sqrt{\frac{2\omega}{\mu\sigma}}$$

\vec{E} leads \vec{H} by 45°

$$\lambda = \frac{2\pi}{\beta}$$

$$\vec{E} = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \hat{a}_x$$

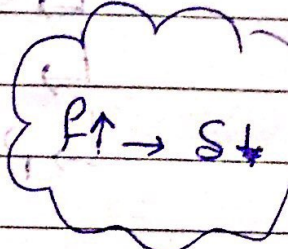
$$\delta = \frac{1}{\alpha} = \frac{1}{\sqrt{\pi f \mu \sigma}}$$

$$\vec{H} = \frac{E_0}{\eta} e^{-\alpha z} \cos(\omega t - \beta z - 45^\circ) \hat{a}_y$$

* Application of skin depth (Coaxial cable) :-

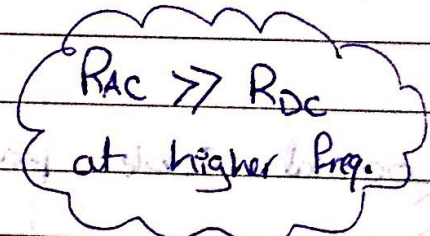
at DC ($f=0$)

$$R = \frac{L}{\sigma_c A}, \quad A = \pi a^2$$



at AC ($f > 0$)

$$R = \frac{L}{\sigma_c A}, \quad A = 2\pi a$$



* Power -

$$\vec{P} = \vec{E} \times \vec{H} \quad (\text{W/m}^2)$$

↓
Poynting vector

$$\overline{P}_{avg} = \frac{1}{T} \int \vec{E} \times \vec{H} dt$$

$$\overline{P}_{avg} = \frac{1}{2} \text{Re} \{ \vec{E}_s \times \vec{H}_s^* \} \quad (\text{W/m}^2)$$

* total power -

$$P_{avg} = \int_S \overline{P}_{avg} \cdot d\vec{s}$$

* CH II Transmission Lines (T.L.)

- ↳ Coaxial cable
- ↳ Twin wire cable
- ↳ Planar lines → Strip line
 - ↳ micro strip line
 - ↳ Slot line

* Coaxial Cable Parameters :-

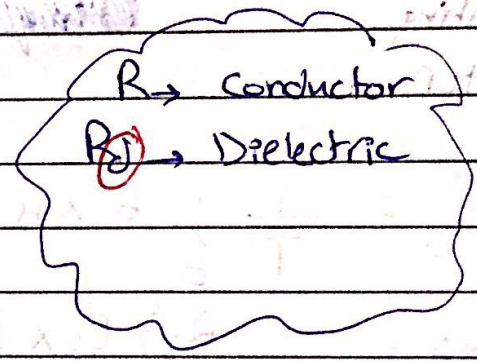
$$\frac{R}{L} = \frac{1}{2\pi \epsilon_0 \sigma} \left(\frac{1}{a} + \frac{1}{b} \right) \quad (\Omega/m)$$

Conductor

$$\frac{G}{L} = \frac{2\pi \sigma}{\ln(\frac{b}{a})} \quad \text{Dielectric} \quad (S/m)$$

$$\frac{C}{L} = \frac{2\pi \epsilon_0 \epsilon_r}{\ln(\frac{b}{a})} \quad \text{Dielectric} \quad (F/m)$$

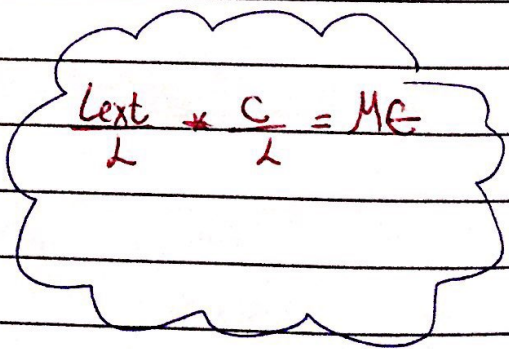
$$\frac{L}{L} = \frac{\mu_0 \mu_r}{2\pi} \ln(\frac{b}{a}) \quad \text{Dielectric} \quad (H/m)$$



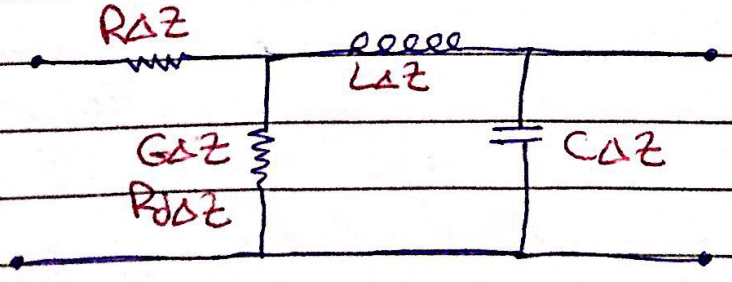
* Relaxation Time (Tr)

$$T_r = \frac{\epsilon_0 \epsilon_r}{\sigma}$$

$$\frac{C}{G} = \frac{\epsilon}{\sigma}$$

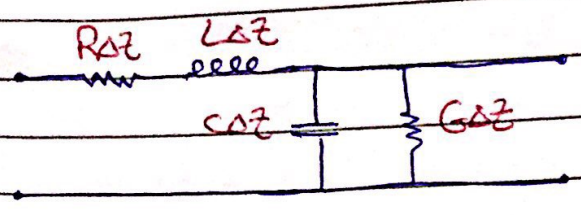


* Exact circuit for ~~microstrip~~ T.L.



* T.L. equivalent circuits (Approximate)

L-Type circuit (95% accurate)



T.L. equations - (For L-Type)

$$\frac{d^2 V_s(z)}{dz^2} - \gamma^2 V_s(z) = 0 \quad , \quad \frac{d^2 I_s(z)}{dz^2} - \gamma^2 I_s(z) = 0$$

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

- Solution to the T.L. equ. (For L-Type)

$$V_s(z) = V_0^+ e^{-\gamma z} + V_0^- e^{\gamma z}$$

$$I_s(z) = I_0^+ e^{-\gamma z} + I_0^- e^{\gamma z}$$

* Z_0 : Characteristic impedance (Ω)

$$Z_0 = \frac{V_0^+}{I_0^+}$$

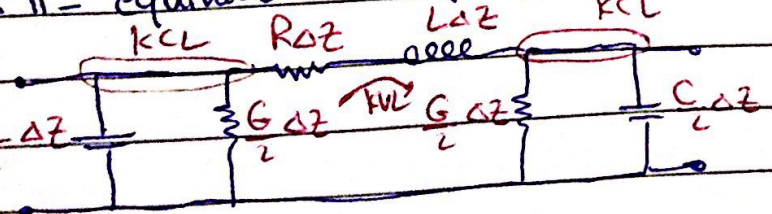
$$Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$$

$$\alpha = \frac{\omega}{\beta} \quad , \quad \lambda = \frac{2\pi}{\beta}$$

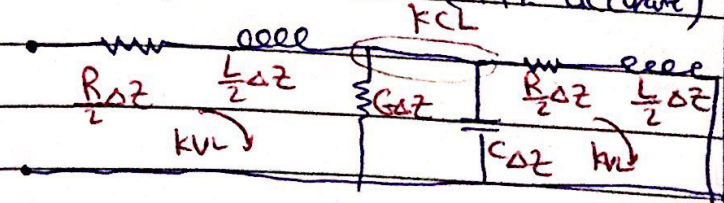
* Γ : reflection coefficient

$$\Gamma = \frac{V_0^-}{V_0^+}$$

* Π -equivalent ckt (99% accurate)



* T-equivalent ckt (99% accurate)



* Lossless T.L.

$(G = \infty \rightarrow R = 0)$

$(G = 0 \rightarrow R = 0)$

$Z = j\omega \sqrt{LC}$

$Z_0 = \sqrt{\frac{L}{C}}$

$\beta = \omega \sqrt{LC}, \alpha = 0$

$u = \frac{\omega}{\beta}$

$\lambda = \frac{2\pi}{\beta}$

$V(z,t) = V_0^+ \cos(\omega t - \beta z) + V_0^- \cos(\omega t + \beta z)$

$I(z,t) = \left(\frac{V_0^+}{Z_0}\right) \cos(\omega t - \beta z) + \left(\frac{V_0^-}{Z_0}\right) \cos(\omega t + \beta z)$

$I_0^+ \qquad I_0^-$

* Distortionless T.L.

$\frac{R}{L} = \frac{G}{C}$

$Z = \sqrt{RG} + j \frac{\omega L}{R} \sqrt{RG}$

$\beta = \omega \sqrt{LC}$

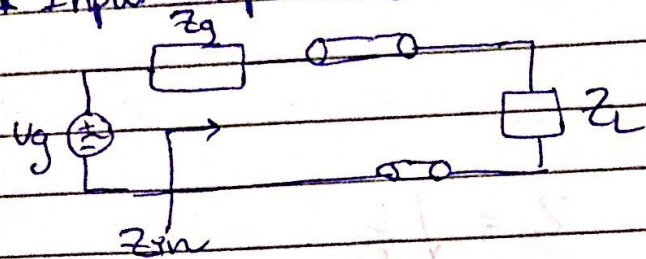
$Z_0 = \sqrt{\frac{L}{C}}$

$u = \frac{\omega}{\beta}$

$\lambda = \frac{2\pi}{\beta}$

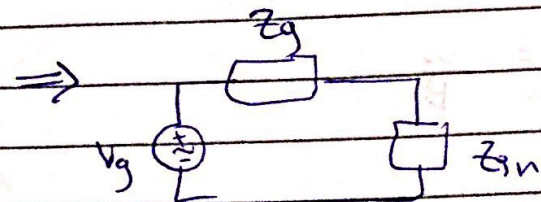
$V_s(z) = V_0^+ e^{-\alpha z} e^{-j\beta z} + V_0^- e^{\alpha z} e^{j\beta z}$

* Input impedance :-



$$Z_{in} = \frac{Z_0 Z_L + Z_0 \tanh \gamma L}{Z_0 + Z_L \tanh \gamma L}$$

for lossy & distortionless T.L.



$$V_0 = V_g \frac{Z_{in}}{Z_{in} + Z_g} \quad (\text{Voltage division})$$

$$V(z=0) = V_0, \quad V(z=L) = V_L$$

$$I(z=0) = I_0, \quad I(z=L) = I_L$$

$$I_0 = \frac{V_g}{Z_{in} + Z_g} \quad (\text{Ohm's Law})$$

* Standing wave Ratio (SWR) :-

$$S = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

$$|\Gamma| = \frac{|V_0^-|}{|V_0^+|}$$

* Reflection coefficient at the load :-

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} \quad (\text{if } Z_L \neq Z_0)$$

$$\text{Power} = \frac{1}{2} \text{Re} \left\{ \underset{\text{Peak}}{V_s} * \underset{\text{Peak}}{I_s^*} \right\}$$

$$V_{rms} = \frac{V_{peak}}{\sqrt{2}}$$

* Max power transfer :-

$$P = \frac{|V_0^+|^2}{2Z_0} (1 - |\Gamma|^2) \quad (\text{when } Z_L = Z_0)$$

\uparrow
 P_i

$$Z_{in \text{ s.c.}} = jZ_0 \tan(\beta L)$$

$$Z_{in \text{ o.c.}} = -jZ_0 \cot(\beta L)$$

Lossless

Max power transfer :- (Maximum Power Transfer Theorem)

$$P = \frac{|V_o|^2}{2Z_o} (1 - |P|^2)$$

(Note: In the original image, a red arrow labeled P_i points to the denominator $2Z_o$, and another red arrow labeled P_r points to the term $(1 - |P|^2)$.)

$$P_t = P_i - P_r$$

$P_t = \frac{|V_o|^2}{2Z_o}$

 max power transfer
($Z_L = Z_o$) (if $P_r = 0$)

* CHG

Parallel plate capacitor -

$$C = \frac{\epsilon S}{d}$$

$$R_d = \frac{d}{\epsilon S}$$

$$W_E = \frac{1}{2} CV^2$$

Cylindrical capacitor (coaxial capacitor)

$$C = \frac{2\pi\epsilon L}{\ln\left(\frac{b}{a}\right)}$$

$$R_d = \frac{\ln(b/a)}{2\pi\epsilon L}$$

$$W_E = \frac{1}{2} CV^2$$

Spherical capacitor

$$C = \frac{4\pi\epsilon}{\left(\frac{1}{a} - \frac{1}{b}\right)}$$

$$R_d = \frac{\left(\frac{1}{a} - \frac{1}{b}\right)}{4\pi\epsilon}$$

Isolated capacitor

$$C = 4\pi\epsilon a$$

$$R_d = \frac{1}{4\pi\epsilon a}$$