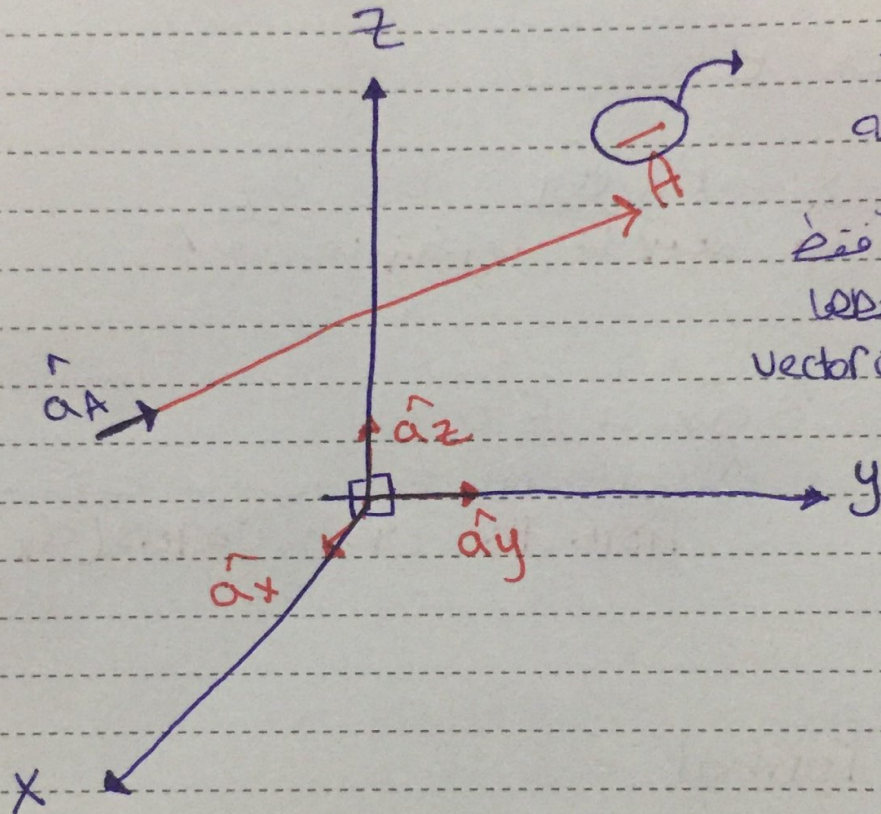


# CH1 Vectors Review

- How to write a vector -

$\vec{A}$   $\equiv$  Vector A (Magnitude of vector)

- in cartesian coordinates



هنا إشارة متجهة  
مقدارها فقط  
بدون اتجاه  
(Scalar) قيمة فقط  
- ما تبقى نحتاجها  
لحل نحكي عن Vector

\* Unit vector (Direction only) (magnitude =  $\frac{1}{\vec{v}}$ )

$\hat{a}_x$   $\equiv$  Unit vector in x-direction

هنا إشارة متجهة  
بدون اتجاه  
Unit vector

$$\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z \text{ (Long Format)}$$

$A_x, A_y, A_z$  = Vector components (Magnitude only)  
(Scalar)      vector  $A$   $\rightarrow$  ,  $\hat{a}_x$   $\leftarrow$

- if vector  $B$

$$\vec{B} = B_x \hat{a}_x + B_y \hat{a}_y + B_z \hat{a}_z$$

$\rightarrow$   $\hat{a}_x$   $\hat{a}_y$   $\hat{a}_z$   $\hat{a}_z$   $\hat{a}_y$   $\hat{a}_x$

- ex  $\vec{C} = 3 \hat{a}_x + 5 \hat{a}_z$

! Cartesian,  $\hat{a}_i$  ! كيف عرفت

From the unit vectors ( $\hat{a}_x, \hat{a}_z$ )

## (2) Short Format

$$\vec{A} = (A_x, A_y, A_z)$$

ex  $\vec{C} = (3, 0, 5)$

### \*\* Note

Don't mix between points & vectors.

$\vec{A} = (A_x, A_y, A_z) \rightarrow$  vector

$P(x, y, z) \rightarrow$  point.



\* Vector Magnitude (Scalar Quantity)

$$|\vec{A}| = A = \sqrt{A_x^2 + A_y^2 + A_z^2}$$

\* Unit vector along  $\vec{A}$  -

$$\hat{a}_A = \frac{\vec{A}}{A} = \frac{A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z}{\sqrt{A_x^2 + A_y^2 + A_z^2}}$$

$\vec{C} = 3\hat{a}_x + 5\hat{a}_z$

$$\hat{a}_C = \frac{3}{\sqrt{34}} \hat{a}_x + \frac{5}{\sqrt{34}} \hat{a}_z$$

③  $\vec{A} = A \hat{a}_A \rightarrow$  vector  $\hat{a}_A$  کی مقدار اور  
دائریہ جیسے  $\vec{A}$  کی

## \* Operations on vectors :-

### II Addition and Subtraction

المتجه هو كمية لها مقدار واتجاه

$$\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$$

$$\vec{B} = B_x \hat{a}_x + B_y \hat{a}_y + B_z \hat{a}_z$$

$$\vec{C} = \vec{A} + \vec{B}$$

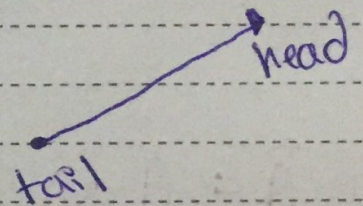
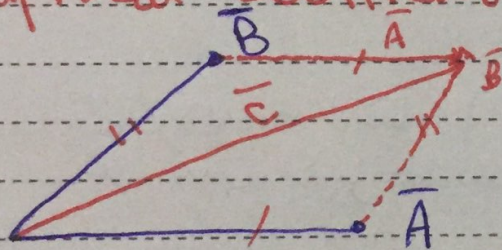
$$= (A_x + B_x) \hat{a}_x + (A_y + B_y) \hat{a}_y + (A_z + B_z) \hat{a}_z$$

بداية على نقطة  
الى هنا

From vector definition

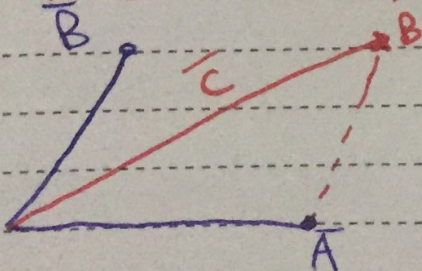
$$= C_x \hat{a}_x + C_y \hat{a}_y + C_z \hat{a}_z$$

### \* Graphical additions :-



نظرياً متوازي الأضلاع كل Vector يرسم الى Vector ويكون parallel معه من tail البداية ل head النهاية

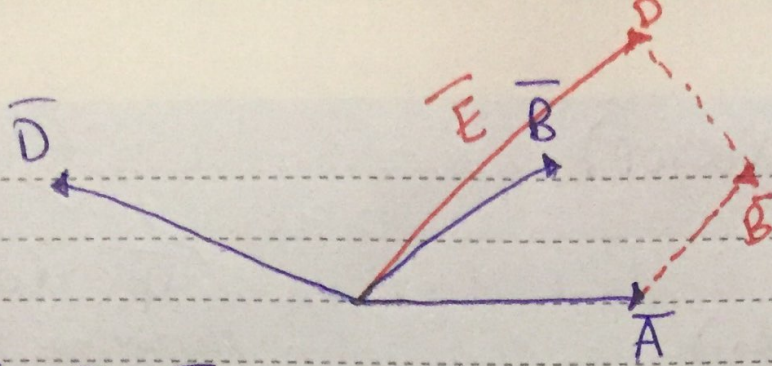
### Arrow method :-



عند رسم ال Vector الاول من tail الى head  
من ال Vector الثاني من tail الى head



ex



$$\vec{E} = \vec{A} + \vec{B} + \vec{D}$$

A کے لیے B کی طرف (1)

B کے لیے D کی طرف (2)

head D سے tail A تک (3)

### \* Subtraction :-

$$\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$$

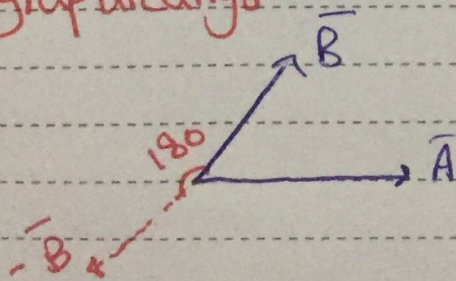
$$\vec{B} = B_x \hat{a}_x + B_y \hat{a}_y + B_z \hat{a}_z$$

$$\vec{D} = \vec{A} - \vec{B}$$

$$= (A_x - B_x) \hat{a}_x + (A_y - B_y) \hat{a}_y + (A_z - B_z) \hat{a}_z$$

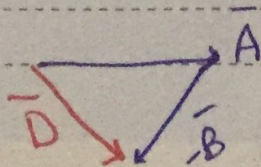
$$= D_x \hat{a}_x + D_y \hat{a}_y + D_z \hat{a}_z$$

### \* graphically :-



$$\vec{D} = \vec{A} - \vec{B}$$

$$= \vec{A} + (-\vec{B})$$



## \* Distance - (Vector)

•  $P(x_1, y_1, z_1)$

$$\vec{r}_P = r_{OP}$$

هو المتجه الذي يمتد من  
المنشأ إلى النقطة P

$\vec{r}_{PQ}$

•  $Q(x_2, y_2, z_2)$

↳ point هو

المسافة بين  
Q و P هو

$$\vec{r}_{PQ} = \vec{r}_Q - \vec{r}_P$$

$$= (x_2, y_2, z_2) - (x_1, y_1, z_1)$$

↳ Vector هو

$$= (x_2 - x_1)\hat{a}_x + (y_2 - y_1)\hat{a}_y + (z_2 - z_1)\hat{a}_z \quad \text{meters}$$

$$* \vec{r}_{PQ} = -\vec{r}_{QP}$$

$$\rightarrow |\vec{r}_{PQ}| = r_{PQ} = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$

متر  
↓  
(m)

هو مقدار  
المسافة magnitude

↳ direction gives

$$a \hat{r}_{PQ} = \frac{\vec{r}_{PQ}}{r_{PQ}} = -a \hat{r}_{QP}$$

هو المتجه الذي يمتد من  
النقطة P إلى Q هو direction  
magnitude



## ② Multiplication :-

a) Dot product  $\vec{A} \cdot \vec{B} \rightarrow$  Scalar quantity.

$$\vec{A} = (A_x, A_y, A_z)$$

$$\vec{B} = (B_x, B_y, B_z)$$

$$\vec{A} \cdot \vec{B} = |\vec{A}| |\vec{B}| \cos \theta_{AB}$$

لہ ہوں عندی معلوم الیٰی هو الزاویۃ  
عشان ہیک ضربن اد Vectors بیویں  
کس term صا  $\vec{A}$  ضربیہ ب  $\vec{B}$

$$\hookrightarrow A_x \hat{a}_x \cdot B_x \hat{a}_x$$

$$= A_x B_x (\hat{a}_x \cdot \hat{a}_x) \stackrel{1}{\rightarrow} \text{لسن ہاں لکوس قیمتہ } 1 =$$

$$= A_x B_x$$

زاویۃ لزاویۃ بیہ  $\hat{a}_x$  و  $\hat{a}_x$

$\hookrightarrow$  that's why it's scalar.  $1 = \cos(0)$

$$\Rightarrow \vec{A} \cdot \vec{B} = A_x B_x + A_y B_y + A_z B_z$$

$$* \hat{a}_n \cdot \hat{a}_m = \begin{cases} 1, & n = m \\ 0, & n \neq m \end{cases}$$

$$* \theta_{AB} = \cos^{-1} \left( \frac{\vec{A} \cdot \vec{B}}{AB} \right)$$

\* Properties -

$$\boxed{1} \vec{A} \cdot \vec{B} = \vec{B} \cdot \vec{A}$$

$$\boxed{2} \vec{A} \cdot \vec{A} = A^2 = A_x^2 + A_y^2 + A_z^2$$

$$\boxed{3} \vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$$



b) cross product  $\rightarrow$  vector

$$|\vec{A} \times \vec{B}| = AB \sin \theta_{AB}$$

$$\theta_{AB} = \sin^{-1} \frac{|\vec{A} \times \vec{B}|}{AB}$$

$$\vec{A} \times \vec{B} \perp \vec{A}, \vec{B}$$

$$\vec{A} \times \vec{B} = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$$

والتي أولها  $\hat{a}_x, \hat{a}_y, \hat{a}_z$   
وهي Unit  
Vector  
وهي Vector  
وهي Vector

3x3

$$\begin{aligned} \vec{A} \times \vec{B} &= (-1)^{1+1} (A_y B_z - A_z B_y) \hat{a}_x \\ &+ (-1)^{1+2} (A_x B_z - A_z B_x) \hat{a}_y \\ &+ (-1)^{1+3} (A_x B_y - A_y B_x) \hat{a}_z \end{aligned}$$

\* Properties -

$$\boxed{1} \vec{A} \times \vec{B} \neq \vec{B} \times \vec{A} \quad (\vec{A} \times \vec{B} = -\vec{B} \times \vec{A})$$

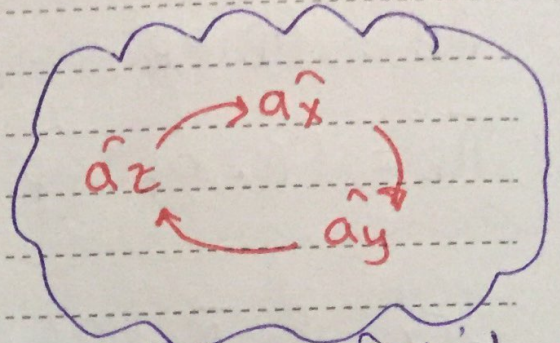
$$\boxed{2} \vec{A} \times (\vec{B} \times \vec{C}) \neq (\vec{A} \times \vec{B}) \times \vec{C} \quad (\text{الأولوية للأقواس})$$

$$\boxed{3} |\hat{a}_x \times \hat{a}_x| = (1)(1) \sin 0 = 0$$



\*  $|\hat{a}_x \times \hat{a}_y| = (1)(1) \sin 90^\circ = 1$

$\hat{a}_x \times \hat{a}_y = +\hat{a}_z$

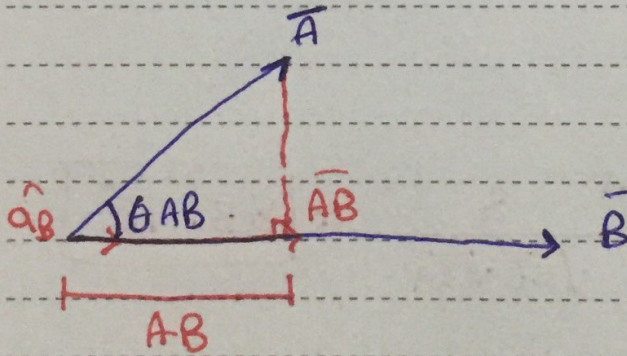


إذا امتسيت مع عقارب الساعة  
 الساعة تكون موجبة  
 إذا عكس عقارب الساعة  
 سالبة

\* Vector projection along another vector s-

→  $A_B$  = Scalar projection of (A) along (B)

$\vec{A}_B$  = Vector projection of (A) along (B)



$\cos \theta_{AB} = \frac{A_B}{A}$  المجاور  
الوتر

\*  $A_B = A \cos \theta_{AB}$

\*  $\cos \theta_{AB} = \frac{\vec{A} \cdot \vec{B}}{AB} = \frac{\vec{A} \cdot \hat{a}_B}{A(1)}$  ,  $\hat{a}_B = \frac{\vec{B}}{B}$

$\vec{A}_B = \vec{A} \cdot \hat{a}_B$  → لما ما أعرفه angle



$$A_B = \bar{A} \cdot \hat{a}_B$$

$$\bar{A}_B = AB \hat{a}_B$$

$$\bar{A}_B = (\bar{A} \cdot \hat{a}_B) \hat{a}_B$$

- Ex 3F  $\bar{A} = 3\hat{a}_x + 4\hat{a}_y + \hat{a}_z$

$$\bar{B} = 2\hat{a}_y - 5\hat{a}_z$$

Find a)  $\theta_{AB}$

b)  $\bar{A}_B$

Sol a)  $\theta_{AB} = \cos^{-1} \frac{\bar{A} \cdot \bar{B}}{AB} = \sin^{-1} \frac{|\bar{A} \times \bar{B}|}{AB}$

$$\bar{A} \cdot \bar{B} = 0 + 8 - 5 = 3$$

$$A = \sqrt{26}$$

$$B = \sqrt{29}$$

$$\theta_{AB} = \cos^{-1} \frac{3}{\sqrt{26}\sqrt{29}} = \boxed{83.73^\circ}$$

b)  $\bar{A}_B = (\bar{A} \cdot \hat{a}_B) \hat{a}_B$

$$\hat{a}_B = \frac{\bar{B}}{B} = \frac{(0, 2, -5)}{\sqrt{29}}$$

$$\hat{a}_B = \frac{2}{\sqrt{29}} \hat{a}_y - \frac{5}{\sqrt{29}} \hat{a}_z$$

$$\vec{AB} = \left( 0 + \frac{8}{\sqrt{29}} - \frac{5}{\sqrt{29}} \right) \left( 0, \frac{2}{\sqrt{29}}, \frac{-5}{\sqrt{29}} \right)$$

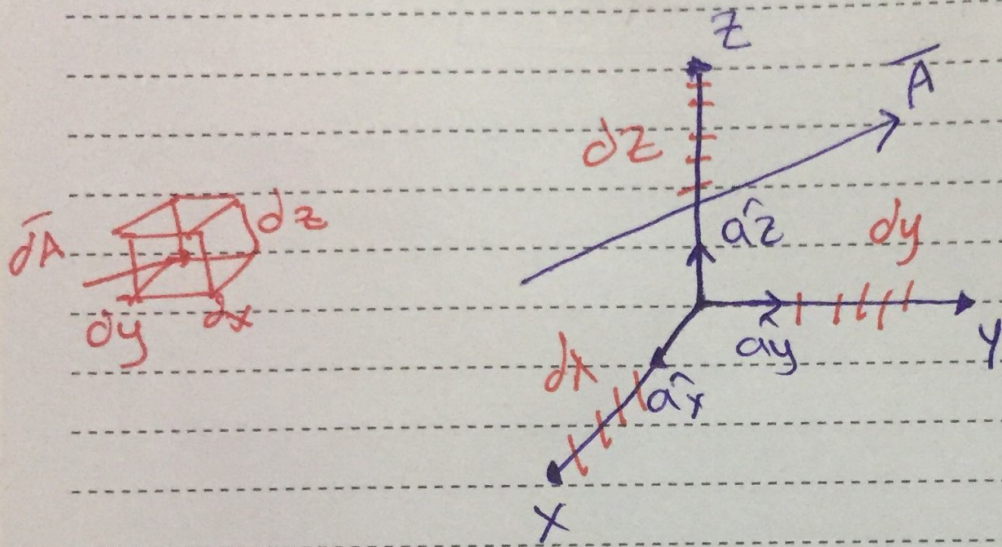
$$= \frac{3}{\sqrt{29}} \cdot \frac{1}{\sqrt{29}} (0, 2, -5)$$

$$= \cancel{\frac{3}{29}} \left[ \frac{6}{29} \hat{a}_y - \frac{15}{29} \hat{a}_z \right]$$

# CH2 Coordinate Systems and Transformations

## 1) Cartesian coordinates:-

$$\left. \begin{aligned} -\infty < x < \infty \\ -\infty < y < \infty \\ -\infty < z < \infty \end{aligned} \right\} \rightarrow \text{3D object Infinite Box}$$



## Differential elements:-

$$dx, dy, dz$$

## \* Differential length ( $dL$ ) (vector).

$$dL = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

## \* Differential Normal Surface Area ( $dS$ ) (vector).

$$dS_{\text{front}} = dy dz \hat{a}_x$$

all sides  $\vec{S}$

(top, front, bottom, left, right, back)

Normal surface is outside of the object.

$$d\vec{s}_{\text{back}} = dy dz (-\hat{a}_x)$$

اطراف حوضت سائبة  
بين للاجاء

$$d\vec{s}_{\text{right}} = dx dz \hat{a}_y$$

- حدد لفاوري بالاول  
بعد بين فتره اللي  
فلاو بولان

$$d\vec{s}_{\text{left}} = -dx dz \hat{a}_y$$

$$d\vec{s}_{\text{top}} = dx dy \hat{a}_z$$

$$d\vec{s}_{\text{bottom}} = -dx dy \hat{a}_z$$

\* Differential Volume ( $dV$ ) (Scalar).

$$dV = dx dy dz$$

\* 2D Surfaces -

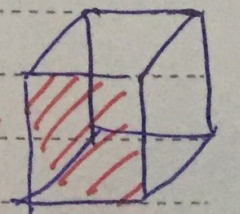
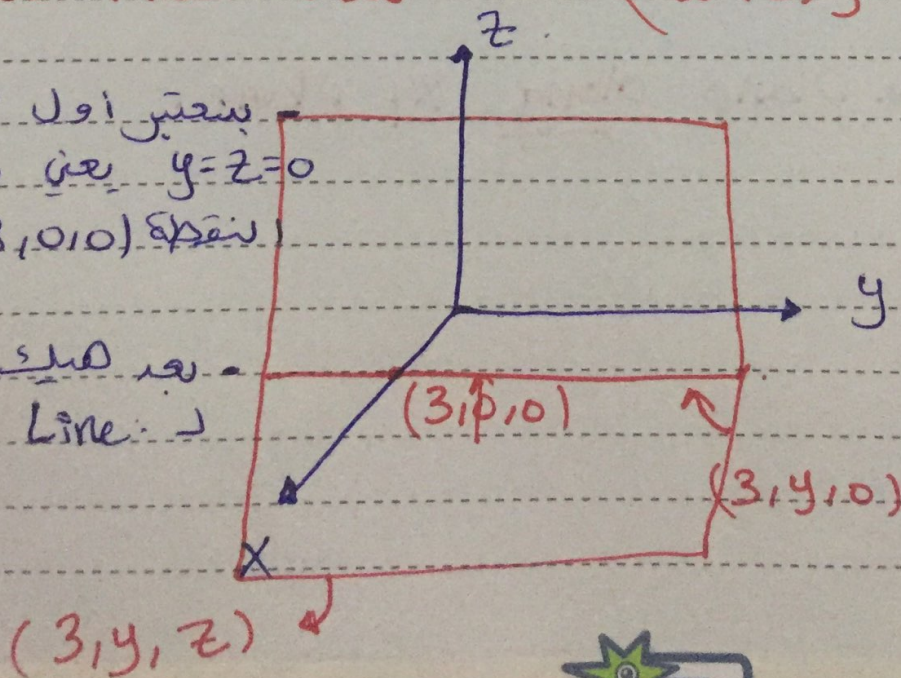
↳ by fixing one variable.

-if  $x=3$

↳ we know now that  $(-\infty < z, y < \infty)$

بينعتين اول اشئ انه  
 $y=z=0$  يعني بينوعى  
نقطة  $(3,0,0)$

بعد هيك كقول y  
Line



infinite  
plane  
parallel to  
yz plane.

- what is the normal on that surface?

-  $a\hat{x}$  or  $(-a\hat{x})$

مثلاً  $a = \cos \alpha$

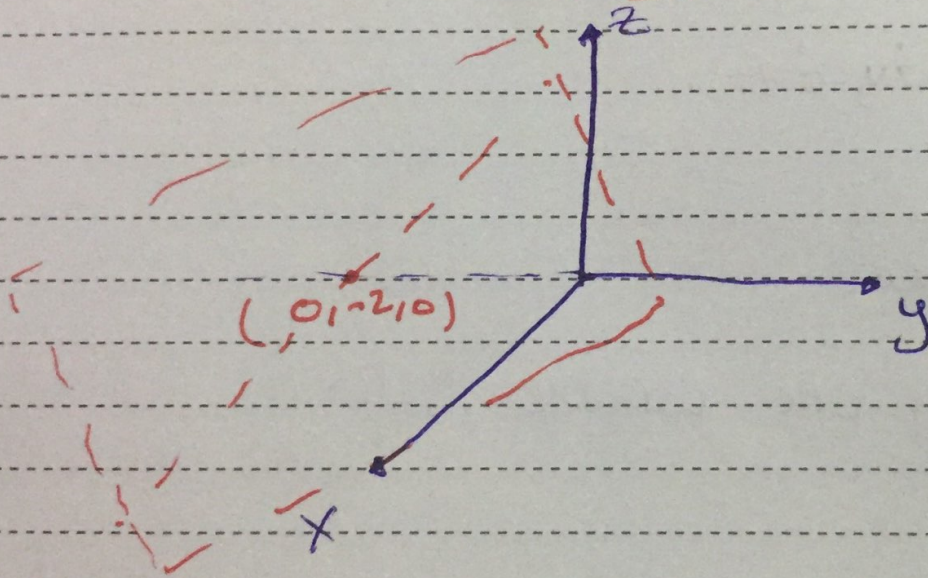
if  $(10, 0, 0) \rightarrow$  is a normal  
to plane  $x=10$

- if  $x=0$

$\rightarrow$  infinite plane along  $yz$  plane.

- if  $y=-2$

$\rightarrow$  infinite plane parallel to  $xz$  plane.



- if  $z=0$

$\rightarrow$  infinite plane along  $xy$  plane.

\* 1 D Segment :

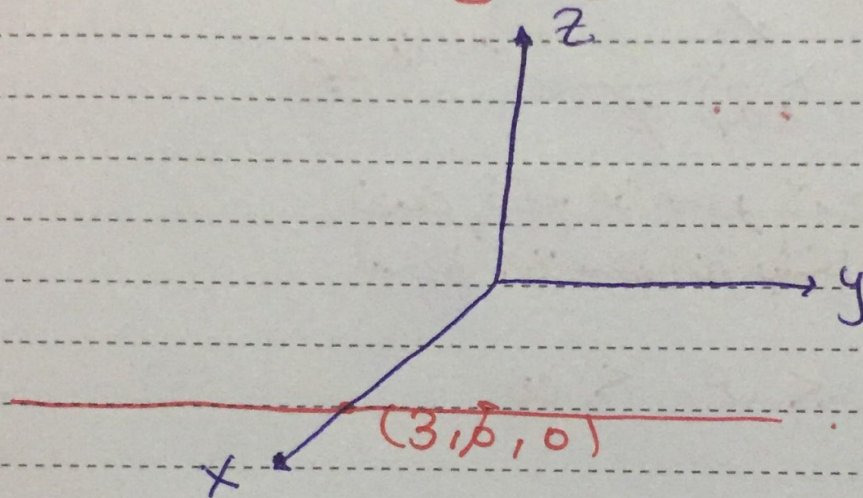
↳ by fixing 2 variables.

if  $x, z$  are constants. ( $x \neq 0, z \neq 0$ )

↳ infinite line //  $y$ -axis.

-if  $x=0, z=0$ .

↳ infinite line along  $y$ -axis.



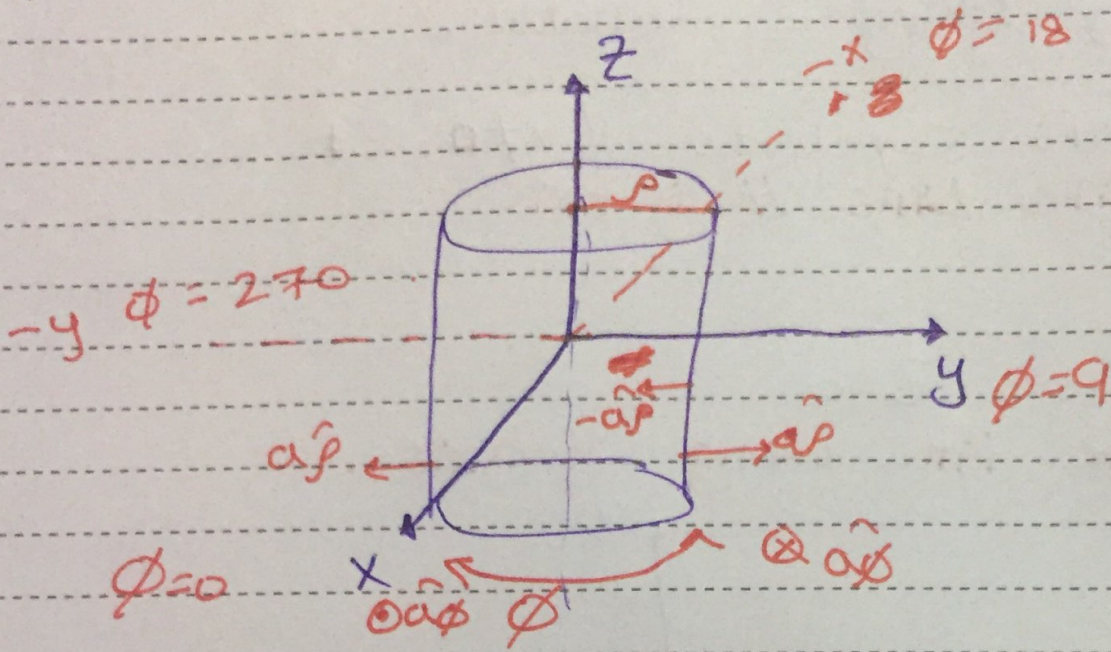
-if  $y = -2, z = -2$

↳ infinite line //  $x$ -axis.

-infinite line along  $z$ -axis.

↳  $x=0, y=0$ .

# \* Cylindrical coordinates -



$\rho \rightarrow$  نصف القطر من محور الاستوانة  
 لسطح الاستوانة بشكل عام  $\rho$

$$0 < \rho < \infty$$

$\phi \rightarrow$  rotation.

$$0 < \phi < 2\pi$$

بجذورها، إنه يخلف الأبعاد باتجاه المحاور  
 وحركته، ليد يتأون حركته الاستوانة

$$\infty > z > \infty$$



- How to write a vector in cylindrical coordinates -

$$\vec{A} = A_\rho \hat{a}_\rho + A_\phi \hat{a}_\phi + A_z \hat{a}_z$$

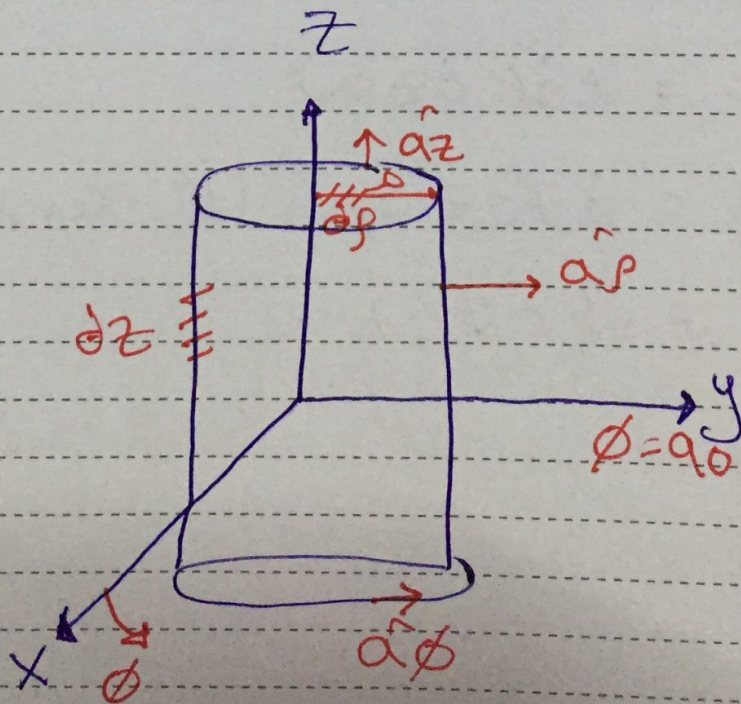
\* Unit vectors -

$$\hat{a}_\rho, \hat{a}_\phi, \hat{a}_z$$

\*  $(3, 60^\circ, 4)$

$$\begin{array}{ccc} \uparrow & \uparrow & \uparrow \\ \rho & \phi & z \end{array}$$

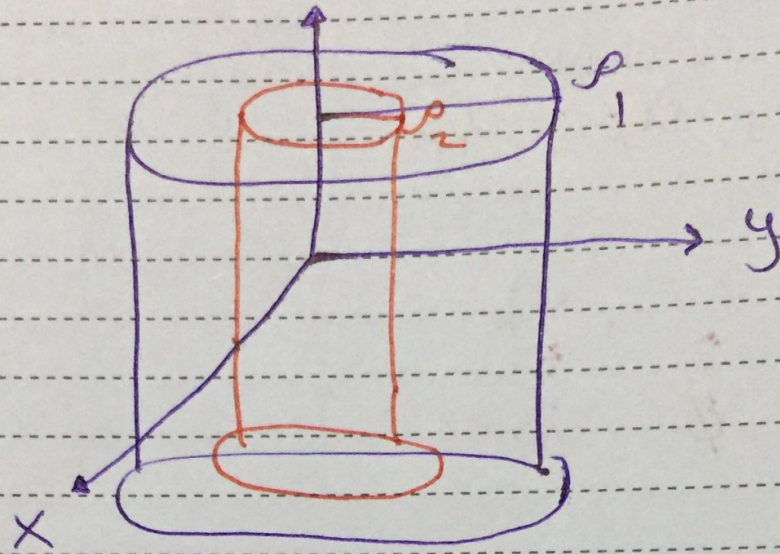
\*  $0 \leq \rho < \infty$   
 $0 \leq \phi < 2\pi$   
 $-\infty < z < \infty$  }  $\rightarrow$  infinite solid cylindrical



## \* Differential Elements:-

$$dp, \rho d\phi, dz$$

$$p_1 > p_2$$



$$\vec{dL} = dp \hat{a}_p + \rho d\phi \hat{a}_\phi + dz \hat{a}_z$$

$$\vec{ds}_{top} = \rho dp d\phi \hat{a}_z$$

$$\vec{ds}_{bottom} = -\rho dp d\phi \hat{a}_z$$

$$\vec{ds}_{side} = \rho d\phi dz \hat{a}_p$$

$$\vec{ds}_{cut} = dp dz \hat{a}_\phi \quad (\phi = \text{constant})$$

$$dV = \rho dp d\phi dz$$

## \* 2D Surface s -

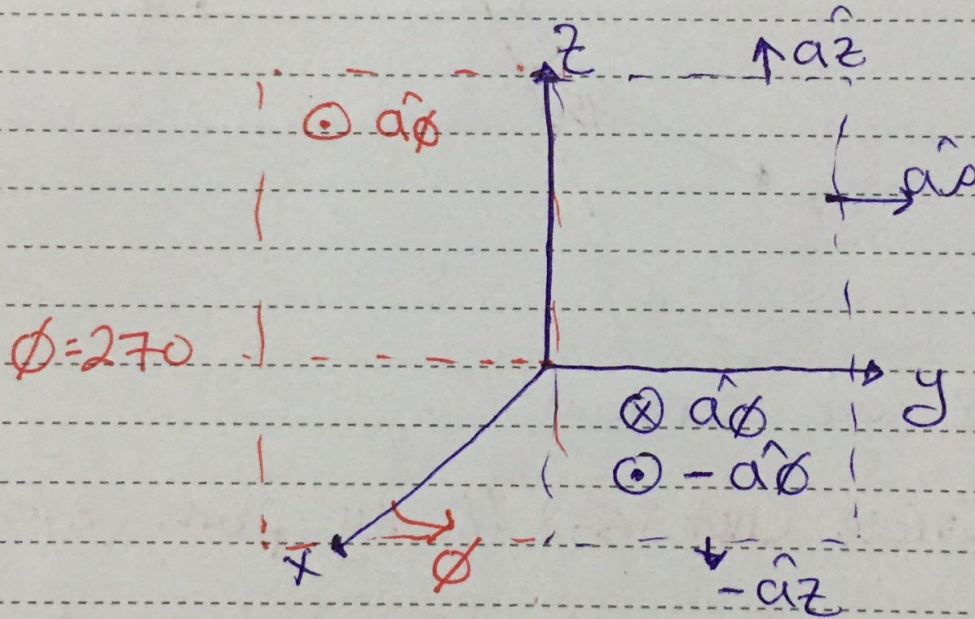
-  $\rho = \text{constant} \rightarrow$  inf. hollow cylinder

i.e.  $\rho = 5, \phi, z \rightarrow$  Variables

if  $\rho = 0 \rightarrow$  inf. line along z-axis.

-  $\phi = \text{constant} \rightarrow$  inf. plane.

i.e.  $\phi = 90^\circ \rightarrow$  inf. plane along yz plane.



-  $z = \text{constant} \rightarrow$  inf. Disk // xy plane (if  $z \neq 0$ )

inf. Disk along xy plane (if  $z = 0$ )



## \* 1D Segments -

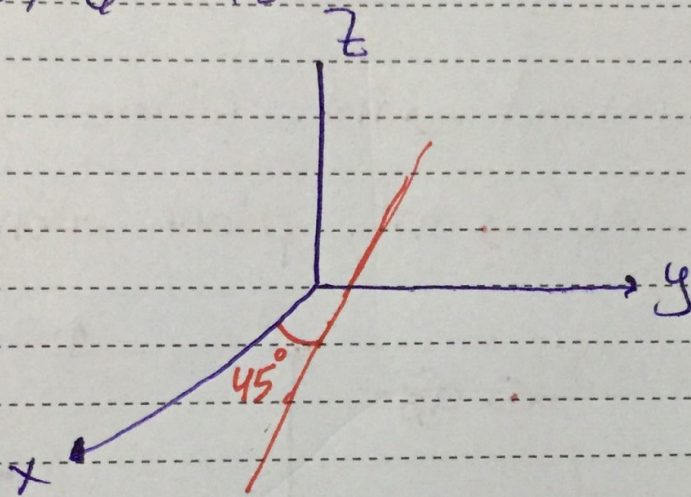
①  $\rho, \phi$  are constants

↳ inf. Line // z-axis ( $\rho \neq 0$ )

↳ inf. Line along z-axis ( $\rho = 0$ )

i.e.  $\rho = 3, \phi = 45^\circ$

$$dL = dz \hat{a}_z$$



②  $\rho, z$  are constants

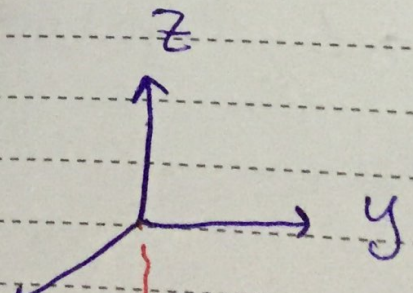
↳ Circle (not inf.) // xy plane ( $z \neq 0$ ) ( $\rho > 0$ )

↳ Circle along xy ( $z = 0$ ) ( $\rho > 0$ )

↳ point ( $\rho = 0$ )

i.e.  $\rho = 3, z = -3$

$$dL = 3d\phi \hat{a}_\phi$$

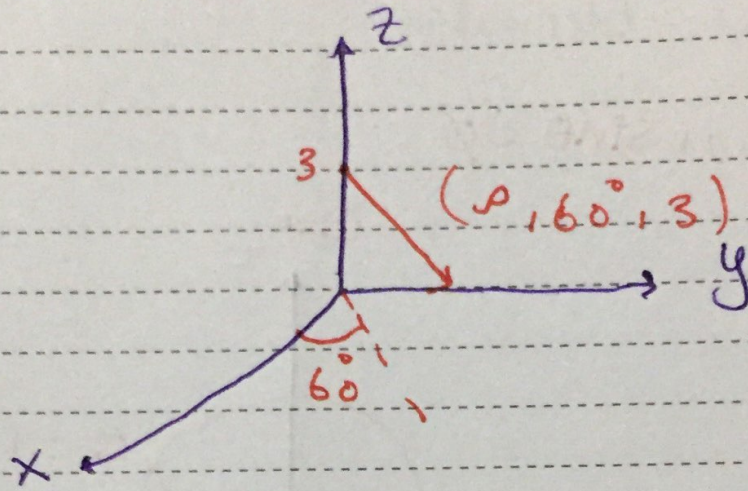


$\rho = 3$   
 $(3, \phi, -3)$

③  $\phi, z$  are constants.

↳ Semi-inf. Line.

i.e.  $\phi = 60^\circ, z = 3$



\* Spherical coordinates :-

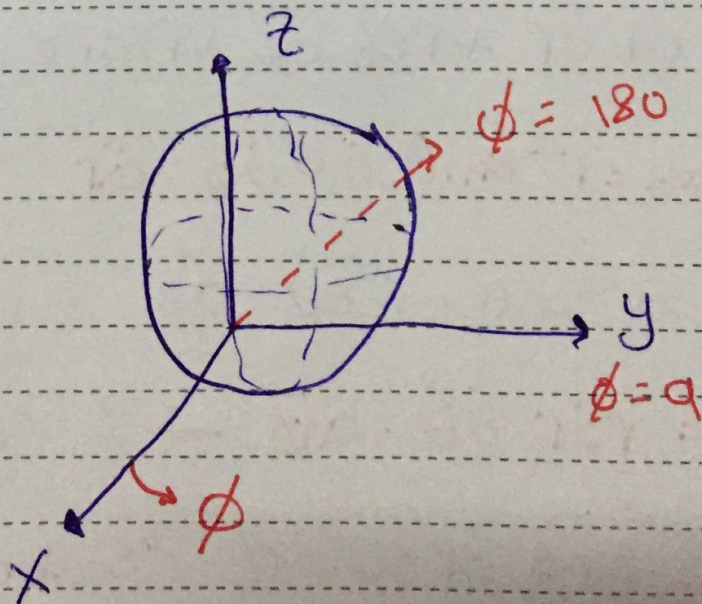
$$0 < r < \infty$$

$$0 \leq \theta \leq \pi$$

$$0 \leq \phi \leq 2\pi$$

} 3D object  
Inf. solid  
sphere.

360  $\phi$   $\rightarrow$  180  $\theta$   $\rightarrow$  0  $\leq \phi \leq \theta$   $\rightarrow$

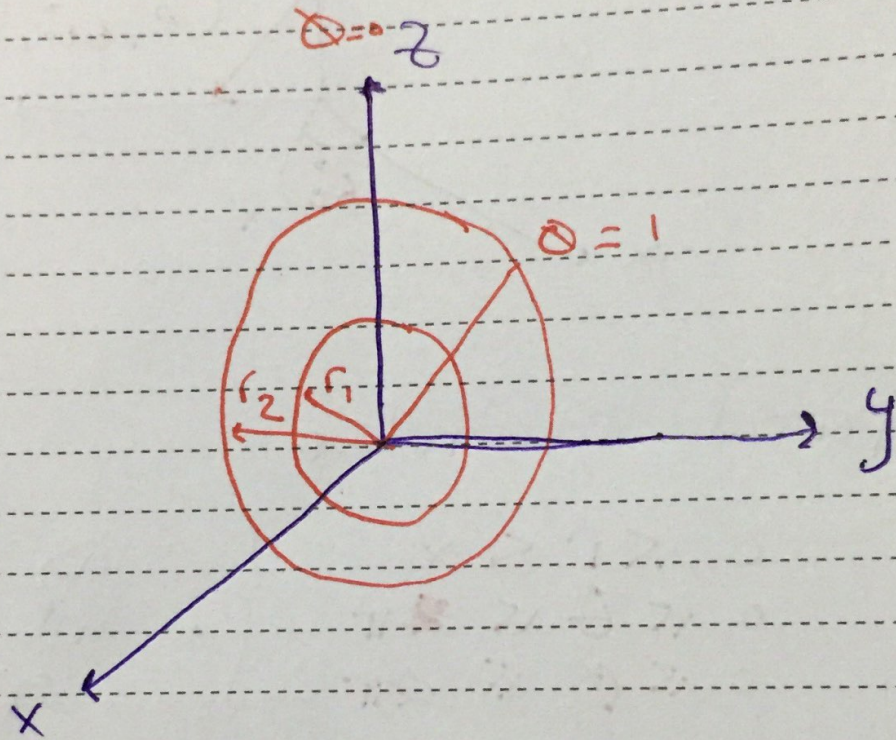


← Unit vectors -

$$\hat{a}_r, \hat{a}_\theta, \hat{a}_\phi$$

- Differential Elements -

$$dr, r d\theta, r \sin\theta d\phi$$



$$- d\vec{L} = dr \hat{a}_r + r d\theta \hat{a}_\theta + r \sin\theta d\phi \hat{a}_\phi \rightarrow r \text{ const.}$$

$$- dS_{\text{surface}} = r^2 \sin\theta d\theta d\phi \hat{a}_r$$

$$- dS_\theta = r \sin\theta dr d\phi \hat{a}_\theta$$

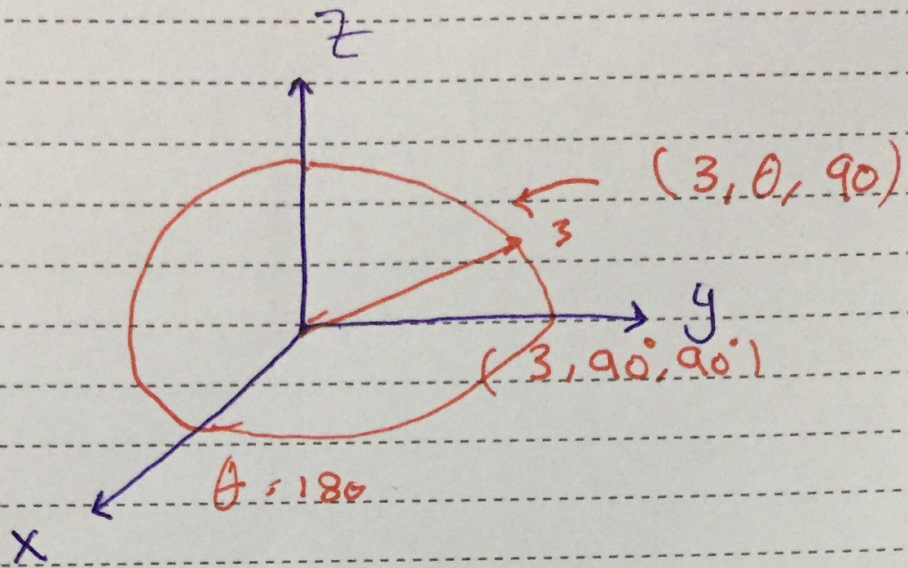
$$- dS_\phi = r dr d\theta \hat{a}_\phi \rightarrow \phi \text{ const.}$$

$$- dV = r^2 \sin\theta dr d\theta d\phi \text{ "Scalar"}$$

\* 2D Surface.

-  $r = \text{constant} \rightarrow \text{hollow sphere } (r > 0)$

ie  $r = 3$

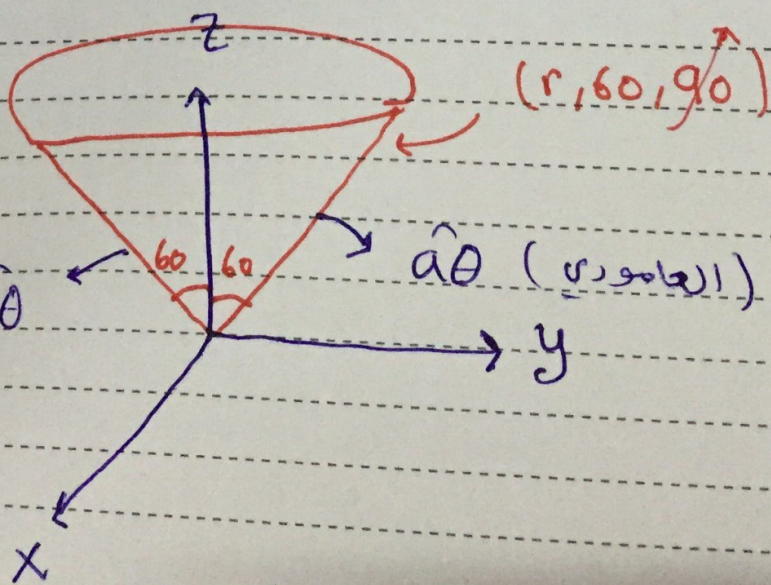


- if  $r = 0 \rightarrow \text{point.}$

-  $\theta = \text{constant}$

- $\rightarrow$  inf. hollow cone  $\theta \in (0, 90)$  and  $(90, 180)$
- $\rightarrow$  inf. disk along xy plane ( $\theta = 90^\circ$ )
- $\rightarrow$  semi-inf. line  $\rightarrow$  +ve z-axis ( $\theta = 0^\circ$ )
- $\rightarrow$  -ve z-axis ( $\theta = 180^\circ$ )

ie.  $\theta = 60^\circ$

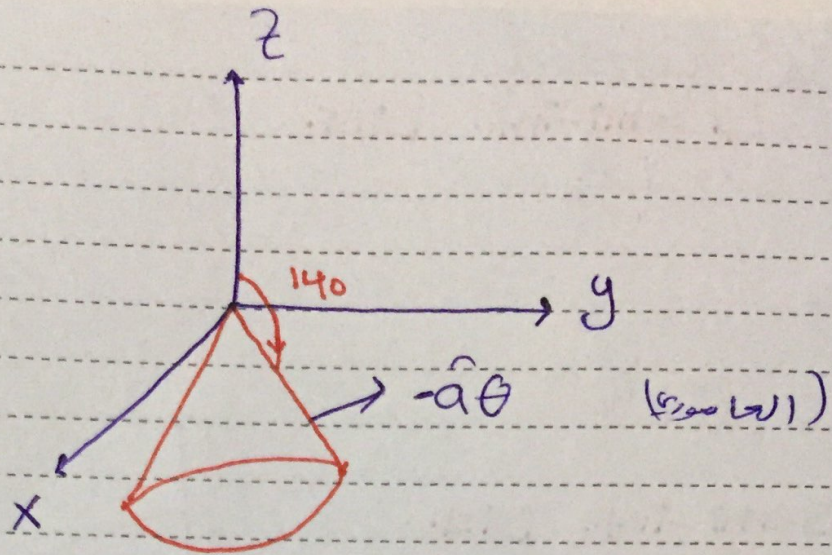


$\theta < 90$   
Cone ال  
لغوق

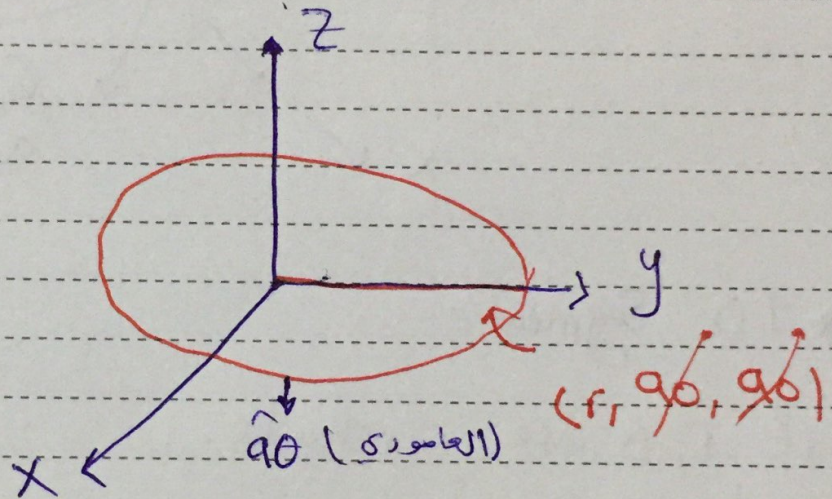
$\hat{a}_\theta$  (العاصوري)

-if  $\theta = 140^\circ$

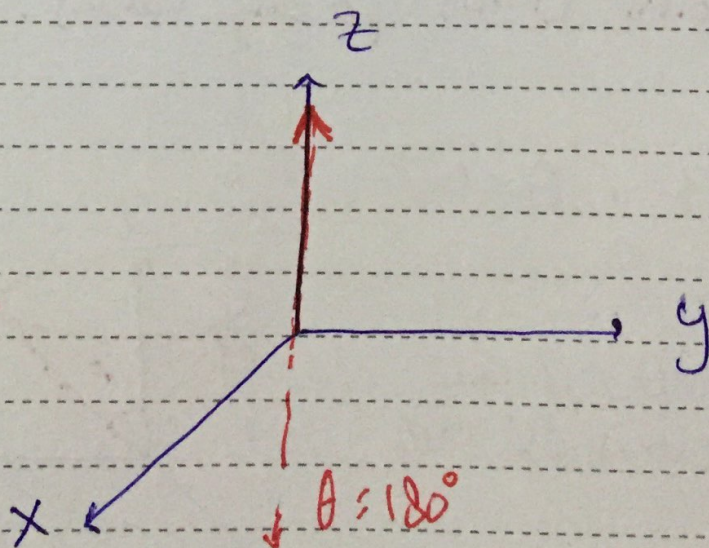
$\theta > 90$   
اد Cone لثابت



-if  $\theta = 90^\circ$



-if  $\theta = 0^\circ$

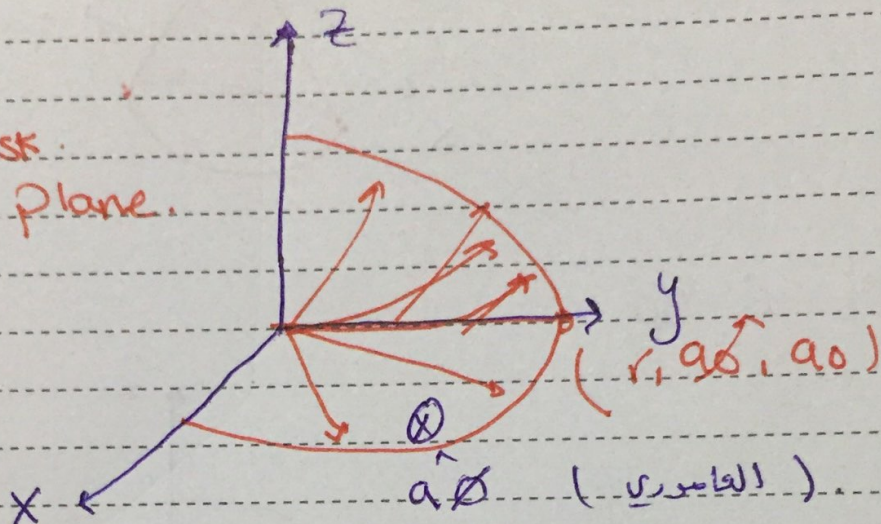




if  $\phi = \text{constant}$ .  
 $\rightarrow$  semi-inf. Disk.

i.e.  $\phi = 90^\circ$

Semi-inf. Disk  
 along yz plane.



\* 1D Segments -

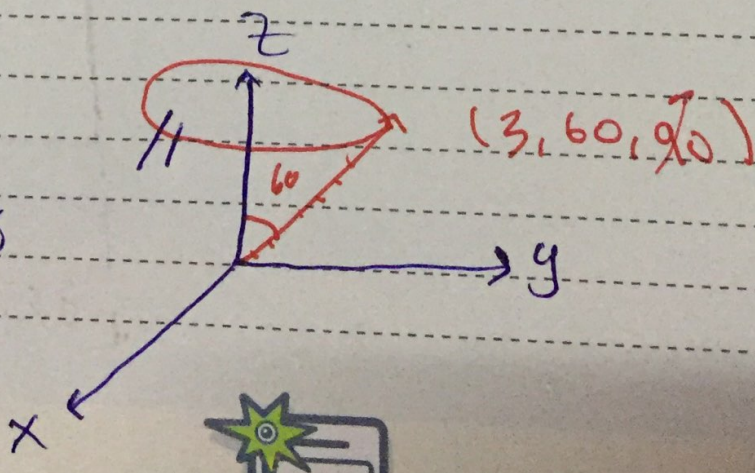
if  $r, \theta$  are constants.

- $\rightarrow$  Circle // xy plane.  $(r > 0, \theta \neq 90)$
- $\rightarrow$  Circle along xy plane  $(r > 0, \theta = 90)$
- $\rightarrow$  point  $(r=0)$  ( $\theta$  any value).

if  $r=3, \theta=60^\circ$

$$dL = r \sin \theta d\phi \hat{a}_\phi$$

$$= 3 \sin(60) d\phi \hat{a}_\phi$$



-  $r, \theta$  are constants.

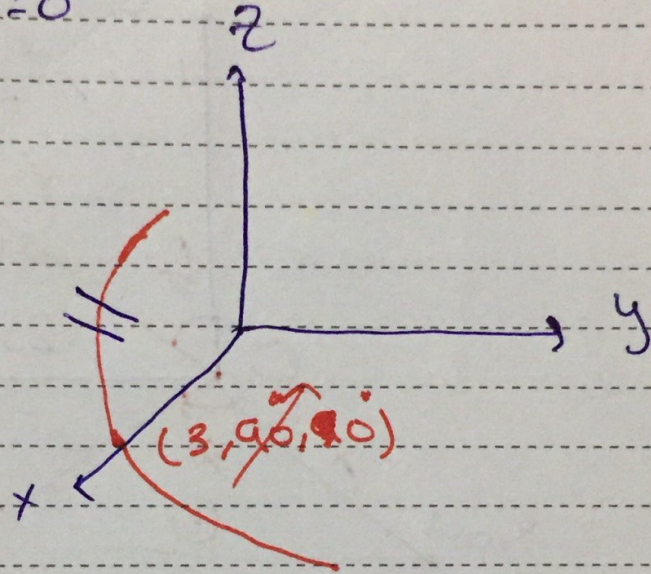
↳ half-circle ( $r > 0$ )

↳ point ( $r = 0$ )

↳

i.e.  $r = 3, \phi = 0^\circ$

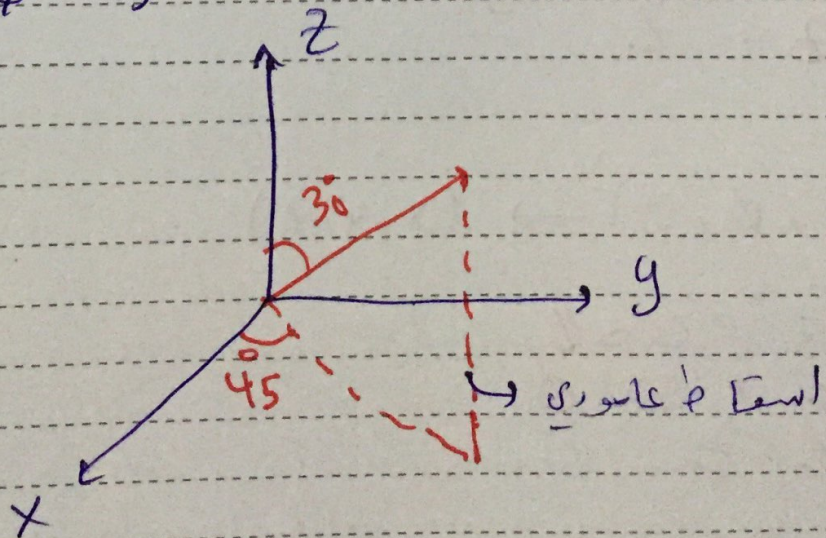
$$\begin{aligned} \widehat{dl} &= r d\theta \widehat{a}_\theta \\ &= 3 d\theta \widehat{a}_\theta \end{aligned}$$



-  $\theta, \phi$  are constants.

↳ Semi-inf. Line (Ray).

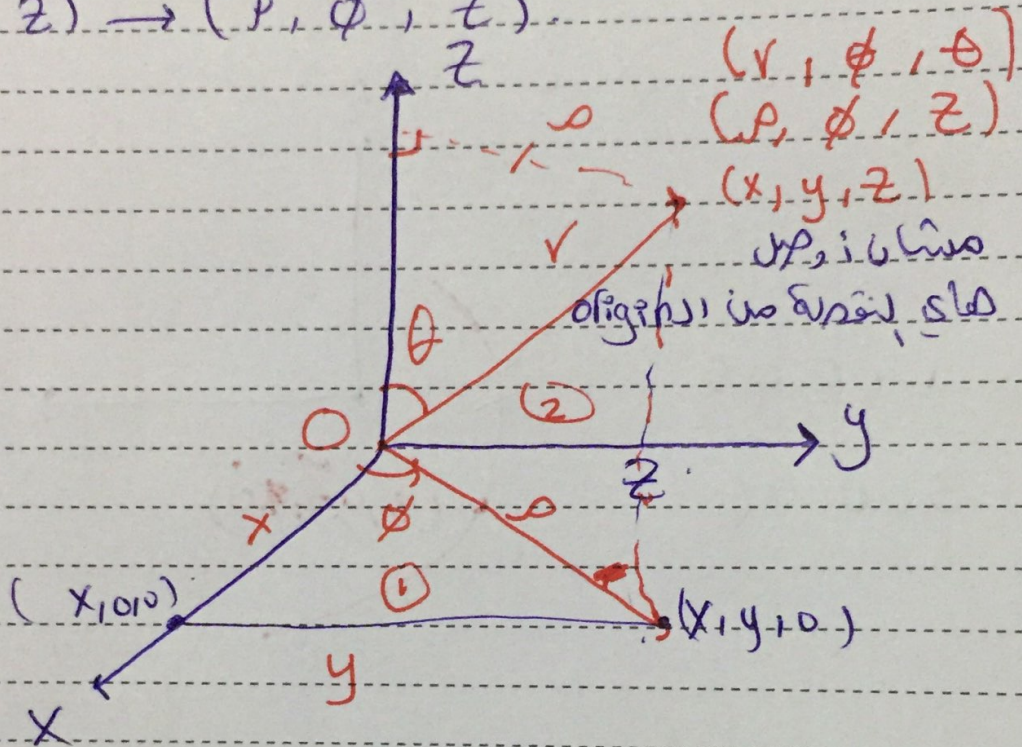
i.e.  $\theta = 30^\circ, \phi = 45^\circ$



# \* Transformation between coordinates:

## - Point conversions -

↳ if given cartesian and we want cylindrical.  
 $(x, y, z) \rightarrow (\rho, \phi, z)$



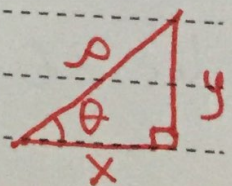
\*  $(x, y, z) \rightarrow (\rho, \phi, z)$

$$\rho = \sqrt{x^2 + y^2}$$

$$\phi = \tan^{-1}(y/x)$$

$$z = z$$

① Given



\*  $(\rho, \phi, z) \rightarrow (x, y, z)$

$$x = \rho \cos \phi$$

$$y = \rho \sin \phi$$

$$z = z$$

$$\sin \theta = y/\rho$$

$$\cos \theta = x/\rho$$

$$\tan \theta = y/x$$

\* Cart.  $\rightarrow$  Spherical

$$r = \sqrt{x^2 + y^2 + z^2}$$

$$\theta = \tan^{-1} \left( \frac{\sqrt{x^2 + y^2}}{z} \right)$$

~~$\phi = \phi$~~

$$\phi = \tan^{-1} (y/x)$$

\* Spherical  $\rightarrow$  Cart.

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

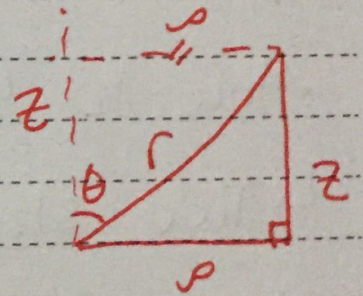
$$z = r \cos \theta$$

\* Cylindrical  $\rightarrow$  sph.

$$r = \sqrt{\rho^2 + z^2}$$

$$\theta = \tan^{-1} (\rho/z)$$

$$\phi = \phi$$



$$\sin \theta = \rho/r$$

$$\cos \theta = z/r$$

$$\tan \theta = \rho/z$$

\* sph.  $\rightarrow$  cyl.

$$\rho = r \sin \theta$$

$$\phi = \phi$$

$$z = r \cos \theta$$

- Vectors conversion :-

- Cart.  $\rightarrow$  Cyl.

i.e.  $\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$

$\hookrightarrow \vec{A} = A_\rho \hat{a}_\rho + A_\phi \hat{a}_\phi + A_z \hat{a}_z$

المطلوب  $\leftarrow$  هاد

$$\begin{bmatrix} A_\rho \\ A_\phi \\ A_z \end{bmatrix} = \begin{bmatrix} \cos\phi & \sin\phi & 0 \\ -\sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix}$$

$\downarrow$  هاد المظني

$\hookrightarrow$  This matrix is given

- How to use this matrix?

$\hookrightarrow$  Two steps.

1)  $A_\rho = \cos\phi A_x + \sin\phi A_y$  ضرب المصنف الأول بالمتجه

$A_\phi = -\sin\phi A_x + \cos\phi A_y$  ضرب المصنف الثاني بالمتجه

$A_z = A_z$  i.e.  $A_x = x/y$

2)  $x = \rho \cos\phi$

$y = \rho \sin\phi$

$xy = \rho^2 \cos\phi \sin\phi$

\* Cyl.  $\rightarrow$  Cart.

$$\begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} = \begin{bmatrix} \cos\phi & -\sin\phi & 0 \\ \sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A_\rho \\ A_\phi \\ A_z \end{bmatrix}$$

له ممكن يكون مطين الماتريكس اللي قبل وانا اطلع  
 هاي الماتريكس كيف P ياخذ انا transpose للماتريكس ! انه  
 كل صفت بهن خاصور .

- Unit Vector Conversion

$$\hat{a}_x = \cos\phi \hat{a}_\rho + \sin\phi \hat{a}_\phi$$

\* Cart.  $\rightarrow$  Sph.

$$\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$$

$$\vec{A} = A_r \hat{a}_r + A_\theta \hat{a}_\theta + A_\phi \hat{a}_\phi$$

$$\begin{bmatrix} A_r \\ A_\theta \\ A_\phi \end{bmatrix} = \begin{bmatrix} \sin\theta \cos\phi & \sin\theta \sin\phi & \cos\theta \\ \cos\theta \cos\phi & \cos\theta \sin\phi & -\sin\theta \\ -\sin\phi & \cos\phi & 0 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix}$$

$$\hat{a}_\phi = -\sin\phi \hat{a}_x + \cos\phi \hat{a}_y$$

\* Cyl.  $\rightarrow$  Sph.

$$\vec{A} = A_\rho \hat{a}_\rho + A_\phi \hat{a}_\phi + A_z \hat{a}_z$$

$$\hookrightarrow \vec{A} = A_r \hat{a}_r + A_\theta \hat{a}_\theta + A_\phi \hat{a}_\phi$$

Sph.  $\rightarrow$  cyl.

$$\begin{bmatrix} A_\rho \\ A_\phi \\ A_z \end{bmatrix} = \begin{bmatrix} \sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \\ \cos\theta & -\sin\theta & 0 \end{bmatrix} \begin{bmatrix} A_r \\ A_\theta \\ A_\phi \end{bmatrix}$$

Given

$$A_\phi = A_\phi$$

## \* CH3 Vector Calculus.

### - Integration.

↳ 1) Line Integral.

$$\int_C \vec{A} \cdot d\vec{L}$$

,  $d\vec{L}$  (differential length).

$$\hookrightarrow dx\hat{x} + dy\hat{y} + dz\hat{z}$$

$$\hookrightarrow \rho d\rho\hat{\rho} + \rho d\phi\hat{\phi} + dz\hat{z}$$

$$\hookrightarrow \rho dr\hat{r} + r d\theta\hat{\theta} + r \sin\theta d\phi\hat{\phi}$$

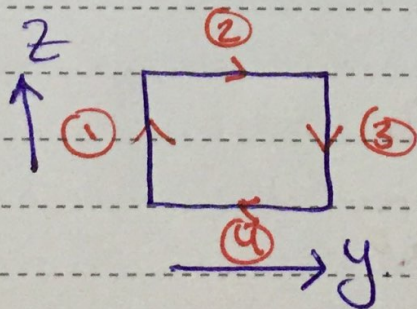
-i.e.  $\vec{A} = (A_\rho, A_\phi, A_z)$ .

$$\int_C (A_\rho, A_\phi, A_z) \cdot (d\rho, \rho d\phi, dz)$$

$$= \int_{\rho} A_\rho d\rho + \int_{\phi} \rho A_\phi d\phi + \int_z A_z dz$$

### \* Closed Line Integral

$$\oint_C \vec{A} \cdot d\vec{L}$$

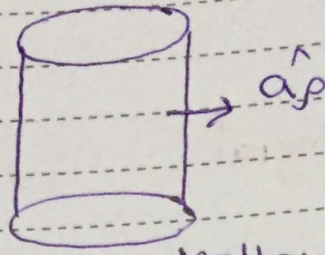


$$\oint_C \vec{A} \cdot d\vec{L} = \int_{l_1} \vec{A} \cdot d\vec{L}_1 + \int_{l_2} \vec{A} \cdot d\vec{L}_2 + \int_{l_3} \vec{A} \cdot d\vec{L}_3 + \int_{l_4} \vec{A} \cdot d\vec{L}_4$$



\* Surface Integral :-

$$\int_S \vec{A} \cdot d\vec{s}$$



hollow cylinder

$\vec{A} = (A_x, A_y, A_z)$   
Using matrix

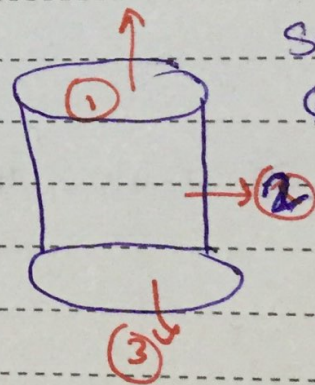
$\vec{A} = (A_\rho, A_\phi, A_z)$

$d\vec{s} = \rho d\phi dz \hat{a}_\rho$

$$\int_S \vec{A} \cdot d\vec{s} = \int_z \int_\phi A_\rho \rho d\phi dz$$

\* Closed Surface Integrals -

$$\oint_S \vec{A} \cdot d\vec{s}$$



solid cylinder

$d\vec{s}_1 = \rho d\rho d\phi \hat{a}_z$

$d\vec{s}_2 = \rho d\phi dz \hat{a}_\rho$

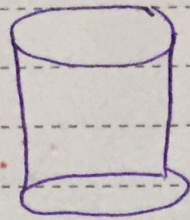
$d\vec{s}_3 = -\rho d\rho d\phi \hat{a}_z$

$$\oint \vec{A} \cdot d\vec{s} = \int_{s_1} \vec{A} \cdot d\vec{s}_1 + \int_{s_2} \vec{A} \cdot d\vec{s}_2 + \int_{s_3} \vec{A} \cdot d\vec{s}_3$$

$s_1 \downarrow A_z$        $s_2 \downarrow A_\rho$        $s_3 \downarrow A_z$

\* Volume Integrals -

$$\int |\vec{A}| dV$$



Solid cylinder.

i.e.  $dV = \rho d\rho d\phi dz$

$$\int_z \int_\phi \int_\rho \vec{A} \cdot \rho d\rho d\phi dz$$

\* Del operator ( $\nabla$ )

↳ vector

- in Cartesian -

$$\nabla_v = \frac{\partial v}{\partial x} \hat{a}_x + \frac{\partial v}{\partial y} \hat{a}_y + \frac{\partial v}{\partial z} \hat{a}_z$$

Partial partial

- in cylindrical

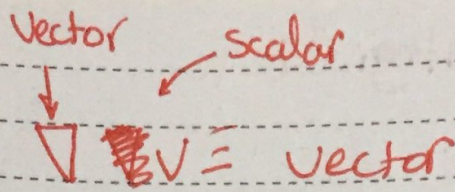
$$\nabla_u = \frac{\partial u}{\partial \rho} \hat{a}_\rho + \frac{1}{\rho} \frac{\partial u}{\partial \phi} \hat{a}_\phi + \frac{\partial u}{\partial z} \hat{a}_z$$

- in spherical

$$\nabla_T = \frac{\partial T}{\partial r} \hat{a}_r + \frac{1}{r} \frac{\partial T}{\partial \phi} \hat{a}_\phi + \frac{\partial T}{\partial \theta} \hat{a}_\theta$$

کے لیے  
فوق  
(د) بار  
بہت سے  
different  
element

\* Del Usage:-



1) Gradient

2) Divergence

3) Curl

4) Laplacian

$\nabla \cdot \vec{A} \equiv \text{scalar}$

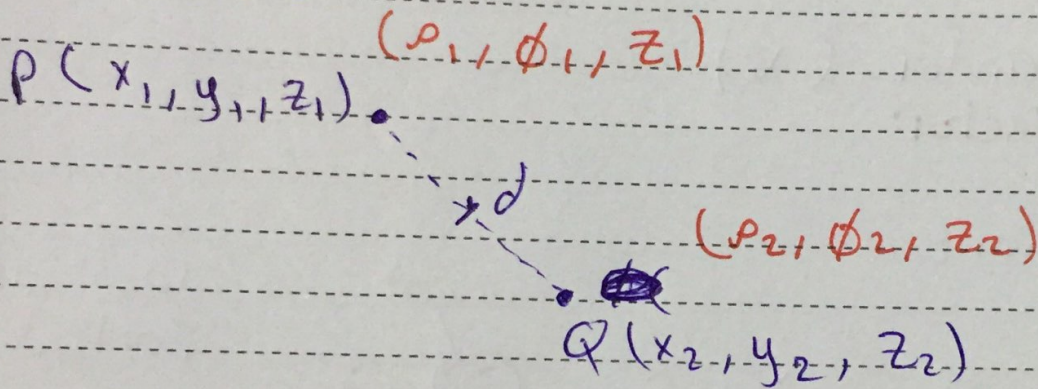
$\nabla \times \vec{A} \equiv \text{vector}$

$\nabla \cdot \nabla V \equiv \nabla^2 V$

X  
X  
X

وہو  
وہو

\* Distance :-



$d^2 = (x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2$  cart.

$d^2 = \rho_2^2 + \rho_1^2 - 2\rho_1\rho_2 \cos(\phi_2 - \phi_1) + (z_2 - z_1)^2$  Cylindrical

degree  $\rho_1, \rho_2 \rightarrow r$   $\phi_1, \phi_2 \rightarrow \theta$   
 $z_1, z_2 \rightarrow z$

$\hookrightarrow$  if  $\phi_1 = \phi_2 \rightarrow (\rho_2 - \rho_1)^2 + (z_2 - z_1)^2$

In sph.  $d^2 = (r_2 - r_1)^2$  if  $\phi_1 = \phi_2$   
 $\theta_1 = \theta_2$



# \* CH4 Electrostatic Fields.

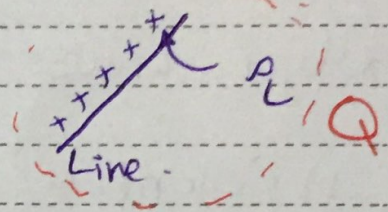
## - Electrostatic Sources -

1) point charge ( $Q$ ). (Unit in ~~C/m~~)  
↳ كولم

2) Continuous charge distribution.

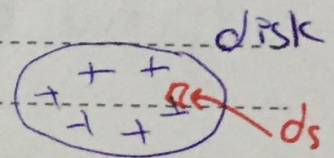
↳ a) Line charge. (1D segment).  
( $\rho_L$ )  $\rightarrow$  (C/m)  
(جول/متر)

$$Q = \int_L \rho_L dl$$



↳ b) Surface charge. ( $\rho_s$ ) (2D surfaces)  
(C/m<sup>2</sup>)

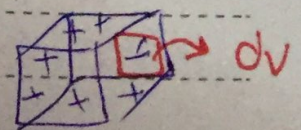
$$Q = \int_s \rho_s ds$$



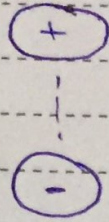
عنصر مساحة  
inf و s ل s  
انواع

↳ c) Volume charge. (3D obj) ( $\rho_v$ ) (C/m<sup>3</sup>).

$$Q = \int_v \rho_v dv$$



### 3) Electric Dipole



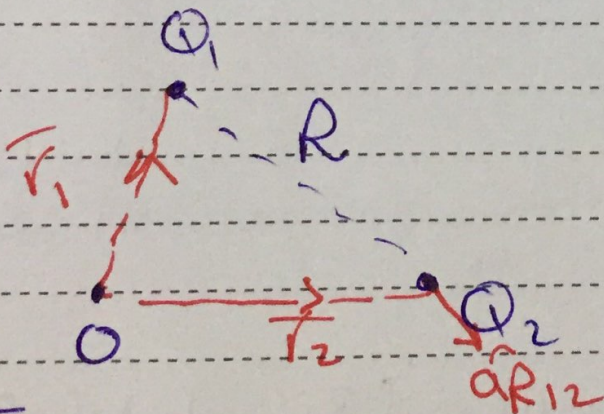
### 4) Polarized Dielectric

#### \*Major Laws-

1) Colomb's Law (General)

2) Gauss's Law (Special case).

#### \*Colomb's Law :- (point charge).



$F_e = F \equiv$  Electrical Force (N)

$$F \propto \frac{Q_1 Q_2}{R^2} \quad (\text{Relation})$$

$\rightarrow F = \frac{k Q_1 Q_2}{R^2} (N) \rightarrow$  this gives magnitude only

$k$ : proportionality constant

$$k = \frac{1}{4\pi\epsilon_0}$$

Units used ( $\frac{1}{4\pi}$ )  
Media surrounded the two charges ( $\epsilon_0$ )

$\epsilon$  &  $\rho$  permittivity (F/m)  
 $\rightarrow$  Farad.

$\epsilon_0$  Free space permittivity (F/m).

$$= \frac{10^{-9}}{36\pi} \text{ F/m} = 8.85 \times 10^{-12} \text{ F/m}$$

\*  $F$  as a vector Quantity.

- The force on ( $Q_2$ ) due to ( $Q_1$ )

$$\vec{F}_{12} = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} \hat{a}_{R_{12}} (N)$$

$$\vec{R}_{12} = \vec{r}_2 - \vec{r}_1$$

$$\vec{R}_{12} = \vec{r}_2 - \vec{r}_1$$

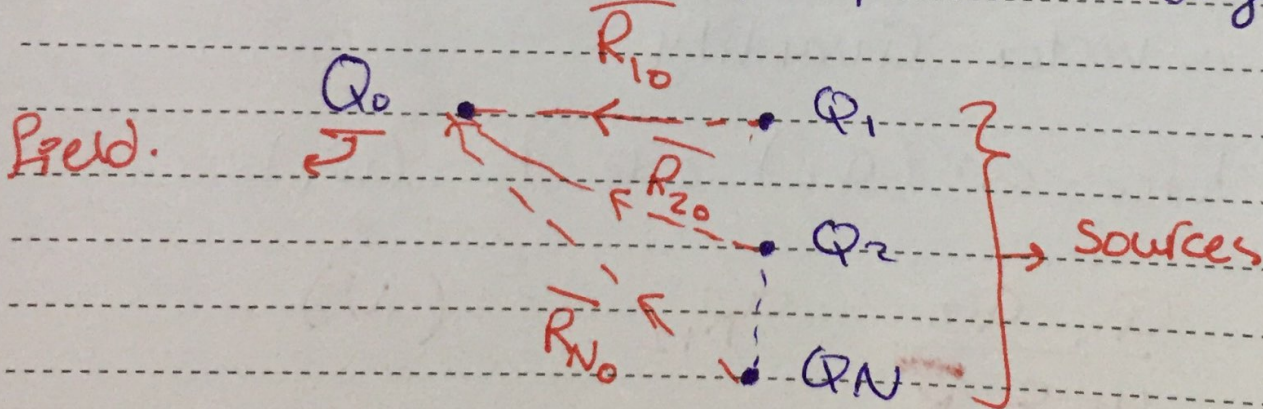
$$\vec{F}_{12} = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} \hat{a}_{R_{12}} \quad \hat{a}_{R_{12}} \rightarrow \frac{\vec{R}_{12}}{R_{12}}$$

②  $\vec{F}_{12} = \frac{Q_1 Q_2 \vec{R}_{12}}{4\pi\epsilon_0 R_{12}^3} \quad (N)$  كذلك نفس القانون ولكن في شكل متجه

③  $\vec{F}_{12} = \frac{Q_1 Q_2 (\vec{r}_2 - \vec{r}_1)}{4\pi\epsilon_0 |\vec{r}_2 - \vec{r}_1|^3} \quad (N)$

$\vec{F}_{21} = -\vec{F}_{12}$  نفس المقدار و لكن عكس الاتجاه .  
↪ . الاتجاه

\* The force due to N-point charges -



- The force on  $Q_0$  :-

$$\vec{F} = \frac{Q_1 Q_0 (\vec{r}_0 - \vec{r}_1)}{4\pi\epsilon_0 |\vec{r}_0 - \vec{r}_1|^3} + \frac{Q_2 Q_0 (\vec{r}_0 - \vec{r}_2)}{4\pi\epsilon_0 |\vec{r}_0 - \vec{r}_2|^3} + \dots + \frac{Q_N Q_0 (\vec{r}_0 - \vec{r}_N)}{4\pi\epsilon_0 |\vec{r}_0 - \vec{r}_N|^3} \quad (N)$$

$$\rightarrow \vec{F} = \frac{Q_0}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k (\vec{r}_0 - \vec{r}_k)}{|\vec{r}_0 - \vec{r}_k|^3} \quad (N)$$

\* Electric Field Intensity ( $\vec{E}$ )

$$\vec{E} = \frac{\vec{F}}{Q} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \quad \left(\frac{N}{C}\right) \text{ or } \left(\frac{V}{m}\right)$$

Field point  $\left(\begin{array}{c} \text{---} \\ \circ \\ \text{---} \end{array}\right)$   $\left(\begin{array}{c} \text{---} \\ \bullet \\ \text{---} \end{array}\right)$  for a point charge.

$$\vec{E} = \frac{Q (\vec{r} - \vec{r}')}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|^3}$$

Use dashes with the source and without dashes with the field.

- For N point charges :-

$$\vec{F} = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k (\vec{r} - \vec{r}_k')}{|\vec{r} - \vec{r}_k'|^3}$$



Source 1

Source 2.

- Ex point charges ( $1 \text{ mc}$ ) and ( $-2 \text{ mc}$ ) are located at  $(3, 2, -1)$  and  $(-1, -1, 4)$ . Find  $\vec{F}$  and  $\vec{E}$  at  $(10 \text{ nc})$  charge located at  $(0, 3, 1)$  ?  $\rightarrow$  Field.

Sol

$$\vec{F} = (1 \times 10^{-3}) * (10 \times 10^{-9}) * (-3, 1, 2)$$

قوة للشحنة الأولى

$$4\pi * \frac{10^{-9}}{36\pi} * (14)^{3/2}$$

Vector

$$+ (-2 \times 10^{-3}) (10 \times 10^{-9}) * (1, 4, -3)$$

قوة للشحنة الثانية

$$4\pi * \frac{10^{-9}}{36\pi} * (26)^{3/2}$$

vector

= ~~max~~

$$= -6.507 \hat{a}_x + -3.817 \hat{a}_y + 7.506 \hat{a}_z \text{ (mN)}$$

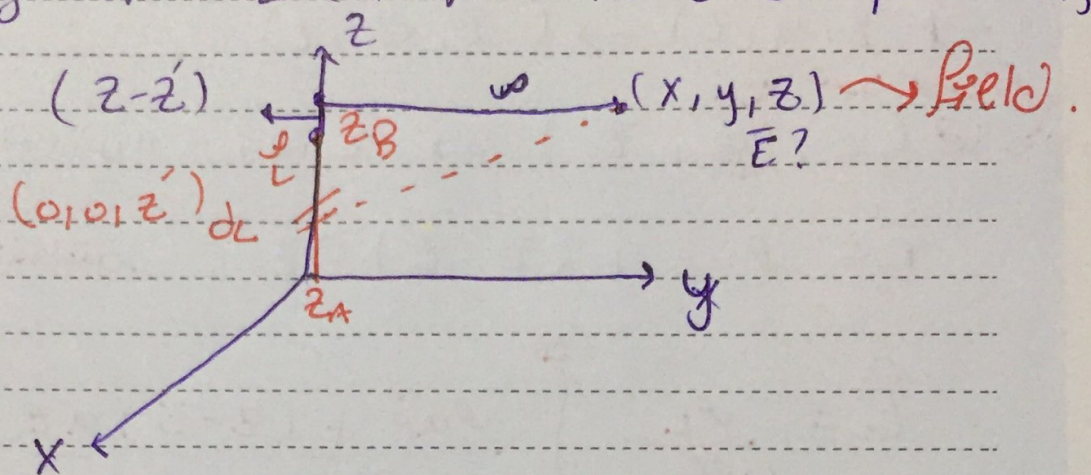
$$\vec{E} = \frac{\vec{F}}{Q} = \frac{\vec{F}}{10 \times 10^{-9}}$$

$$= -650.7 \hat{a}_x - 381.7 \hat{a}_y + 750.6 \hat{a}_z \text{ (kN/C)}$$

or (kV/m)

\* Continuous charge distribution -  
 → Line charge ( $\rho_L$ ) in (C/m)

-ex Consider a finite line along z-axis carry a charge of  $\rho_L$  (C/m). Find  $\vec{E}$  at point  $(x, y, z)$



Sol  $\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \rightarrow$  point charge.

$\vec{E} = \int \frac{\rho_L dL}{4\pi\epsilon_0 r^2} \hat{a}_r \rightarrow$  For Line charge.

$dL = dz'$

$\vec{r} = x\hat{a}_x + y\hat{a}_y + (z - z')\hat{a}_z$

$r = \sqrt{x^2 + y^2 + (z - z')^2}$

$\vec{E} = \frac{\rho_L}{4\pi\epsilon_0} \int_{z_A}^{z_B} \frac{(x, y, (z - z'))}{[x^2 + y^2 + (z - z')^2]^{3/2}} dz'$

$z_A, z_B$

المجال الكهربائي

Note الشكامل الذي طرح هنا صعب حلها! لا بد من table cylindrical coordinates  $\rho, \phi, z$  Line  $\rightarrow$  حل  
 - Line is a cylinder of  $\rho=0$  So convert to cyl.

$\rightarrow (x, y, z) \rightarrow (\rho, \phi, z)$

صوبون ممكن تكونه زي  $(0, \phi, z')$   $\rightarrow$  Line. هاي من ال

$\vec{r} = \rho \hat{a}_\rho + (z-z') \hat{a}_z$  فرضيتا ان  $\phi$  بالنقطتين يساوي

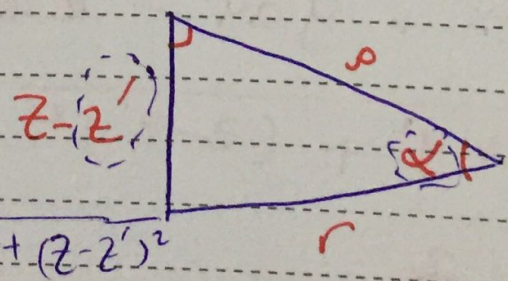
$$\vec{E} = \frac{\rho_L}{4\pi\epsilon_0} \int_{z_A}^{z_B} \frac{\rho \hat{a}_\rho + (z-z') \hat{a}_z}{(\rho^2 + (z-z')^2)^{3/2}} dz$$

table of integral  $\rightarrow$  هار بنقسم الشكاملين الاول بنجد عن والباقي بتعويضه لانه صعب!

Solution is introduce Angles!

- Introduce angles:  $\alpha_1, \alpha_2, \alpha_3$

$\alpha$  بي احوّل من  $z$  ل  $\alpha$



$\sin \alpha = (z-z') / r$   
 $\cos \alpha = \rho / r$   
 $\tan \alpha = (z-z') / \rho \rightarrow z-z' = \rho \tan \alpha$   
 $d(z-z') = \rho \sec^2 \alpha d\alpha$

$$r^2 = \rho^2 + (z - z')^2$$

$$= \rho^2 + \rho^2 \tan^2 \alpha$$

$$= \rho^2 (1 + \tan^2 \alpha)$$

$$= \rho^2 \left( 1 + \frac{\sin^2 \alpha}{\cos^2 \alpha} \right)$$

$$= \rho^2 \left( \frac{\cos^2 \alpha}{\cos^2 \alpha} + \frac{\sin^2 \alpha}{\cos^2 \alpha} \right)$$

$$r^2 = \rho^2 \sec^2 \alpha$$

$$r^3 = \rho^3 \sec^3 \alpha$$

$$\vec{E} = \frac{\rho L}{4\pi\epsilon_0} \int_{\alpha_1}^{\alpha_2} \frac{\rho \sec \alpha (\cos \alpha \hat{a}_\rho + \sin \alpha \hat{a}_z)}{\rho^3 \sec^3 \alpha} (-\rho \sec \alpha d\alpha)$$

$\downarrow$   $\downarrow$   $\downarrow$   
 لکھو صاف کرنے کے لیے  $\alpha$  کی بجائے  $\alpha$   $\downarrow$   $\downarrow$   $\downarrow$   
 صاف کرنے کے لیے  $\alpha$   $\downarrow$   $\downarrow$   $\downarrow$   
 صاف کرنے کے لیے  $\alpha$   $\downarrow$   $\downarrow$   $\downarrow$

لکھو صاف کرنے کے لیے  $\alpha$  کی بجائے  $\alpha$

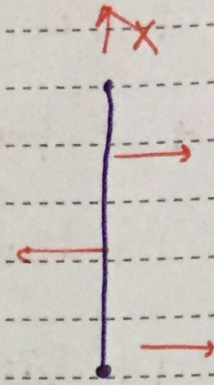
صاف کرنے کے لیے  $\alpha$

صاف کرنے کے لیے  $\alpha$

$$\vec{E} = \frac{-\rho L}{4\pi\epsilon_0 \rho} (\sin \alpha_2 - \sin \alpha_1) \hat{a}_\rho - (\cos \alpha_2 - \cos \alpha_1) \hat{a}_z \quad (V/m)$$

\* For an infinite line.

ما عندي عامودي من فوق وما تحت  
~~من فوق وما تحت~~  
 يختص به حد الجازم



$$\alpha_1 = 90^\circ$$

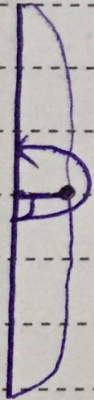
$$\alpha_2 = 270^\circ \text{ or } -90^\circ$$

$$\vec{E} = \frac{\rho_L}{2\pi\epsilon_0 r} \hat{a}_r$$

حفظ

Always for any infinite line.

كيف اطلع  $\alpha_1, \alpha_2$  ؟

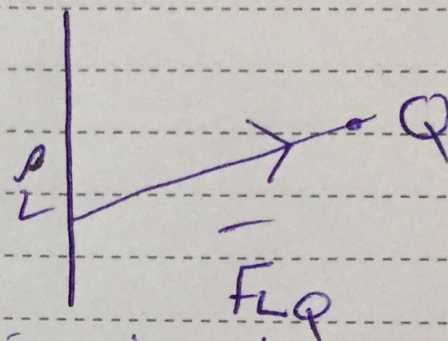


فمسك النقطة التي عندي وبتطلع  
 من عندها لتجاه ال Line  
 إذا الزاوية الأولى  $\alpha_1 = 90^\circ$   
 و الثاني صورة بتطلع من النقطة  
 لبدأ الخط (من نفس الموضع)  
 و بتسوف الزاوية

$$\vec{E} = \frac{\rho L}{2\pi\epsilon_0} \hat{a}_r$$

the shortest distance between the source & the field.

$$\vec{F} = Q\vec{E}$$



Q غرض، فاعل المجال  $\vec{E}$  فاعل  $\vec{F}$

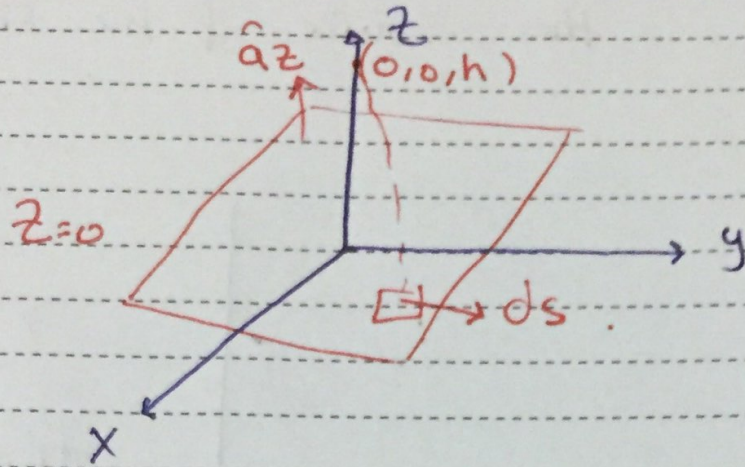
if we want  $F_{QL}$

$$F_{QL} = Q E_Q$$

$$\int \rho dL \quad \downarrow \quad \downarrow \quad \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

\* E-Field due to a surface charges -

- Ex. Consider a  $z=0$  plane carry a charge  $\rho_s$  C/m<sup>2</sup>. Find  $\vec{E}$  at  $(0,0,h)$  where  $h > 0$



Sol  $\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{q}{r^2} \hat{r}$  → point charge

$$Q = \int_S \rho_s ds$$

$$\vec{E} = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r^2} \hat{r}$$

$$ds = dx' dy'$$

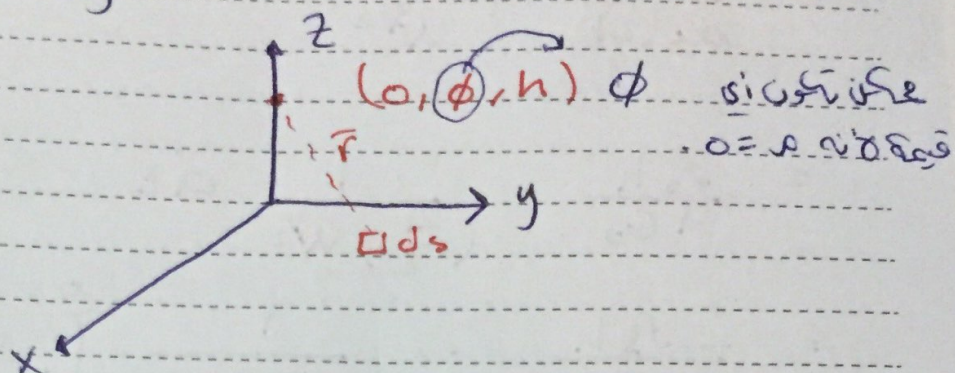
$$\vec{r} = -x' \hat{x} - y' \hat{y} + h \hat{z}$$

$$r = \sqrt{x'^2 + y'^2 + h^2}$$

$$\vec{E} = \frac{\rho_s}{4\pi\epsilon_0} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{(-x', -y', h)}{[x'^2 + y'^2 + h^2]^{3/2}} dx' dy'$$

↳ table of integral.

→ Convert to cylindrical because  $z=0$  can be represented in cyl.



$$ds = \rho d\rho d\phi$$

$$\vec{r} = -\rho\hat{\rho} + h\hat{z}$$

$$r = \sqrt{\rho^2 + h^2}$$

$$\phi \leftarrow 2\pi \quad \rho \leftarrow \infty$$

$$\vec{E} = \frac{\rho_s}{4\pi\epsilon_0} \int_0^\infty \int_0^{2\pi} \frac{-\rho\hat{\rho} + h\hat{z}}{[\rho^2 + h^2]^{3/2}} \rho d\rho d\phi$$

- due to symmetry the  $\rho$ -component will be cancelled.

$$\vec{E} = \frac{\rho_s}{4\pi\epsilon_0} \int_0^{2\pi} \int_0^\infty \frac{\rho h \hat{z}}{[\rho^2 + h^2]^{3/2}} d\rho d\phi$$

$$= \frac{\rho_s h}{2\epsilon_0} \int_0^\infty \frac{\rho \hat{z}}{[\rho^2 + h^2]^{3/2}} d\rho$$

Let  $u = \rho^2 + h^2$

$$du = 2\rho d\rho \rightarrow \rho d\rho = \frac{du}{2}$$



$$\vec{E} = \frac{\rho_s h}{2\epsilon_0(z)} \int \frac{du}{u^{3/2}} \hat{a}_z$$

$$= \frac{\rho_s h}{4\epsilon_0} \cdot \frac{1}{\left(-\frac{1}{2}\right) u^{1/2}} \hat{a}_z$$

$$= \frac{-\rho_s h}{2\epsilon_0} \cdot \frac{1}{\sqrt{\rho^2 + h^2}} \Bigg|_0^\infty \hat{a}_z$$

$$= \frac{-\rho_s h}{2\epsilon_0} \left(0 - \frac{1}{h}\right) \hat{a}_z$$

$$= \boxed{\frac{\rho_s}{2\epsilon_0} \hat{a}_z}$$

For infinite sheet along xy plane.

$$\vec{E} = \boxed{\frac{\rho_s}{2\epsilon_0} \hat{a}_n}$$

Always for any infinite sheet.

\*  $\vec{E}$  - field due to volume charge.

$$\vec{E} = \int_r \frac{\rho_v \, dv}{4\pi\epsilon_0 r^2} \hat{a}_r \quad \text{V/m}$$

\* Electrical Flux Density ( $\vec{D}$ )

$$\vec{D} = \epsilon_0 \vec{E} \quad \left(\frac{FV}{m^2}\right) \left(\frac{C}{m^2}\right)$$

$\downarrow \qquad \downarrow$   
F/m      V/m

- For a point charge.

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

$$\vec{D} = \frac{Q}{4\pi r^2} \hat{a}_r$$

For point charge

$$\vec{D} = \frac{Q}{4\pi r^2} \hat{a}_r$$

For inf. line

$$\vec{D} = \frac{\rho_L}{2\pi r} \hat{a}_r$$

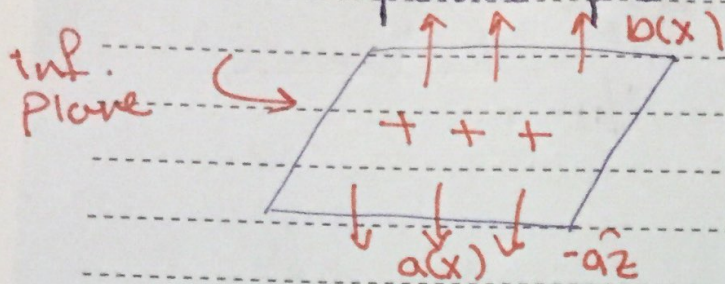
For inf. sheet

$$\vec{D} = \frac{\rho_s}{2} \hat{a}_n$$

$$\vec{E} = \frac{\rho_s}{2\pi\epsilon_0} \hat{a}_n$$



\* for a parallel plate capacitor:



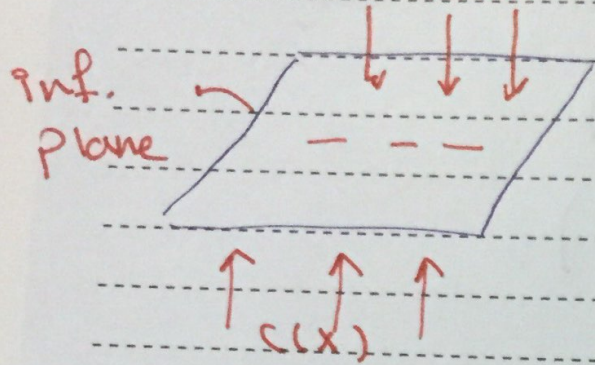
at point (a)

$$\vec{E} = \vec{E}_+ + \vec{E}_-$$

$$= \frac{\rho_s}{2\epsilon_0} (-\hat{a}z) + -\frac{\rho_s}{2\epsilon_0} (\hat{a}z)$$

$$= \left( \frac{-\rho_s}{2\epsilon_0} - \frac{\rho_s}{2\epsilon_0} \right) \hat{a}z$$

$$= \frac{-\rho_s}{\epsilon_0} \hat{a}z \quad \text{V/m}$$



- at point b ( $z > d$ )

$$\vec{E} = \vec{E}_+ + \vec{E}_-$$

$$= \frac{\rho_s}{2\epsilon_0} \hat{a}z + \frac{-\rho_s}{2\epsilon_0} \hat{a}z = 0$$

- Ex Find  $\vec{D}$  at  $(4, 0, 3)$  if there is a point charge  $-5\pi \text{ mc}$  at  $(4, 0, 0)$  and a line charge  $3\pi \text{ mc}$  along  $y$ -axis.

Sol  $\vec{D} = \vec{D}_Q + \vec{D}_L$

$$= \frac{Q}{4\pi r^2} \hat{a}_r + \frac{\rho_L}{2\pi \rho} \hat{a}_\rho$$

$$= \frac{Q\vec{r}}{4\pi r^3} + \frac{\rho_L \vec{\rho}}{2\pi \rho^2}$$

$$\vec{D} = 2\mu_0 \hat{a}_x + 42\hat{a}_z \text{ } \mu\text{C}/\text{m}^2$$

Field  $\rightarrow$  الى  
 في  $\hat{a}_x$  حسب طول  
 - o inc

$$\vec{r} = 3\hat{a}_z$$

$$r = 3$$

$$\vec{\rho} = 4\hat{a}_x + 3\hat{a}_z$$

$$\rho = 5 \text{ m}$$

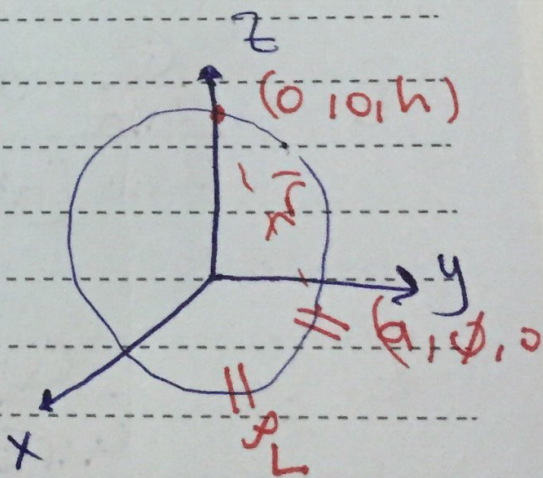
$\hookrightarrow$  shortest distance.

- Ex For a ring of radius  $(a)$  placed along  $xy$  plane carry  $\rho_L \text{ C/m}$  (1) Find  $\vec{E}$  at  $(0, 0, h)$ .

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

$$= \int_L \frac{\rho_L dL}{4\pi\epsilon_0 r^3} \vec{r}$$

$$= \frac{\rho_L}{4\pi\epsilon_0} \int_0^{2\pi} \frac{-a\hat{a}_\rho + h\hat{a}_z}{[a^2 + h^2]^{3/2}} a d\phi$$



$$Q = \rho_L dL$$

$$dL = a d\phi = a d\phi$$

$$\vec{r} = -a\hat{a}_\rho + h\hat{a}_z$$

$$r = \sqrt{a^2 + h^2}$$

due to symmetry  $\rightarrow$  the  $\rho$  component will be cancelled.



$$\vec{E} = \frac{\rho_L a h}{2\epsilon_0 [a^2 + h^2]^{3/2}} \hat{a}z \quad \text{V/m}$$

② if  $a \rightarrow 0$ , show that the  $\vec{E}$  will look like the  $\vec{E}$  of a point charge.

Sol  $\vec{E} = \frac{\rho_L a h}{2\epsilon_0 [a^2 + h^2]^{3/2}} \hat{a}z \quad \Big|_{a=0} \stackrel{?}{=} \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}r$

$$Q = \int_L \rho_L dL$$

$$= \int_0^{2\pi} \rho_L a d\phi \Rightarrow Q = \rho_L 2\pi a$$

$$\rho_L = \frac{Q}{2\pi a}$$

$$\vec{E} = \frac{\frac{Q}{2\pi a} a h}{2\epsilon_0 [a^2 + h^2]^{3/2}} \hat{a}z \quad \Big|_{a \rightarrow 0}$$

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 h^2} \hat{a}z$$

$$r = h$$

$$\hat{a}r = \hat{a}z$$

\* Gauss's Law -

↳ special case from Coulomb's law

$$\Psi_e = \oint_S \underbrace{\vec{D}}_{\substack{\downarrow \\ \text{m}^2}} \cdot \underbrace{d\vec{s}}_{\substack{\downarrow \\ \text{m}^2}} = \underbrace{Q}_{\downarrow \text{C}}$$

- Electric Flux ( $\Psi_e$ ) in (C)

$$\Psi_e = \int_S \vec{D} \cdot d\vec{s} \quad \text{Scalar.}$$

\* Applications of Gauss's Law -

$$\oint_S \vec{D} \cdot d\vec{s} = Q = \int_L \rho_L dL \quad \text{Point / Line.}$$

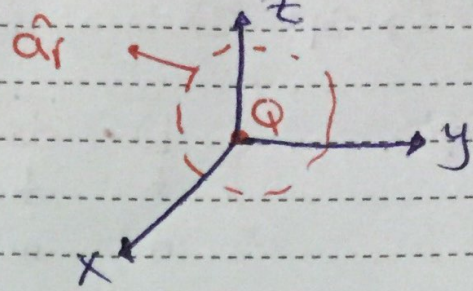
$$= \int_S \rho_S dS \quad \text{Surface.}$$

$$= \int_V \rho_V dV \quad \text{Volume.}$$

$$\star \oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_V dV$$

First Maxwell's eq. in integral form (Gauss's Law)

①  $\vec{E}$  or  $\vec{D}$  due to a point charge



$$\vec{D} = D r \hat{a}_r$$

$$d\vec{s} = r^2 \sin\theta d\theta d\phi \hat{a}_r$$

$$\oint_S \vec{D} \cdot d\vec{s} = \int_S \vec{D} \cdot d\vec{s} = \int_0^{2\pi} \int_0^{\pi} D r \hat{a}_r \cdot r^2 \sin\theta d\phi d\theta \hat{a}_r = Q$$

$$= r^2 D r (2\pi) = Q$$

$$= 4\pi r^2 D r = Q$$

$$D r = \frac{Q}{4\pi r^2}$$

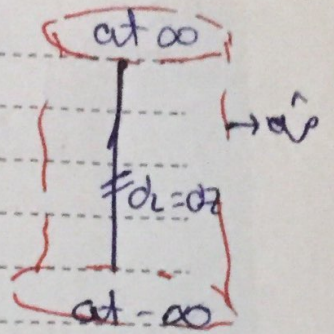
$$\vec{D} = D r \hat{a}_r$$

$$\vec{D} = \frac{Q}{4\pi \epsilon_0} \hat{a}_r$$

$$\vec{E} = \frac{\vec{D}}{\epsilon_0} = \frac{Q}{4\pi r^2 \epsilon_0} \hat{a}_r$$

$$\vec{D} = D \rho \hat{a}_\rho$$

$$d\vec{s} = \rho d\phi dz \hat{a}_\rho$$



$$\int_L \vec{D} \cdot d\vec{s}$$

$$= \int_{-L/2}^{L/2} \int_0^{2\pi} D \rho \hat{a}_\rho \cdot \rho d\phi dz \hat{a}_\rho$$

$$= \int_{-L/2}^{L/2} \rho L dz$$

$$L \rightarrow \infty$$

$$D \rho (\rho 2\pi L) = \rho L L$$

$$\vec{D} = \frac{\rho L}{2\pi \rho} \hat{a}_\rho$$

$$\vec{E} = \frac{\rho L}{2\pi \epsilon_0 \rho} \hat{a}_\rho$$

3)  $\vec{E}$  or  $\vec{D}$  due to an infinite sheet of charge

$$\oint_S \vec{D} \cdot d\vec{s} = Q_{en} = \int_S \rho_s d\vec{s}$$

$$\int_{S_{top}} \vec{D} \cdot d\vec{s}_{top} + \int_{S_{bot}} \vec{D} \cdot d\vec{s}_{bot} = \int_S \rho_s d\vec{s}$$



$$\vec{D} = \int D_z \hat{a}_z, \quad z > 0$$

$$D_z(-\hat{a}_z), \quad z < 0$$

$$\left. \begin{aligned} \vec{ds}_{top} &= dx dy \hat{a}_z \\ \vec{ds}_{bot} &= -dx dy \hat{a}_z \end{aligned} \right\}$$

$$D_z A + D_z A = \rho_s A$$

$$D_z = \frac{\rho_s}{2}$$

$$\vec{D} = \frac{\rho_s}{2} \hat{a}_n$$

$$\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_n$$

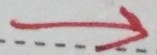
4)  $\vec{E}$  or  $\vec{D}$  due to uniform volume charge

- Ex consider a sphere of radius (a) has:

$$\rho_r = \begin{cases} \rho_0, & r < a \\ 0, & r > a \end{cases}$$

Find  $\vec{E}$  &  $\vec{D}$  everywhere.

↳ Gauss's Law.



$$\underline{\text{Sol}} \int_S \vec{D} \cdot \vec{ds} = Q_{enc} = \int \rho_v dv$$

For  $r < a$

$$\vec{D} = D_r \hat{a}_r$$

$$ds = r^2 \sin\theta \, d\theta \, d\phi \, \hat{a}_r$$

$$\int_0^{2\pi} \int_0^{\pi} \int_0^r D_r \hat{a}_r \cdot r^2 \sin\theta \, d\theta \, d\phi \, \hat{a}_r$$

$$= \int_0^{2\pi} \int_0^{\pi} \int_0^r \rho_0 r^2 \sin\theta \, dr \, d\theta \, d\phi$$

$$D_r (r^2) (2) (2\pi) = \rho_0 \frac{r^3}{3} (2) (2\pi)$$

$$D_r = \frac{\rho_0 r}{3}$$

$$\vec{D}_r = \frac{\rho_0 r}{3} \hat{a}_r$$

$$\vec{E} = \frac{\rho_0 r}{3\epsilon_0} \hat{a}_r$$

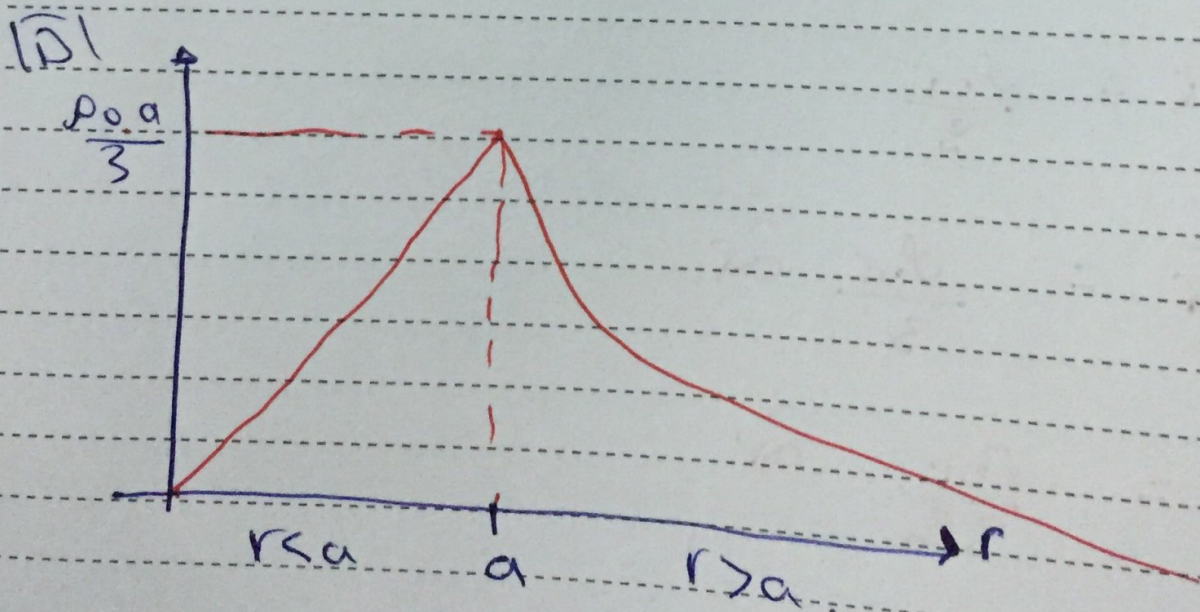
For  $r > a$ .

$$4\pi r^2 D_r = \int_0^a \int_0^\pi \int_0^{2\pi} \rho_0 r^2 \sin\theta dr d\theta d\phi$$
$$+ \int_0^r \int_0^\pi \int_0^{2\pi} \text{zero}$$

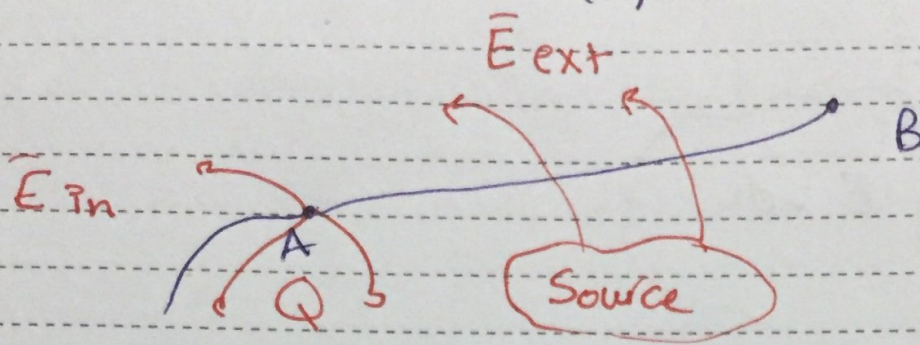
$$4\pi r^2 D_r = \rho_0 \frac{a^3}{3} (2)(2\pi)$$

$$D = \frac{\rho_0 a^3}{3r^2} \hat{a}_r \quad \left. \vphantom{\frac{\rho_0 a^3}{3r^2}} \right\} \rightarrow \text{for } r > a$$

$$E = \frac{\rho_0 a^3}{3\epsilon_0 r^2} \hat{a}_r$$



\* Electric Potential in (V) Scalar quantity.



To move Q from A to B

$$V_{AB} = V_B - V_A$$

$$\text{Voltage} = \frac{\text{Work}}{\text{charge}}$$

$$1V = \frac{1J}{1C}$$

Work = Voltage \* charge.

$$W = Q V_{AB}$$

↳ potential difference between two points.

$$W = \vec{F} \cdot \vec{L} \quad (N \cdot m).$$

$$= (-Q \vec{E}_{ext} \cdot \vec{L})$$

↳ the work is done by the external field.

$$\frac{W}{Q} = - \int \vec{E} \cdot d\vec{L}$$

$$V_{AB} = - \int_{r_A}^{r_B} \vec{E} \cdot d\vec{L}$$

- for a point charge :-

$$V_{AB} = - \int_{r_A}^{r_B} \frac{Q}{4\pi\epsilon_0 r^2} \hat{r} \cdot dr \hat{r}$$

$$V_{AB} = \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_B} - \frac{1}{r_A} \right) V$$

$$= \frac{Q}{4\pi\epsilon_0 r_B} - \frac{Q}{4\pi\epsilon_0 r_A}$$

$$V_{AB} = V_B - V_A$$

\* if point A is at  $\infty$

$$r_A = \infty$$

$$V_{\infty B} = \frac{Q}{4\pi\epsilon_0 r_B} - \frac{Q}{4\pi\epsilon_0 \infty} \rightarrow 0$$

$$= V_B - V_{\infty}$$

$$= V_B - 0$$

$$= \boxed{V_B}$$



## \* Notes

$V_{\infty} = 0$  Always, Since  $r = \infty$

- لو حكاى فرق، عن نقطة معينة فرق الكه بيه  
النقطة وال  $\infty$

$$V = - \int \vec{E} \cdot d\vec{r}$$

- إذا طلب منى potential استخدم

- To find  $(V) =$

↳ From  $\vec{E}$   $V = - \int \vec{E} \cdot d\vec{L}$

↳ From the source

↳ point charge

$$V = \frac{Q}{4\pi\epsilon_0 r}$$

↳ Line charge

$$V = \int \frac{\rho_L dL}{4\pi\epsilon_0 r}$$

↳ Surface charge

$$V = \int \frac{\rho_s ds}{4\pi\epsilon_0 r}$$

↳ Volume charge

$$V = \int$$

$\frac{\rho_v dV}{4\pi\epsilon_0 r}$  Volume

Voltage

Volume

Ex Two point charges  $(-4\mu C)$  and  $(5\mu C)$  are located at  $(2, -1, 3)$  and  $(0, 4, -2)$ . Find the potential at  $P(1, 0, 1)$ .

Sol reference is at  $\infty$

$$\begin{aligned} V_{\infty P} &= V_P - V_{\infty} \\ &= V_P - 0 \\ &= V_P \rightarrow \text{المطلوب} \end{aligned}$$

$$V_P = \sum_{k=1}^N \frac{Q_k}{4\pi\epsilon_0 r_k}$$

هذا هو  
 عندي أكثر  
 من نقطة  
 اخترت هذا القانون  
 عندي في  
 point charge.

$$= \frac{-4 \times 10^{-6}}{4\pi \times 10^9 \times \sqrt{6}} + \frac{5 \times 10^{-6}}{4\pi \times 10^9 \times \frac{5}{36\pi}}$$

$$\begin{aligned} \vec{r}_1 &= (1, 0, 1) - (2, -1, 3) \\ &= (-1, 1, -2) \end{aligned}$$

$$\begin{aligned} \vec{r}_2 &= (1, 0, 1) - (0, 4, -2) \\ &= (1, -4, 3) \end{aligned}$$

$$V = -5.872 \text{ kV}$$



- What is the meaning of the minus sign?

if  $V$  is -ve

↳ drop in potential.

↳ the work is done by the field itself.

~~↳ the work is done by the field~~

↳  $\int E \cdot dl$  is +ve.

- if  $V$  is +ve

↳ gain in potential.

↳ the work is done by an external field.

- Ex At point charge of (5nC) located at (-3, 4, 0) and a line  $y=1, z=1$  carries  $\rho_L = 2 \text{ nC/m}$  if  $V = 100 \text{ V}$  at  $B(1, 2, 1)$  Find the potential at  $C(-2, 5, 3)$ ??

sol  $V = V_Q + V_L$   
reference is (B)

$$V_{BC} = V_{BCQ} + V_{BCL}$$

$$= V_C - V_B$$

$$= V_C - 100$$

$$V_C = V_{BC} + 100$$



$$V_{BCQ} = \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_C} - \frac{1}{r_B} \right)$$

or

$$V_{BCQ} = - \int_P \vec{E} \cdot d\vec{L} = - \int_{r_B}^{r_C} \frac{Q}{4\pi\epsilon_0 r^2} \hat{r} \cdot dr \hat{r}$$

$$= \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_C} - \frac{1}{r_B} \right)$$

بسیستم  
های ایزا  
صافیت حافظه  
القانون الی  
فوق

$$r_C = |(1, 1, 3)| = \sqrt{11}$$

$$r_B = |(4, -2, 1)| = \sqrt{21}$$

$$V_{BC} = \int_{-\infty}^{\infty} \frac{\rho_L dL}{4\pi\epsilon_0 r} \rightarrow \text{complicated}$$

$$\text{So } V_{BC} = - \int_P \vec{E} \cdot d\vec{L}$$

$$= - \int_{r_B}^{r_C} \frac{\rho_L}{2\pi\epsilon_0 r} \hat{r} \cdot dr \hat{r}$$

$$= \frac{-\rho_L}{2\pi\epsilon_0} \ln(r_C) - \ln(r_B)$$



$$\frac{-\rho_L}{2\pi\epsilon_0} \cdot \ln\left(\frac{\rho_C}{\rho_B}\right)$$

$$= \frac{\rho_L}{2\pi\epsilon_0} \ln\left(\frac{\rho_B}{\rho_C}\right)$$

$$\rho_C = |(0, 4, 2)| = \sqrt{20}$$

أقصى مسافة

$$\rho_B = |(0, 1, 0)| = \sqrt{1}$$

$$V_{BC} = -50.175 \text{ V}$$

$$V_C = 49.825 \text{ W}$$

\* Electric potential :-

$$V = - \int_L \vec{E} \cdot d\vec{L}$$

$$\text{potential } dV = - \vec{E} \cdot d\vec{L}$$

-if in cart. coordinates-

$$\vec{E} = E_x \hat{a}_x + E_y \hat{a}_y + E_z \hat{a}_z$$

$$d\vec{L} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

$$\vec{E} \cdot d\vec{l} = E_x dx + E_y dy + E_z dz$$

$$dV = \frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz$$

Equating similar components -

$$\frac{\partial V}{\partial x} dx = -E_x dx$$

$$E_x = -\frac{\partial V}{\partial x}$$

$$E_y = -\frac{\partial V}{\partial y}$$

$$E_z = -\frac{\partial V}{\partial z}$$

$$\vec{E} = -\left(\frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z\right)$$

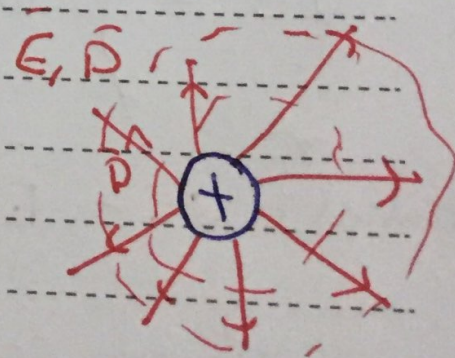
$\vec{E} = -\nabla V$  → to find  $\vec{E}$  if potential is given.

\* point charge.

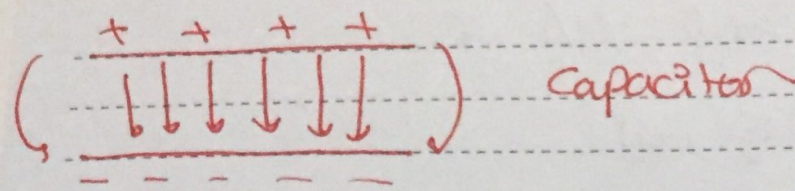
$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

Flux lines:  $V = \frac{Q}{4\pi\epsilon_0 r}$

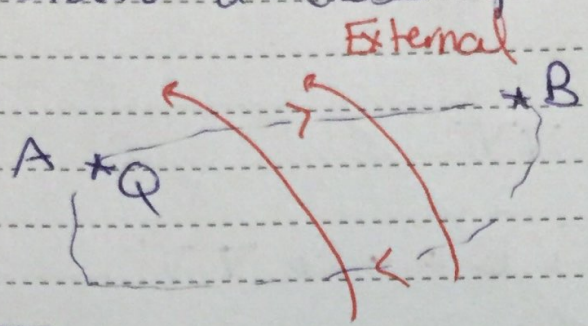
$$\vec{D} = \epsilon_0 \vec{E}$$



$\vec{E}, \vec{D}$   
 $\frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$



\* Potential around a closed paths -



Q في B  
B في A

$$W = Q V_{AB}$$

if Q is moved from A to B.

$$V_{AB} = - \int_A^B \vec{E} \cdot d\vec{L}$$

2nd Maxwell's equation  
in integral form

$$\oint \vec{E} \cdot d\vec{L} = 0$$

1st Maxwell's equ.

$$\oint \vec{D} \cdot d\vec{s} = \int_V \rho_v dv$$

$$V = \int_L \vec{E} \cdot d\vec{L}$$

$$V_{AA} = - \int_{r_A}^{r_B} \vec{E} \cdot d\vec{L} + - \int_{r_B}^{r_A} \vec{E} \cdot d\vec{L}$$

$$= - \int_{r_A}^{r_B} \vec{E} \cdot d\vec{L} + \int_{r_A}^{r_B} \vec{E} \cdot d\vec{L} = 0$$

$$V_{AA} = V_A - V_A = 0$$

-Ex Given  $V = \frac{10}{r^2} \sin\theta \cos\phi$  V

a) Find  $\vec{D}$  at  $(2, \frac{\pi}{2}, 0)$

b) calculate the work in moving a  $(10 \mu\text{C})$  charge from  $A(1, 30^\circ, 120^\circ)$  to  $B(4, 90^\circ, 60^\circ)$

Sol a)  $\vec{E} = -\nabla V$

$$\vec{D} = \epsilon_0 \vec{E} = -\epsilon_0 \nabla V$$

$$\vec{E} = - \left( \frac{\partial V}{\partial r} \hat{r} + \frac{\partial V}{r \partial \theta} \hat{\theta} + \frac{\partial V}{r \sin\theta \partial \phi} \hat{\phi} \right)$$

$$\vec{E} = - \left( \frac{-20}{r^3} \sin\theta \cos\phi \hat{r} + \frac{10}{r^3} \cos\theta \cos\phi \hat{\theta} \right)$$

$$= \frac{10}{r^3} \sin\theta \hat{\phi}$$

$$\rightarrow \vec{D} = \epsilon_0 \vec{E} \Big|_{(2, \frac{\pi}{2}, 0)} = \frac{10^{-9}}{36\pi} \left( \frac{20}{8} \hat{r} \right)$$

$$= 22 \hat{r} \cdot \text{pC/m}^2$$

b) Method (1)

$$W = Q V_{AB} = Q (V_B - V_A) \rightarrow V_B \text{ كيف انصب}$$

بعوض لنقطه B

$$= 10 \times 10^{-6} \left( \frac{10}{16} - \frac{1}{2} - 10 \left( \frac{1}{2} \right) \left( \frac{-1}{2} \right) \right) \text{ جوا معادله ادر V}$$

$$= 10 \times 10^{-6} \left( \frac{5}{16} + \frac{40}{16} \right)$$

$$= 10 \times 10^{-6} \left( \frac{45}{16} \right)$$

$$= \boxed{28.125 \text{ MJ}}$$

- Method (2)

$$W = -Q \int_{r_A}^{r_B} \vec{E} \cdot d\vec{l} \quad V = - \int \vec{E} \cdot d\vec{l}$$

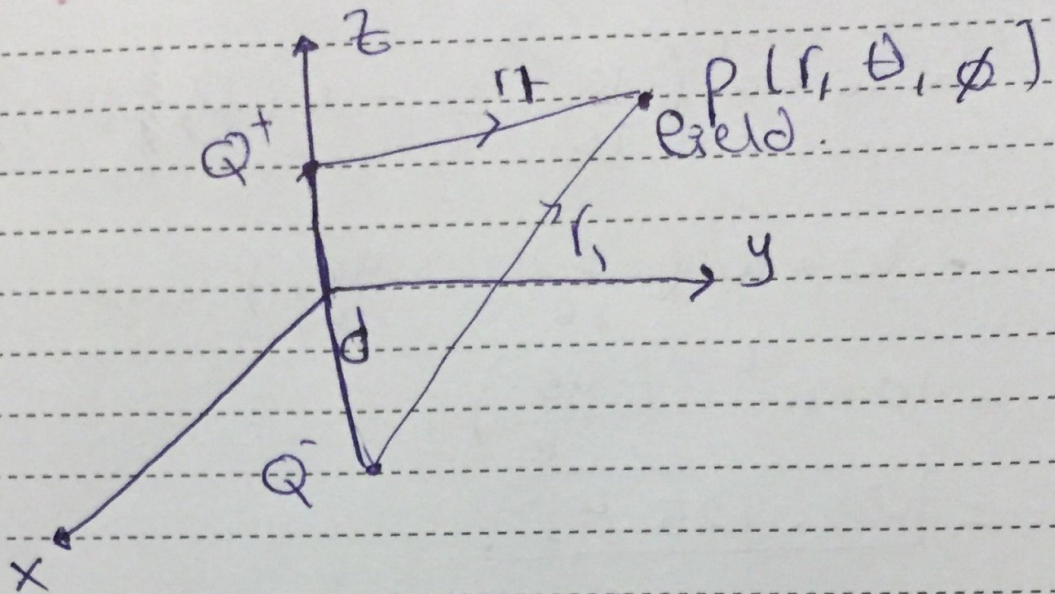
$$= -10 \times 10^{-6} \left[ \int_1^4 E_r dr + \int_{30^\circ}^{90^\circ} E_\theta r d\theta + \int_{120^\circ}^{60^\circ} E_\phi r \sin\theta d\phi \right]$$

$\theta = 30^\circ \quad \phi = 120^\circ \quad r = 4 \quad \theta = 90^\circ$   
 $\phi = 120^\circ \quad \phi = 120^\circ$

## \* Electric Dipoles -

- How to find  $\vec{E}$ ,  $\vec{D}$  and  $V$

$r \gg d$   
must  
for a  
dipole



- if  $r \gg d$  then it's two point charges.

- find  $V$ : (ref is at  $\infty$ )

$$V = V^+ + V^-$$

$$= \frac{Q}{4\pi\epsilon_0 r_1} + \frac{-Q}{4\pi\epsilon_0 r_2}$$

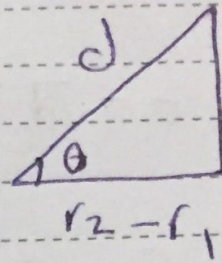
$$= \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_1} - \frac{1}{r_2} \right)$$

$$V = \frac{Q (r_2 - r_1)}{4\pi\epsilon_0 r_1 r_2}$$

$Q$  and it's location  
are not given

- Approximations :-

$$r_1, r_2 \approx r^2$$



$$\cos \theta = \frac{r_2 - r_1}{d}$$

$$r_2 - r_1 = d \cos \theta$$

$$\rightarrow V = \frac{Q d \cos \theta}{4\pi \epsilon_0 r^2}$$

- define a dipole moment as  $\vec{p} = Q\vec{d}$  in (C.m)

$$\rightarrow V = \frac{p \cos \theta}{4\pi \epsilon_0 r^2}$$

( $\vec{p}$ ) and the center of the dipole ~~are~~ are usually given.

$r =$  | Field - center of the dipole |

$\theta$  is the angle between ( $\vec{p}$ ) and ( $\vec{r}$ ).

$$V = \frac{\vec{p} \cdot \hat{a}_r}{4\pi \epsilon_0 r^2}$$

$$\rightarrow \vec{p} \cdot \hat{a}_r = p(1) \cos \theta \\ = p \cos \theta$$



$$\vec{E} = \vec{E}^+ + \vec{E}^-$$

$$\text{or } \vec{E} = -\nabla V$$

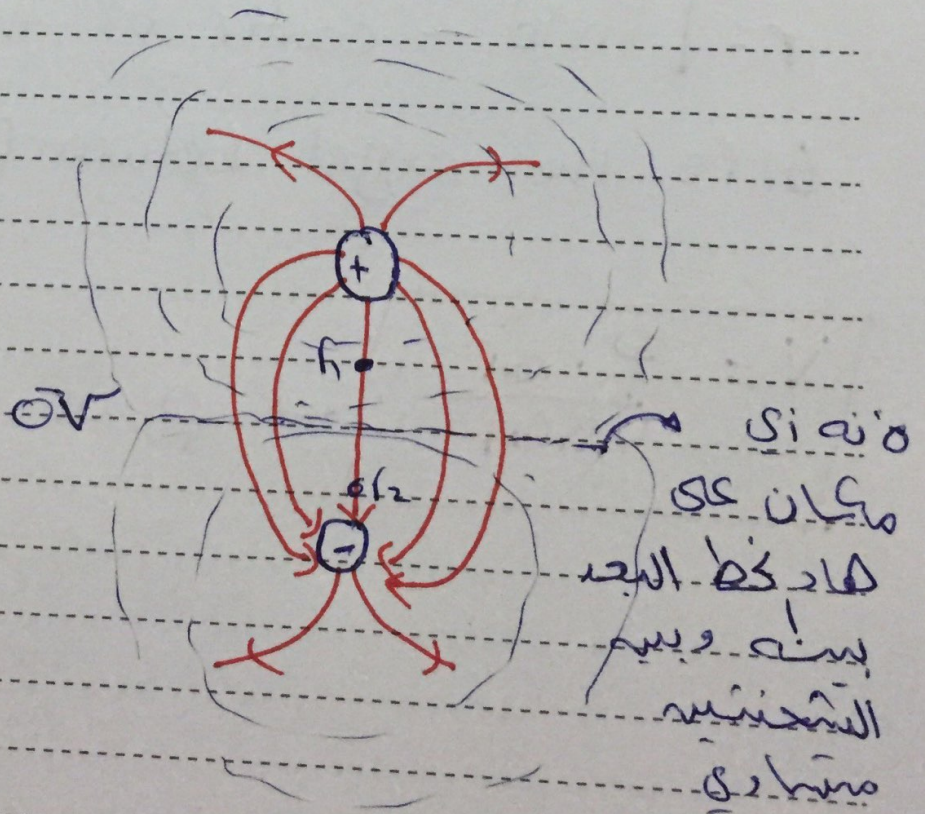
$$V = \frac{p \cos \theta}{4\pi\epsilon_0 r^2} \text{ (V)}$$

$$\begin{aligned} \vec{E} &= -\nabla V = -\left( \frac{\partial V}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial V}{\partial \theta} \hat{\theta} + \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi} \hat{\phi} \right) \\ &= \frac{p}{4\pi\epsilon_0 r^3} \left( -2 \cos \theta \hat{r} - \frac{\sin \theta}{r} \hat{\theta} \right) \end{aligned}$$

$$\vec{E} = \frac{p}{4\pi\epsilon_0 r^3} (2 \cos \theta \hat{r} + \sin \theta \hat{\theta})$$

$$\vec{D} = \epsilon_0 \vec{E}$$

Flux lines for the dipole.



- For  $N$ -dipoles -

$$V = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^N \frac{\vec{P}_k \cdot (\vec{r} - \vec{r}'_k)}{(\vec{r} - \vec{r}'_k)^3} \quad (1)$$

- Ex Two dipoles with dipole moments  $(-5a\hat{z})$  nc and  $(9a\hat{z})$  nc.m located at  $(0, 0, -2)$  and  $(0, 0, 3)$ . Find the potential at the origin.

Sol

$$V_{\infty} = \frac{-5a\hat{z} * 10^{-9} \cdot 2a\hat{z}}{4\pi * 10^{-9} * 8}$$

$$+ \frac{9a\hat{z} * 10^{-9} \cdot (-3a\hat{z})}{4\pi * 10^{-9} * 27} = \ominus 20.25 \text{ V}$$

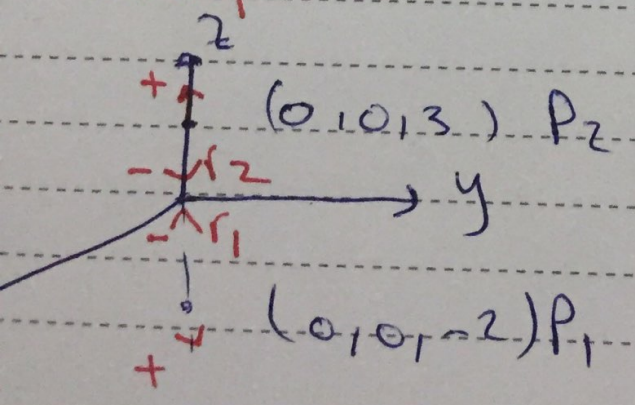
↳ drop, work done by field itself.

- Find  $\vec{E}$  at origin?

$$\vec{E} = \vec{E}_1 + \vec{E}_2$$

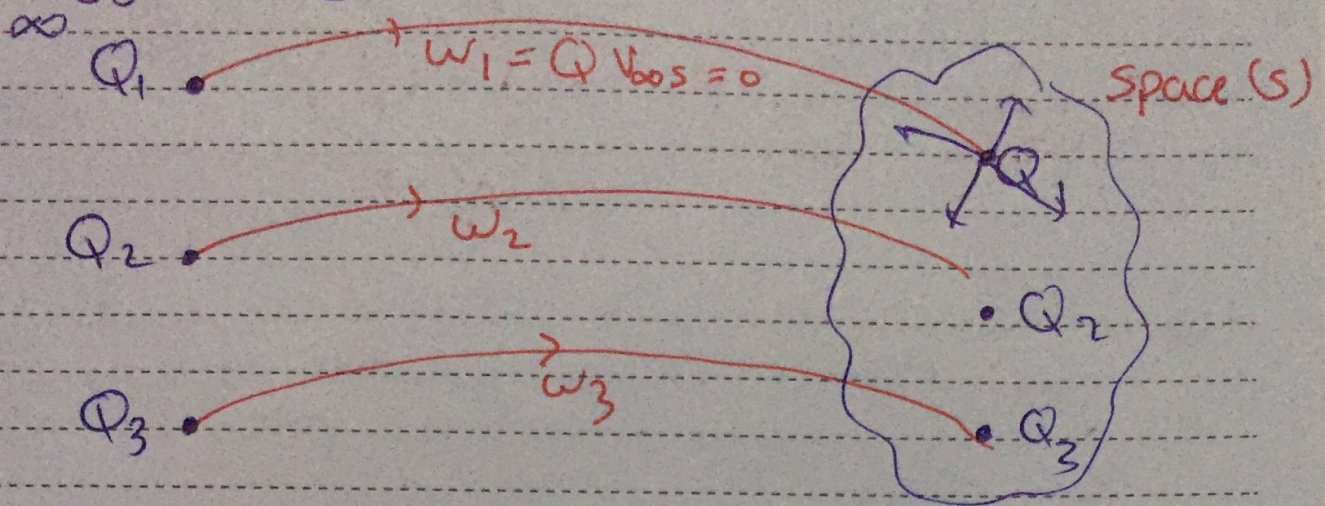
$$= \frac{P}{4\pi\epsilon_0 r^3} (2\cos\theta, \hat{a}_r + \sin\theta, a\hat{\theta})$$

- $P_1 = 5 \text{ nc.m}$
- $P_2 = 9 \text{ nc.m}$
- $r_1 = 2$
- $r_2 = 3$



rep.  $\theta_1 = 180$   
 $\theta_2 = 180$

# \*Energy Density of Electrostatic Fields:-



$Q_1, Q_2, Q_3$

$W_E$  : Electrical Energy (J).

$$W_E = W_1 + W_2 + W_3$$

$$0 + Q_2(V_{12}) + Q_3(V_{13} + V_{23}) \dots \textcircled{1}$$

\*  $Q_3 \rightarrow Q_2 \rightarrow Q_1$

$$W_E = W_1 + W_2 + W_3$$

$$Q_1(V_{21} + V_{31}) + Q_2(V_{32}) + 0 \dots \textcircled{2}$$

$\textcircled{1} + \textcircled{2}$

$$2W_E = Q_1(\underbrace{V_{21} + V_{31}}_{V_1}) + Q_2(\underbrace{V_{12} + V_{32}}_{V_2}) + Q_3(\underbrace{V_{13} + V_{23}}_{V_3})$$

$$W_E = \frac{1}{2} (Q_1 V_1 + Q_2 V_2 + Q_3 V_3)$$

$$W_E = \frac{1}{2} \sum_{k=1}^N Q_k V_k \quad (\text{J}) \quad \text{for } N\text{-point charges.}$$

- For Line charges -

$$W_E = \frac{1}{2} \int_L \rho_L V dl \quad \text{potential.}$$

- For surface charges -

$$W_E = \frac{1}{2} \int_S \rho_s V ds$$

- For volume charges -

$$W_E = \frac{1}{2} \int_V \rho_v V dv$$

\* How to relate energy to  $E$ ?

$$W_E = \frac{1}{2} \int_V \rho_v V dv$$

Using Gauss Law

$$\oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_v dv$$

$$W_E = \frac{1}{2} \int_V \vec{E} \cdot \vec{D} \, dV$$

or

$$W_E = \frac{1}{2} \int_V \epsilon_0 E^2 \, dV$$

$$(\vec{D} = \epsilon_0 \vec{E})$$

or

$$W_E = \frac{1}{2} \int_V \frac{D^2}{\epsilon_0} \, dV$$

$$(\vec{E} = \frac{\vec{D}}{\epsilon_0})$$

$$\vec{E} \cdot \vec{E} = |\vec{E}|^2$$

\* Energy Density ( $w_E$ )

$$w_E = \frac{W_E}{\text{Volume}} \quad (\text{J/m}^3)$$

or

$$w_E = \frac{1}{2} \vec{E} \cdot \vec{D}$$

$$= \frac{1}{2} \epsilon_0 E^2$$

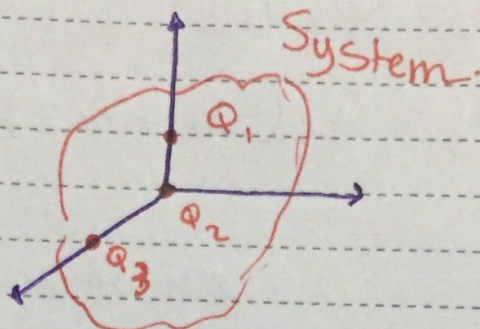
$$= \frac{1}{2} \frac{D^2}{\epsilon_0}$$

$$W_E = \int_V w_E \, dV$$

os,  $w_E$  کثرت  
 $w_E$  چگالی

- Ex The point charges  $(-1 \text{ nC})$ ,  $(4 \text{ nC})$  and  $(3 \text{ nC})$  are located at  $(0, 0, 0)$ ,  $(0, 0, 1)$  and  $(1, 0, 0)$ . Find the energy in the system?

Sol



$$W_E = \frac{1}{2} \sum_{k=1}^3 Q_k V_k$$

$$= \frac{1}{2} [Q_1 V_1 + Q_2 V_2 + Q_3 V_3]$$

$$= \frac{1}{2} [Q_1 (V_{21} + V_{31}) + Q_2 (V_{12} + V_{32}) + Q_3 (V_{13} + V_{23})]$$

$$= \frac{1}{2} \left[ Q_1 \left( \frac{Q_2}{4\pi\epsilon_0(1)} + \frac{Q_3}{4\pi\epsilon_0(1)} \right) + Q_2 \left( \frac{Q_1}{4\pi\epsilon_0(1)} + \frac{Q_3}{4\pi\epsilon_0(\sqrt{2})} \right) \right.$$

$$\left. + Q_3 \left( \frac{Q_1}{4\pi\epsilon_0(1)} + \frac{Q_2}{4\pi\epsilon_0(\sqrt{2})} \right) \right]$$

$$= \frac{1}{2(4\pi\epsilon_0)} \left[ Q_1 Q_2 + Q_1 Q_3 + Q_2 Q_1 + \frac{Q_2 Q_3}{\sqrt{2}} + \frac{Q_3 Q_1}{\sqrt{2}} + \frac{Q_3 Q_2}{\sqrt{2}} \right]$$

$$= \boxed{13.37 \text{ nJ}}$$

$$\hookrightarrow W_1 + W_2 + W_3$$

لو طلبت مني احسب work لـ ~~كل~~ ~~شحنه~~  $Q_1$   $Q_2$   $Q_3$

$Q_1$   
↓  
 $Q_2$   
↓  
 $Q_3$

$$W_1 = 0$$

$$W_2 = Q_2 V_{12}$$

$$W_3 = Q_3 (V_{13} + V_{23})$$

- لو كان السؤال System بيكده معين

$$W_E = \frac{1}{2} \int_V \epsilon_0 E^2 dv$$

$r^2 \sin\theta dr d\theta d\phi$

$$\left( \frac{Q}{4\pi\epsilon_0 r^2} \right)^2$$

$r_{12}$   
 $r_{13}$   
 $r_{23}$

## \* CH5 Electric Field in Materials -

- Classification of materials based on its electrical properties.

↳ Conductors (Metals) ( $\sigma \gg \gg 1$ )  
Cu, Al, Ag, lead

↳ Semi-conductors ( $\sigma \approx 1$ )  
Si, GaAs, Ge

↳ Dielectric (Insulators) ( $0.5 < \sigma < 1$ )  
Li, Mica, Polythelene, Polysthen

$\sigma \equiv$  conductivity (S/m) or  $(\Omega \cdot m)^{-1}$

-  $\sigma = \sigma_0 \rightarrow$  Free space

$\sigma$  depends on -

↳ Temperature ( $^{\circ}K$ )

↳ Frequency (Hz)

ie lead at ( $20^{\circ}C$ ) ( $293^{\circ}K$ )

$$\sigma = 10^6 \text{ S/m}$$

at ( $4^{\circ}K$ )

$$\sigma = 10^{20} \text{ (S/m)}$$

(super conductor)

perfect "

good "



\*  $T \uparrow \rightarrow \sigma \downarrow$

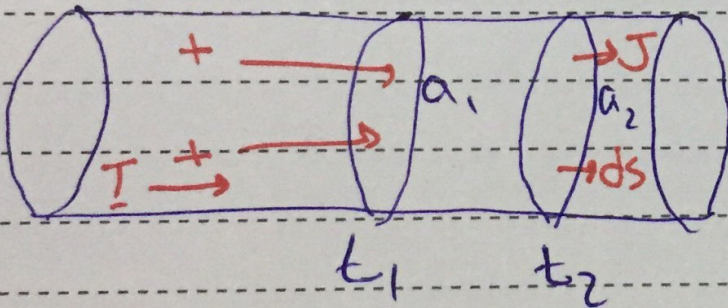
$\sigma = \frac{1}{\rho}$   
 $\rho \rightarrow$  resistivity ( $\Omega m$ )

\* Types of currents:-

- 1) Conduction current (DC or AC)
- 2) convection current (DC) - *بصر باطارية، لاجزای*
- 3) Displacement current (AC)

①

\*  $I = \frac{\Delta q}{\Delta t} = \frac{a_2 - a_1}{t_2 - t_1}$



Unit  $\rightarrow \frac{C}{s} = [A]$

\* define  $J =$  current density

$$J = \frac{I}{S} = (A/m^2)$$

$$I = JS \quad (\text{if uniform})$$

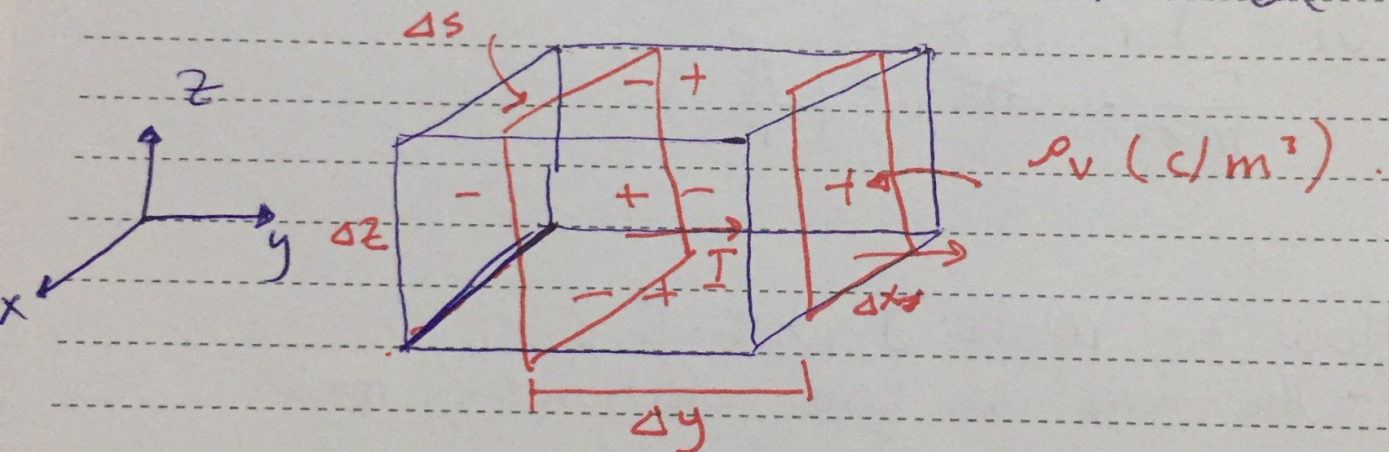
(2)

$$I = \int_S \vec{J} \cdot d\vec{S}$$

Scalar

\* Convection Current (Density) :-

- A portion of a dielectric material



$$\Delta S = \Delta x \Delta z$$

$$\Delta V = \Delta x \Delta y \Delta z = \Delta y \Delta S$$

$$Q = \int_V \rho_v dV$$

$$dq = \rho_v dV$$

$$I = \frac{\Delta q}{\Delta t} = \frac{dq}{dt} = \frac{\rho_v dV}{dt}$$

$$= \frac{\rho_v \Delta y \Delta S}{dt}$$

$\frac{dy}{dt}$  : drift velocity (m/s)

$$\frac{dy}{dt} = u_y$$

→  $I = \rho_v u_y \Delta S$       $I$ : convection current.

$$J = \frac{I}{\Delta S} = \rho_v u_y$$

$\vec{J} = \rho_v \vec{u}$  ,  $\vec{u} = u_y \hat{a}_y$

Convection current density.

Unit for  $\vec{J}$  :-

$$\frac{C}{m^2} \cdot \frac{m}{s} = \left( \frac{A}{m^2} \right)$$

\* How to relate  $\vec{J}$  with  $\vec{E}$  ?

- The force on one electron - mass

$Q = -e$  ,  $\vec{F} = Q \vec{E} = -e \vec{E} = m \vec{a}$  → acceleration

$$\vec{a} = \frac{du}{dt} = \frac{\Delta u}{\Delta t} = \frac{u}{\tau}$$

$\tau$  : time between collisions (s) → affected by Temperature  
الزمن الذي يحتاجه الإلكترون للتحرك مسافة موجبة

$$\rightarrow -e\bar{E} = m \frac{\bar{u}}{\tau}$$

$$\bar{u} = \frac{-e\tau}{m} \bar{E}$$

at a certain Temperature.

$\frac{-e\tau}{m}$  is constant =  $\mu$  = mobility  $\left(\frac{\text{C}\cdot\text{s}}{\text{kg}}\right)$  <sup>unit</sup>

$$\bar{v}_d = \bar{u} = \mu \bar{E}$$

- For  $\rho_v = -ne$ ,  $n = \#$  of charges per volume (#/m<sup>3</sup>)

$n$  depends on the portion volume.

$$\bar{u} = \mu \bar{E}$$

$$\bar{J} = \rho_v \bar{u}$$

$$\bar{J} = -ne \mu \bar{E} = -ne \left(\frac{-e\tau}{m}\right) \bar{E}$$

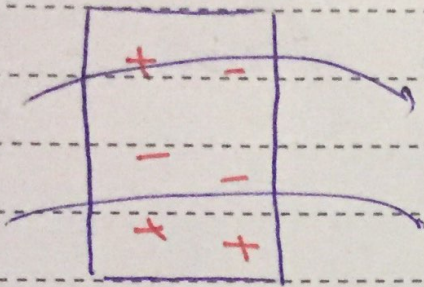
$$\bar{J} = \left(\frac{ne^2\tau}{m}\right) \bar{E}$$

$\sigma$  conductivity

$$\bar{J} = \sigma \bar{E}$$

Conduction current density.

# + Conductors

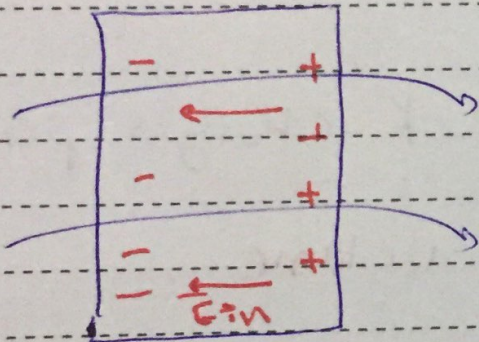


$\vec{E}_{\text{external}}$

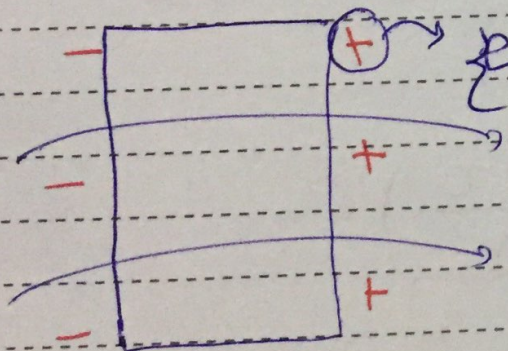
$$\vec{E} = -\nabla V$$

$$Q_{\text{total}} = 0$$

$$\vec{F} = Q \vec{E}_{\text{external}}$$



$\vec{E}_{\text{external}}$



الداخل فارغ تماماً

$\vec{E}_{\text{external}}$

inside-

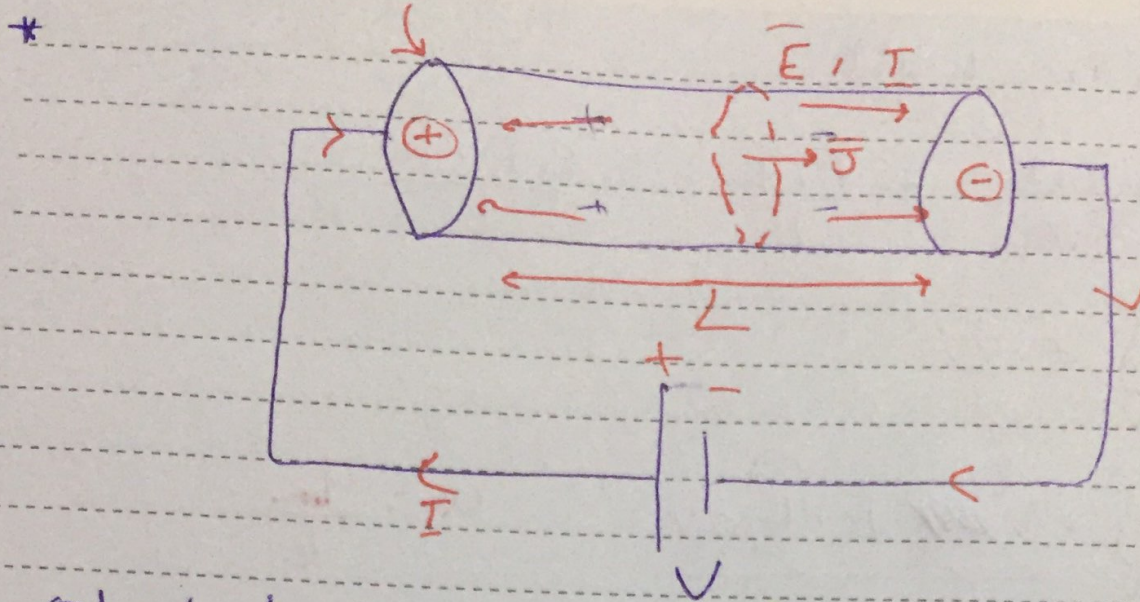
$$\vec{E} = 0$$

$$\vec{D} = 0$$

$$\rho = 0$$

$$\nabla \phi = 0$$

conductor



- Ohm's Law

$$R = \frac{V}{I} = \frac{L}{\sigma S} = \frac{\rho L}{S} \quad (\Omega) \quad \text{if uniform.}$$

$$R = \frac{-\int \vec{E} \cdot d\vec{l}}{\int_S \sigma \vec{E} \cdot d\vec{s}}$$

in general

↳ if uniform

$$\hookrightarrow R = \frac{E \cdot L}{\sigma E S} = \frac{\rho L}{S}$$

\* power in watt

$$P = \frac{\text{Work}}{\text{Time}} = \frac{\vec{F} \cdot \vec{L}}{t} = \frac{Q \vec{E} \cdot \vec{L}}{t}$$

$$Q = \int_V \rho dv$$

$$\rightarrow P = \int_V \rho v \vec{E} \cdot \vec{L} dv \quad \vec{u} = \frac{\vec{L}}{t}$$

$$P = \int_V \rho v \vec{E} \cdot \vec{u} dv = \int_V \vec{J} \cdot \vec{E} dv$$

$$P = \int_V \vec{J} \cdot \vec{E} dv$$

or

$$P = \int_V \sigma E^2 dv, \quad \vec{J} = \sigma \vec{E}$$

or

$$P = \int_V \frac{\vec{J}^2}{\sigma} dv, \quad E = \frac{\vec{J}}{\sigma}$$

- in circuit,  $P = V \cdot i = \frac{V^2}{R} = i^2 R = G V^2 = \frac{i^2}{G}$

$$* P = \int_V \vec{J} \cdot \vec{E} \, dV \quad \text{in general}$$

- if uniform

$$V = \int dV$$

$$P = \int_S \int \vec{J} \cdot \vec{E} \, d\vec{s} \, ds$$

$$P = \int_S \vec{J} \cdot d\vec{s} \int \vec{E} \cdot d\vec{L}$$

$$P = IV$$

\* Power Density -

$$w_p = \frac{\text{Power}}{\text{Volume}} \quad (\text{W/m}^3)$$

$$w_p = \vec{J} \cdot \vec{E}$$

$$= \epsilon E^2$$

$$= \frac{J^2}{\sigma}$$

$$P = \int_V w_p \, dV$$



\*Ex 3) if  $\vec{J} = \frac{1}{r^3} (2 \cos\theta \hat{r} + \sin\theta \hat{\theta}) \text{ A/m}^2$

Find the current passing through:

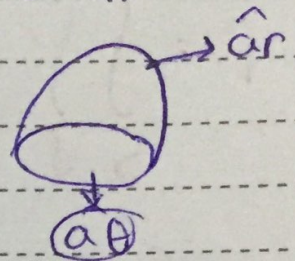
a) A hemi spherical shell of radius 20 cm  
 $0 < \theta < \frac{\pi}{2}$ ,  $0 < \phi < 2\pi$

b) A spherical shell of radius 10 cm.

Sol a)  $I = \int_S \vec{J} \cdot \vec{ds}$

$$= \int_0^{2\pi} \int_0^{\pi/2} \frac{1}{r} \frac{2 \cos\theta \sin\theta}{\sin^2\theta} d\theta d\phi \Big|_{r=0.2m}$$

$$= 10\pi \text{ A} = 31.4 \text{ A}$$



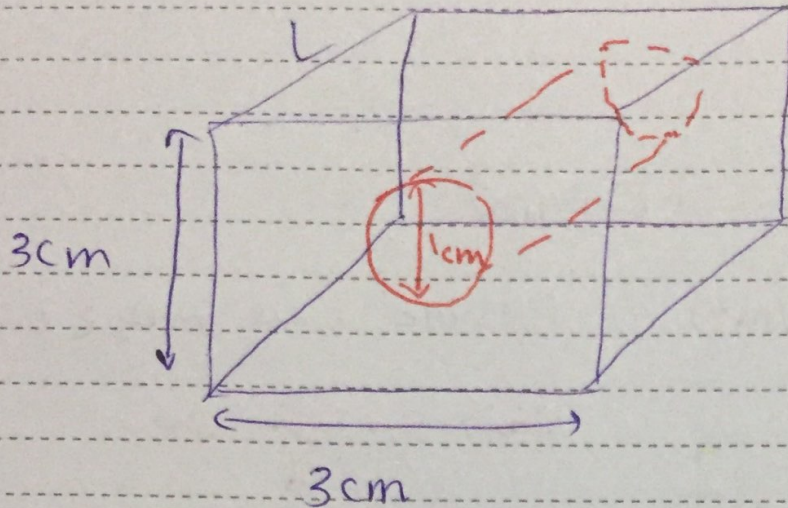
هذا نصف كروي  
 مع محور z  
 نصفه Shell  
 نصفه من هذا  
 $ds = r^2 \sin\theta d\theta d\phi \hat{r}$

b)  $I = \int_S \vec{J} \cdot \vec{ds}$

$$= \int_0^{2\pi} \int_0^{\pi} \frac{1}{r} \sin^2\theta d\theta d\phi \Big|_{r=0.1m}$$

$$= 0 \text{ A}$$

\* Ex 5 A lead  $\sigma = 5 \times 10^6$  S/m,  $L = 4$  m, Find R?



Sol  $R = \frac{L}{\sigma A}$

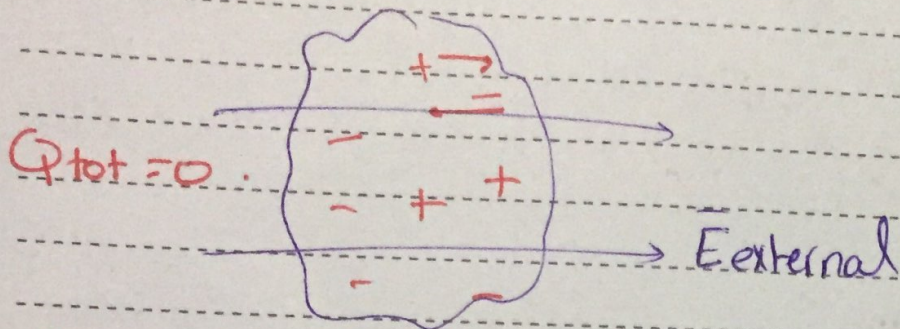
$$A = (3 \times 10^{-2})^2 - \pi \left(\frac{1}{2} \times 10^{-2}\right)^2$$

$$R = 974 \mu\Omega$$

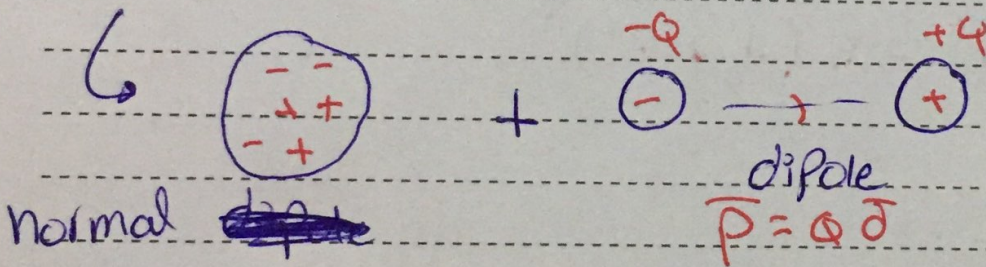
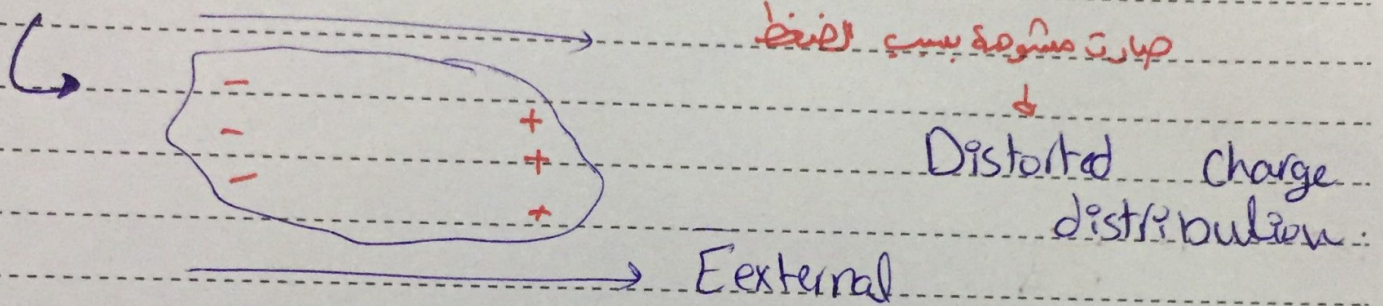
\* Polarization in Dielectrics -

- ① Non-polar Dielectrics  
 $O_2, H_2, N_2, \text{Rare gases}$   
(Kr, Xe, Ne)
- ② Polar Dielectrics  
(permanent dipoles)  
 $H_2O, NH_3, HCl$

- Non-polar dielectrics.



pressure =  $\frac{F}{S}$  (N/m<sup>2</sup>)      Pressure دى عىس دى عىس



دو ائسئىل عىس بىر ائسئىل دى عىس دى عىس دى عىس

$\rho_s$  Free ~~volume~~ surface charge distribution ( $C/m^2$ )

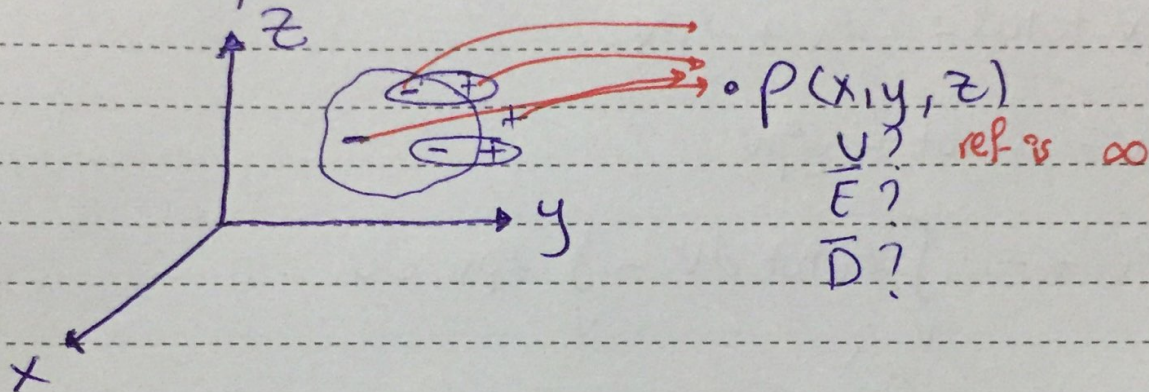
$\rho_v$  Free volume charge distribution ( $C/m^3$ )

$\rho_{ps}$  polarized (bound) surface charge dist. ( $C/m^2$ )

$\rho_{pv}$  polarized ~~volume~~ (bound) volume charge dist. ( $C/m^3$ )

\*  $\vec{P} = \lim_{\Delta V \rightarrow 0} \frac{\sum_{k=1}^N \vec{p}_k}{\Delta V}$  dipole moment.  
 (C/m<sup>2</sup>)

\* For a polarized Dielectric -



$V = \int_S \frac{\rho_{ps} ds}{4\pi\epsilon_0 r}$        $V = \int_V \frac{\rho_{pv} dv}{4\pi\epsilon_0 r}$

dielectric  $\rho_{ps}$  و  $\rho_{pv}$  للشحنات الحرة

$V = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r}$        $V = \int_V \frac{\rho_v dv}{4\pi\epsilon_0 r}$

Free charges.

$\vec{E} = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r^2} \hat{r}$

$\vec{E} = \int_S \frac{\rho_{ps} ds}{4\pi\epsilon_0 r^2} \hat{r}$

or  $\vec{E} = -\nabla V$

$\vec{D} = \epsilon_0 \vec{E}$

$$\rho_s = \bar{D} \cdot \hat{a}_n$$

$$\rho_v = \oint_S \bar{D} \cdot d\vec{s} = \int_V \rho_v dV$$

- Duality :-

$$\rho_s = \bar{P} \cdot \hat{a}_n$$

$$\rho_{pv} = -\nabla \cdot \bar{P} \quad \text{القانون الثاني لغاز ستيفان}$$

$$\rho_v \text{ total} = \rho_v + \rho_{pv}$$

$$\rho_v = \rho_{v \text{ tot}} - \rho_{pv}$$

$$\int_V \rho_v dV = \int_V \rho_{v \text{ tot}} dV - \int_V \rho_{pv} dV$$

$$\oint_S \bar{D} \cdot d\vec{s} = \int_S \bar{E} \cdot d\vec{s} - \int_S \bar{P} \cdot d\vec{s}$$

$$\bar{D} = \epsilon_0 \bar{E} + \bar{P}$$

- For some dielectrics

↳ linear, isotropic

$$\bar{P} = \chi_e \epsilon_0 \bar{E}$$

$\chi_e$  : electric susceptibility (constant for each material)

$$\bar{D} = \epsilon_0 \bar{E} + \chi_e \epsilon_0 \bar{E}$$

$$= \epsilon_0 \bar{E} (1 + \chi_e)$$

$\epsilon_r \equiv$  relative permittivity.

$$\bar{D} = \epsilon_0 \epsilon_r \bar{E}$$

F/m

F/m



$$, \bar{E} = \epsilon_0 \epsilon_r$$



↳ unitless

permittivity

in the air  $\rightarrow \epsilon_r = 1$

$$\epsilon_r = 1 + \chi_e$$

$$\epsilon_r = \frac{\epsilon}{\epsilon_0}$$

\*  $\epsilon_r$  : Dielectric constant (Dk)

i.e: Teflon: 2.15

water: 81

FR-4: 4.4

Free space: 1

air : 1.0006  $\approx$  1

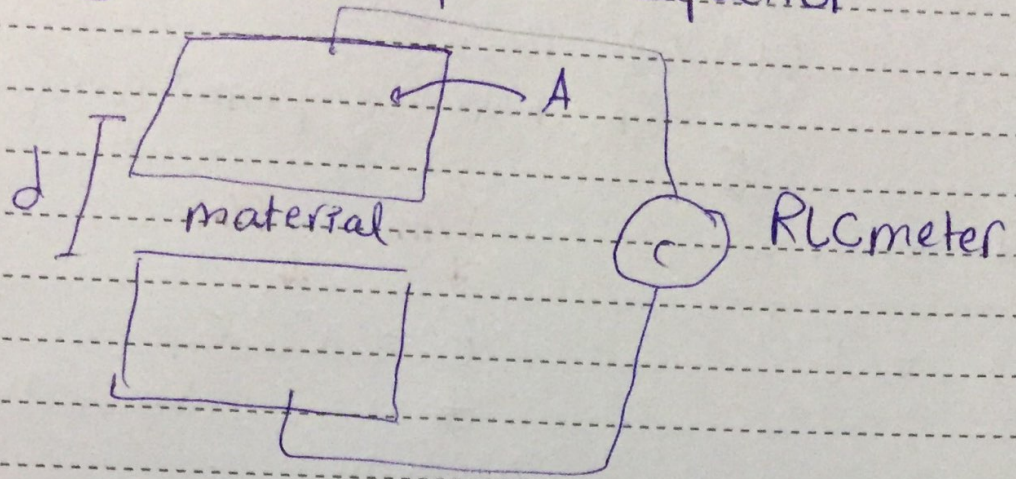
conductors : 0.999  $\approx$  1

$$\bar{P} = (\epsilon_r - 1) \epsilon_0 \bar{E}$$

! إذا كنت متطابقين مع السؤال

- How to measure  $\epsilon_r$  -

- by using parallel plate capacitor



- Fix  $d = 1 \text{ cm}$

material: Air  $\rightarrow \epsilon_r = 1$

مع يقرأ قراءة اسها  $C_0$

$C_0$  is Capacitance of Free space.

- بغير material (خشب / زجاج / ...)  
و يقرأ قراءة اسها  $C_{mat}$

$$\epsilon_r = \frac{C_{mat}}{C_0}$$

$$* C = \frac{\epsilon_0 A}{d}$$

$$C_0 = \frac{\epsilon_0 A}{d}$$

$$C_{mat} = \frac{\epsilon_0 \epsilon_r A}{d}$$

$$* D | \gg \gg D |$$

Dielectric  
( $\epsilon_r > 1$ )

air  
Conde

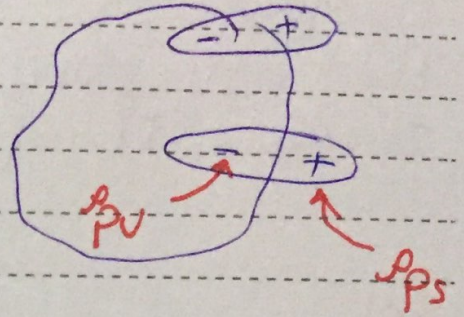
$$[\bar{D} = \epsilon_0 \bar{E} + \bar{P}]$$

$$\bar{D} = \epsilon_0 \bar{E} + \bar{P}$$

\* Bound Charges - ( $Q_b$ ) in (c)

$$Q_{b+} = \int_S \rho_s ds$$

$$Q_{b-} = \int_V \rho_v dv$$



$$Q_{b\text{tot}} = Q_{b+} + Q_{b-} = 0$$

~~Material~~ material is electrically neutralized.

\* Dielectric Breakdowns -

1) Nature of the material

2) Temperature ( $T \uparrow$ ,  $\epsilon \downarrow$ )

3) Humidity ( $H \uparrow$ ,  $\epsilon \uparrow$ )

4) Applied  $\bar{E}$ -Field

5) Time of applied Field

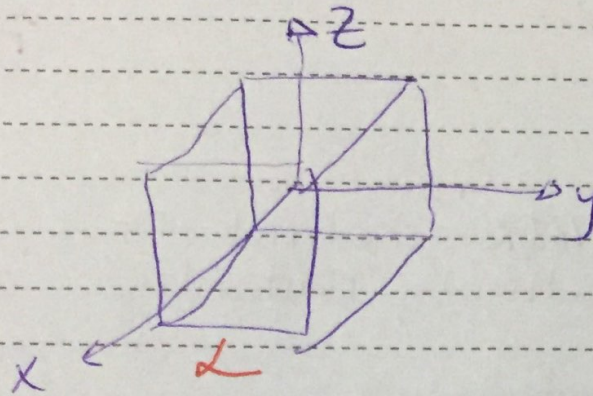
\* Dielectric Strengths -

Maximum value of  $\bar{E}$ -Field that the dielectric can tolerate without being broken down.



- Ex A dielectric cube of length ( $L$ ) centered at the origin has  $\vec{P} = a\vec{r}$ ,  $a$  is constant. Find all bound charge densities & the total charge if  $\rho_f = -3a \text{ C/m}^3$

Sol



$$\rho_{ps} = \vec{P} \cdot \hat{n}$$

$$\vec{P} = -ax \hat{a}_x + ay \hat{a}_y + az \hat{a}_z$$

$$\rho_{ps}|_{\text{front}} = ax \Big|_{x=\frac{L}{2}} = \frac{aL}{2} \text{ C/m}^2$$

$$\rho_{ps}|_{\text{back}} = -ax \Big|_{x=-\frac{L}{2}} = \frac{aL}{2} \text{ C/m}^2 \quad (\hat{n} = -\hat{a}_x)$$

- All surfaces have  $\rho_{ps} = \frac{aL}{2} \text{ C/m}^2$

$$Q_b(\text{total}) = Q_{b^+} + Q_{b^-} = 0.$$

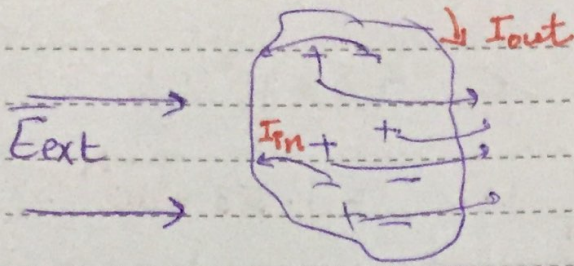
$$Q_{b^+} = 6 \int \rho_{ps} ds$$

$$ds = L \cdot L$$

$$Q_{b^+} = 3aL^3 \text{ C}$$

$$Q_{b^-} = \int \rho_f dv = -3aL^3$$

## \* Continuity Equation and Relaxation time ( $T_r$ )



KCL:  $I_{out} = I_{in}$

$$\oint_S \vec{J} \cdot d\vec{s} = - \frac{dq}{dt}$$

الشحنات التي تتركها هي سالبة  
 للشحنات التي تدخلها هي موجبة  
 شحنات يتطلع على سطح

$$\oint_S \vec{J} \cdot d\vec{s} = - \int_V \frac{d\rho}{dt} dV \quad Q = \int_V \rho dV$$

Continuity Equation in integral form.

$$\nabla \cdot \vec{J} = - \frac{d\rho}{dt} \quad X$$

## \* Relaxation Time ( $T_r$ )

- till ~~62.8%~~ of charges are on the outer surface  
 of **62.8%** start conduction  
 of **36.8%** are still inside the volume.

	$\vec{e} = 0.368 \rightarrow 1 T_r$	$(1 - \vec{e}) * 100\%$ outside
inside	$\vec{e} = 0.14 \rightarrow 2 T_r$	
	$\vec{e} \approx 0.05 \rightarrow 3 T_r$	
	$\vec{e} \approx 0.018 \rightarrow 4 T_r$	
	$\vec{e} < 0.1 \approx 0.006 \rightarrow 5 T_r$	

$$* T_r = \frac{\epsilon_0 \epsilon_r}{\sigma}$$

- i.e. copper  $\epsilon_r = 1$ ,  $\sigma = 5.8 \times 10^7 \text{ S/m}$

$$T_r = \frac{\epsilon}{\sigma} = \frac{10^{-9}}{36\pi} (1) = 1.53 \times 10^{-19} \text{ S}$$

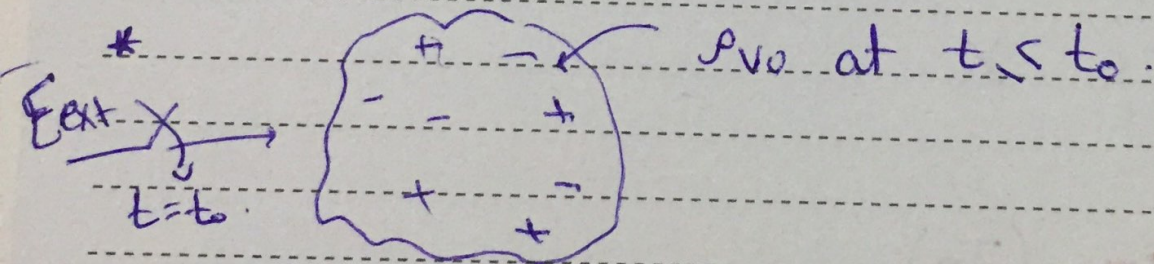
$$\frac{10^{-9}}{5.8 \times 10^7}$$

$$5 T_r \approx 7.5 \times 10^{-19}$$

- Fused Quartz  
 $\epsilon_r = 5$ ,  $\sigma = 10^{-17} \text{ S/m}$

$$T_r = \frac{\epsilon}{\sigma} = \frac{10^{-9}}{36\pi} (5) = 51.2 \text{ days}$$

$$\frac{10^{-9}}{10^{-17}}$$



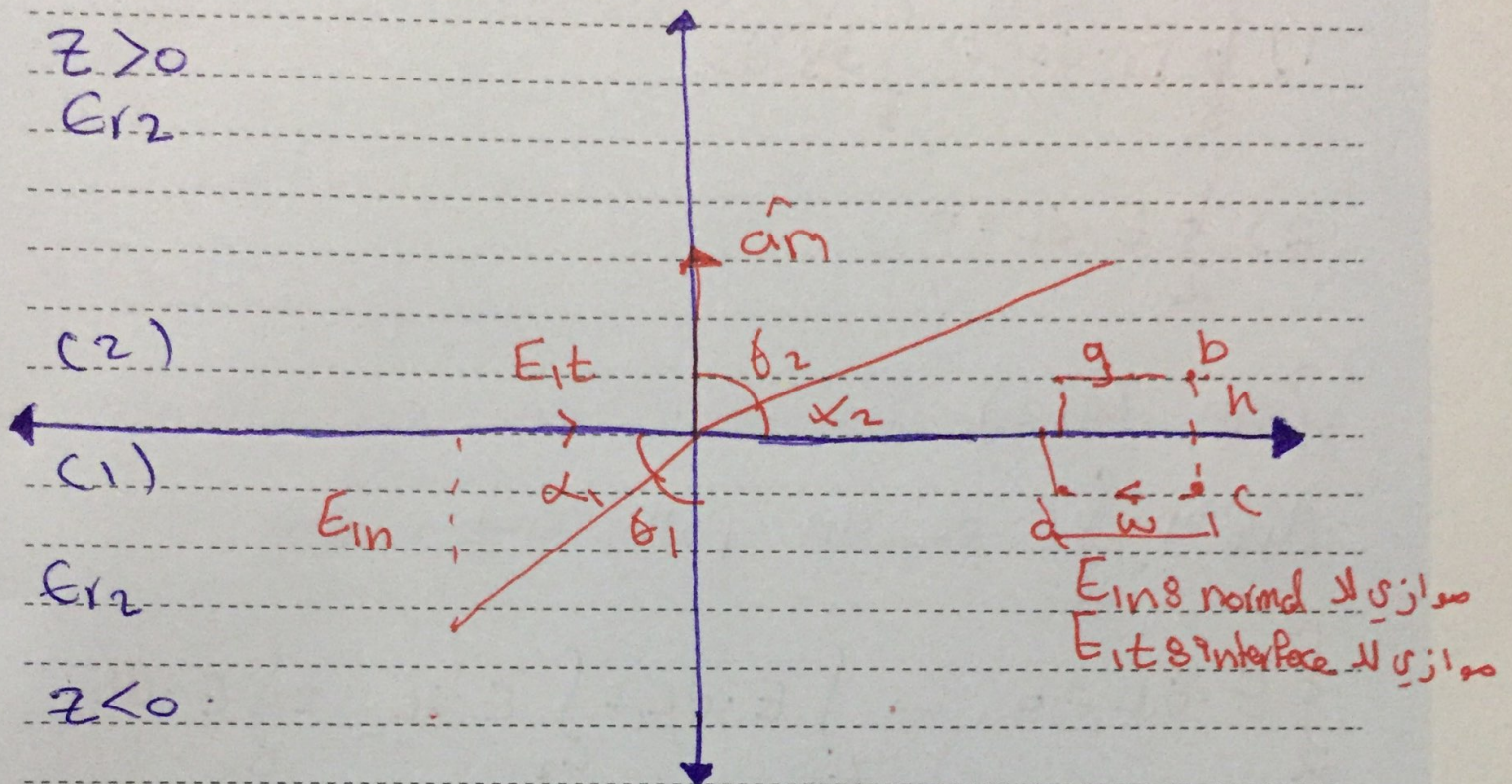
$t < t_0 \rightarrow \rho_v = \rho_{v0} \rightarrow$  initial condition.

$t = t_0^+ \rightarrow \rho_v < \rho_{v0}$

$$\rho_v = \rho_{v0} e^{-t/T_r} \text{ C/m}^3$$

# \* Boundary Conditions.

## A) Dielectric - to - Dielectric Interface



- To find  $\vec{E}_2$ ,  $\vec{D}_2$ ,  $\vec{P}_2$  and angles -  
 Start with  $\vec{E}_1$

$$\vec{E}_1 = \vec{E}_{1n} + \vec{E}_{1t}$$

$$\hat{a}_n = \hat{a}_z$$

$$\vec{E}_{1n} = (\vec{E}_1 \cdot \hat{a}_n) \hat{a}_n$$

$$\vec{E}_{1t} = \vec{E}_1 - \vec{E}_{1n}$$

$$\sin \theta_1 = E_{1t} / E_1$$

$$\cos \theta_1 = E_{1n} / E_1$$

$$\tan \theta_1 = E_{1t} / E_{1n}$$

$$\alpha_1 = 90^\circ - \theta_1$$

- To find  $\bar{E}_2$ ?

Apply 2-

$$1) \oint_S \bar{D} \cdot d\bar{s} = \int_S \rho_s \cdot d\bar{s}$$

$$2) \oint_L \bar{E} \cdot d\bar{L} = 0$$

From Eq(2)

Apply  $\oint_L \bar{E} \cdot d\bar{L}$  on path a-b-c-d-a.

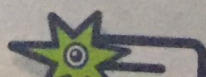
$$\oint_L \bar{E} \cdot d\bar{L} = 0 \rightarrow \int_{L_1} \bar{E} \cdot d\bar{L}_1 + \int_{L_2} \bar{E} \cdot d\bar{L}_2 + \int_{L_3} \bar{E} \cdot d\bar{L}_3$$

$$+ \int_{L_4} \bar{E} \cdot d\bar{L}_4 = 0$$

$$E_2 t w - E_2 t w \frac{h}{2} + E_1 t w \frac{h}{2} - E_1 t w + E_1 t w \frac{h}{2} + E_1 t w \frac{h}{2} = 0$$

$$E_2 t w - E_1 t w = 0$$

$$\boxed{E_2 t = E_1 t} \text{ Always}$$



To find  $\overline{E}_2$

- Apply  $\int_S \overline{D} \cdot \overline{ds} = \int_S \rho_s ds$  at  $z=0$ .

$$\overline{D}_{2n} \cdot \overline{ds} + - \overline{D}_{1n} \cdot \overline{ds} = \rho_s \nabla s$$

$$\overline{D}_{2n} - \overline{D}_{1n} = \rho_s$$

$$\overline{D}_{1n} = \epsilon_0 \epsilon_{r1} \overline{E}_{1n}$$

$$\overline{D}_{2n} = \epsilon_0 \epsilon_{r2} \overline{E}_{2n}$$

$$\overline{E}_{2n} = \frac{\overline{D}_{2n}}{\epsilon_0 \epsilon_{r2}} \hat{a}_n$$

$$\overline{E}_2 = \overline{E}_{2t} + \overline{E}_{2n}$$

$$\overline{D}_2 = \epsilon_0 \epsilon_{r2} \overline{E}_2$$

$$\overline{P} = (\epsilon_{r2} - 1) \epsilon_0 \overline{E}_2$$

- if  $\rho_s = 0$

$$\overline{D}_{2n} = \overline{D}_{1n}$$

$$\epsilon_0 \epsilon_{r1} \overline{E}_{1n} = \epsilon_0 \epsilon_{r2} \overline{E}_{2n}$$

$$\overline{E}_{2n} = \frac{\epsilon_{r1}}{\epsilon_{r2}} \overline{E}_{1n}$$

$$\theta_2 = \sin^{-1} \left( \frac{E_{2t}}{E_2} \right)$$

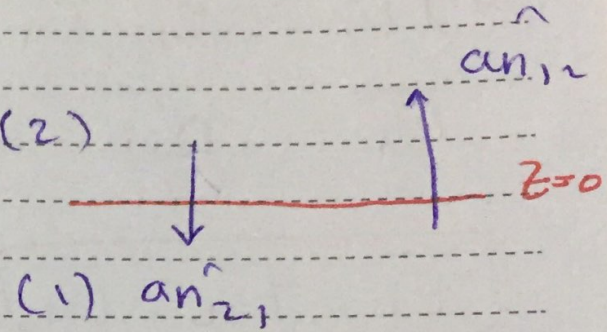
$$= \cos^{-1} \left( \frac{E_{2n}}{E_2} \right)$$

$$= \tan^{-1} \left( \frac{E_{2t}}{E_{2n}} \right)$$

$$\alpha_2 = 90^\circ - \theta_2$$

$$\rho_{ps2} = \vec{P}_2 \cdot \hat{a}_{n_{21}} \quad (2)$$

$$\rho_{ps1} = \vec{P}_1 \cdot \hat{a}_{n_{12}}$$



### \* Dielectric - to - conductor

normal

$\epsilon_0$

$\sigma = \infty$

(2)

$\epsilon_{r1}$

$\hat{z}$

$\vec{E}_2 = 0$   
 $E_{2n} = 0$   
 $E_{2t} = 0$

$D_2 = 0 \rightarrow D_{2n} = 0, D_{2t} = 0$

$\rho_s \neq 0$   $z=0$  interface.

Air  $\rightarrow \epsilon = \epsilon_0, \sigma = 0$

Cond.  $\rightarrow \epsilon = \epsilon_0, \sigma = \infty$

$$\vec{E}_1 ?$$

$$\vec{E}_{1t} = \vec{E}_{2t} = 0$$

$$\vec{E}_{1n} ?$$

$$\vec{D}_{2n} - \vec{D}_{1n} = \rho_s$$

$$\vec{D}_{1n} = -\rho_s \hat{a}_n$$

$$\vec{E}_{1n} = \frac{\vec{D}_{1n}}{\epsilon_0 \epsilon_1}$$

$$\vec{E}_{1n} = \frac{+\rho_s}{\epsilon_0 \epsilon_1} (-\hat{a}_z) \quad \leftarrow \epsilon \approx \infty$$

- Ex Two homogeneous isotropic Dielectrics meet on plane  $z=0$  for  $z > 0$ ,  $\epsilon_{r1} = 4$  and for  $z < 0$ ,  $\epsilon_{r2} = 3$ . A uniform  $\vec{E}_1 = 5\hat{a}_x - 2\hat{a}_y + 3\hat{a}_z$  kV/m exists for  $z > 0$ . Find -

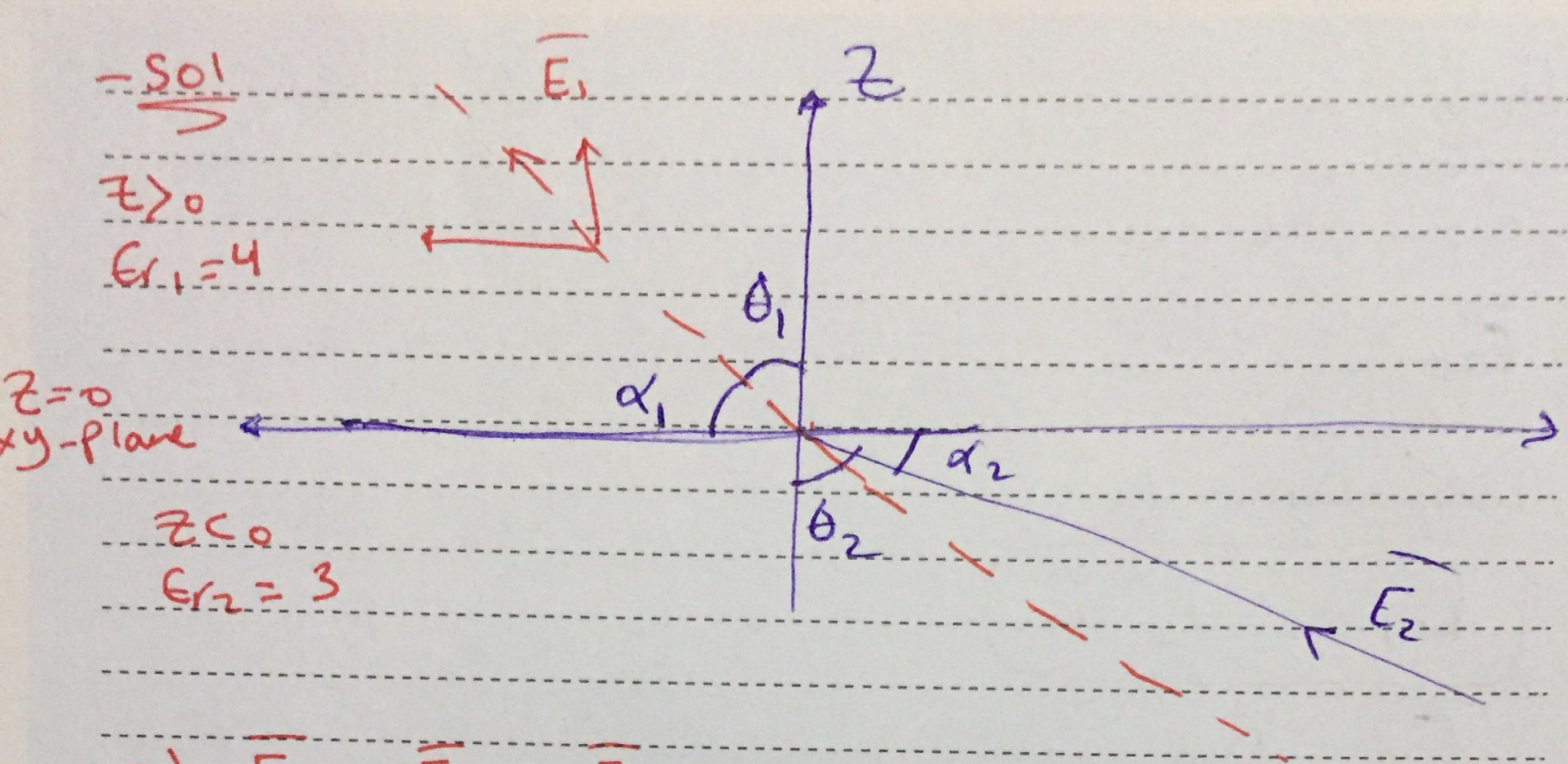
a)  $E_2$  for  $z < 0$ .

b)  $\theta_1, \theta_2, \alpha_1, \alpha_2$

c) Energy density in both regions.

d) Energy in a cube of side (2m) centered at  $(3, 4, -5)$ .





$$a) \vec{E}_1 = \vec{E}_{in} + \vec{E}_{it}$$

$$\hat{a}_n = \hat{a}_z$$

$\vec{E}$  above  $z=0$  plane is  
 $\hat{a}_n = +\hat{a}_z$  or  $+3\hat{a}_z$

$$\vec{E}_{in} = (\vec{E}_1 \cdot \hat{a}_n) \hat{a}_n$$

$$= 3\hat{a}_z \text{ kV/m}$$

$$\vec{E}_{it} = \vec{E}_1 - \vec{E}_{in}$$

$$= 5\hat{a}_x - 2\hat{a}_y \text{ kV/m}$$

$$= \boxed{\vec{E}_{2t}}$$

$$b) \theta_1 = \sin^{-1} \frac{E_{it}}{E_1} = \sin^{-1} \left( \frac{\sqrt{29}}{\sqrt{38}} \right) = \boxed{60.9^\circ}$$

$$\alpha_1 = 90^\circ - \theta_1 = \boxed{29.1^\circ}$$

$$\vec{E}_{2n} \rightarrow \text{Div} - D_{2n} = 0$$

8 جلد Field منتقل  
من ج 1

$$\vec{D}_{1n} = \vec{D}_{2n}$$

$$\epsilon_{r1} \vec{E}_{1n} = \epsilon_{r2} \vec{E}_{2n}$$

$$\vec{E}_{2n} = \frac{\epsilon_{r1}}{\epsilon_{r2}} \vec{E}_{1n}$$

$$= \frac{4}{3} (3 \text{ kV/m}) \hat{a}_z$$

$$\vec{E}_{2n} = \cancel{4} \hat{a}_z \text{ kV/m}$$

$$\vec{E}_2 = \vec{E}_{2n} + \vec{E}_{2t}$$

$$\vec{E}_2 = 5\hat{a}_x - 2\hat{a}_y + 4\hat{a}_z \text{ kV/m}$$

$$\theta_2 = \sin^{-1} \left( \frac{E_{2t}}{E_2} \right)$$

$$= \cos^{-1} \left( \frac{E_{2n}}{E_2} \right)$$

$$= \tan^{-1} \left( \frac{E_{2t}}{E_{2n}} \right)$$

$$= \tan \theta_2 = \frac{\epsilon_{r2} \tan(\theta_1)}{\epsilon_{r1}}$$

استنتاج هار لقانون مور  
الوجه الثاني

$$= \frac{3}{4} \tan(60.9^\circ)$$

$$\theta_2 = 53.4^\circ$$

$$\alpha_2 = 36.6^\circ$$

To find  $\theta_2$ ?

$$\vec{E}_{1t} = \vec{E}_{2t} \quad \dots \textcircled{1}$$

$$D_{2n} - D_{1n} = \rho_s = 0 \quad \dots \textcircled{2} \quad \text{if } \rho_s = 0$$

$$\rightarrow E_1 \sin \theta_1 = E_2 \sin \theta_2 \quad \dots \textcircled{a}$$

$$\rightarrow D_{2n} = D_{1n}$$

~~Div. of E~~

$$\epsilon_0 \epsilon_2 E_2 \tan \theta_2 = \epsilon_0 \epsilon_1 E_1 \tan \theta_1$$

$$E_2 \epsilon_2 \cos \theta_2 = E_1 \epsilon_1 \cos \theta_1 \quad \dots \textcircled{b}$$

divide  $\frac{\textcircled{a}}{\textcircled{b}}$

$$\frac{E_1 \sin \theta_1}{E_1 \epsilon_1 \cos \theta_1} = \frac{E_2 \sin \theta_2}{E_2 \epsilon_2 \cos \theta_2}$$

$$\frac{\tan \theta_1}{\epsilon_1} = \frac{\tan \theta_2}{\epsilon_2}$$

$$\frac{\tan(\theta_1)}{\epsilon_1} = \frac{\tan(\theta_2)}{\epsilon_2}$$

$$\frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_1}{\epsilon_2}$$

~~Div. of E~~  $\rho_s = 0$   $\therefore \theta_2$

$$c) W_{E_1} = \frac{1}{2} \epsilon_1 E_1^2, \quad \epsilon_1 = \epsilon_0 \epsilon_{r1}$$

$$= \frac{1}{2} * \frac{10^{-9}}{36\pi} * 4 * 38 * 10^6$$

$$= 672 \mu\text{J}/\text{m}^3$$

dielectric energy density

$$W_{E_2} = \frac{1}{2} \epsilon_2 E_2^2$$

$$= \frac{1}{2} * \frac{10^{-9}}{36\pi} * 3 * 45 * 10^6$$

$$= 597 \mu\text{J}/\text{m}^3$$

$$d) W_E = \frac{1}{2} \int_V \epsilon E^2 dV \rightarrow W_E = \int_V W_E dV$$

$$W_E = \int_V W_{E_2} dV$$

zählt die Energie in jedem Volumen

$$= 597 \mu\text{J}/\text{m}^3$$

$$= \int_{z=-4}^{-4} \int_{y=5}^5 \int_{x=2}^4 597 * 10^{-6} dx dy dz = \boxed{4.776 \text{ mJ}}$$

- if the cube is centered at  $(\frac{3}{2}, \frac{4}{2}, 0)$ .

$$W_E = \int_0^1 \int_0^1 \int_0^1 W_{E_1} dx dy dz + \int_{-1}^0 \int_{-1}^0 \int_{-1}^0 W_{E_2} dx dy dz$$

$$= W_{E_1} * 4$$

+

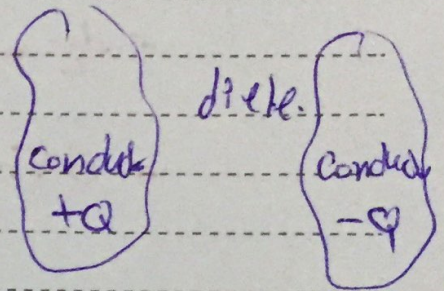
$$W_{E_2} * 4$$

# CH6 Boundary Value Problems

## Section 6.5 Resistance & Capacitance

$$R = \frac{V}{I} = \frac{-\int \vec{E} \cdot d\vec{L}}{\int_S \sigma \vec{E} \cdot d\vec{s}}$$

$$C = \frac{Q}{V} = \frac{\int_S \epsilon \vec{E} \cdot d\vec{s}}{-\int \vec{E} \cdot d\vec{L}}$$



\* Procedure to find (C) and (R)

- 1) Choose a suitable coordinate
- 2) Assume  $\begin{pmatrix} + \\ - \end{pmatrix} Q$  on each plate.
- 3) Find  $\vec{E}$  from  $\oint_S \vec{E} \cdot d\vec{s} = Q$  (Gauss Law)
- 4) Find  $V = -\int_L \vec{E} \cdot d\vec{L}$

$$C = \frac{Q}{V} \quad \begin{matrix} \text{(step 2)} \\ \text{(step 4)} \end{matrix}$$

$$5) I = \int_S \sigma \vec{E} \cdot d\vec{s}$$

$$R = \frac{V}{I} \rightarrow \text{(step 4)}$$

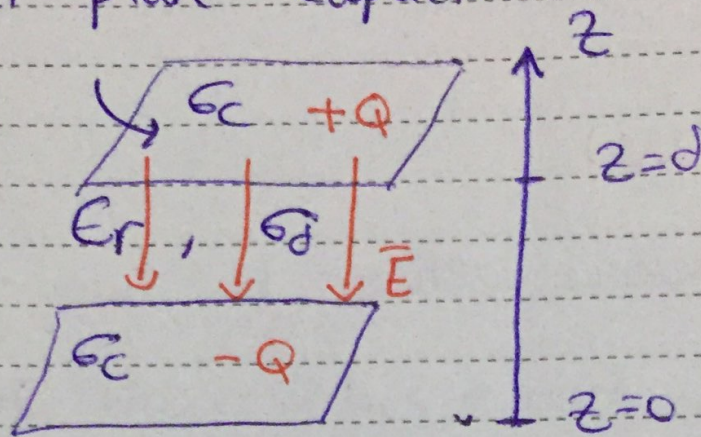
$$I \rightarrow \text{(step 5)}$$

Dielectric resistance  
Leakage resistance.



## \* Types of capacitors -

### 1) Parallel plate capacitor



Find C? R<sub>d</sub>?

Sol

Cartesian coordinate

بیشوف سوا ال coordinate الختصاص  
ويفرض  $Q+$  و  $Q-$  ويكون  
اتجاه  $\vec{E}$  من الموجب للسالب

$$\vec{E} = \vec{E}_+ + \vec{E}_-$$

$$= \frac{\rho_s}{2\epsilon_0} (-\hat{a}_z) + \frac{-\rho_s}{2\epsilon_0} (\hat{a}_z)$$

$$= \frac{-\rho_s}{\epsilon} \hat{a}_z$$

$$Q = \int_S \rho_s ds$$

$$\rho_s = \frac{Q}{S}$$

$$\vec{E} = \frac{Q}{S\epsilon} (-\hat{a}_z) \text{ V/m}$$

$$V = - \int \vec{E} \cdot d\vec{L}, \quad d\vec{L} = dz \hat{a}_z$$

Higher potential (+ve)

$$V = + \int \frac{Q}{SE} (+dz) \cdot dz$$

Lower potential (-ve)

ولمياً حدود الكمال  
من الأعلى للأعلى

$$V = \frac{Qd}{SE}$$

potential difference between the two plates

\* لو فرضت Q+ لحي و Q- لحي  
عنه ما فيه عيه سالب  
فوقه ايسر حدود الكمال

$$C = \frac{Q}{V} = \frac{Q}{\frac{Qd}{SE}} = \boxed{\frac{ES}{d}} \quad (F)$$

if  $\epsilon_r$  is homogenous  
(يعني  $\epsilon_r$  تكون رقم)

-if  $\epsilon_r$  is non homogenous (function)  
Then apply the procedure.  
(هذا مشق القانون)

$$I = \int_S \sigma E \cdot ds$$

$$I = \iint \sigma \frac{Q}{SE} dz \cdot dx dy dz$$

$$\iint dx dy = S$$

$$I = \frac{\sigma d Q}{SE} \rightarrow \boxed{I = \frac{\sigma Q}{\epsilon}} \quad (A)$$



$$R = \frac{V}{I} = \frac{Qd}{\cancel{S\sigma}} \cdot \frac{\cancel{\sigma}}{\epsilon} \rightarrow \boxed{R = \frac{d}{\sigma S}} = \frac{\rho L}{A}$$

$d = L$   
 $S = A$   
 $\frac{1}{\sigma} = \rho$

$\sigma$  is homogeneous.

$$* T_r = \frac{\epsilon}{\sigma_0} = R_0 C$$

$$R_0 * C = \frac{d}{\sigma_0 S} * \frac{\epsilon S}{d} = \frac{\epsilon}{\sigma_0}$$

\* Energy in capacitor.

$$W_E = \frac{1}{2} \int_V \epsilon E^2 dV = \frac{1}{2} CV^2 \quad \text{--- (1)}$$

$$W_E = \frac{1}{2} \epsilon \frac{Q^2}{S^2 \epsilon^2} S d$$

$$= \frac{Q^2 d}{2 \epsilon S} \frac{1}{C}$$

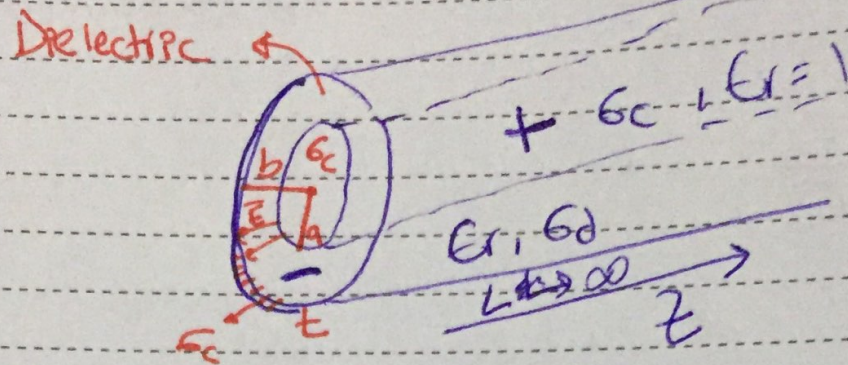
$$= \frac{Q^2}{2C} \quad , \quad C = \frac{Q}{V} \rightarrow Q = CV$$

$$= \frac{C^2 V^2}{2C} = \frac{1}{2} CV^2 \quad \#$$

if uniform.



## 2) Cylindrical capacitor (coaxial capacitor) (coaxial cable)



Cylindrical coordinates.

$$\vec{E} = E_{\rho} \hat{a}_{\rho}$$

$$d\vec{s} = \rho d\phi dz \hat{a}_{\rho}$$

$$\int_S \epsilon \vec{E} \cdot d\vec{s} = Q$$

$L \rightarrow \infty$

$$\iiint_{z=0, \phi=0} \epsilon E_{\rho} \hat{a}_{\rho} \cdot \rho d\phi dz \hat{a}_{\rho}$$

$z=0, \phi=0$

$$= \epsilon E_{\rho} \underbrace{2\pi \rho L}_{\text{Area}} = Q$$

$$E = \frac{Q}{2\pi \epsilon \rho L} \hat{a}_{\rho} \quad \text{V/m}$$

$$V = - \int_L \vec{E} \cdot d\vec{L}$$

$$= - \int_b^a \frac{Q}{2\pi\epsilon L r} \cancel{dr} \cdot \cancel{dr} \cdot \cancel{dr}$$

$$V = \frac{Q}{2\pi\epsilon L} \ln\left(\frac{b}{a}\right) \quad (V)$$

$$C = \frac{Q}{V} = \frac{Q}{\frac{Q \ln(b/a)}{2\pi\epsilon L}} = \frac{2\pi\epsilon L}{\ln(b/a)} \quad (F)$$

$$\frac{C}{L} = \frac{2\pi\epsilon}{\ln(b/a)} \quad F/m \quad \text{if } \epsilon_r \text{ is homo.}$$

$$R_d = \frac{V}{I}$$

$$I = \int_S \nabla \cdot \vec{E} \cdot d\vec{s} = \int_0^L \int_0^{2\pi} \frac{\epsilon_0 Q}{2\pi\epsilon L r} \cancel{dr} \cdot \cancel{r} \cdot \cancel{d\phi} \cdot \cancel{dz}$$

$$I = \frac{\epsilon_0 Q}{\epsilon} \quad (A)$$

$$R_d = \frac{\frac{Q}{2\pi\epsilon L} \ln(b/a)}{\frac{\epsilon_0 Q}{\epsilon}} = \frac{\ln(b/a)}{2\pi\epsilon_0 L} \quad \Omega$$

$$R_d C = \tau = \frac{\epsilon}{\sigma}$$



$$* G = \frac{1}{R_d} = \frac{2\pi\epsilon_0 d}{\ln(b/a)} \text{ (S)}$$

$$G/d = \frac{2\pi\epsilon_0}{\ln(b/a)} \text{ (S/m)} \text{ (Like } \epsilon_0 \text{)}$$

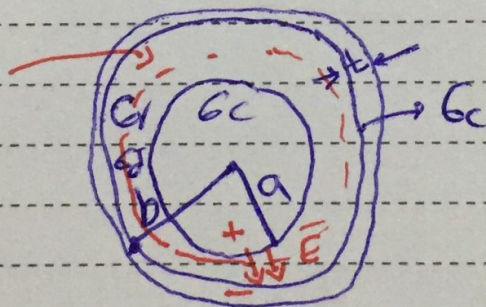
$$R_d \cdot d = \frac{\ln(b/a)}{2\pi\epsilon_0} \text{ (}\Omega \cdot \text{m)} \text{ (Like } \rho \text{)}$$

$$W_E = \frac{1}{2} \int_V \epsilon E^2 dV = \frac{1}{2} CV^2$$

$$C = \frac{2\pi\epsilon_0 d}{\ln(b/a)}$$

### 3) Spherical Capacitor

Gaussian Surface



- Spherical coordinates

$$\oint_S \vec{E} \cdot d\vec{s} = Q$$

$$\vec{E} = E_r \hat{a}_r$$

$$d\vec{s} = r^2 \sin\theta d\theta d\phi \hat{a}_r$$

$$\rightarrow 4\pi r^2 \epsilon E_r = Q$$

$$\vec{E} = \frac{Q}{4\pi \epsilon r^2} \hat{a}_r$$

قانون كولوم في قانون نقطة شحنة  
كل الشحنات تتجمع في نقطة شحنة  
point charge

$$V = - \int_a^b \vec{E} \cdot d\vec{L}$$

$$V = - \frac{Q}{4\pi \epsilon} \left[ \frac{1}{r} \right]_a^b$$

$$V = \frac{Q}{4\pi \epsilon} \left( \frac{1}{a} - \frac{1}{b} \right) \quad (V)$$

$$C = \frac{Q}{V} = \frac{4\pi \epsilon}{\left( \frac{1}{a} - \frac{1}{b} \right)} \quad (F)$$

$$R_d = \frac{V}{I}$$

$$I = \int_S \epsilon_d \vec{E} \cdot d\vec{s} = \int_0^{2\pi} \int_0^{\pi} \frac{\epsilon_d Q}{4\pi \epsilon r^2} \hat{a}_r \cdot r^2 \sin\theta d\theta d\phi \hat{a}_r$$

$$I = \frac{\epsilon_d Q}{\epsilon} \quad A$$

$$R_d = \frac{V}{I} = \frac{\frac{1}{a} - \frac{1}{b}}{4\pi \epsilon_d} \quad \Omega$$

$$G = \frac{1}{R_d} = \frac{4\pi \epsilon_d}{\frac{1}{a} - \frac{1}{b}}$$

$$R_d C = \frac{\epsilon}{\epsilon_0} = T_r$$

$$W_E = \frac{1}{2} C V^2 \quad (J)$$

$$\frac{4\pi\epsilon}{\frac{1}{a} - \frac{1}{b}}$$

#### 4) Isolated Capacitor (Isolated sphere)

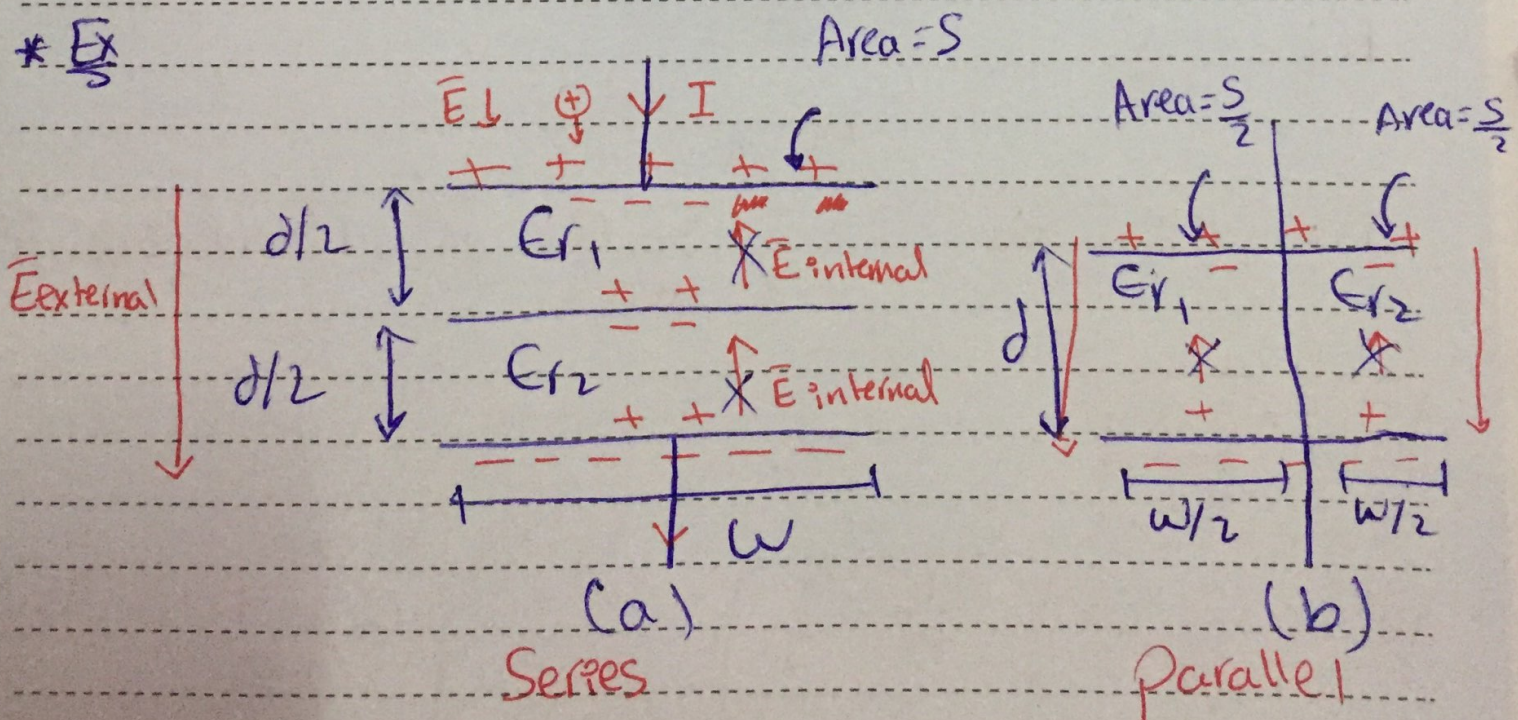
$$b \rightarrow \infty$$

$$C = 4\pi\epsilon a \quad (F)$$

$$G = 4\pi\epsilon_0 a \quad (S)$$

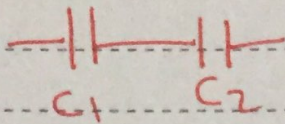
$$R_d = \frac{1}{4\pi\epsilon_0 a} \quad (\Omega)$$

\*  $\frac{E_x}{S}$

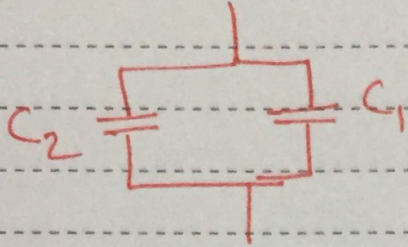


Sol

- Recall

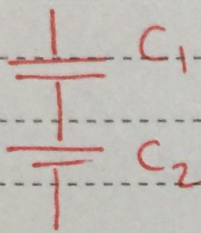


$$C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$$



$$C_{eq} = C_1 + C_2$$

a)

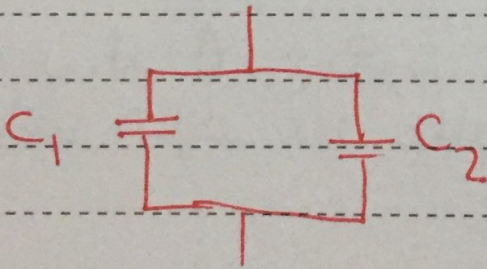


$$C_1 = \frac{\epsilon_0 \epsilon_{r1} S}{d/2}$$

$$C_2 = \frac{\epsilon_0 \epsilon_{r2} S}{d/2}$$

$$C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$$

b)

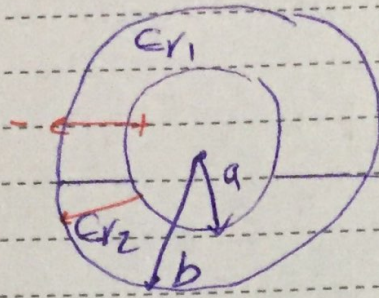


$$C_1 = \frac{\epsilon_0 \epsilon_{r1} S/2}{d}$$

$$C_2 = \frac{\epsilon_0 \epsilon_{r2} S/2}{d}$$

$$C_{eq} = C_1 + C_2$$

$-\frac{E_x}{\sqrt{E_x}}$



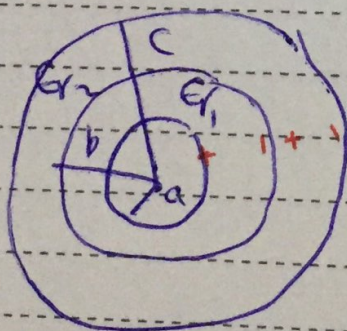
Sol Parallel  
 $C_{eq} = C_1 + C_2$

$C_1 = \frac{4\pi \epsilon_0 \epsilon_{r1}}{\frac{1}{a} - \frac{1}{b}} \cdot \left(\frac{1}{2}\right)$  عنه نصف كره

$C_2 = \frac{4\pi \epsilon_0 \epsilon_{r2}}{\frac{1}{a} - \frac{1}{b}} \cdot \frac{1}{2}$

التي كامل لـ  $\pi$  ربع يكون من  $0 \rightarrow \pi$  ومن  $\frac{\pi}{2} \rightarrow \pi$   
 مساهم ههنا ربع  $\frac{1}{2}$  سطح عندي ضرب  $\frac{1}{2}$

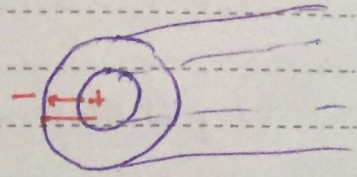
$-\frac{E_x}{\sqrt{E_x}}$



$C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$

$C_1 = \frac{4\pi \epsilon_0 \epsilon_{r1} (F)}{\frac{1}{a} - \frac{1}{b}}$  ,  $C_2 = \frac{4\pi \epsilon_0 \epsilon_{r2} (F)}{\frac{1}{b} - \frac{1}{c}}$

Ex A Coaxial cable has  $\epsilon_r = 10$  where  $\rho$  is in cm  
 if  $a = 1$  cm  
 $b = 2.5$  cm  
 find  $C/d$  ??



Sol  $\int_S \vec{E} \cdot d\vec{s} = Q$

$$\int_0^L \int_0^{2\pi} \int_0^{\infty} \epsilon E_{\rho} \cdot \rho d\phi dz = Q$$

$$\vec{E} = \frac{Q}{2\pi\epsilon\rho L} \hat{\rho}$$

$$V = - \int_{\infty}^{\rho} \vec{E} \cdot d\vec{L}$$

$$= - \frac{Q}{2\pi\epsilon_0 d} \int \frac{1}{\frac{10+\rho}{\rho}} \cdot d\rho$$

$$= - \frac{Q}{2\pi\epsilon_0 d} \left[ \ln(10+\rho) \right]_b^a$$

$$= \frac{Q}{2\pi\epsilon_0 d} \ln\left(\frac{10+b}{10+a}\right) \text{ (V)}$$

$$C = \frac{Q}{V} = \frac{2\pi\epsilon_0 d}{\ln\left(\frac{10+b}{10+a}\right)}$$

$$C/d = \frac{2\pi\epsilon_0}{\ln\left(\frac{12.5}{11}\right)} = 434.6 \text{ PF/m}$$



# CH 7 Magnetostatic Fields

- Sources -

1) permanent Magnet

2) charge moving with uniform velocity (zero acceleration)

3) DC Current flowing in the wire

\* Major laws -

1) Biot-Savart's Law (General)

2) Ampere's Law (Special case)

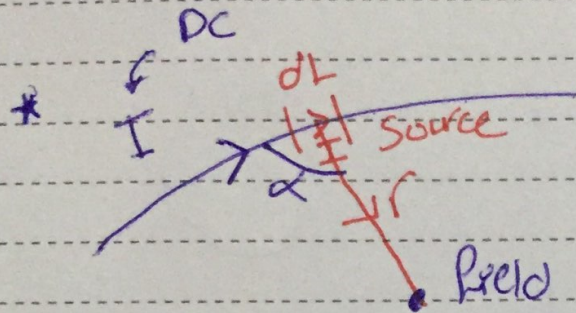
\* Duality between Electrostatic and Magnetostatic

	Elec.	Magn.
	$\vec{E}$ (V/m)	$\vec{H}$ (A/m)
Electric Flux density	$\vec{D}$ (C/m <sup>2</sup> )	$\vec{B}$ (Wb/m <sup>2</sup> ) magnetic flux density
	$\psi_e = \int_S \vec{D} \cdot d\vec{s}$	$\psi_m = \int_S \vec{B} \cdot d\vec{s}$
	$\vec{E}$	$\vec{H}$
	$V = - \int \vec{E} \cdot d\vec{L}$	$I = \int_C \vec{H} \cdot d\vec{L}$
	$W_E = \frac{1}{2} \int_V \vec{E} \cdot \vec{D} dV$	$W_m = \frac{1}{2} \int_V \vec{H} \cdot \vec{B} dV$

# \* Biot-Savart's Law

- Orsted exp.

$I \nearrow$  Magnetic Field  
around the  
wire



$$\frac{30^\circ}{\sin(30^\circ)} = \frac{150^\circ}{\sin(150^\circ)}$$

$H$  : Magnetic Field intensity

- by exp -

$$dH \propto \frac{I dL \sin(\alpha)}{r^2}$$

$\alpha$ : is the angle between the conductor ( $dL$ ) and the distance ( $r$ ).

$$dH = \frac{k I dL \sin(\alpha)}{r^2}$$

$k$  = proportionality constant =  $\frac{1}{4\pi}$

لذا يتم تبسيط الوسط الى حوله

$$H = \int \frac{I \sin \alpha}{4\pi r^2} dL$$

Magnitude only.



\* Direction of  $\vec{H}$  :-

$$\vec{H} = \int_L \frac{I \, d\vec{L} \times \hat{a}_r}{4\pi r^2}$$

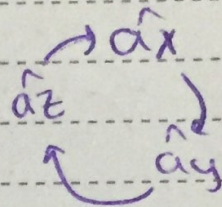
(A/m)

$$|d\vec{L} \times \hat{a}_r| = dL \sin\alpha$$

$$d\vec{L} \times \hat{a}_r \perp d\vec{L}$$

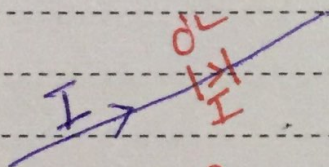
$$d\vec{L} \times \hat{a}_r \perp \hat{a}_r$$

For Line current



\* Types of current distributions:-

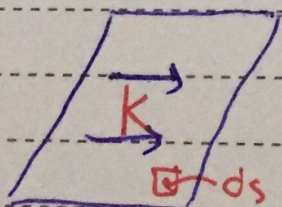
1) Line Current  $\rightarrow$  1D segment



$I dL =$  Line current (A.m)

$$\vec{H} = \int_L \frac{I \, d\vec{L} \times \hat{a}_r}{4\pi r^2} = \int_L \frac{I \, d\vec{L} \times \vec{r}}{4\pi r^3}$$

2) Surface Current  $\rightarrow$  2D Surface.

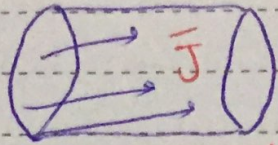


$K ds =$  Surface current (A.m)

$K$  Surface current density (A/m)

$$\vec{H} = \int_S \frac{K \, ds \times \vec{r}}{4\pi r^3} = \int_S \frac{K \times \vec{r}}{4\pi r^3} \, ds$$

3) Volume Current distribution  $\rightarrow$  3D object



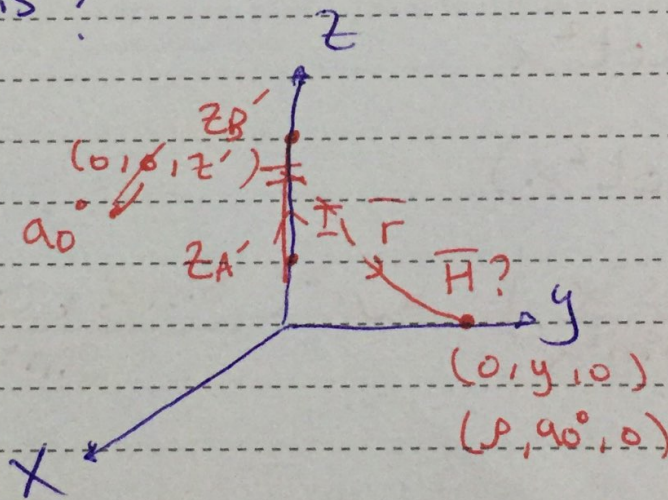
$\vec{J}$  : Volume current density. ( $A/m^2$ )

$\vec{J} dv$  = Volume current distribution. ( $A \cdot m$ )

$$\vec{H} = \int_V \frac{\vec{J} \times \vec{r}}{4\pi r^3} dv$$

\*Ex Find  $\vec{H}$  due to a finite <sup>straight</sup> wire along z-axis?

Sol



$$\vec{r} = (\rho, 90^\circ, 0) - (0, 90^\circ, z') = \rho \hat{a}_\rho - z' \hat{a}_z$$

$$r^2 = \sqrt{\rho^2 + z'^2}$$

$$dL = dz' \hat{a}_z$$

$$\vec{H} = \int_L \frac{I dL \times \vec{r}}{4\pi r^3} = \frac{I}{4\pi} \int_{z_{A'}}^{z_{B'}} \frac{\hat{a}_z (\rho \hat{a}_\rho - z' \hat{a}_z)}{(\rho^2 + z'^2)^{3/2}} dz'$$

$$\bar{H} = \frac{I\rho}{4\pi} \int_{z_A'}^{z_B'} \frac{\hat{a}_\phi}{[\rho^2 + z'^2]^{3/2}} dz'$$

$$\sin\alpha = \frac{\rho}{r}$$

$$\cos\alpha = \frac{z'}{r}$$

$$\tan\alpha = \frac{\rho}{z'} \rightarrow z' = \frac{\rho}{\tan\alpha} = \rho \cot\alpha$$

$$dz' = \rho \csc^2\alpha d\alpha$$

$$r^2 = \rho^2 + z'^2$$

$$= \rho^2 + \rho^2 \cot^2\alpha$$

$$= \rho^2 (1 + \cot^2\alpha)$$

$$= \rho^2 \left(1 + \frac{\cos^2\alpha}{\sin^2\alpha}\right) = \rho^2 \left(\frac{\sin^2\alpha + \cos^2\alpha}{\sin^2\alpha}\right)$$

$$r^2 = \rho^2 \csc^2\alpha$$

$$r^3 = \rho^3 \csc^3\alpha$$

sub. in integral

$$\bar{H} = \frac{I\rho}{4\pi} \int_{\alpha_1}^{\alpha_2} \frac{\rho \csc^2\alpha}{\rho^3 \csc^3\alpha} d\alpha \hat{a}_\phi$$

$$\bar{H} = \frac{I}{4\pi\rho} \int_{\alpha_1}^{\alpha_2} -\sin\alpha d\alpha \hat{a}_\phi$$

الزاوية الخارجية الزاوية الداخلية

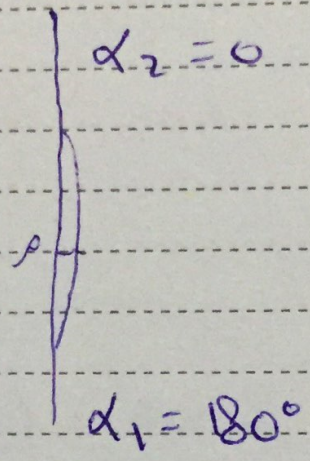
$$\vec{H} = \frac{I}{4\pi\rho} (\cos\alpha_2 - \cos\alpha_1) \hat{a}_\phi$$

A/m

$$\hat{a}_\phi = \hat{a}_l \times \hat{a}_\rho$$

For finite straight wire

- For infinite line

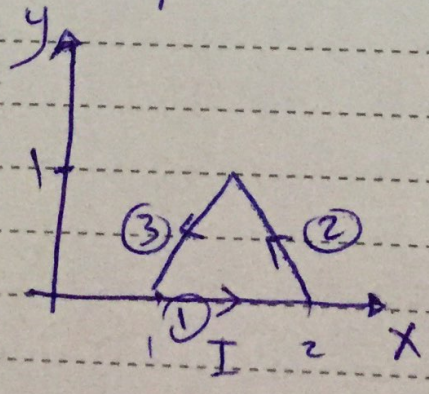


$$\vec{H} = \frac{I}{2\pi\rho} \hat{a}_\phi$$

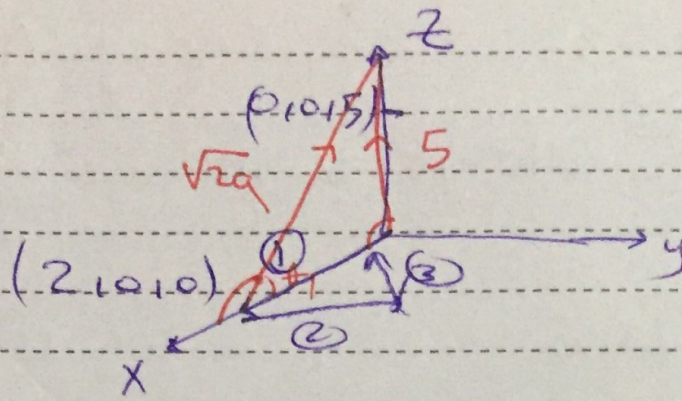
$$\hat{a}_\phi = \hat{a}_z \times \hat{a}_\rho$$

For infinite line

Ex \* The conducting Triangular loop carries a current of 10 A. Find  $\vec{A}$  at (0, 0, 5) due to side (1) of the loop.



Sol



$$\vec{H} = \frac{I}{4\pi r} (\cos \alpha_2 - \cos \alpha_1) \hat{a}_\phi$$

$$\cos \alpha_1 = \frac{-2}{\sqrt{29}}$$

$\alpha_2 = 90^\circ$  الزاوية بين Z-axis و X-axis

$$\cos \theta_1 = \frac{2}{\sqrt{29}}$$

$$\cos \alpha_1 = -\cos \theta_1 \quad (\text{only if } \alpha_1 + \theta_1 = 180^\circ)$$

$$r = 5, \quad \vec{r} = 5 \hat{a}_z$$

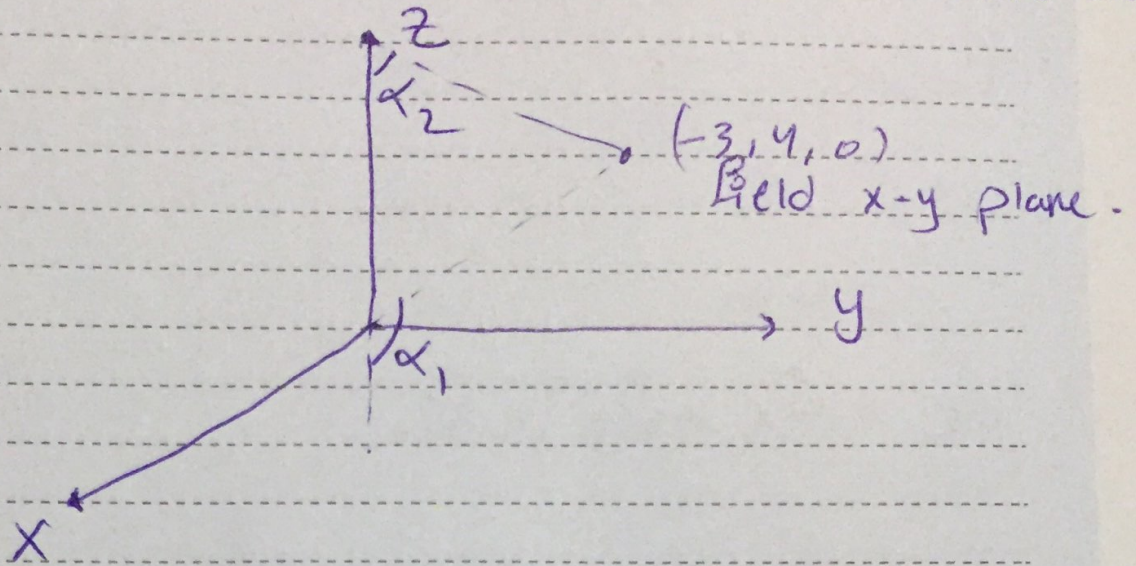
$$\hat{a}_\phi = \hat{a}_r \times \hat{a}_r$$

$$= \hat{a}_x \times \hat{a}_z = -\hat{a}_y$$

$$\vec{H} = \frac{10}{4\pi(5)} (\cos 90 + \frac{2}{\sqrt{29}}) (-\hat{a}_y)$$

$$H = -59.1 \hat{a}_y \text{ mA/m}$$

Ex Find  $\vec{H}$  at  $(-3, 4, 0)$  due to a current filament shown:



Sol  $\vec{H} = \vec{H}_1 + \vec{H}_2$

$\alpha_2 = 0$  Since the line extends to  $\infty$

$\alpha_1 = 90^\circ$

$\vec{\rho} = (-3, 4, 0)$

$\hat{a}_\phi = \hat{a}_l \times \hat{a}_\rho$

$= -\hat{a}_z \times \frac{\vec{\rho}}{\rho}$

$= -\hat{a}_z \times \left( \frac{-3}{5} \hat{a}_x + \frac{4}{5} \hat{a}_y \right)$

$\hat{a}_\phi = \frac{3}{5} \hat{a}_y + \frac{4}{5} \hat{a}_x$

$\vec{H}_1 = \frac{I}{4\pi r} \hat{a}_\phi = 38.2 \hat{a}_x + 28.65 \hat{a}_y \text{ mA/m}$



For line ②

$$\cos \alpha_1 = \frac{-3}{5}$$

$$\alpha_2 = 0$$

$$\rho = 4 \text{ m}$$

$$\hat{a}_\phi = \hat{a}_x \times \hat{a}_y = \hat{a}_z$$

$$\vec{H}_2 = \frac{I}{4\pi\rho} \left(1 + \frac{3}{5}\right) \hat{a}_\phi \neq \frac{I}{4\pi\rho} \hat{a}_\phi$$

$$\vec{H}_2 = 23.88 \hat{a}_z \text{ mA/m}$$

$$\vec{H} = \vec{H}_1 + \vec{H}_2$$

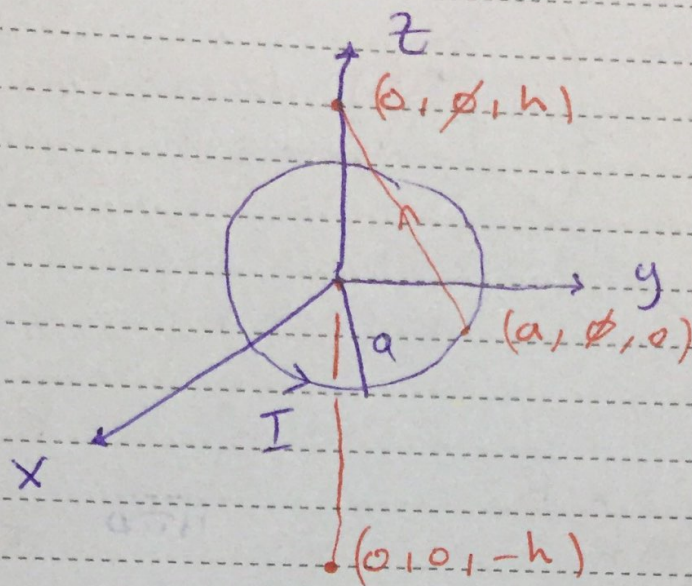
$$= 38.2 \hat{a}_x + 28.65 \hat{a}_y + 23.88 \hat{a}_z \text{ mA/m}$$

(Carto)

in cyl

$$\vec{H} = -47.75 \hat{a}_\phi + 23.88 \hat{a}_z$$

Ex Find  $\vec{H}$  at  $(0,0,h)$  and  $(0,0,-h)$  due to current ~~source~~ shown if  $I = 5A$ .



$$\text{Sol } \vec{H} = \int \frac{I \vec{dl} \times \vec{R}}{4\pi R^3}$$

$$\vec{dl} = \rho d\phi \hat{a}_\phi \Big|_{\rho=a}$$

$$\vec{R} = -a \hat{a}_\rho + h \hat{a}_z$$

$$|\vec{R}| = \sqrt{a^2 + h^2}$$

$$\vec{H} = \frac{Ia}{4\pi} \int_0^{2\pi} \frac{\hat{a}_\phi \times (-a \hat{a}_\rho + h \hat{a}_z)}{[a^2 + h^2]^{3/2}} a d\phi$$

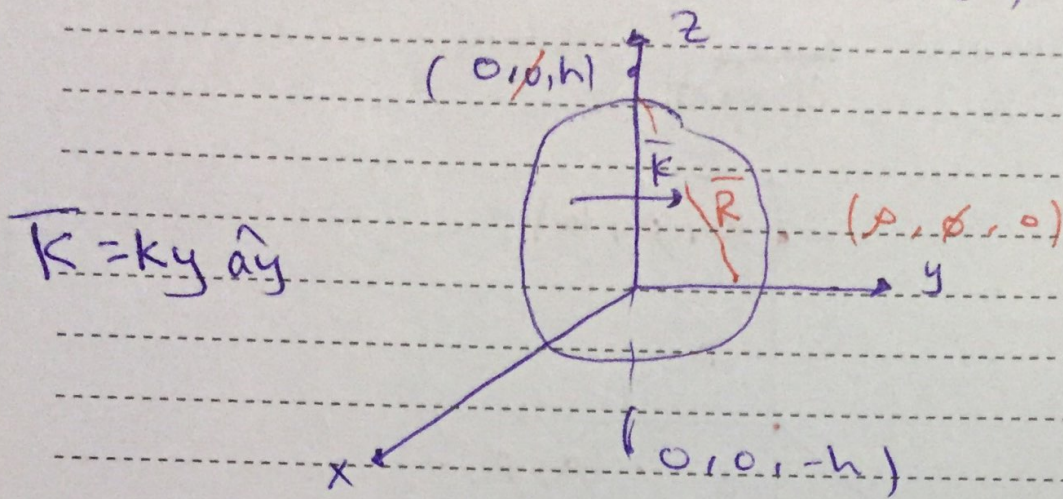
due to symmetry the  $\rho$ -component will be cancelled

$$\vec{H} = \frac{Ia^2}{2[a^2 + h^2]^{3/2}} \hat{a}_z \text{ A/m}$$

at  $(0,0,h)$  same for  $(0,0,-h)$ .



\* Ex if a disk of radius (a)



Sol 
$$\vec{H} = \int_S \frac{\vec{K} \times \vec{R}}{4\pi R^3}$$

$$\vec{R} = -\rho \hat{\rho} + h \hat{z}$$

$$|\vec{R}| = \sqrt{\rho^2 + h^2}$$

$$\vec{H} = \frac{ky}{4\pi} \int_0^{2\pi} \int_0^a \frac{\hat{a}_y \times (-\rho \hat{\rho} + h \hat{z}) \rho d\rho d\phi}{[\rho^2 + h^2]^{3/2}} \quad d\vec{s} = \rho d\rho d\phi$$

we need matrix to convert  
 $\hat{a}_y \rightarrow$  cyli  
 or  $\hat{a}_z \rightarrow$  cart.

\*Ampere's Law (special cases)

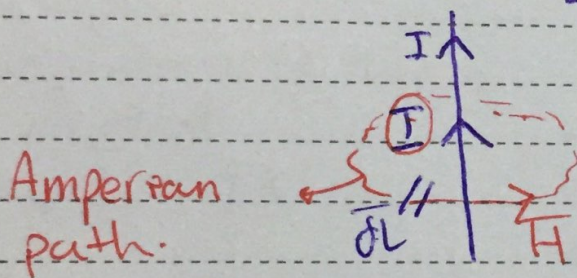
$$\oint \vec{H} \cdot d\vec{L} = I_{enc}$$

↳ 3<sup>rd</sup> Maxwell's eq. in integral form.

\*Applications on Ampere's Law -

① Find  $\vec{H}$  for an infinite line of current

$$\vec{H} = \frac{I}{2\pi r} \hat{\phi}$$



Right hand Rule (R.H.R)

$I \downarrow \Rightarrow \vec{B} \text{ is } \hat{\phi}$   
 $H \text{ direction is } \hat{\phi}$

$$\oint \vec{H} \cdot d\vec{L} = I_{enc} = I$$

↳ From R.H.R  
 $\vec{H} = H_{\phi} \hat{\phi}$

$$d\vec{L} = r d\phi \hat{\phi}$$

$$\int_0^{2\pi} H_{\phi} \hat{\phi} \cdot r d\phi \hat{\phi} = I$$

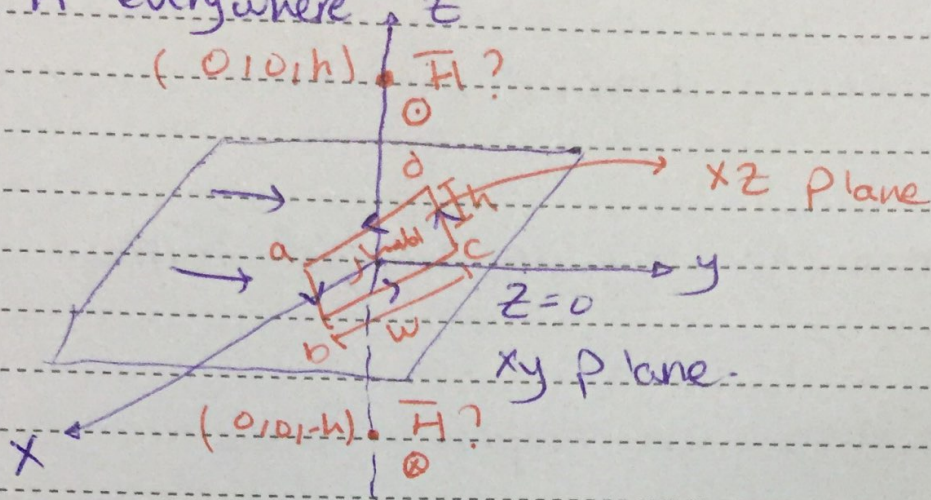
$$2\pi r H_{\phi} = I$$

$$\vec{H} = \frac{I}{2\pi r} \hat{\phi}$$

Same as Biot-Savart.

2) Find  $\vec{H}$  for an infinite sheet of current.

- Ex  $z=0$  carry current  $\vec{K} = K_y \hat{a}_y$   
 Find  $\vec{H}$  everywhere  $z$



Sol  $\oint \vec{H} \cdot d\vec{L} = I_{enc} = K_y w$  کاملاً اختیار کیا گیا ہے  
 صرف ان عرفی کوان  
 اظہار کیوں عاموری کی K

$$\vec{H} = \begin{cases} H_0 \hat{a}_x & , z > 0 \\ H_0 (-\hat{a}_x) & , z < 0 \end{cases}$$

$K = K_y \hat{a}_y$   
 اظہار کیوں کیوں  $xz$

$d\vec{L} = \dots$

Apply Ampere's Law on path a-b-c-d

$$\oint_L \vec{H} \cdot d\vec{L} = \int_a^b \vec{H} \cdot d\vec{L}_1 + \int_b^c \vec{H} \cdot d\vec{L}_2 + \int_c^d \vec{H} \cdot d\vec{L}_3 + \int_d^a \vec{H} \cdot d\vec{L}_4 = K_y w$$

Since  $d\vec{L} = dz \hat{a}_z$  and  $\hat{a}_x \cdot \hat{a}_z = 0$

$$\int_b^c \vec{H} \cdot d\vec{L}_2 = \int_b^c H_0 (-\hat{a}_x) \cdot dx (-\hat{a}_x) = \boxed{H_0 w}$$

$$\int_d^a \vec{H} \cdot d\vec{L} = H_0 w$$

$$H_0 w + H_0 w = K_y w$$

$$\boxed{H_0 = \frac{K_y}{2}}$$

$$\vec{H} = \begin{cases} \frac{K_y}{2} \hat{a}_x, & z > 0 \end{cases}$$

$$\begin{cases} \frac{K_y}{2} (-\hat{a}_x), & z < 0 \end{cases}$$

Always.

For infinite sheet.

$$\vec{H} = \frac{1}{2} \vec{K} \times \hat{a}_n$$

نصف لقا توی صورت آخری

$$\vec{K} = K_x \hat{a}_x$$

$$\vec{H} = \frac{1}{2} \vec{K} \times \hat{a}_n$$

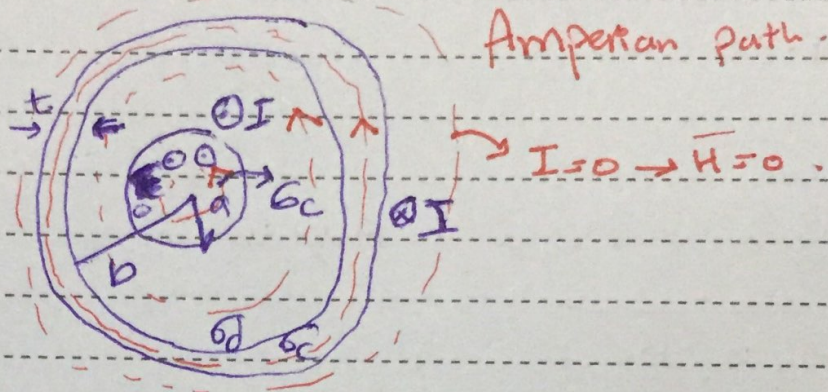
$$\vec{K} = K_x \hat{a}_x + K_y \hat{a}_y$$

$$\vec{H} = \frac{1}{2} \vec{K} \times \hat{a}_n$$

3] Find  $\vec{H}$  For a volume current

- Ex Find  $\vec{H}$  everywhere For a coaxial cable.

(infinitely long)



Sol  $\oint \vec{H} \cdot d\vec{L} = I_{enc}$ .

- For  $0 < \rho < a$

$$\vec{H} = H_\phi \hat{a}_\phi$$

$$d\vec{L} = \rho d\phi \hat{a}_\phi$$

$$\oint \vec{H} \cdot d\vec{L} = \int_0^{2\pi} H_\phi \hat{a}_\phi \cdot \rho d\phi \hat{a}_\phi$$

$$\oint \vec{H} \cdot d\vec{L} = 2\pi \rho H_\phi$$

For  $0 < \rho < a$

$$2\pi\rho H\phi = I_{enc} = \int_S \vec{J} \cdot d\vec{s} \dots \textcircled{1}$$

at  $\rho = a \rightarrow I_{enc} = I$

$$I = \int_S \vec{J} \cdot d\vec{s} = \int_0^{2\pi} \int_0^a J_z \hat{z} \cdot \rho d\rho d\phi \hat{z}$$

$$I = J_z \frac{a^2}{2} (2\pi)$$

$$\vec{J} = \frac{I}{\pi a^2} \hat{z} \quad \text{A/m}^2 \rightarrow \text{Sub in } \textcircled{1}$$

From equ  $\textcircled{1}$

$$2\pi\rho H\phi = \int_0^{2\pi} \int_0^{\rho} \frac{I}{\pi a^2} \hat{z} \cdot \rho d\rho d\phi \hat{z}$$

$$2\pi\rho H\phi = \frac{I}{\pi a^2} \frac{\rho^2}{2} (2\pi)$$

$$2\pi\rho H\phi = I \left( \frac{\pi\rho^2}{\pi a^2} \right)$$

$$\vec{H} = \frac{I\rho}{2\pi a^2} \hat{\phi} \quad \text{For } 0 < \rho < a$$



\* For  $a \leq \rho \leq b$

$$2\pi\rho H\phi = I_{enc} = I$$

$$\boxed{\vec{H} = \frac{I}{2\pi\rho} \hat{\phi}} \quad \text{for } a \leq \rho \leq b$$

Infinite line.

- For  $b < \rho < b+t$

$$2\pi\rho H\phi = I_{enc} = \underbrace{I}_{\rho \rightarrow a} - \int_S \vec{J} \cdot \vec{ds} \quad \text{--- (2)}$$

to find  $\vec{J}$

$$\rho = b+t \rightarrow I_{enc} = I$$

$$I = \int_S \vec{J} \cdot \vec{ds} = \int_0^{2\pi} \int_b^{b+t} J_z (-\hat{z}) \cdot \rho d\rho d\phi (-\hat{z})$$

~~XXXXXXXXXX~~

$$I = J_z \frac{(b+t)^2 - b^2}{2} (2\pi)$$

$$\vec{J} = \frac{I}{\pi((b+t)^2 - b^2)} \hat{z} \quad \text{A/m}^2 \quad \text{--- sub in (2)}$$

$$2\pi\rho H\phi = I - \int_0^{2\pi} \int_b^{\rho} \frac{I}{\pi(2bt+t^2)} \hat{z} \cdot \rho d\rho d\phi \hat{z}$$

$$\bullet 2\pi\rho H\phi = I \left( 1 - \frac{1}{\pi(2bt+t^2)} \frac{(\rho^2-b^2)}{2} \right)$$

$$\bar{H} = \frac{I}{2\pi\rho} \left( 1 - \frac{\rho^2-b^2}{2bt+t^2} \right) \hat{\phi} \text{ A/m}$$

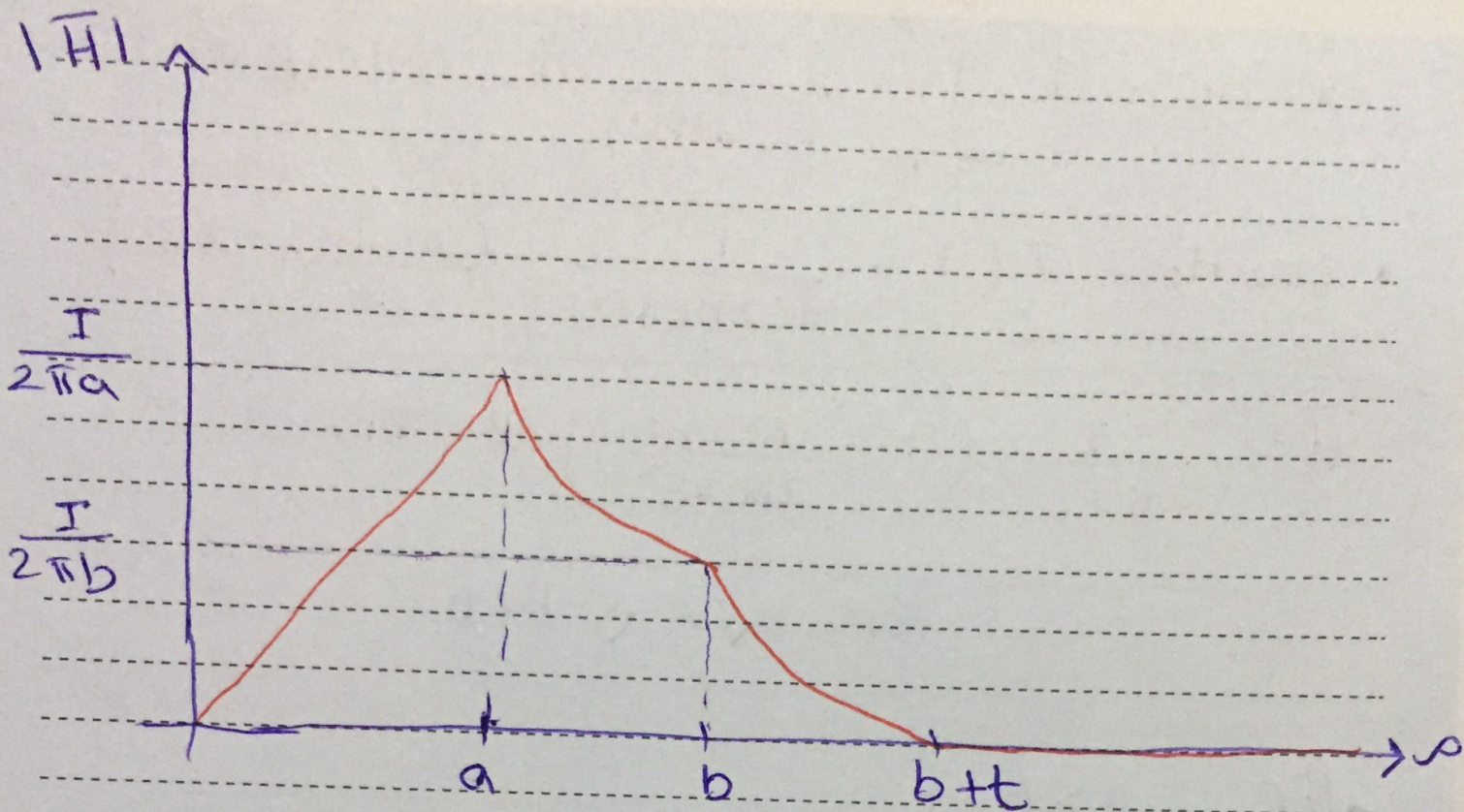
for  $b \leq \rho \leq b+t$

- for  $\rho > b+t$

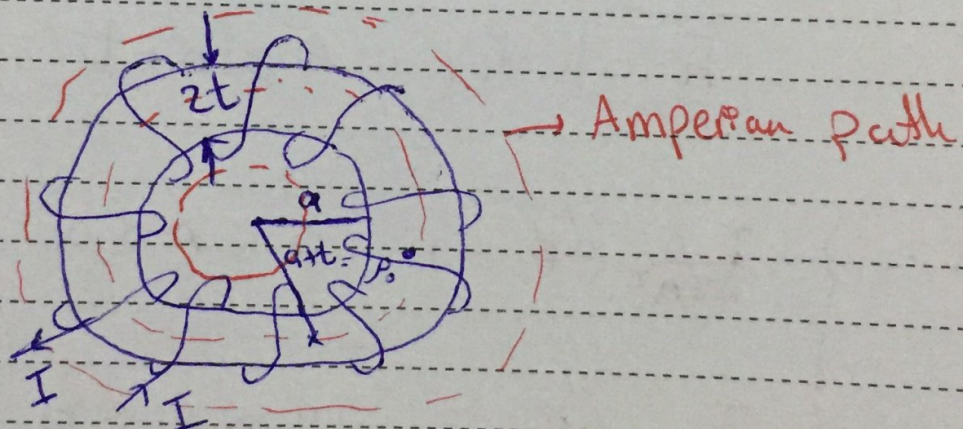
$$2\pi\rho H\phi = I_{enc} = I - I = 0.$$

$$\bar{H} = 0 \text{ for } \rho \geq b+t.$$

$$\bar{H} = \left\{ \begin{array}{l} \frac{I\rho}{2\pi a^2} \hat{\phi}, \quad 0 \leq \rho \leq a \\ \frac{I}{2\pi\rho} \hat{\phi}, \quad a \leq \rho \leq b \\ \frac{I}{2\pi\rho} \left( 1 - \frac{\rho^2-b^2}{2bt+t^2} \right) \hat{\phi}, \quad b \leq \rho \leq b+t \\ 0, \quad \rho \geq b+t \end{array} \right.$$



4) Toroid



Find  $\vec{H}$  everywhere?

Sol  $\oint \vec{H} \cdot d\vec{l} = I_{enc}$

$0 < \rho < a$

$I = 0 \rightarrow H = 0$

$\rho > b+t \rightarrow I_{enc} = I - I = 0$   
 $H = 0$

for  $\rho_0 - t < \rho < \rho_0 + t$  ( $a < \rho < a + 2t$ )

$$\vec{H} = H_\phi \hat{a}_\phi$$

$$dL = \rho d\phi \hat{a}_\phi$$

$$2\pi\rho H_\phi = I_{enc} = NI$$

↳ # of turns

$$\vec{H} = \frac{NI}{2\pi\rho} \hat{a}_\phi$$

$$\vec{H} = \frac{NI}{L} \quad , \quad L = 2\pi\rho$$

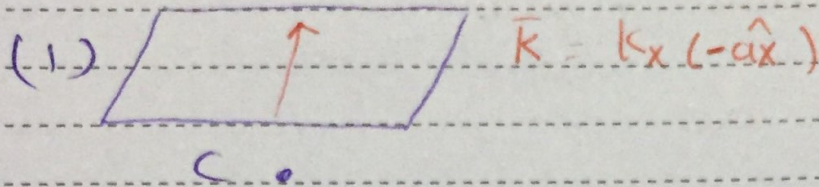
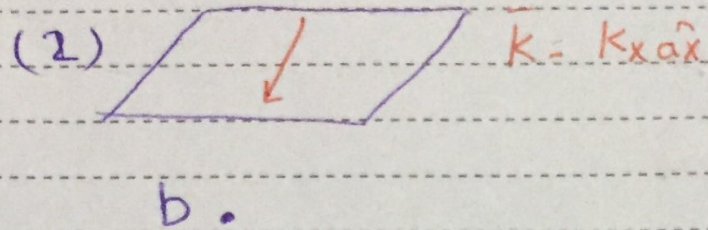
$$\vec{H} = nI \hat{a}_\phi \quad , \quad n = \frac{N}{L}$$

turns density

$$\vec{H} \cdot \vec{L} = NI \quad \text{if uniform}$$

$$\int_L \vec{H} \cdot d\vec{L} = NI \quad \text{Ampere's Law for } N\text{-turns}$$

$\vec{E}_x$   $\int_{-\infty}^{\infty}$  parallel plate capacitor



find  $\vec{H}$  at a, b, c?

Sol at point (b).

$$\vec{H} = \vec{H}_1 + \vec{H}_2$$

$$\vec{H}_1 = -\frac{1}{2} K_x \hat{a}_x \times \hat{a}_z + \frac{1}{2} K_x \hat{a}_x \times (-\hat{a}_z)$$

$$= \frac{K_x}{2} \hat{a}_y + \frac{K_x}{2} \hat{a}_y$$

$$\vec{H} = K_x \hat{a}_y$$

at point (a)  $\rightarrow$  zero

at point (c)  $\rightarrow$  zero.

\* Magnetic Flux Density ( $\vec{B}$ )

$$\vec{B} = \mu_0 \vec{H}$$

$\mu_0$  is free space permeability =  $4\pi \times 10^{-7}$  H/m

ie For finite straight line

$$\vec{B} = \frac{\mu_0 I}{4\pi \rho} (\cos \alpha_2 - \cos \alpha_1) \hat{a}_\phi$$

- For infinite sheet

$$\vec{B} = \frac{\mu_0}{2} \vec{k} \times \hat{a}_n$$

\* Units of  $\vec{B}$ : (MKS)

$$1) \frac{\text{H}}{\text{m}} \frac{\text{A}}{\text{m}} = \frac{\text{H} \cdot \text{A}}{\text{m}^2}$$

$$2) \frac{\text{Wb}}{\text{m}^2}, \text{Wb} = \text{Weber} \quad 1 \text{Wb} = 1 \text{H} \cdot 1 \text{A}$$

$$3) \text{T}, \text{Tesla}$$

- Old unit (cgs)

$$4) \text{G} = 10^{-5} \text{T}$$

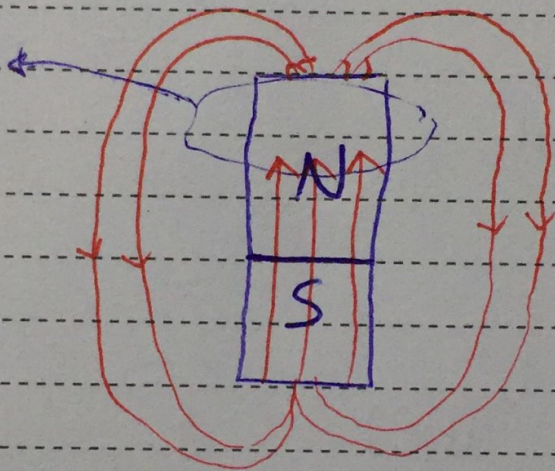
## \* Magnetic Flux ( $\Psi_m$ )

$$\Psi_e = \int_S \vec{D} \cdot d\vec{s}$$

$$\Psi_m = \int_S \vec{B} \cdot d\vec{s} \quad \text{in wb}$$

## \* Flux Lines -

Gaussian Surface



خواص خط دایره ای  
continuous  
From N  $\rightarrow$  S  
outside and from  
S  $\rightarrow$  N inside.

$$\Psi_m = \oint_S \vec{B} \cdot d\vec{s} = 0$$

because there is no single pole magnet.

→ Magnetic Gauss's Law

• 4<sup>th</sup> Maxwell equ. in integral form.

\* Maxwell's equ. For Static Fields :-

$$\boxed{1} \oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_v dV = 0$$

$$\boxed{2} \oint_L \vec{E} \cdot d\vec{L} = 0$$

$$\boxed{3} \oint_L \vec{H} \cdot d\vec{L} = I_{enc} = \int_S \vec{J} \cdot d\vec{s}$$

$$\boxed{4} \oint_S \vec{B} \cdot d\vec{s} = 0$$

+

$$\vec{D} = \epsilon \vec{E}$$

$$\vec{J} = \sigma \vec{E}$$

$$\vec{B} = \mu \vec{H}$$



## \* Magnetic Potentials -

- ↳ Scalar potential ( $V_m$ ) in (A)
- ↳ vector potential ( $\vec{A}$ ) in (wb/m)

## - Duality -

$$\vec{E} = -\nabla V \quad \longrightarrow \quad \boxed{\vec{H} = -\nabla V_m}$$

$\downarrow$                        $\downarrow$                        $\downarrow$   
 A/m                      V/m                      A

$$V = -\int_L \vec{E} \cdot d\vec{L} \quad \longrightarrow \quad \boxed{I = \oint_L \vec{H} \cdot d\vec{L}}$$

$$V = \int_L \vec{E} \cdot d\vec{L} = 0$$

## \* For $\vec{A}$ Duality -

- For line charge

$$V = \int_L \frac{\rho_L dL}{4\pi\epsilon_0 r}$$

for line current

$$\vec{A} = \int \frac{\mu_0 I d\vec{L}}{4\pi r}$$

- For surface charge

$$V = \int_S \frac{\rho_s ds}{4\pi\epsilon_0 r}$$

$$\vec{A} = \int_S \frac{\mu_0 \vec{K} ds}{4\pi r}$$

- For volume charge

$$V = \int_V \frac{\rho_v dv}{4\pi\epsilon_0 r}$$

$$\vec{A} = \int_V \frac{\mu_0 \vec{J} dv}{4\pi r}$$

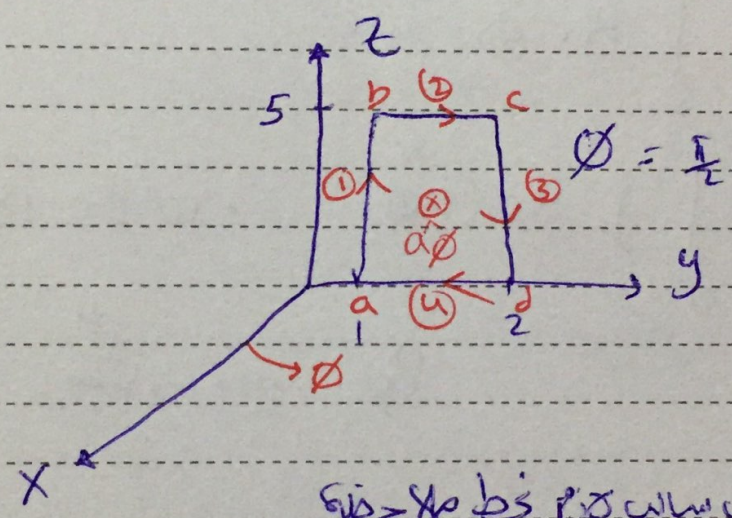


$$\Psi_m = \int \vec{A} \cdot d\vec{L}$$

$$\Psi_m = \int_S \vec{B} \cdot d\vec{s}$$

\* Ex Given the magnetic potential  $\vec{A} = -\frac{\rho^2}{4} \hat{a}_z$  wbm  
 Calculate the total flux crossing the surface  $\phi = \frac{\pi}{2}$ ,  $1 \leq \rho \leq 2m$ ,  $10 \leq z \leq 5m$ .

Sol



از اطلع کجا اب سالب هم خط ما را قطع  
 انه لتتفق ما اطلع سالب مع  
 تغيره سالبه من

$$\Psi_m = \int_C \vec{A} \cdot d\vec{L} \text{ on path } abcda$$

$$\Psi_m = \int_{L_1} \vec{A} \cdot d\vec{L}_1 + \int_{L_2} \vec{A} \cdot d\vec{L}_2 + \int_{L_3} \vec{A} \cdot d\vec{L}_3 + \int_{L_4} \vec{A} \cdot d\vec{L}_4$$

$$d\vec{L}_4 = dz \hat{a}_z$$

$$d\vec{L}_2 = d\rho \hat{a}_\rho$$

همیشه نه از  $\vec{A}$  و  $\hat{a}_z$   
 و اسکالر الی و لراچ با  $\hat{a}_\rho$   
 هم ←

~~.....~~



$$\Psi_m = \int_0^5 \frac{-\rho^2}{4} \hat{a}_z \cdot d\tau \hat{a}_z \Big|_{\rho=1} + \int_5^0 \frac{-\rho^2}{4} \hat{a}_z \cdot d\tau \hat{a}_z \Big|_{\rho}$$

$$= \frac{-1}{4} (5) - (1) (-5) = \frac{-5}{4} + 5$$

$$= \frac{-5}{4} + 5 = \boxed{\frac{15}{4} \text{ Wb}}$$

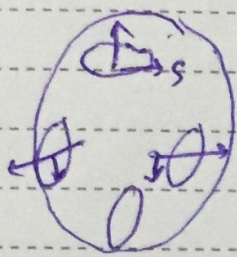
$$\Psi_m = \int_S \vec{B} \cdot d\vec{s}$$

$$\frac{15}{4} = \int_0^5 \int_1^2 B_\phi \hat{a}_\phi \cdot d\rho dz \hat{a}_\phi$$

↓  
By integration

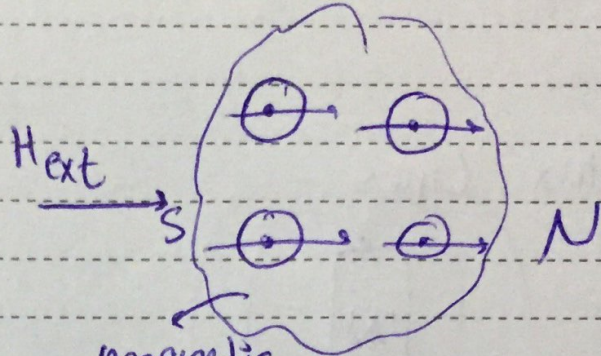
CH 8 Magnetic fields in materials 8 -  
 Section 8.5 magnetization ( $\vec{M}$ ) Unit (A/m)

$$\vec{M} = \lim_{\Delta V \rightarrow 0} \sum_{k=1}^N \frac{\vec{m}_k}{\Delta V}$$



$$\vec{M} = 0$$

Atom



magnetic material

$$\vec{P} = \chi_e \epsilon_0 \vec{E}$$

- for some materials -

$$\vec{M} = \chi_m \vec{H}$$

$$\vec{B} = \mu_0 \vec{H} \text{ in Free space } (\mu_r = 1)$$

Currents

free

bound

$$\vec{k} = \vec{H} \cdot \hat{a}_n$$

$$\vec{k}_b = M \times \hat{a}_n$$

$$\vec{J} = \nabla \times \vec{H} \leftarrow \times$$

$$\vec{J}_b = \nabla \times \vec{M} \leftarrow \times$$

$$\oint \vec{H} \cdot d\vec{L} = I_{enc}$$

$$\int \vec{J} \cdot d\vec{s}$$

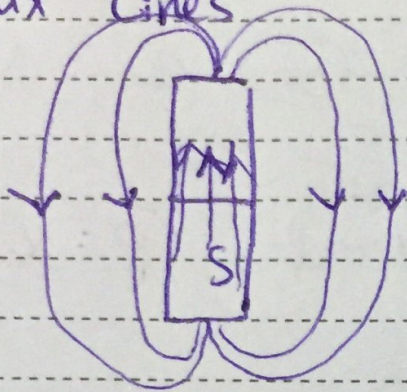


\*  $\vec{B} = \mu \vec{H}$  \*

$\mu \rightarrow \mu_0 \mu_r$   $\rightarrow$  ~~relative~~ relative permeability (Unitless)

in general  $\chi_m = \mu_r - 1$

\* Flux Lines



- Classification of magnetic materials

↳ Dia magnetic (Cu, Al, lead) ( $\mu_r < 1$ )

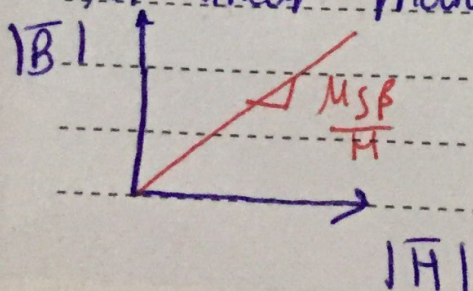
↳ Paramagnetic (Air) ( $\mu_r > 1$ )

↳ Ferro magnetic ( $\mu_r > 771$ )

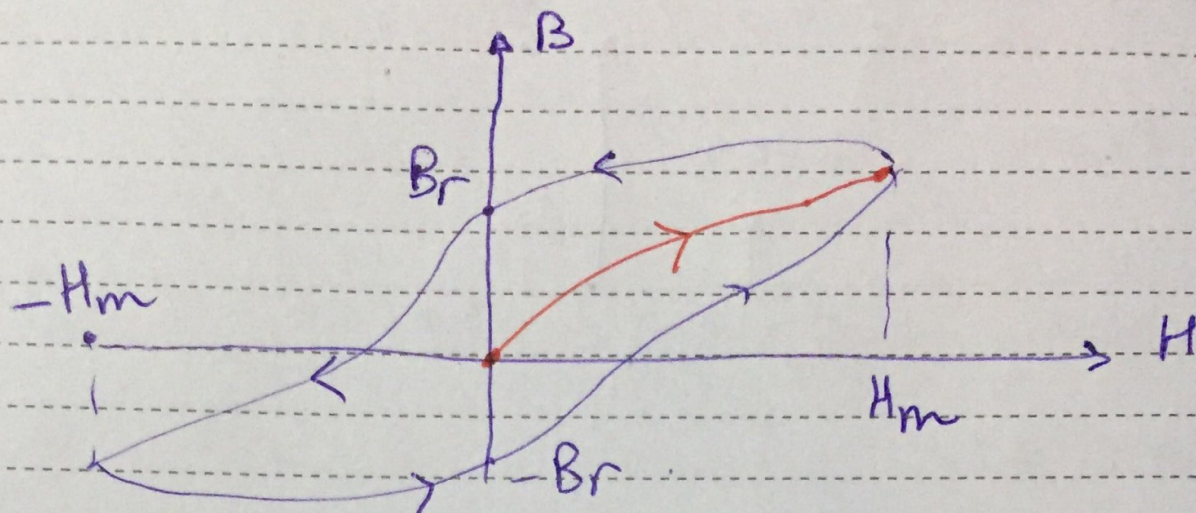
(Iron, Nickel, cobalt, Ferrite, )  $\rightarrow$  Non linear material

\* B/H curve

For linear material



- For non-linear materials -



\*  $T_c$  = Curie temp  
Iron =  $790^\circ\text{C}$

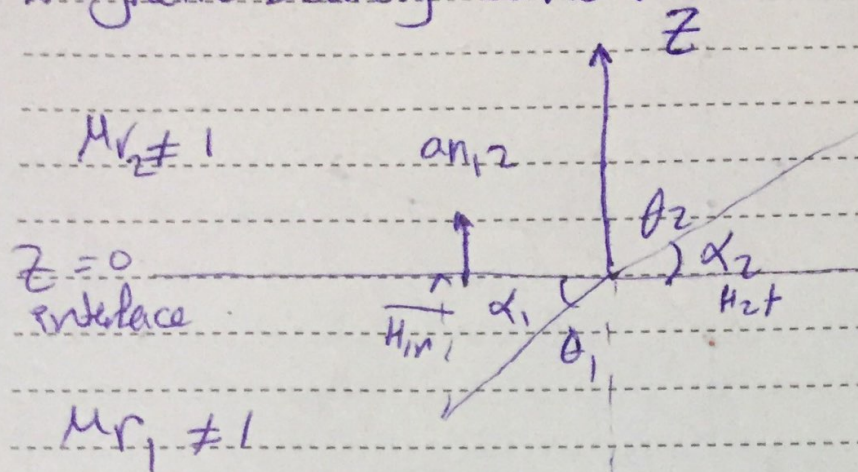
\*  $B_r$  = Residual magnetic flux density  
 $H_c$  = Demagnetization magnetic field intensity

- Area  $\uparrow$   $\rightarrow$  Hard magnetic material  $\uparrow$

$$\bar{B} = \mu \bar{H}$$

only at point (not in general).

# \*Magnetic boundary conditions -



- Start with  $\vec{H}_1$

$$\vec{H}_1 = \vec{H}_{in} + \vec{H}_{rt}$$

$$\vec{H}_{in} = (H_1 \cdot \hat{n}) \hat{n}$$

$$\vec{H}_{rt} = \vec{H}_1 - \vec{H}_{in}$$

$$\sin \theta_1 = \frac{H_{rt}}{H_1}$$

$$\alpha_1 = 90 - \theta_1$$

$$\cos \theta_1 = \frac{H_{in}}{H_1}$$

$$\tan \theta_1 = \frac{H_{rt}}{H_{in}}$$

- To find  $\vec{H}_2$

$$\vec{H}_2 = \vec{H}_{2n} + \vec{H}_{2t}$$

Apply the 3rd and 4th Maxwell's equation at the interface.

$$\oint \vec{H} \cdot d\vec{l} = I_{enc}$$

$$\oint \vec{B} \cdot d\vec{s} = 0$$



Given that  $\vec{H} = -2\hat{x} + 6\hat{y} + 4\hat{z}$  A/m  
 in region  $y - x - 2 \leq 0$  where  $\mu_1 = 5\mu_0$   
 calculate:-

1)  $\vec{H}_1$  and  $\vec{B}_1$

2)  $\vec{H}_2$  and  $\vec{B}_2$  in region  $y - x - 2 \geq 0$  if  $\mu_2 = 2\mu_0$

Sol 1)  $\vec{H}_1 = (\mu_1 - 1)\vec{H}$

$= 4\vec{H}_1 = (-8, 24, 16)$  A/m

$\vec{B}_1 = \mu_1 \vec{H}_1$

$= 5\mu_0 \vec{H}_1 = (-10, 30, 20)$   $\mu_0$

2)  $\vec{H}_1 = \vec{H}_{it} + \vec{H}_{in}$

$\vec{H}_{in} = (\vec{H}_1 \cdot \hat{a}_n) \hat{a}_n$

$= \left( (-2, 6, 4) \cdot \frac{(-1, 1, 0)}{\sqrt{2}} \right) \cdot \frac{(-1, 1, 0)}{\sqrt{2}}$

$\vec{H}_{in} = (-4, 4, 0)$  A/m

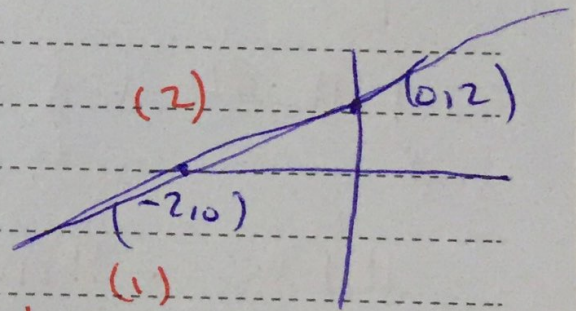
$\vec{H}_{it} = \vec{H}_1 - \vec{H}_{in}$

$= (2, 2, 4)$  A/m

$= \vec{H}_2$  (since  $\vec{K} = 0$ )

$\hat{a}_n = \frac{\nabla f}{|\nabla f|}$

$= \frac{(-1, 1, 0)}{\sqrt{2}}$





$$\overline{B_{1n}} = \overline{B_{2n}}$$

$$\overline{H_{2n}} = \frac{\mu r_1}{\mu r_2} \overline{H_{1n}}$$

$$\overline{H_{2n}} = (-10, 10, 0)$$

$$\overline{H_2} = -8\hat{a}_x + 12\hat{a}_y + 4\hat{a}_z \text{ A/m}$$

$$\overline{B_2} = 20\mu_0 H_2 = -16\hat{a}_x + 24\hat{a}_y + 8\hat{a}_z \text{ H-P}$$

$$\mu_2 = \overline{H_2}$$

-  $z=0$  Apply  $\oint \overline{H} \cdot d\overline{L} = I_{enc}$  on path ~~ab~~  
(infinite sheet)  $a-b-c-d-a$

$$\int_a^b \overline{H} \cdot d\overline{L} + \int_b^c \overline{H} \cdot d\overline{L} + \int_c^d \overline{H} \cdot d\overline{L} + \int_d^a \overline{H} \cdot d\overline{L} = k_x W$$

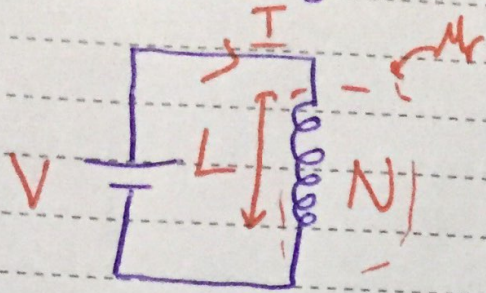
$$H_{2t} W - H_{2n} \frac{h}{2} - H_{1n} \frac{h}{2} - H_{1t} W + H_{1n} \frac{h}{2} + H_{2n} \frac{h}{2} = k_x W$$

$$H_{2t} = H_{1t} = k_x$$

$$\text{if } k=0 \rightarrow H_{2t} = H_{1t}$$

$$\overline{H_{2n}} = \frac{\mu r_1}{\mu r_2} \overline{H_{1n}}$$

### \* Inductors -



$\lambda \propto I$   
 $\lambda = L I$   
 $L$  is proportionality constant  
 $L = \text{inductance}$

$$I \propto B \propto \psi \propto \lambda$$

$$\psi = \int \vec{B} \cdot d\vec{s}$$

$$\lambda = N \psi$$

$\hookrightarrow$  Flux linkage (Wb)

$$L = \frac{\lambda}{I} \text{ (H)}$$

### \* Magnetic energy ( $w_m$ ) in (J).

$$w_m = \frac{1}{2} \int_V \vec{H} \cdot \vec{B} \, dV$$

$$= \frac{1}{2} \int_V \mu H^2 \, dV$$

$$= \frac{1}{2} \int_V \frac{B^2}{\mu} \, dV$$

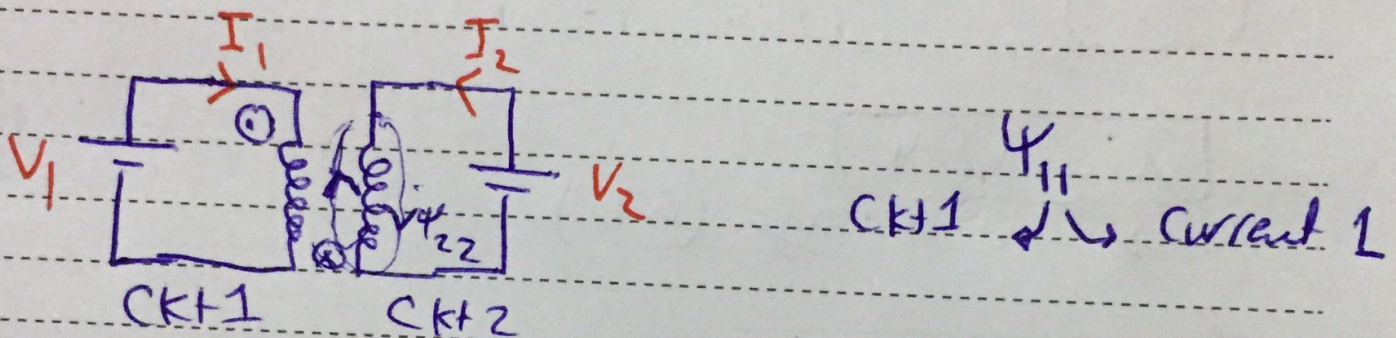
} in general

- if uniform -

$$W_m = \frac{1}{2} L I^2$$

$$I = \frac{2 W_m}{L}$$

- Self and mutual Inductance -



$\Psi_{22}$  : Self fluxes

$\Psi_{12}, \Psi_{21}$  : Mutual flux

- Self Inductance -

$$L_{11} = \frac{\lambda_{11}}{I_1} = \frac{N_1 \Psi_{11}}{I_1}$$

$$L_{22} = \frac{\lambda_{22}}{I_2} = \frac{N_2 \Psi_{22}}{I_2}$$

→ Mutual Inductance

$$M_{12} = \frac{\lambda_{12}}{I_2} = \frac{N_1 \psi_{12}}{I_2}$$

$$M_{21} = \frac{\lambda_{21}}{I_1} = \frac{N_2 \psi_{21}}{I_1}$$

- Total flux -

$\psi_1$  is total flux in ckt 1

$$\psi_1 = \psi_{11} \begin{cases} + & \text{if in the same direction} \\ - & \text{if in the opposite direction} \end{cases} \psi_{12}$$

-  $L_1$  is total Inductance of ckt 1

$$L_1 = L_{11} \begin{cases} + & \text{if flux +} \\ - & \text{if flux -} \end{cases} M_{12}$$

must be positive.

$$W_m = \frac{1}{2} L_{11} I_1^2 + \frac{1}{2} L_{22} I_2^2 \pm \left( \frac{1}{2} M_{12} I_2^2 + \frac{1}{2} M_{21} I_1^2 \right)$$

$$W_m = W_{m1} + W_{m2}$$

$$= \frac{1}{2} L_1 I_1^2 + \frac{1}{2} L_2 I_2^2$$

$$\frac{V_1}{V_2} = \frac{N_1}{N_2} \rightarrow \boxed{\frac{I_2}{I_1} = \frac{N_1}{N_2}}$$

\* procedure to find (L) or (M) :-

1) Choose suitable coordinates.

2) Assume current

3) Find B (As you did in CH 7)

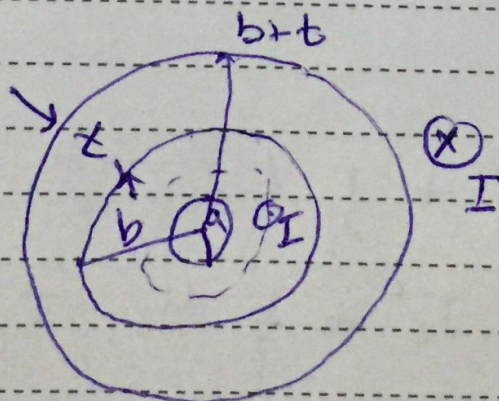
$$4) \Psi = \int B \cdot ds$$

$$4) W_m = \frac{1}{2} \int \frac{B^2}{\mu} dV$$

$$5) L = \frac{N\Psi}{I} = \frac{2}{I}$$

$$5) L = \frac{2W_m}{I^2}$$

- Ex For a coaxial cable, find all self inductance



Sol 1) Cylindrical

2) on the figure.

$$\text{From CH7} \rightarrow \vec{B} = \begin{cases} \frac{\mu_0 I \rho}{2\pi a^2} \hat{\phi} & , 0 < \rho < a \\ \frac{\mu_0 \mu_r I}{2\pi \rho} \hat{\phi} & , a < \rho < b \end{cases}$$

series

$$L = L_{int} \oplus L_{ext}$$

For  $L_{int}$

$$W_m = \frac{1}{2} \int_0^L \int_0^{2\pi} \int_0^a \frac{\mu_0^2 I^2 \rho^2}{\mu_0 \mu_r^2 a^4} \rho d\rho d\phi dz$$

$$\frac{\mu_0 I^2}{2 \mu_r^2 a^4} \left( \frac{a^4}{4} \right) (2\pi) (L)$$

$$W_m = \frac{\mu_0 I^2 L}{16 \pi} \text{ (J)}$$

$$5) L_{ext} = \frac{\mu_0 L}{8\pi} \rightarrow \frac{L_{int}}{L} = \frac{\mu_0}{8\pi} \text{ H/m}$$

For  $L_{ext}$

$$\begin{aligned}\psi &= \int_L^s \bar{B} \cdot d\bar{s} \\ &= \int_0^L \int_a^b \frac{\mu_0 \mu_r I}{2\pi \rho} \hat{a}_\rho d\rho dz \hat{a}_\rho\end{aligned}$$

$$= \frac{\mu_0 \mu_r I L}{2\pi} \ln\left(\frac{b}{a}\right) \quad (\text{wb})$$

$$L_{ext} = \frac{\psi}{I} = \frac{\mu_0 \mu_r L}{2\pi} \ln\left(\frac{b}{a}\right) \quad (\text{H})$$

$$\frac{L_{ext}}{L} = \frac{\mu_0 \mu_r}{2\pi} \ln\left(\frac{b}{a}\right) \quad (\text{H/m})$$

$$\frac{L}{L} = \frac{\mu_0}{2\pi} \left[ \frac{1}{4} + \mu_r \ln\left(\frac{b}{a}\right) \right] \quad (\text{H/m})$$

# - Magnetic Circuits

Electrical Circuit

Magnetic Circuit

$$V_{emf}$$

$$I$$

$$R = \frac{V}{I} = \frac{l}{\sigma S}$$

$$G = \frac{1}{R}$$

$$I = \int_S \vec{J} \cdot d\vec{s}$$

$$W_E = \frac{1}{2} \int_V \epsilon E^2 dV$$

$$V_{emf} = F$$

$$\Psi_m \text{ or } \Phi$$

$$R_m = \frac{F}{\Phi} = \frac{l_c}{\mu A_c}$$

$$P = \frac{1}{R_m}$$

$$\Psi = \int_S \vec{R}_B \cdot d\vec{s}$$

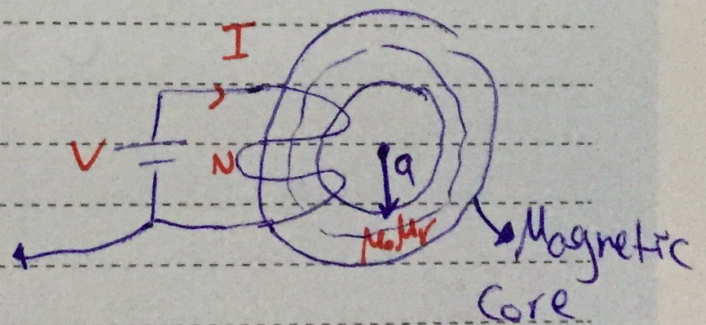
$$W_m = \frac{1}{2} \int_V \mu H^2 dV$$

## \* Magnetic Structures -

↳ magnetic core

↳ Excitation coil

Excitation coil





-  $R_m$  is magnetic resistance (Reluctance)

$$R_m = \frac{l_c}{\mu_0 \mu_r A_c}$$

$$V_m \cdot I = F = NI$$

$$= \Psi R_m$$

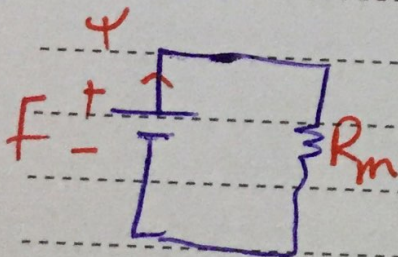
$$= H l_c$$

$$l_c = 2\pi r_0 \quad (\text{Toroid})$$

$A_c$  is Cross sectional Area of the core

$$A_c = \pi t^2 \quad (\text{Toroid})$$

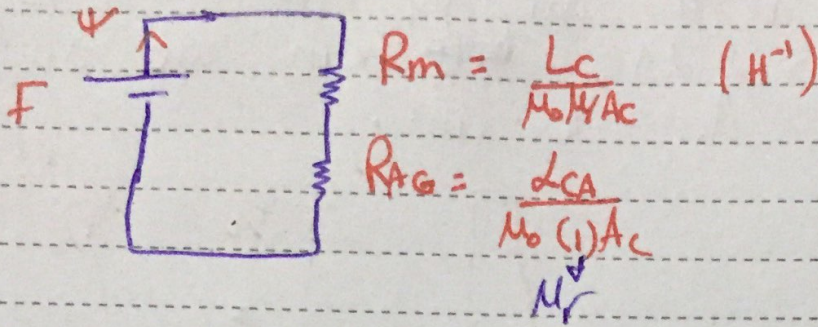
- Convert magnetic structure to a magnetic circuit



$$\Psi = \frac{F}{R_m} = \frac{NI}{\frac{l_c}{\mu_0 \mu_r A_c}}$$

$$\Psi = B A_c \rightarrow B = \frac{\Psi}{A_c}$$

- Magnetic structure with air gap



$$R_{eq} = R_m + R_{AG} \quad , \quad \Psi = \frac{F}{R_{eq}}$$

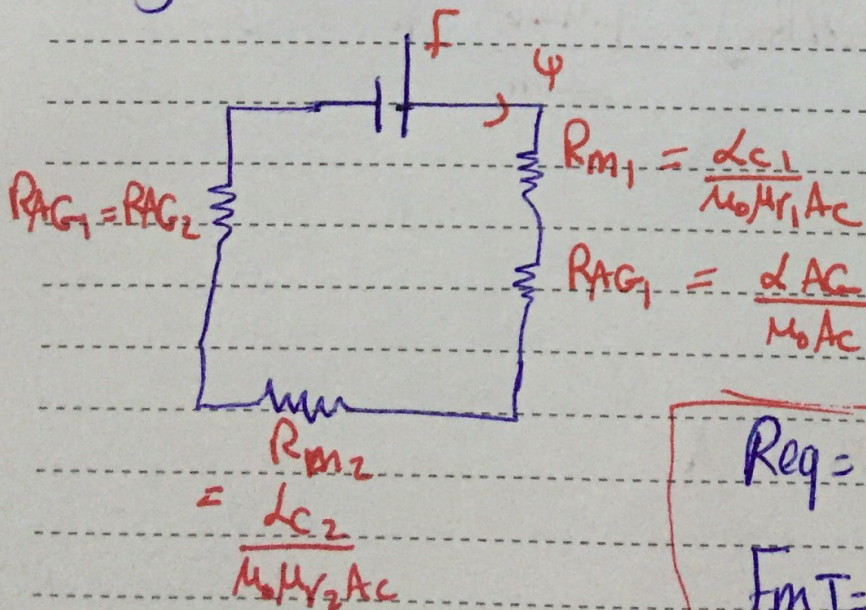
- Force in the air gap -

Magnetic Tractive Force ( $F_{MT}$ ) in (N)

$$F_{MT} = \frac{B^2 A_c}{2 \mu_0} \quad B = \frac{\Psi}{A_c}$$

$$\text{Pressure} = \frac{F_{MT}}{A_c} \quad (\text{pascal})$$

\* Magnetic Limitations



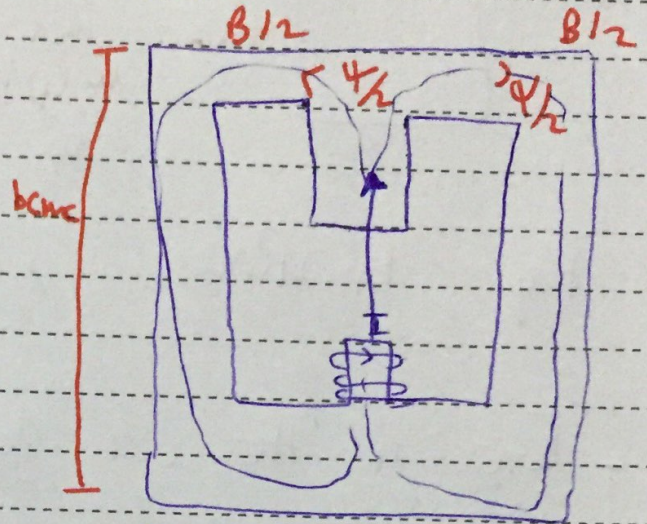
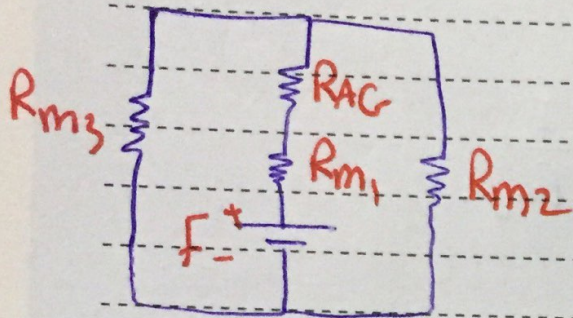
$$R_{eq} = 2R_{AG} + R_{m1} + R_{m2}$$

$$F_{MT} = mg = \left( \frac{B^2 A_c}{2 \mu_0} \right) \times 2$$

$$\Psi = B A_c = \frac{NI}{R_{eq}}$$

- Ex Calculate the current in the coil to produce  $1.5 \text{ wb/m}^2$  in the air gap, if  $\mu = 50\mu_0$ ,  $N = 400$  turns,  $l_{AC} = 10 \text{ cm}$  and all the branches have  $A_c = 10 \text{ cm}^2$ .

Sol



Parallel  $\leftarrow \Psi$  تفرع

$$R_{m1} = \frac{9 \times 10^{-2}}{(4\pi \times 10^{-7})(50)(10 \times 10^{-4})}$$

$$R_{m2} = \frac{30 \times 10^{-2}}{(4\pi \times 10^{-7})(50)(10 \times 10^{-4})}$$

$$R_{eq} = R_{m1} + R_{AG} + (R_{m2} // R_{m3}) = \frac{7.4 \times 10^8}{20\pi} \text{ H}^{-1}$$

$$F = NI = \Psi R_{eq}$$

$$\Psi = BA$$

$$I = \frac{\Psi R_{eq}}{N} = 44.16 \text{ A}$$

# CH 9 Maxwell's equations (Time Varying Fields) (Electromagnetics)

- Source for time varying fields -

- 1) Charge moving with acceleration
- 2) AC current flowing in the wire

- Maxwell's eq.  $\rightarrow$  For static field

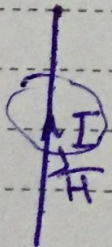
$$\oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_v dV$$

$$\oint_L \vec{E} \cdot d\vec{L} = 0$$

$$\oint_L \vec{H} \cdot d\vec{L} = I_{enc} = \oint_S \vec{J} \cdot d\vec{s}$$

$$\oint_S \vec{B} \cdot d\vec{s} = 0$$

- Faraday's Law -



to find  $V_{emf}$  from  $\vec{H}$   
 $\hookrightarrow$  generator principle.

$$V_{emf} = - \frac{d\lambda}{dt}$$

$$V_{emf} = - \frac{d\psi}{dt}$$

$\psi(x, y, z, t)$  time  
space

$$V_{emf} = \frac{d}{dt} \int \vec{B} \cdot d\vec{s}$$

From CHU

$$\oint V = - \int \vec{E} \cdot d\vec{L}$$

$$\oint V = \int \vec{E} \cdot d\vec{L} = 0$$

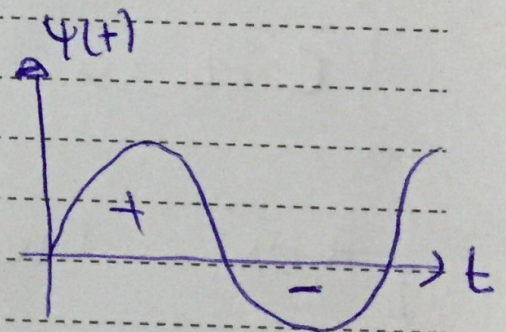
$$V_{emf} = \int \vec{E} \cdot d\vec{L} = \frac{d}{dt} \int \vec{B} \cdot d\vec{s}$$

Faraday's Law  
for  $N=1$  turn

- AC source (Time varying  $\vec{B}$ )

$$v(t) \rightarrow i(t) \rightarrow B(t) \rightarrow \Phi(t) \rightarrow \lambda(t)$$

$$V_{emf,1} = - \frac{N d\Phi}{dt}$$



$$V_{emf} = \int \vec{E} \cdot d\vec{L} = \int \frac{-dB}{dt} \cdot d\vec{s}$$

2) Static Fields on a moving loop

$$V_{emf} = \int_L \vec{E} \cdot d\vec{l} = \int_L \underbrace{\vec{u} \times \vec{B}}_{\text{velocity}} \cdot d\vec{l}$$

$$\vec{E} = \vec{u} \times \vec{B}$$

3) Time Varying Field on a moving loop

$$V_{emf} = \int_L \vec{E} \cdot d\vec{l} = \int_S \frac{-d\vec{B}}{dt} \cdot d\vec{s} + \int_L \vec{u} \times \vec{B} \cdot d\vec{l}$$

$$V_{emf} = \int_L \vec{E} \cdot d\vec{l} = \frac{-d}{dt} \int_S \vec{B} \cdot d\vec{s}$$

\* Displacement current  $I_d$  found by Maxwell.

$$I_c = \int_S \vec{J} \cdot d\vec{s} \Rightarrow \vec{J} = \sigma \vec{E} \quad , \quad \vec{J} = \rho v \vec{u}$$

Conduction                      Convection

$$I_d = \int_S \vec{J}_d \cdot d\vec{s}$$

displacement current density.

- Continuity equations -

$$\oint_S \vec{J} \cdot d\vec{s} = - \int_V \frac{d\rho_V}{dt} dV$$

$$I_c + I_d = 0 \rightarrow \vec{H} = 0$$

$$I_c = -I_d$$

$$I_d = \oint_S \vec{J} \cdot d\vec{s} = \int_V \frac{d\rho_V}{dt} dV$$

$$\vec{J}_d = \frac{d\vec{D}}{dt} \rightarrow \text{electric flux density } (\vec{D} = \epsilon_0 \vec{E})$$

$$\oint_L \vec{H} \cdot d\vec{l} = (\vec{J}_m + \vec{J}_d) \cdot d\vec{s}$$

3<sup>rd</sup> Maxwell eq. in Time varying fields

~~Maxwell's eq.~~

~~9.5 Maxwell's eq.~~

9.5 Maxwell's equ in Time Varying Fields e-

$$\oint_S \vec{D} \cdot d\vec{s} = \int_V \rho_V dV$$

$$\oint_L \vec{E} \cdot d\vec{L} = -\frac{d}{dt} \int_S \vec{B} \cdot d\vec{s}$$

$$\oint_L \vec{H} \cdot d\vec{a} = \int_S (\vec{J} + \vec{J}_d) \cdot d\vec{s}$$

$$\oint_S \vec{B} \cdot d\vec{s} = 0 \rightarrow \oint_S \vec{H} \cdot d\vec{s} = 0$$



# 9.7 Time Harmonic Fields periodic (sinusoidal)

- Start with the revision of complex No

\* How to convert between time domain and frequency domain and vice-versa -

- Maxwell's equ.

$$\oint_S \bar{D} \cdot d\bar{s} = \int_V \rho_v dV$$

$$\oint_L \bar{E} \cdot d\bar{L} = - \int_S \frac{d\bar{B}}{dt} \cdot d\bar{s}$$

$$\oint_L \bar{H} \cdot d\bar{L} = \int_S (\epsilon \bar{E} + \frac{d\bar{D}}{dt}) \cdot d\bar{s}$$

$$\oint_S \bar{B} \cdot d\bar{s} = 0$$

Note:

$$\frac{d}{dt} (e^{j\omega t}) = j\omega e^{j\omega t}$$

$$\int e^{j\omega t} dt = \frac{1}{j\omega} e^{j\omega t}$$

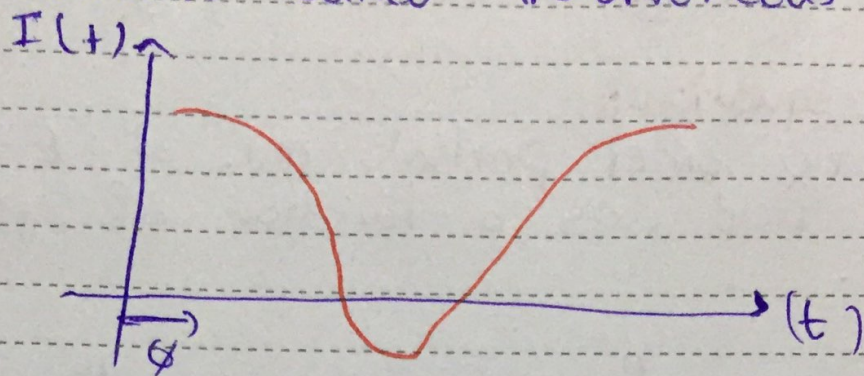
- i.e.  $I(t) = I_0 \cos(\omega t + \phi)$  Phase shift (Argument)

Amplitude  
Magnitude  
Absolute

radian freq (rad/s)  
 $\omega = 2\pi f$   
 $f = \frac{1}{T}$

↘ period

- in time domain called instantaneous form.



- Euler's identity :-

$$e^{j\theta} = \cos\theta + j\sin\theta$$

$$e^{-j\theta} = \cos\theta - j\sin\theta = (e^{j\theta})^* \leftarrow \text{conjugate}$$

$$I(t) = I_0 \cos(\omega t + \phi) \Rightarrow I_s = I_0 e^{j\phi} = I_0 \angle \phi$$

$$\cos\theta = \frac{e^{j\theta} + e^{-j\theta}}{2}$$

$$\sin\theta = \frac{e^{j\theta} - e^{-j\theta}}{2}$$

$$I(t) = \operatorname{Re} \left\{ I_0 e^{j(\omega t + \phi)} \right\}$$

$$I(t) = \operatorname{Re} \left\{ I_0 e^{j\phi} \underbrace{e^{j\omega t}} \right\}$$

Isolate the time ~~dependent~~ term.

$$I_s = I_0 e^{j\phi}$$

Phasor

# CH 10 Electromagnetic wave propagation -

## - Wave equation -

Second order partial equ. of  $\vec{E}$ -field or mag. field as a function of space and time.

- wave equ. of an  $\vec{E}$ -field in the z-direction

↓  
wave direction

- partial  $\frac{d^2 E}{dt^2} - u^2 \frac{d^2 E}{dz^2} = 0$

↑ time                      ↑ space

- diff  $\frac{d^2 E}{dt^2} - u^2 \frac{d^2 E}{dz^2} = 0$

$$E(x, y, z, t) = \text{Re} \{ E_s e^{j\omega t} \}$$

$$(j\omega)^2 e^{j\omega t} E_s - u^2 \frac{d^2 E_s}{dz^2} e^{j\omega t} = 0$$

OR source

$$\frac{d^2 E_s}{dz^2} + \frac{\omega^2}{u^2} E_s = 0$$

بعقد على الوقت

Let  $\beta = \frac{\omega}{u}$  (phase constant) (rad/m)

$$\frac{d^2 E_s}{dz^2} + \beta^2 E_s = 0 \quad \text{wave in z-direction.}$$

$$\text{- Let } \frac{d}{dz} = m$$

$$m^2 E_s + \beta^2 E_s = 0$$

$$\sqrt{m^2} = \sqrt{-\beta^2}$$

$$m = \pm \sqrt{-1} \sqrt{\beta^2}$$

$$m = \pm j \beta$$

if the roots are imaginary then the solution is either  $\sin(B?)$  or  $\cos(B?)$  or  $e^{jB}$  or  $e^{-jB}$

- Solution to the wave equ. is -

$$E_s(z) = E_0^+ e^{-j\beta z} + E_0^- e^{+j\beta z} \quad \text{V/m}$$

Wave travels in the +ve z-dir.      Wave travels in the -ve z-dir.

↓  
(Forward-wave)  
(Incident wave)

↓  
(Backward wave)  
(Reflected wave)

if the wave encounters different media.

- Convert to time domain -

$$E(z;t) = \text{Re} \left\{ E_0^+ e^{-j(\omega t - \beta z)} + E_0^- e^{+j(\omega t + \beta z)} \right\}$$

$$E(z;t) = \underbrace{E_0^+ \cos(\omega t - \beta z)}_{\text{Forward}} + \underbrace{E_0^- \cos(\omega t + \beta z)}_{\text{Backward}} \quad \text{V/m}$$

Forward  
 $\hat{a}_k = +\hat{a}_z$

Backward  
 $\hat{a}_k = -\hat{a}_z$

$\hat{a}_k$  is unit vector in the wave direction

$$u = \frac{\text{distance}}{\text{time}} = \frac{\omega}{\beta}$$

$$\omega t - \beta z = 0$$

$$\omega t = \beta z$$

$$\omega dt = \beta dz \rightarrow \frac{dz}{dt} = \frac{\omega}{\beta}$$

$$\frac{dz}{dt} = \frac{\omega}{\beta}$$

- Continue for exp. with the Forward wave:

$$E(z;t) = E_0^+ \cos(\omega t - \beta z) \quad \text{V/m}$$

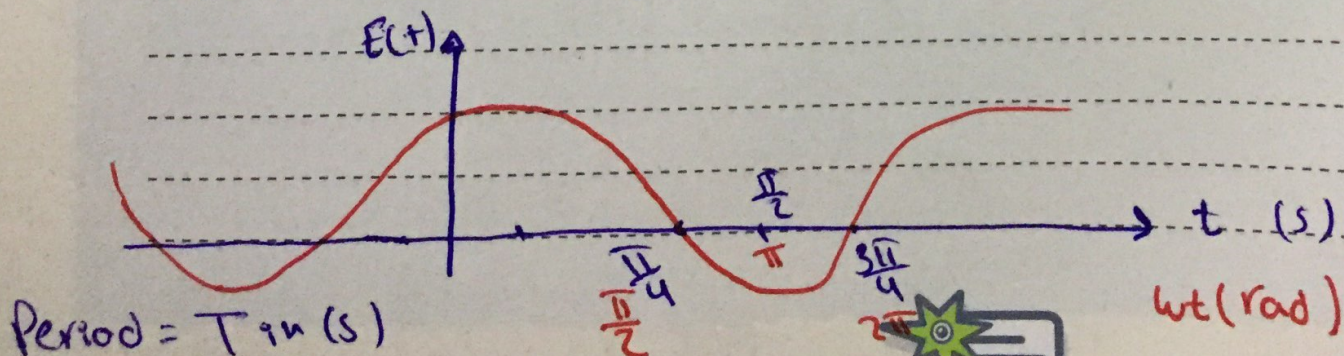
Sketch: -

in Time domain

$z$  is constant

i.e.  $z=0$

$$E(t) = E_0^+ \cos(\omega t) \quad \text{V/m}$$



- in Freq. domain -

Let  $t=0$

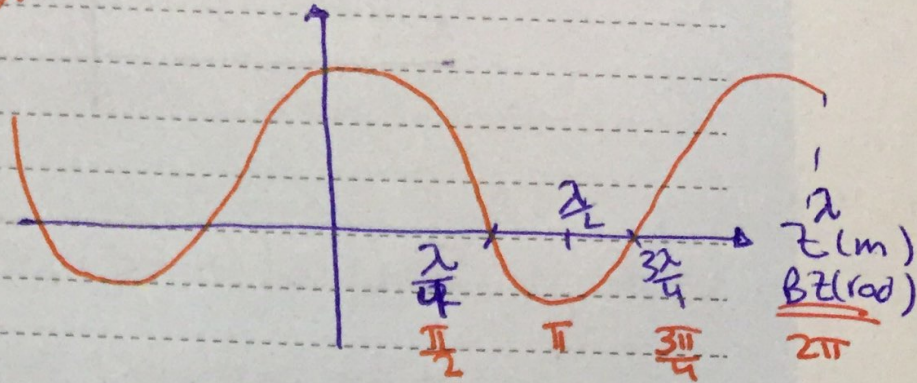
$$E(z) = E_0^+ \cos(\beta z)$$

$$\frac{2\pi}{\lambda} \leftarrow \rightarrow \lambda$$

$$u = \frac{\omega}{\beta} = \frac{\lambda}{T}$$

$$\beta = \frac{\omega T}{\lambda}$$

$\lambda$ : Wave length (m)



- Ex Given  $\vec{E} = 50 \cos(10^8 t + \beta x) \hat{a}_y$  V/m in Free space  $u = 3 \times 10^8$
- Find the direction of wave propagation
  - Calculate  $\beta$  and time it takes to travel a distance of  $\frac{\lambda}{2}$
  - Sketch the wave at  $t=0, \frac{T}{4}, \frac{T}{2}$  in space domain.

So! a)  $\hat{a}_k = -\hat{a}_x$

( $\beta$  does not affect direction)

b)  $\beta = \frac{\omega}{u} = \frac{2\pi}{\lambda} = \frac{10^8}{3 \times 10^8} = \frac{1}{3} \text{ rad/m}$ .

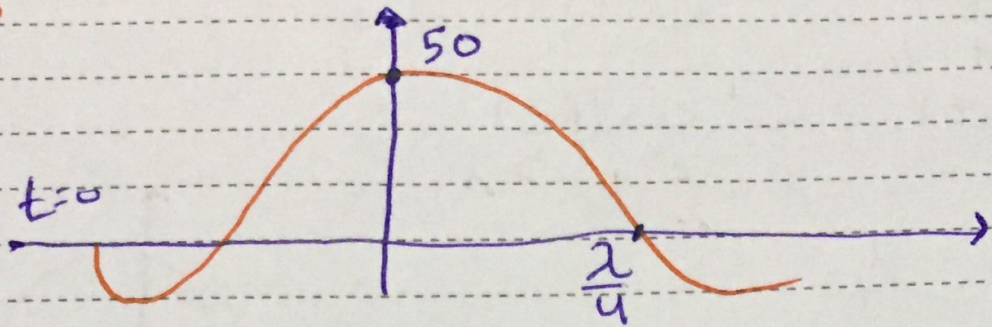
to travel a  $\frac{\lambda}{2}$  distance it requires  $\frac{T}{2}$  (s)

$$T? \rightarrow \omega = \frac{2\pi}{T} \rightarrow \frac{T}{2} = \frac{2\pi}{2 \times 10^8}$$

Time required = 31.4 ns  
Period = 62.8 ns

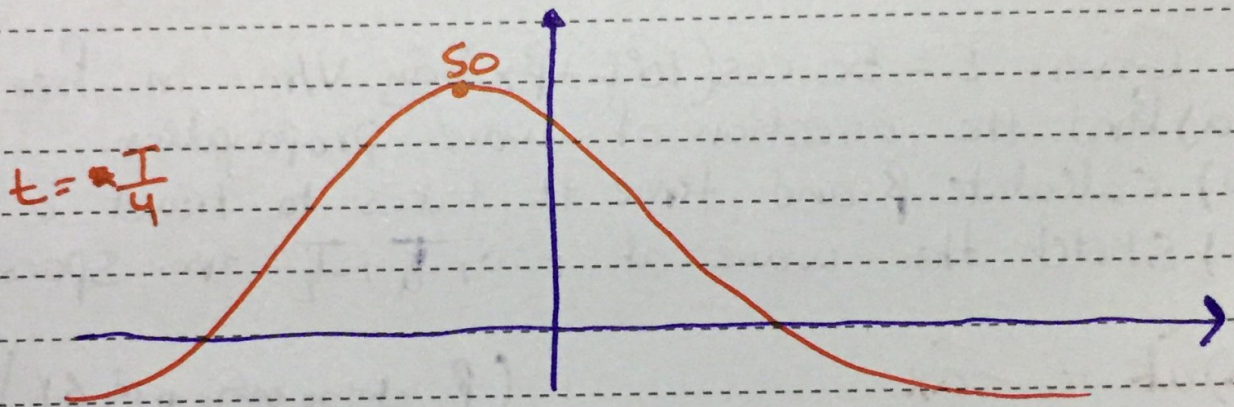


$$c) \textcircled{1} \vec{E} \Big|_{t=0} = 50 \cos(\beta x) \hat{a}_y$$



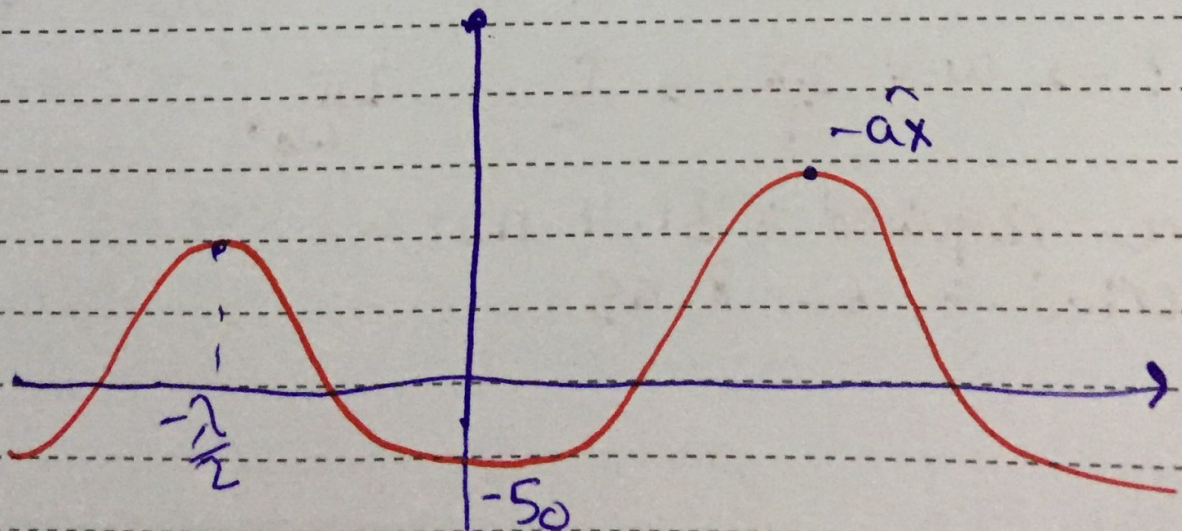
$$\textcircled{2} \vec{E} \Big|_{\frac{T}{4}} = 50 (\cos(\beta x + 90^\circ)) \hat{a}_y$$

$$= -50 \sin(\beta x) \hat{a}_y$$



$$\textcircled{3} \vec{E} \Big|_{\frac{T}{2}} = 50 \cos(\beta x + 180^\circ) \hat{a}_y$$

$$= -50 \cos(\beta x) \hat{a}_y$$



- Types of media :-

- 1) Lossy media ( $\epsilon = \epsilon_0 \epsilon_r$ ,  $\mu = \mu_0 \mu_r$ ,  $G \neq 0$ )
- 2) Lossless media ( $\epsilon = \epsilon_0 \epsilon_r$ ,  $\mu = \mu_0 \mu_r$ ,  $G = 0$ )
- 3) Free space ( $\epsilon = \epsilon_0$ ,  $\mu = \mu_0$ ,  $G = 0$ )
- 4) Good (super) (perfect) conductor ( $\epsilon = \epsilon_0$ ,  $\mu = \mu_0 \mu_r$ ,  $G \approx \infty$ )

\* Wave propagation in lossless media :-

$$\gamma = \alpha + j\beta$$

$\gamma$  : propagation constant  
 $\alpha$  : attenuation constant  
 $\beta$  : phase constant

$$\alpha = 0 \text{ Since } G = 0$$

$$\beta = \omega \sqrt{\mu \epsilon} \quad , \quad u = \frac{\omega}{\beta}$$

$$u = \frac{1}{\sqrt{\mu \epsilon}} = \frac{1}{\sqrt{\mu_0 \mu_r \epsilon_0 \epsilon_r}} = \frac{c}{\sqrt{\mu_r \epsilon_r}} \quad , \quad c = 3 \times 10^8 \text{ Speed of light}$$

$$\lambda = \frac{2\pi}{\beta}$$

$\eta$  : intrinsic impedance in ( $\Omega$ )

$$\eta = \frac{\epsilon}{\mu} \text{ as mag.}$$





$$\mu = \sqrt{\frac{\mu_0 \mu_r}{\epsilon_0 \epsilon_r}}$$

$$\mu = |\mu| \angle 0^\circ$$

$$= \sqrt{\frac{\mu_0}{\epsilon_0}} \sqrt{\frac{\mu_r}{\epsilon_r}} \angle 0^\circ$$

$$\mu = 120\pi \Omega$$

$\vec{E}$  and  $\vec{H}$  are in phase  $\rightarrow \Delta\mu = 0$

$$\vec{E} = E_0 \cos(\omega t - \beta z) \hat{a}_x$$

$$\vec{H} = \frac{E_0}{\mu} \cos(\omega t - \beta z) \hat{a}_y$$

$\rightarrow H_0$

2) Free space -

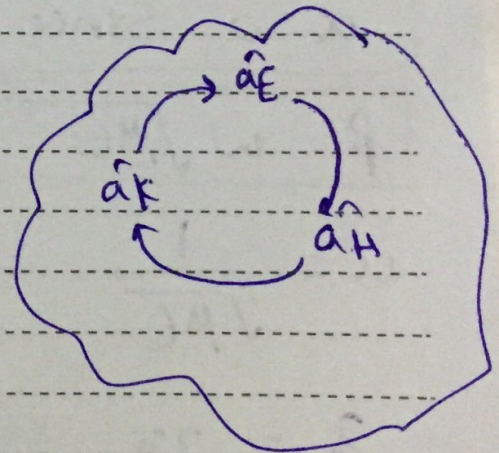
$$\alpha = 0, \quad \beta = \omega \sqrt{\mu_0 \epsilon_0} = \frac{\omega}{c}$$

$$u = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = c$$

$$\mu = \sqrt{\frac{\mu_0}{\epsilon_0}} = 120\pi \Omega$$

$\lambda = 2\pi\beta$ ,  $\vec{E}$  &  $\vec{H}$  are in phase

$$\text{Skin depth } (\delta) = \frac{1}{\alpha} = \infty$$



Transverse  
Electro  
magnetic.

- Wave propagation in a good conductor :-

$$\epsilon = \epsilon_0, \quad \mu = \mu_0 \mu_r, \quad \sigma \approx \infty$$

$\alpha \neq 0$  since  $\sigma \neq 0$

$$\alpha = \sqrt{\frac{\omega \mu \sigma}{2}}$$

$$u = \frac{\omega}{\beta} \neq \frac{1}{\sqrt{\mu \epsilon}}$$

$$\alpha = \sqrt{\pi f \mu \sigma}$$

$$\lambda = \frac{2\pi}{\beta}$$

$$\beta = \sqrt{\pi f \mu \sigma}$$

$$\mu = \sqrt{\frac{j\omega \mu}{\sigma + j\omega \epsilon}}$$

$$= \mu_1 \angle \phi$$

$\alpha = 0$  in good conductor

$\mu$  is complex.

$$\delta = \frac{1}{\alpha} = \frac{1}{\sqrt{\pi f \mu \sigma}}$$

$$\mu = \frac{\sqrt{j\omega \mu}}{\sqrt{\sigma}} = \sqrt{\frac{\omega \mu}{\sigma}} \angle 45^\circ$$

$$Z = r \angle \theta$$

$$\sqrt{Z} = \sqrt{r} \angle \theta/2$$

$$j = 1 \angle \frac{\pi}{2} = 1 \angle 90^\circ$$

$\theta_M = 0$  if lossless or free space

$0 < \theta_M < 45^\circ$  if lossy

$\theta_M = 45^\circ$  if good cond

$$\vec{E}_s = E_0 e^{-\alpha z} \hat{a}_x \quad \text{forward wave}$$

$$\vec{E}_s = E_0 e^{-\alpha z} e^{-j\beta z} \hat{a}_x$$

Amplitude  $\rightarrow$  phase

- convert to time domain

$$\vec{E}(z, t) = \text{Re} \{ \vec{E}_s e^{j\omega t} \}$$

$$\vec{E}(z, t) = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \hat{a}_x \quad \text{V/m}$$

$$\vec{H} = \frac{\vec{E}}{Z} = \frac{\vec{E}}{|Z|} \angle -45^\circ$$

$$\vec{H} = \frac{E_0}{|Z|} e^{-\alpha z} \cos(\omega t - \beta z - 45^\circ) \hat{a}_y \quad \text{A/m}$$

$$\hat{a}_H = \hat{a}_k \times \hat{a}_E$$

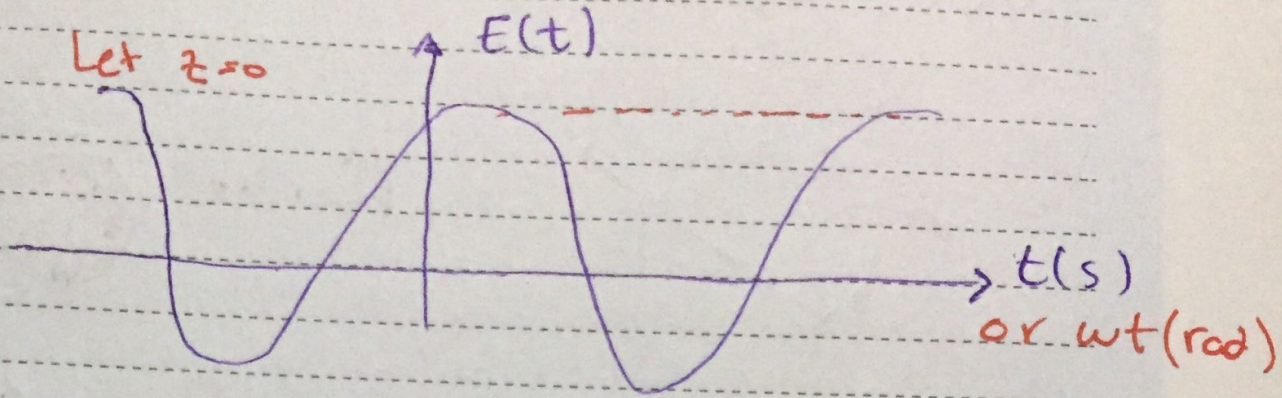
$$= \hat{a}_z \times \hat{a}_x$$

$$= \hat{a}_y$$

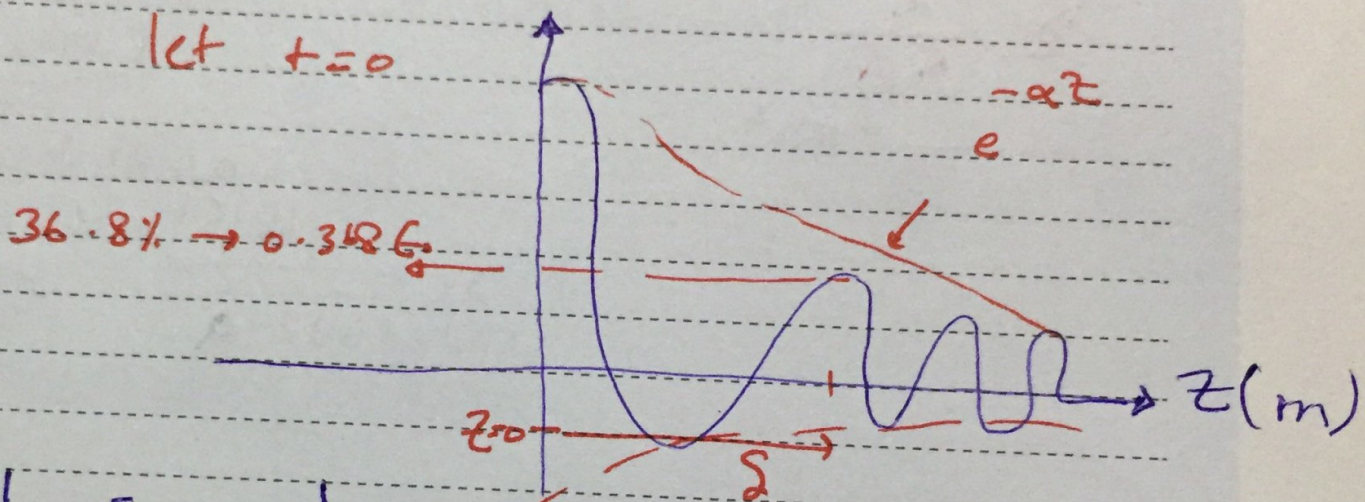
$\vec{E}$  lead  $\vec{H}$  by  $45^\circ$

Inductive media.

- in time domain



- in space domain



$$\delta = \frac{1}{\alpha} = \frac{1}{\sqrt{\pi f \mu \epsilon}}$$

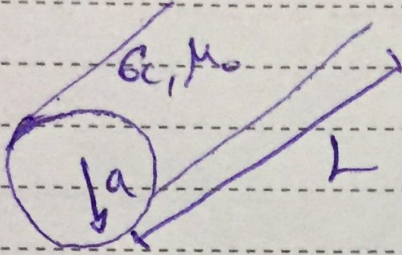
$\alpha$   
 $\downarrow$   
NP/m

$$1 \text{ NP} = 20 \log_{10} e$$

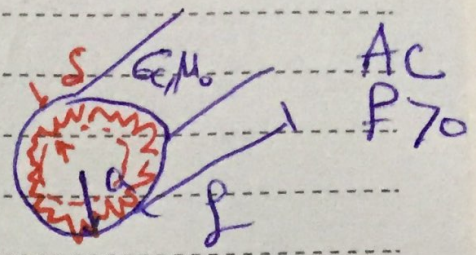
$$1 \text{ NP} = 8.686 \text{ dB}$$

# - Application of Skin effect -

DC  
F=0



$f \uparrow \rightarrow \delta \downarrow$



Diameter =  $2a$

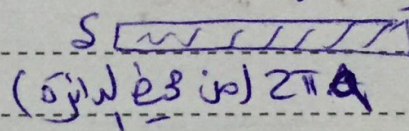
$$R_{dc} = \frac{L}{\sigma_0 \cdot A}$$

$\downarrow \pi a^2$

$$R_{ac} = \frac{L}{\sigma_c \cdot A}$$

$\downarrow (2\pi a) \cdot (\delta)$

و در اینجا که می بینیم  
در سطح به جری است  
مساحت



$$\frac{R_{ac}}{R_{dc}} = \frac{\frac{L}{\sigma_c \cdot 2\pi a \delta}}{\frac{L}{\sigma_0 \cdot \pi a^2}} = \frac{a}{2\delta}$$

$$R_{ac} = R_{dc} \cdot \frac{a}{\delta} \quad \delta \ll a$$

$R_{ac} \gg R_{dc}$  at higher Freq.

- Loss tangent :-

$$0 < \theta_M < 45^\circ$$

$$\tan \theta = \tan (2\theta_M) = \left( \frac{\sigma}{\omega \epsilon} \right)$$

$$0 < \theta < 90^\circ$$

$$\theta = 2\theta_M = \text{loss tangent angle}$$

- Note

$$\sigma = 0 \rightarrow \theta = 0 \rightarrow \theta_M = 0$$

$$\star \tan \theta = \frac{\sigma}{\omega \epsilon} = \frac{|\overline{J}_s|}{|\overline{J}_{d,s}|} = \frac{\sigma |\overline{E}_s|}{|j\omega \epsilon \overline{E}_s|} = \frac{\sigma}{\omega \epsilon} \quad \left\{ \overline{J}_d = \frac{dD}{dt} \right.$$

~~XXXXXXXXXXXXXXXXXXXX~~

$$\overline{P} = \overline{E} \times \overline{H} \quad (\text{power}) \quad (\text{w/m}^2)$$

↓ Poynting vector

↓ in time domain.

$$\star \overline{P}_{\text{avg}} = \frac{1}{T} \int_t \overline{E} \times \overline{H} dt$$

$$\overline{P}_{\text{avg}} = \frac{1}{2} \text{Re} \left\{ \overline{E}_s \times \overline{H}_s^* \right\}$$

time avg poynting vector. (w/m<sup>2</sup>)

$$P_{avg} = \int P_{avg} \cdot ds \quad (w)$$

total power

CH 11 Transmission Lines :- (2 or more conductor T.L.) → Transmission Line

Based on Maxwell's equ.

→ Coaxial cable

→ Twin wire cable

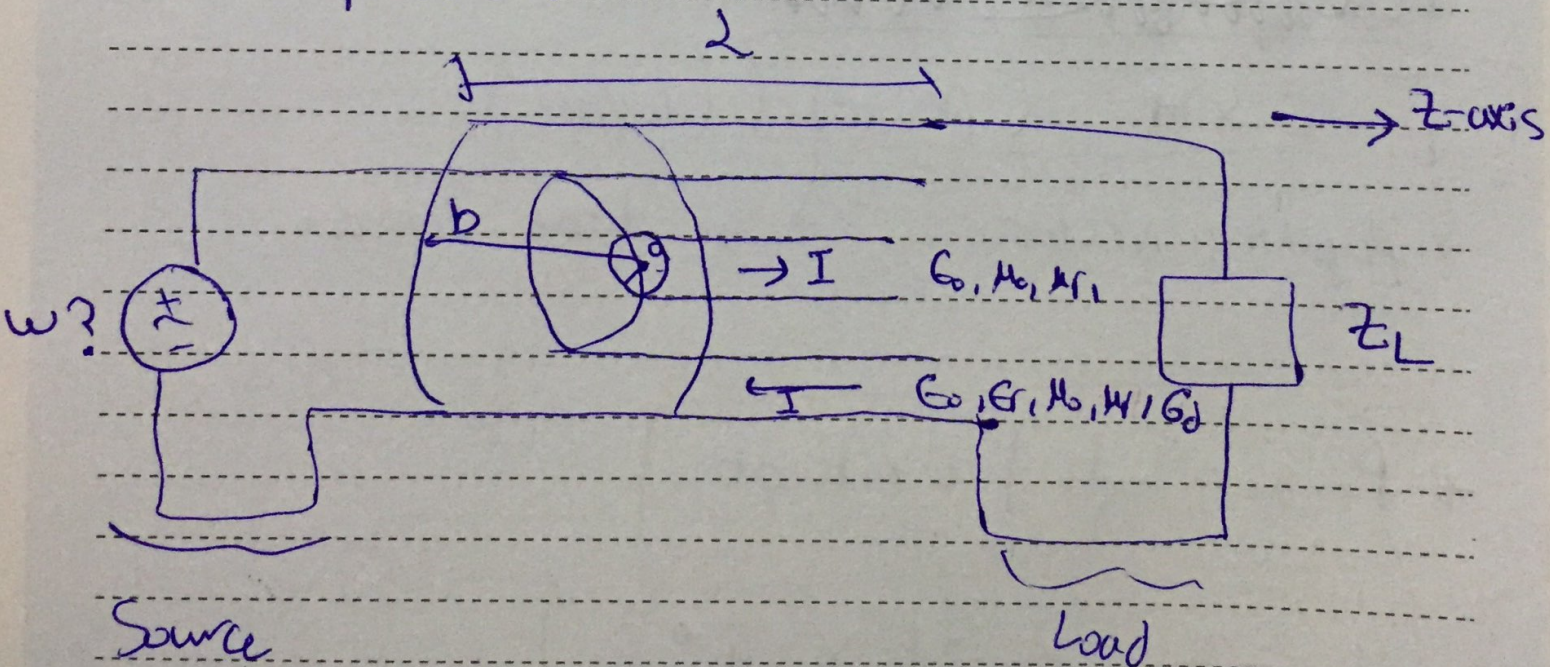
→ Planar Lines

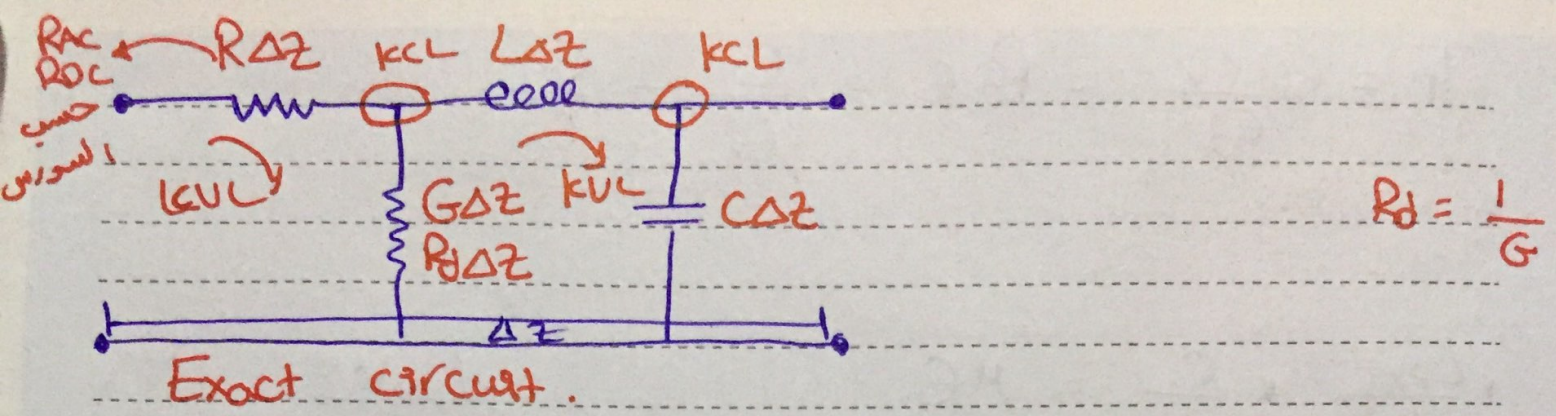
→ Strip line

→ micro Strip line

→ Slot line

- T.L. Parameters





- for a coaxial cables -

$$\frac{R}{\Delta z} = \frac{1}{2\pi \epsilon_0 \sigma} \left( \frac{1}{a} + \frac{1}{b} \right) \quad (\Omega/m)$$

Conductor

$$\frac{G}{\Delta z} = \frac{2\pi \epsilon_0 \epsilon_r}{\ln(b/a)} \quad \text{Dielectric (S/m)}$$

$$\frac{C}{\Delta z} = \frac{2\pi \epsilon_0 \epsilon_r}{\ln(b/a)} \quad \text{Dielectric}$$

ext

$$\frac{L}{\Delta z} = \frac{\mu_0 \mu_r}{2\pi} \ln\left(\frac{b}{a}\right) \quad (\text{H/m})$$

dielectric

\*  $L_{int} \rightarrow 0$  as  $w \rightarrow \infty$



$$\tau_r = \frac{\epsilon_0 \epsilon_r}{\sigma} = RC = \frac{C}{G} = \frac{\epsilon}{\sigma}$$

Relaxation Time

$$\frac{L_{ext}}{l} \times \frac{C}{l} = \mu \epsilon$$

Note:  
 $R \rightarrow$  conductor  
 $\rho \rightarrow$  dielectric

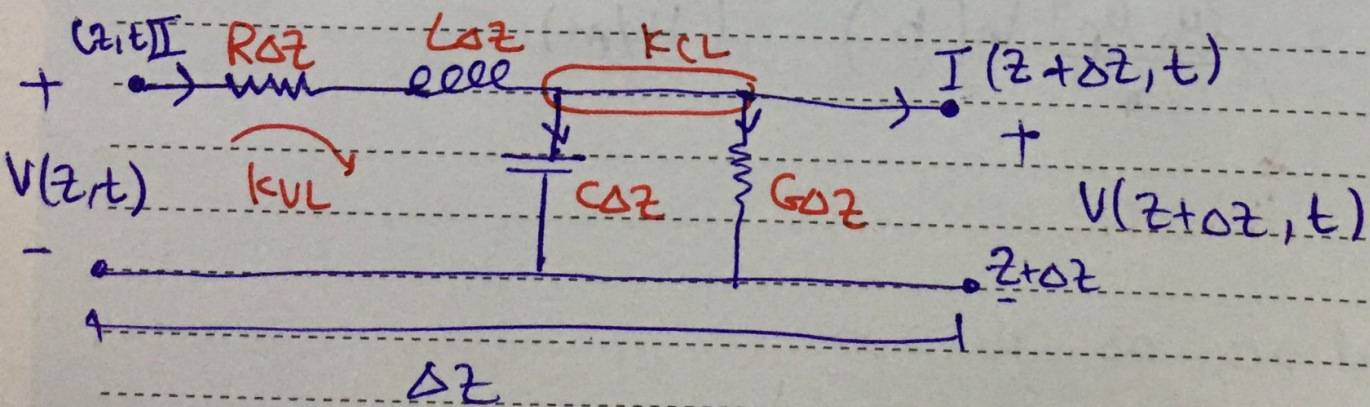
- T.O. equivalent ckt (Approximation):-

$\hookrightarrow$  L-Type (95% accurate)

$\hookrightarrow$   $\pi$ -Type (99% accurate)

$\hookrightarrow$  T-Type (99% accurate)

\* L-Type equ. ckt:-



$V, I$  vs  $z$

T.L. equation through Solving KVL & KCL equ.

- KVL &  $\sum V = 0$   
loop

$$-V(z,t) + R\Delta z I(z,t) + L\Delta z \frac{dI(z,t)}{dt} + V(z+\Delta z,t) = 0$$

Simplify

(دالة الجهد في الموضع  $z$ )

phasor

$$-\frac{dV_s(z)}{dz} = (R + j\omega L) I_s(z) \quad \text{--- (1) Voltage wave equ.}$$

- KCL &  $I_{in} = I_{out}$  at node.

$$I(z,t) = I(z+\Delta z,t) + G\Delta z V(z+\Delta z,t) + C\Delta z \frac{dV(z+\Delta z,t)}{dt}$$

Simplify

phasor

$$-\frac{dI_s(z)}{dz} = (G + j\omega C) V_s(z) \quad \text{--- (2) Current wave equ.}$$

- To find  $V, I$ ?

derive equ (1) and substitute (2) in (1)

or derive equ (2) and substitute (1) in (2).

$$\Rightarrow -\frac{d^2 V_s(z)}{dz^2} = (R + j\omega L) \left( \frac{dI_s(z)}{dz} \right) \quad \text{equ (2)}$$

$$+ \frac{d^2 V_s(z)}{dz^2} = (R + j\omega L)(G + j\omega C) V_s(z)$$

Constant called  $\gamma^2$

$$\frac{d^2 V_s(z)}{dz^2} - \gamma^2 V_s(z) = 0 \rightarrow \text{T.L. equ.}$$

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

↳ Propagation Constant

$$\gamma = \alpha + j\beta$$

attenuation

Constant (NP/m)

phase constant

(rad/m)

$$1 \text{ NP} = 8.686 \text{ dB}$$

$$\frac{d^2 I_s(z)}{dz^2} - \gamma^2 I_s(z) = 0 \rightarrow \text{T.L. equ}$$

\* Solution to the T.L. equations -

$$\frac{d^2 V_s(z)}{dz^2} - \gamma^2 V_s(z) = 0$$

$$\text{let } m = \frac{d}{dz}$$

$$m^2 \cancel{V_s(z)} = \gamma^2 \cancel{V_s(z)} = 0$$

$$m^2 = \gamma^2 \quad (\text{real})$$

$$\text{Sol} \rightarrow \begin{matrix} e^{\gamma z} \\ e^{-\gamma z} \end{matrix}$$

$$V_S(z) = V_0^+ e^{-\gamma z} + V_0^- e^{+\gamma z}$$

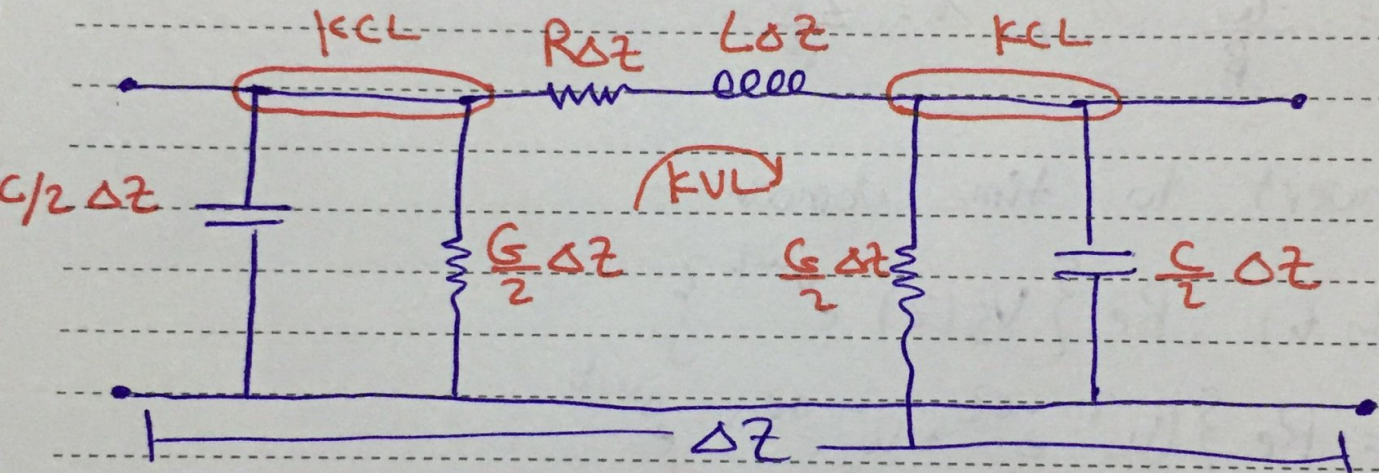
$$I_S(z) = I_0^+ e^{-\gamma z} + I_0^- e^{+\gamma z}$$

Forward  
 $\gamma$  s,  $\omega$ ! v/s  
 (+ve z-dir)

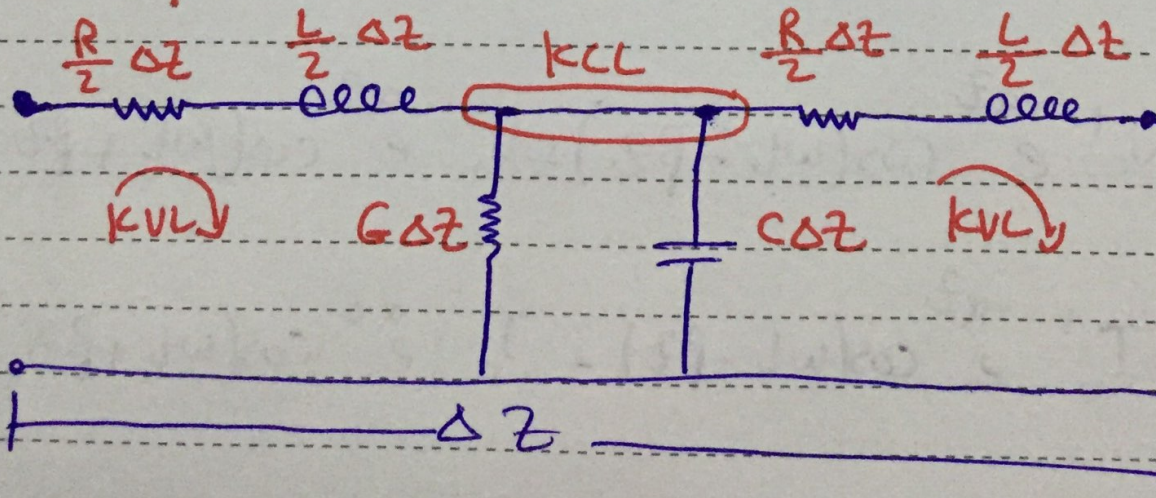
Backward  
 (-ve z-dir)

Backward and Forward  $\underline{v}$   $\rightarrow$   $\underline{i}$   $\rightarrow$   $\underline{p}$   $\rightarrow$   $\underline{s}$

\*  $\Pi$ -equ. ckt.



\*  $T$ -equ. ckt:-



- Voltage equ.

$$\frac{d^2 V_s(z)}{dz^2} - \gamma^2 V_s(z) = 0$$

Solution is

$$V_s(z) = \underbrace{V_0^+ e^{-\gamma z}}_{\text{Incident}} + \underbrace{V_0^- e^{\gamma z}}_{\text{Reflected}}$$

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)} = \alpha + j\beta$$

$$u = \frac{\omega}{\beta}, \quad \lambda = \frac{2\pi}{\beta}$$

Convert to time domain -

$$V(z, t) = \text{Re} \left\{ V_s(z) e^{j\omega t} \right\}$$
$$= \text{Re} \left\{ (V_0^+ e^{-\gamma z} + V_0^- e^{\gamma z}) e^{j\omega t} \right\}$$

$$= \text{Re} \left\{ V_0^+ e^{-\alpha z} e^{-j\beta z} e^{j\omega t} + V_0^- e^{\alpha z} e^{j\beta z} e^{j\omega t} \right\}$$

$$V(z, t) = V_0^+ e^{-\alpha z} \cos(\omega t - \beta z) + V_0^- e^{\alpha z} \cos(\omega t + \beta z)$$

$$I(z, t) = I_0^+ e^{-\alpha z} \cos(\omega t - \beta z) + I_0^- e^{\alpha z} \cos(\omega t + \beta z)$$

- define  $Z_0$ : characteristic impedance ( $\Omega$ )

$$Z_0 = \frac{V_0^+}{I_0^+} = \ominus \frac{V_0^-}{I_0^-}$$

+ve  $Z$  direction      -ve  $Z$  direction

$$Z_0 = \sqrt{\frac{(R + j\omega L)}{(G + j\omega C)}}$$

$$\left( \begin{array}{l} \rightarrow \\ \left[ I_0^+ = \frac{V_0^+}{Z_0} \right] \end{array} \right), \left( \begin{array}{l} \left[ I_0^- = \frac{V_0^-}{Z_0} \right] \end{array} \right)$$

- define  $\Gamma$ : reflection coefficient

$$\Gamma = \frac{\text{reflected signal}}{\text{Incident signal}} = \frac{V_0^-}{V_0^+}$$

$$V_0^- = \Gamma V_0^+$$

\*Note All the equations before are for

a Lossy T.L. Since  $(\alpha \neq 0)$   
 $(\epsilon \neq \infty)$

$(G \neq 0)$

## - Special Types of T.L. :-

$$\begin{aligned} \text{- Lossless T.L.} &\rightarrow \epsilon_c = \infty \rightarrow R = 0 \\ &\rightarrow \epsilon_d = 0 \rightarrow G = 0 \end{aligned}$$

$$R = 0 = G$$

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)} = \sqrt{-\omega^2 LC}$$

$$\gamma = j\omega \sqrt{LC} = \alpha + j\beta$$

$$\alpha = 0, \quad \beta = \omega \sqrt{LC}$$

$$Z_0 = \sqrt{\frac{L}{C}} = R_0 + jX_0$$

$$R_0 = \sqrt{\frac{L}{C}}, \quad X_0 = 0$$

$$u = \frac{\omega}{\beta}, \quad \lambda = \frac{2\pi}{\beta}$$

$$V(z, t) = V_0^+ \cos(\omega t - \beta z) + V_0^- \cos(\omega t + \beta z)$$

$$I(z, t) = \underbrace{\frac{V_0^+}{Z_0}}_{I_0^+} \cos(\omega t + \beta z) - \underbrace{\frac{V_0^-}{Z_0}}_{I_0^-} \cos(\omega t + \beta z)$$

- Distortionless T.L. :-

$$\boxed{\frac{R}{L} = \frac{G}{C}} \quad \text{شرط} \quad R \neq 0, G \neq 0$$

$$\gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

$$= \sqrt{R(1 + j\omega \frac{L}{R})G(1 + j\omega \frac{C}{G})}$$

$$= (1 + j\omega \frac{L}{R}) \sqrt{RG}$$

$$= \underbrace{\sqrt{RG}}_{\alpha \neq 0} + j\omega \frac{L}{R} \underbrace{\sqrt{RG}}_{\beta}$$

$$\beta = \omega \sqrt{\frac{L^2 RG}{R}}$$

$$= \omega \sqrt{\frac{LLG}{R}}$$

$$= \omega \sqrt{\frac{CLG}{G}}$$

$$\boxed{\beta = \omega \sqrt{LC}}$$

$$Z_0 = \frac{\sqrt{R(1 + j\omega \frac{L}{R})}}{\sqrt{G(1 + j\omega \frac{C}{G})}} = \sqrt{\frac{R}{G}} = \sqrt{\frac{L}{C}}$$

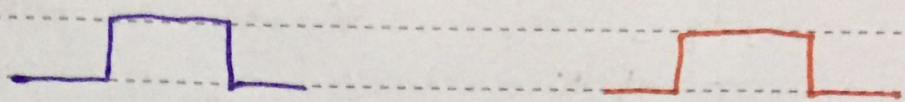
$$u = \frac{\omega}{\beta}, \quad \lambda = \frac{2\pi}{\beta}$$

$$V_s(z) = V_0^+ e^{-\alpha z} e^{-j\beta z} + V_0^- e^{\alpha z} e^{j\beta z} \quad (V)$$

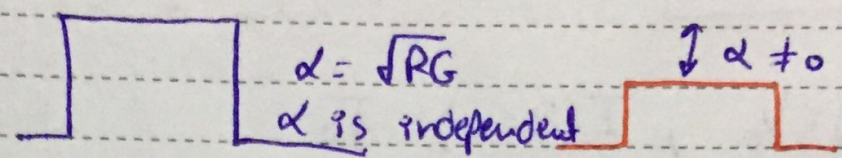


\*  $T_x$   $R_x$

Lossless



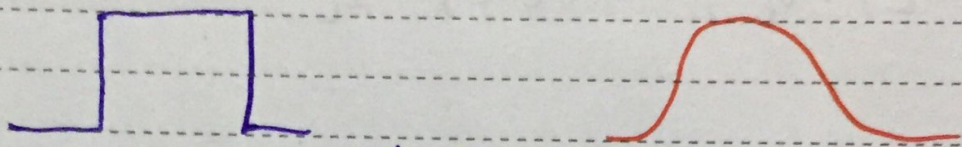
Distortionless



$\alpha = \sqrt{RG}$   
 $\alpha$  is independent  
 on  $(\omega)$

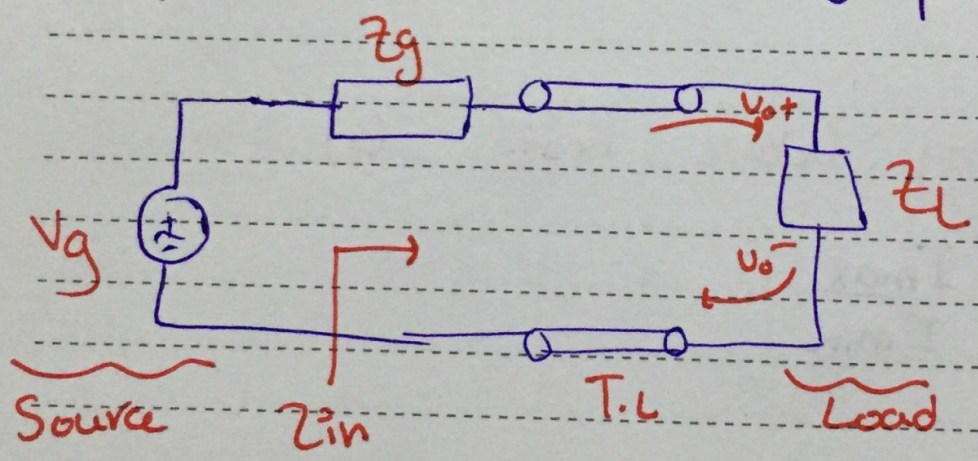
mag.  $\neq 1$

Lossy



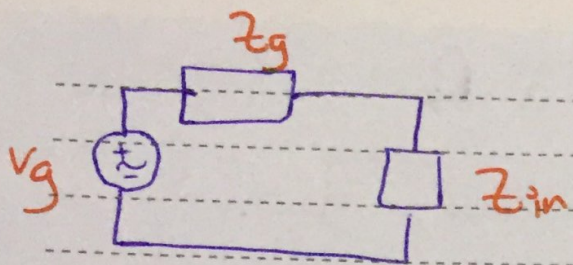
$\alpha$  is dependent  
 on  $(\omega)$

\* Input impedance, SWR and power



$Z_g$ : internal impedance of the src.

$$Z_{in} = \frac{Z_0 Z_L + Z_0 \tanh \gamma l}{Z_0 + Z_L \tanh \gamma l} \rightarrow \text{Lossy and distortionless T.L.}$$



$V_0, I_0 \rightarrow$  عند ادخال Line

$V_L, I_L \rightarrow$  عند اخراج Line

$$V(z=0) = V_0, \quad I(z=0) = I_0$$

$$V(z=L) = V_L, \quad I(z=L) = I_L$$

$$V_0 = V_g \frac{Z_{in}}{Z_{in} + Z_g} \quad (\text{Voltage division})$$

$$I_0 = \frac{V_g}{Z_g + Z_{in}} \quad (\text{Ohm's Law})$$

- SWR & Standing Wave Ratio (s)

$$S = \frac{V_{max}}{V_{min}} = \frac{I_{max}}{I_{min}}$$

$$S = \frac{|V_0^+| + |V_0^-|}{|V_0^+| - |V_0^-|}$$

divide by  $|V_0^+|$

$$S = \frac{1 + \left| \frac{V_0^-}{V_0^+} \right|}{1 - \left| \frac{V_0^-}{V_0^+} \right|}$$

$$|P| = \frac{|V_0^-|}{|V_0^+|}$$

$$S = \frac{1 + |\Gamma|}{1 - |\Gamma|} \rightarrow |\Gamma| = \frac{S - 1}{S + 1} \rightarrow \text{mag. only}$$

$$\star \Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} \quad \text{if } Z_L \neq Z_0$$

↓  
reflection coefficient at the load.

$$\text{if } Z_g \neq Z_0 \rightarrow \Gamma_g = \frac{Z_g - Z_0}{Z_g + Z_0}$$

- to cancel (P)  $\rightarrow Z_L = Z_0, Z_g = Z_0$   
(matched T.L.)  
(max power transfer)

\* Power

$$\text{Power} = \frac{1}{2} \text{Re} \left\{ \underset{\substack{\downarrow \\ \text{Peak}}}{V_s} * \underset{\substack{\downarrow \\ \text{Peak}}}{I_s} \right\} \text{Conjugate} \quad (\omega)$$

$$V_{\text{rms}} = \frac{V_{\text{peak}}}{\sqrt{2}}$$

- For lossless T.L.

$$V_s(z) = V_0^+ e^{-j\beta z} + \Gamma V_0^+ e^{+j\beta z}$$

$$\star I_s(z) = \frac{V_0^+}{Z_0} e^{+j\beta z} - \Gamma \frac{V_0^-}{Z_0} e^{-j\beta z}$$

$$P = \frac{|V_o|^2}{2Z_0} (1 - |\Gamma_L|^2)$$

$P_r$

$$P_t = P_i - P_r$$

→ if  $P_r = 0 \rightarrow P_t = P_i$   
(max power transfer)

$$P_t = \frac{|V_o|^2}{2Z_0} \quad (\text{Max power transfer occurs when } Z_L = Z_0)$$

\*  $Z_{in \text{ s.c.}} = jZ_0 \tan(\beta l)$  (if lossless)

Short  
circuit

$Z_{in \text{ o.c.}} = -jZ_0 \cot(\beta l)$  (if lossless)

open  
circuit

$S = \infty, \Gamma_{L \text{ s.c.}} = -1 = 1 \angle 180^\circ$

$\Gamma_{L \text{ o.c.}} = 1 = 1 \angle 0^\circ$

$$Z_0 = \sqrt{Z_{in \text{ s.c.}} * Z_{in \text{ o.c.}}}$$

$$Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$$

المكان لغاية 11.4 بالتوفيق