# LO6 Practical Operational Amplifiers Op-Amps 2

Chapter 14

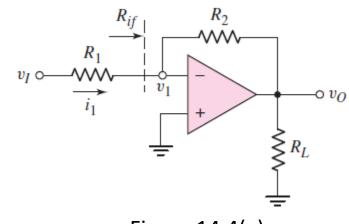
Nonideal Effects in Operational Amplifier

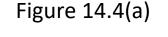
CircuitsDonald A. Neamen (2009). Microelectronics: Circuit Analysis and Design,

4th Edition, Mc-Graw-Hill

Prepared by: Dr. Hani Jamleh, School of Engineering, The University of Jordan

- The closed-loop input resistance  $R_{if}$  of the inverting amplifier is defined in Figure 14.4(a).
  - It includes the effect of feedback.
- The equivalent circuit includes:
  - 1. Finite open-loop gain  $A_{OL}$ ,
  - 2. Finite open-loop input differential resistance  $R_i$ ,
  - 3. Nonzero output resistance  $R_o$ .





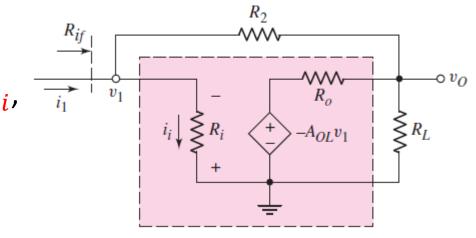
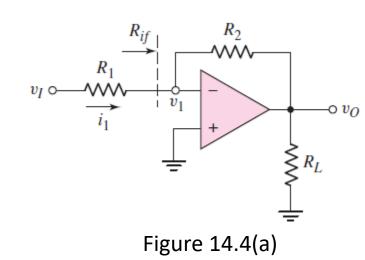


Figure 14.4(b)

- A KCL1 equation at the output node yields:  $\frac{v_0}{R_L} + \frac{v_0 - (-A_{OL}v_1)}{R_0} + \frac{v_0 - v_1}{R_2} = 0$
- Solving for the output voltage, we have:

$$v_{O} = \frac{-v_{1} \left(\frac{A_{OL}}{R_{o}} - \frac{1}{R_{2}}\right)}{\frac{1}{R_{L}} + \frac{1}{R_{o}} + \frac{1}{R_{2}}}$$

• A second **KCL2** equation at the input node yields:  $i_1 = \frac{v_1}{R_2} + \frac{v_1 - v_0}{R_2}$ 



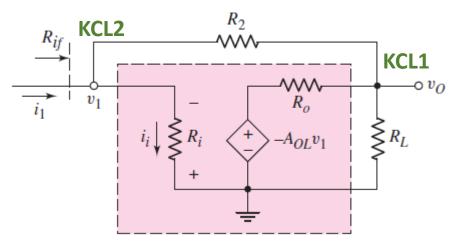
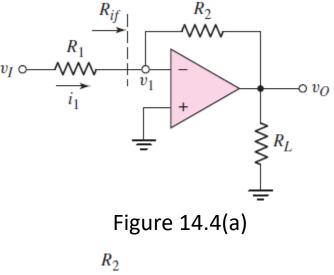


Figure 14.4(b)

• Combining the following two equations:

$$v_{0} = \frac{-v_{1}\left(\frac{R_{0L}}{R_{0}} - \frac{1}{R_{2}}\right)}{\frac{1}{\frac{R_{L}}{R_{1}} + \frac{1}{\frac{R_{0}}{r_{1}} + \frac{1}{\frac{R_{0}}{r_{2}} - \frac{1}{v_{0}}}}}{i_{1} = \frac{\frac{v_{1}}{R_{i}} + \frac{v_{1}}{\frac{v_{1}}{r_{2}} - \frac{v_{0}}{r_{0}}}}{R_{2}}}$$

and rearranging terms produces:  $\frac{i_1}{v_1} = \frac{1}{R_{if}} = \frac{1}{R_i} + \frac{1}{R_2} \frac{\left(1 + A_{OL} + \frac{R_o}{R_L}\right)}{1 + \frac{R_o}{R_L} + \frac{R_o}{R_2}}$ 



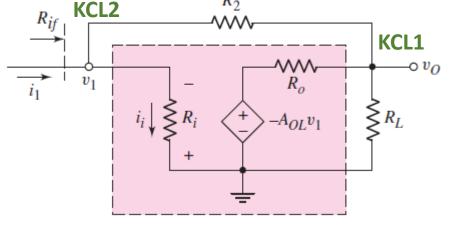


Figure 14.4(b)

$$\frac{i_1}{v_1} = \frac{1}{R_{if}} = \frac{1}{R_i} + \frac{1}{R_2} \frac{\left(1 + A_{OL} + \frac{R_o}{R_L}\right)}{1 + \frac{R_o}{R_L} + \frac{R_o}{R_2}}$$

- $v_{I} \circ \underbrace{\overset{R_{if}}{\underset{i_{1}}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}}{\overset{v}}{\overset{v}}{\overset{v}}{\overset{v}}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}}{\overset{v}{\overset{v}}{\overset{v}}}{\overset{v}{\overset{v}}{\overset{v}}{\overset{v}}{\overset{v}}{\overset{v}}{\overset{v}}{\overset{v}}}$ 
  - Figure 14.4(a)

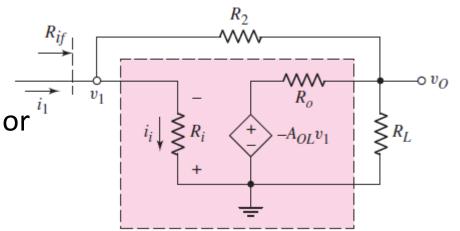


Figure 14.4(b)

- The equation above describes the closed-loop input resistance  $R_{if}$  of the inverting amplifier, with:
  - 1. Finite open-loop gain  $A_{OL}$ ,
  - 2. Finite open-loop input resistance  $R_i$ , and
  - 3. Nonzero output resistance  $R_o$ .
- In the limit as  $A_{OL} \to \infty$ , we see that  $1/R_{if} \to \infty$ , or  $R_{if} \to 0$ .
  - Which means that  $v_1 \rightarrow 0$ , or  $v_1$  is at virtual ground.
- This is a characteristic of an ideal inverting op-amp.

- Consider an inverting amplifier with a feedback resistor  $R_2 = 10k\Omega$ , and an opamp with parameters  $A_{OL} = 10^5$  and  $R_i = 10k\Omega$ .
- Assume the output resistance  $R_o$  of the op-amp is negligible, e.g.  $R_o \rightarrow 0$ .
- Determine the closed-loop input resistance at the inverting terminal of an inverting amplifier.

• Solution: If 
$$R_o = 0$$
, then:  

$$\frac{1}{R_{if}} = \frac{1}{R_i} + \frac{1}{R_2} \frac{\left(1 + A_{OL} + \frac{R_o}{R_L}\right)}{1 + \frac{R_o}{R} + \frac{R_o}{R_0}} = \frac{1}{R_i} + \frac{1 + A_{OL}}{R_2} = \frac{1}{10^4} + \frac{1 + 10^5}{10^4} \approx 10^{-4} + 10$$

• The closed-loop input resistance is then  $R_{if} \approx 0.1\Omega$ . Comments:

 $R_{if}$  of the inverting amplifier is a very strong function of the finite open-loop gain  $A_{OL}$ .

*R<sub>i</sub>* essentially does not affect the closed-loop input Medical Electronics - Dr. Hani Jamleh - JU

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 $\overrightarrow{i_1} \quad \overrightarrow{v_1} \quad \overrightarrow{i_i} \neq \overrightarrow{R_i} \quad \overrightarrow{+} \quad -A_{OL}v_1 \quad \overrightarrow{R_L} \quad$ 

- A nonzero  $R_{if}$  and a finite  $R_i$  implies that:
  - The signal current into the op-amp is not zero, as assumed in the ideal case.
- From Figure 14.4(b), we see that:

$$v_1 = i_1 R_{if}$$

• Therefore:

$$i_i = \frac{v_1}{R_i} = i_1 \left(\frac{R_{if}}{R_i}\right)$$

- The fraction of input signal current shunted away from  $R_2$  and into the op-amp is  $(R_{if}/R_i)$ .
- From the previous example, the fraction is:

$$\frac{R_{if}}{R_i} = \frac{0.1}{10k} = 10^{-5}!$$

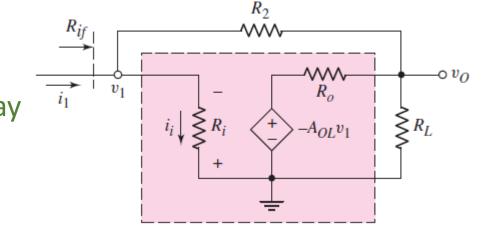
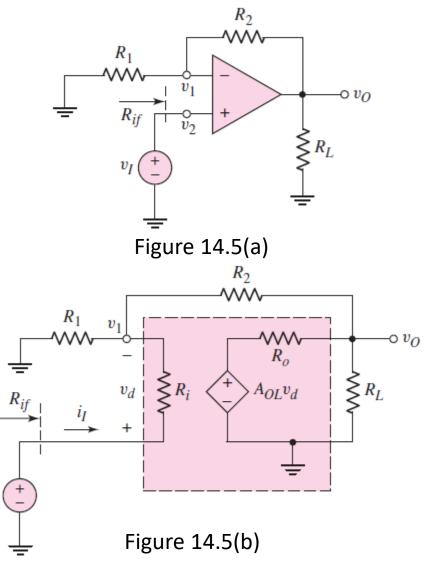


Figure 14.4(b)

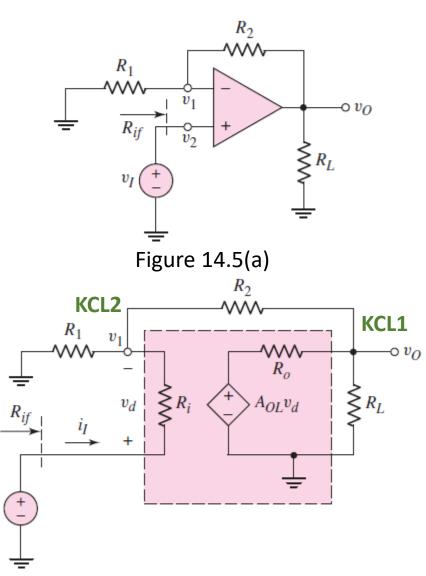
- The input resistance seen by the signal source is designated  $R_{if}$ .
- The equivalent circuit includes:
  - 1. Finite open-loop gain  $A_{OL}$ ,
  - 2. Finite open-loop input differential resistance  $R_i$ ,
  - 3. Non-zero output resistance  $R_o$ .



- Writing a KCL1 equation at the output node:  $\frac{v_0}{R_L} + \frac{v_0 - A_{0L}v_d}{R_0} + \frac{v_0 - v_1}{R_2} = 0$
- Solving for the output voltage, we have:

$$v_{O} = \frac{\frac{v_{1}}{R_{2}} + \frac{A_{OL}v_{d}}{R_{o}}}{\frac{1}{R_{L}} + \frac{1}{R_{o}} + \frac{1}{R_{2}}}$$

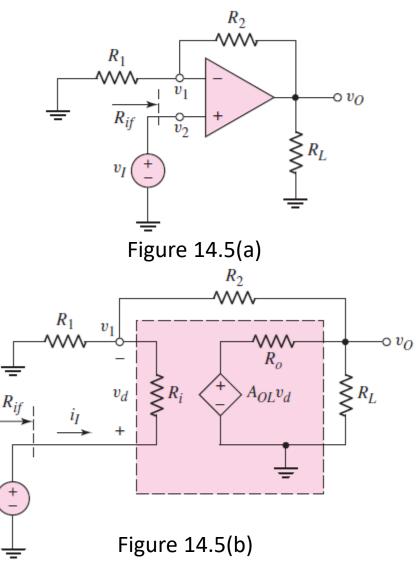
• Another KCL2 equation at the  $v_1$  node yields:  $i_I = \frac{v_1}{R_1} + \frac{v_1 - v_0}{R_2}$ 



• After substituting equations, we find that  $R_{if}$  can be written in the form:

$$R_{if} = \frac{v_I}{i_I} = \frac{R_i(1 + A_{OL}) + R_2\left(1 + \frac{R_i}{R_1}\right)}{1 + \frac{R_2}{R_1}}$$

- In the limit as  $A_{OL} \to \infty$ , or as the  $R_i \to \infty$ , we see that  $R_{if} \to \infty$ .
  - Which is a property of the ideal noninverting amplifier.



- Consider an op-amp with an open-loop gain of  $A_{OL} = 10^5$  and an input resistance of  $R_i = 10k\Omega$  in a noninverting amplifier configuration with resistor values of  $R_1 = R_2 = 10k\Omega$ .
- Determine the closed-loop input resistance at the noninverting terminal of a noninverting amplifier.
- Solution: The input resistance is:

• 
$$R_{if} = \frac{v_I}{i_I} = \frac{R_i(1+A_{OL}) + R_2\left(1 + \frac{R_i}{R_1}\right)}{1 + \frac{R_2}{R_1}} = \frac{10k(1+10^5) + 10k\left(1 + \frac{10k}{10k}\right)}{1 + \frac{10k}{10k}} \approx 500M\Omega$$

 $R_{if} \approx 500 M \Omega$ 

- Comments:
  - As expected, the closed-loop input resistance of the noninverting amplifier is very large.
  - Equation:

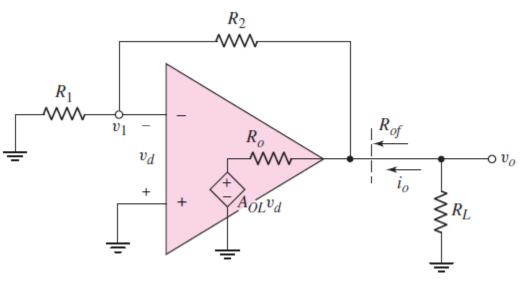
$$R_{if} = \frac{v_I}{i_I} = \frac{R_i(1 + A_{OL}) + R_2\left(1 + \frac{R_i}{R_1}\right)}{1 + \frac{R_2}{R_1}}$$

shows that  $R_{if}$  is dominated by the term  $R_i(\bar{1} + A_{OL})$ .

• The combination of a large  $R_i$  and large  $A_{OL}$  produces an extremely large input resistance, as predicted by ideal feedback theory.

- Since the ideal op-amp has a *zero* output resistance
  - The output voltage is independent of the load impedance.
  - The op-amp acts as an ideal voltage source and there is no loading effect.
- An actual op-amp circuit has a *nonzero*  $R_o$ , which means that:
  - The output voltage and the closed-loop gain are function of the load impedance  $R_L$ .

- Figure 14.6 is the equivalent circuit of both an inverting and noninverting amplifier and is used to find  $R_o$ .
- The op-amp has:
  - 1. Finite open-loop gain  $A_{OL}$ ,
  - 2. Nonzero output resistance  $R_o$ , and
  - 3. An infinite input resistance  $R_i$ .
- To determine *R*<sub>o</sub>:
  - We set the independent input voltages equal to zero.



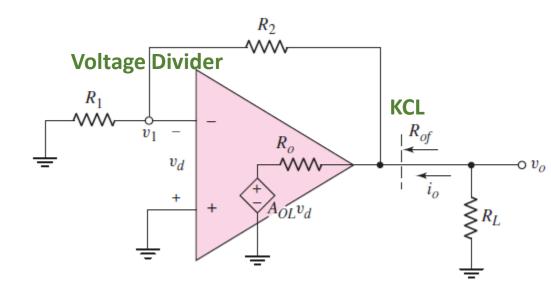


- A KCL equation at the output node yields:  $i_o = \frac{v_o - A_{OL}v_d}{R_o} + \frac{v_o}{R_1 + R_2}$
- The differential input voltage is:  $v_d = v_2 v_1 = -v_1$
- But by voltage divider technique:

$$v_1 = \left(\frac{R_1}{R_1 + R_2}\right) v_o$$
$$v_d = -\left(\frac{R_1}{R_1 + R_2}\right) v_o$$

• Combining the two Equations above, we have:

$$i_{o} = \frac{v_{o}}{R_{o}} - \frac{A_{OL}}{R_{o}} \left[ -\left(\frac{R_{1}}{R_{1} + R_{2}}\right) v_{o} \right] + \left(\frac{v_{o}}{R_{1} + R_{2}}\right) \\ \frac{i_{o}}{v_{o}} = \frac{1}{R_{of}} = \frac{1}{R_{o}} \left[ 1 + \frac{A_{OL}}{1 + R_{2}/R_{1}} \right] + \left(\frac{1}{R_{1} + R_{2}}\right)$$





$$\frac{i_o}{v_o} = \frac{1}{R_{of}} = \frac{1}{R_o} \left[ 1 + \frac{A_{OL}}{1 + R_2/R_1} \right] + \left( \frac{1}{R_1 + R_2} \right)$$
• Since  $R_o$  is normally small and  $A_{OL}$  is   
normally large, the Equation above, to a good approximation, is as follows:  
$$\frac{1}{R_{of}} \approx \frac{1}{R_o} \left[ \frac{A_{OL}}{1 + R_2/R_1} \right]$$
Figure 14.6

$$\frac{1}{R_{of}} \approx \frac{1}{R_o} \left[ \frac{A_{OL}}{1 + R_2/R_1} \right]$$

#### • Comments:

- In most op-amp circuits, the open-loop output resistance  $R_o$  is on the order of  $100\Omega$ .
- Since  $A_{OL}$  is normally much larger than  $(1 + R_2/R_1)$ , the  $R_{of}$  can be very small.
- *R*<sub>of</sub> values in the *milliohm* range are easily attained using opamps.

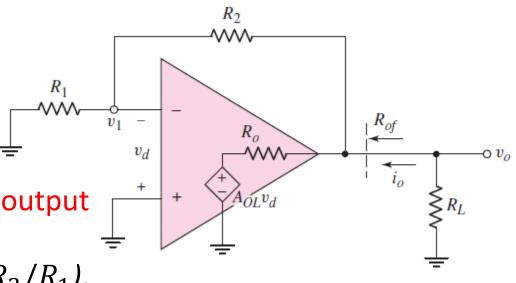


Figure 14.6

- **Objective**: **Determine** the output resistance of an op-amp circuit  $R_{of}$ .
- **Computer Simulation Solution**: Figure 14.7 shows an inverting amplifier circuit with a standard 741 op-amp.

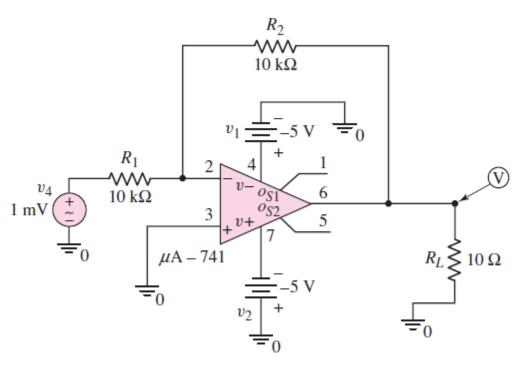
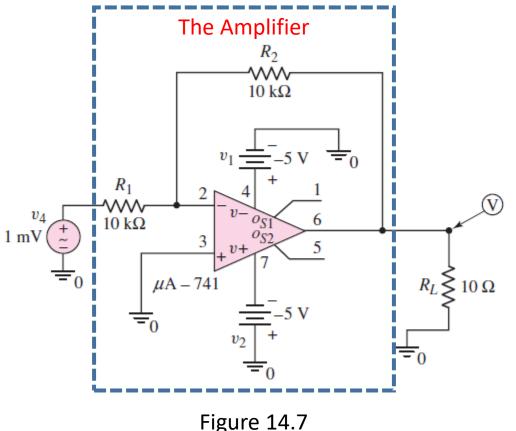


Figure 14.7

# How the Output Resistance of an Opamp Circuit is Measured?

- One method of determining the output resistance is:
  - Measure the output voltage for two different values of load resistance connected to the output, i.e.  $R_{L1}$  and  $R_{L2}$
  - Then, treating the amplifier as a Thevenin equivalent circuit with: a fixed source in series with an output resistance.

$$\boldsymbol{V_{o1}} = A_{v} V_{i} \left( \frac{\boldsymbol{R_{L1}}}{\boldsymbol{R_{L1}} + \boldsymbol{R_{of}}} \right)$$
$$\boldsymbol{V_{o2}} = A_{v} V_{i} \left( \frac{\boldsymbol{R_{L2}}}{\boldsymbol{R_{L2}} + \boldsymbol{R_{of}}} \right)$$



# How the Output Resistance of an Opamp Circuit is Measured?

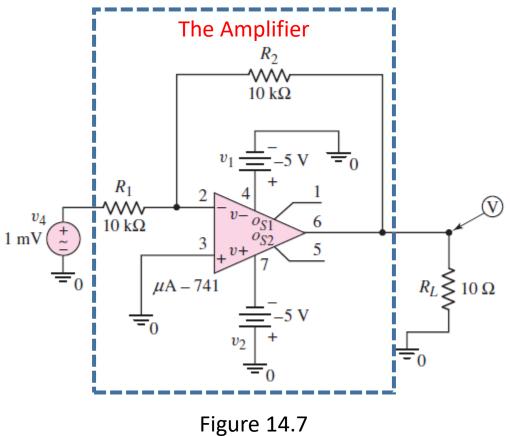
$$\boldsymbol{V_{o1}} = A_{v} V_{i} \left( \frac{\boldsymbol{R_{L1}}}{\boldsymbol{R_{L1}} + \boldsymbol{R_{of}}} \right)$$
$$\boldsymbol{V_{o2}} = A_{v} V_{i} \left( \frac{\boldsymbol{R_{L2}}}{\boldsymbol{R_{L2}} + \boldsymbol{R_{of}}} \right)$$

• Let:

$$\frac{V_{o1}}{V_{o2}} = \left(\frac{R_{L1}}{R_{L1} + R_{of}}\right) \left(\frac{R_{L2} + R_{of}}{R_{L2}}\right)$$

• Then:

$$R_{of} = \frac{R_{L1}R_{L2}\left(1 - \frac{V_{o1}}{V_{o2}}\right)}{R_{L2}\left(\frac{V_{o1}}{V_{o2}}\right) - R_{L1}}$$

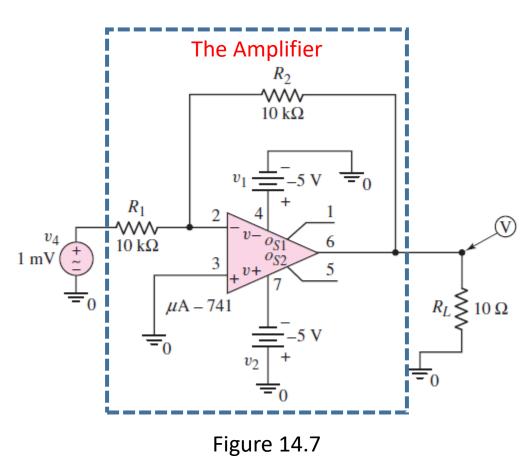


- A 1*mV* signal was applied.
  - For a  $10\Omega\,$  load, the output voltage is 0.999837 mV, and
  - For a  $20\Omega$  load, the output voltage is 0.9999132 mV.

$$R_{of} = \frac{R_{L1}R_{L2}\left(1 - \frac{V_{o1}}{V_{o2}}\right)}{R_{L2}\left(\frac{V_{o1}}{V_{o2}}\right) - R_{L1}}$$
$$= \frac{10 \cdot 20\left(1 - \frac{0.999837 m}{0.9999132 m}\right)}{20\left(\frac{0.9999837 m}{0.9999132 m}\right) - 10}$$

• This gives an output resistance of:

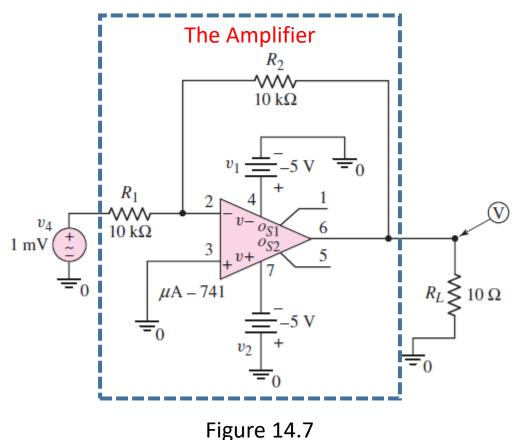
$$R_{of} = 1.53 \ m\Omega$$



$$R_{of} = 1.53 \ m\Omega$$

#### • Comments:

- As mentioned, the output resistance of a voltage amplifier with negative feedback can be very small.
- The ideal output resistance is *zero*, but a practical op-amp circuit can have an output resistance in the *milliohm* range.



# Do it yourself

• Solve all the Exercise Problems as well as the Test Your Understanding Questions.