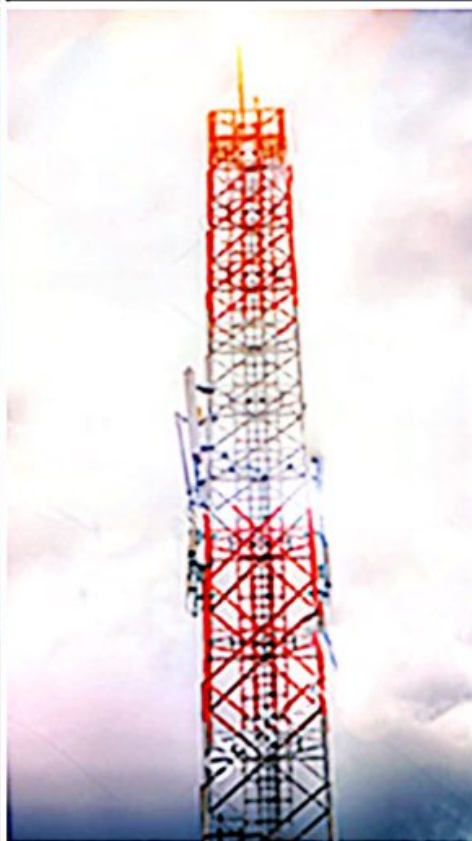


# COMMUNICATIONS CIRCUITS

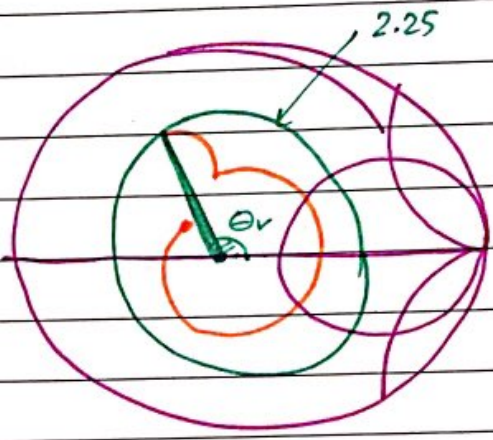
DR. JAMMAL RAHHAL  
BY: ANOUD AL-HALLAQ



POWERUNIT-JU.COM



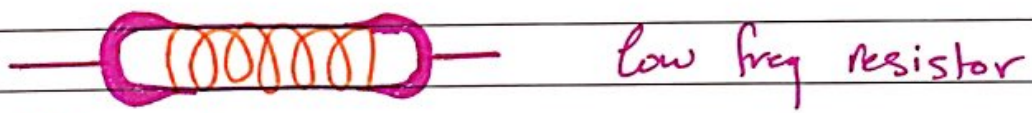
Component that we use  $\rightarrow$  R, L, C  
 $\rightarrow$  Transistor



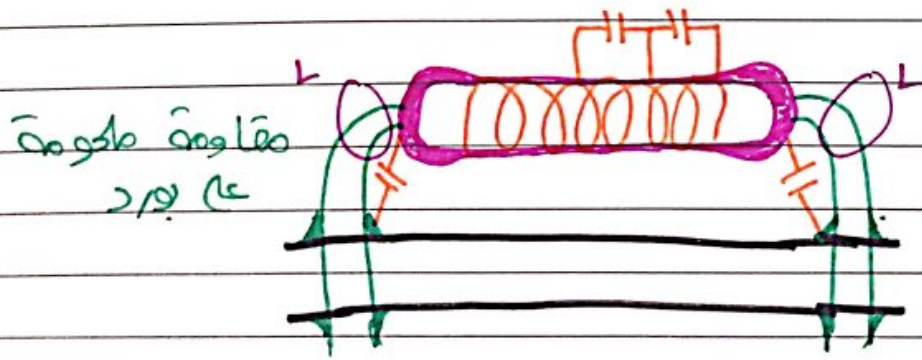
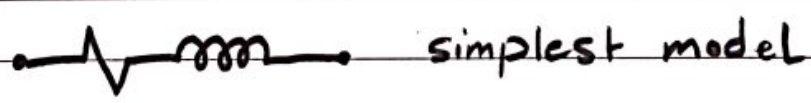
$\Gamma = |\Gamma| \angle \theta_r$

- System  $\rightarrow$  Amplifier
- $\rightarrow$  Mixer
- $\rightarrow$  Filters
- $\rightarrow$  oscillators.

\* R :-



دستور العمل ساده است  
 بهر حال.

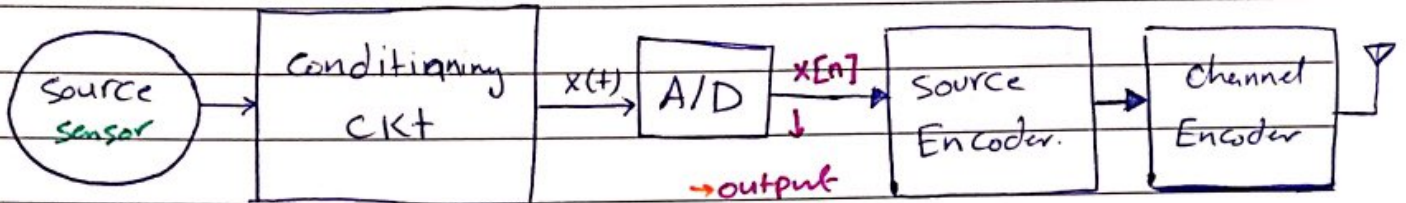


\* Spiral بين (فقدان) في (C).  
\* في drop volt في عنى capacitance

\* preterpation analysis

\* للزيم اجل لا design (preterpation)  $\epsilon$   $\lambda$   $\mu$  اعرف اذا  
ص، على تغيرات يكون System عنى ص (J)  $\mu$ .

\* potential barrier  $\rightarrow$  كايير في فرق بين volt  
between 2 material.



$x(t) \rightarrow$  signal electrical

$\rightarrow$  output digital signal (1/0)  
 $\rightarrow$  binary

A/D  $\rightarrow$  fine quantizer

- $\rightarrow$  Base band signal.  $\leftarrow$  loss det $\hat{e}$ n:  $\leq 1$
- $\rightarrow$  Source Encoder  $\rightarrow$  Compression.
- $\rightarrow$  freq  $\rightarrow$  something repeated it self

$\lambda f = u$  (propagation speed).

$\lambda \uparrow$  in low freq.

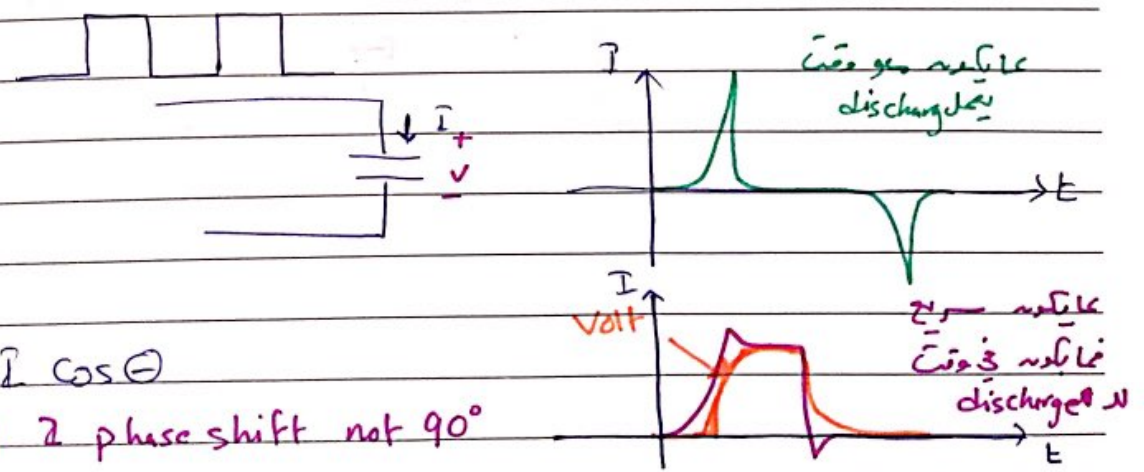
$\rightarrow \lambda \gg$  size of component  $\Rightarrow$  low freq Model.  
 $R, C \rightarrow$  pure

$\left[ \begin{matrix} 1:50 \\ 1:100 \end{matrix} \right] \Rightarrow \lambda \sim >$  size ~~component~~

$\rightarrow \lambda \sim$  size (compared)  $\Rightarrow$  high freq Model  
 physical path  $\leftarrow$   $\lambda$   $\sim$  size of component

\*  $\lambda$   $\sim$  size of component low freq system  $\lambda$   $\gg$  size of component \*

100 Mbps  $\rightarrow$  square signal.



$P = VI \cos \theta$

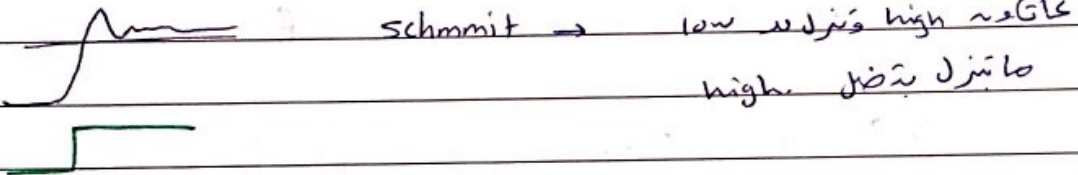
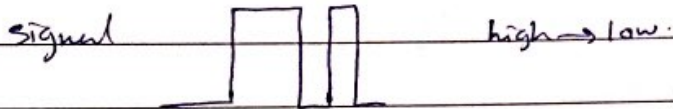
[3] \*  $V$  and  $I$  phase shift not  $90^\circ$

$$P_{\text{heat}} \propto f^2$$



~~Schmitt trigger~~  
Schmitt trigger

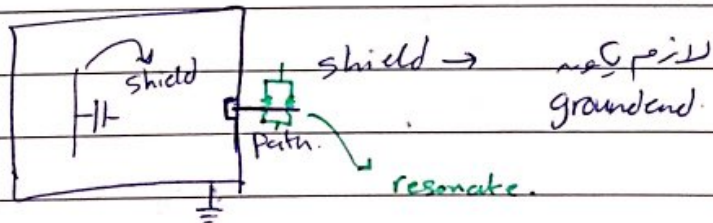
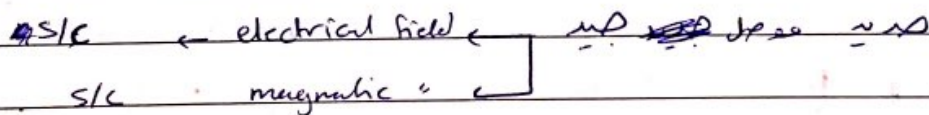
noise margin  $\rightarrow$  ( 0.8 - 3.6 )

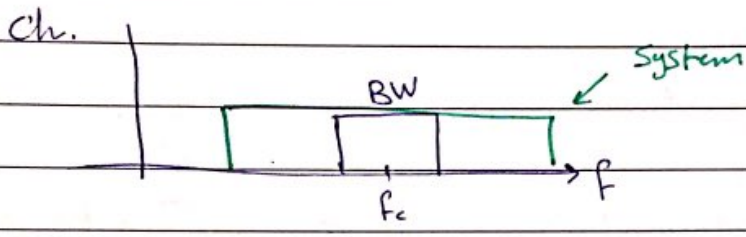
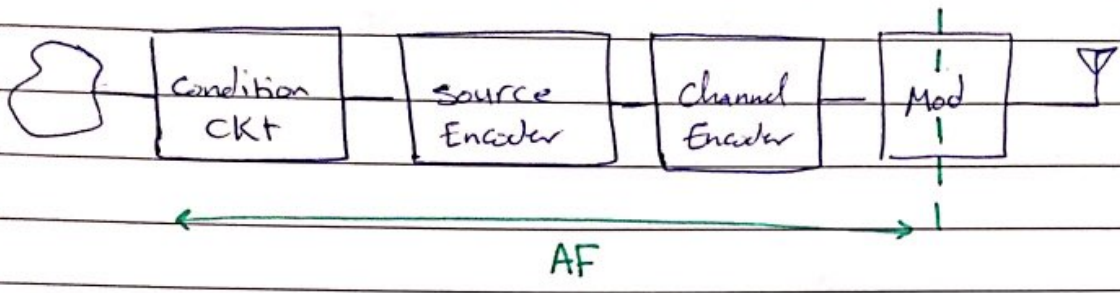


$\rightarrow$  Clock speed eye  $\rightarrow$  120 msec ( 8 frame / sec )

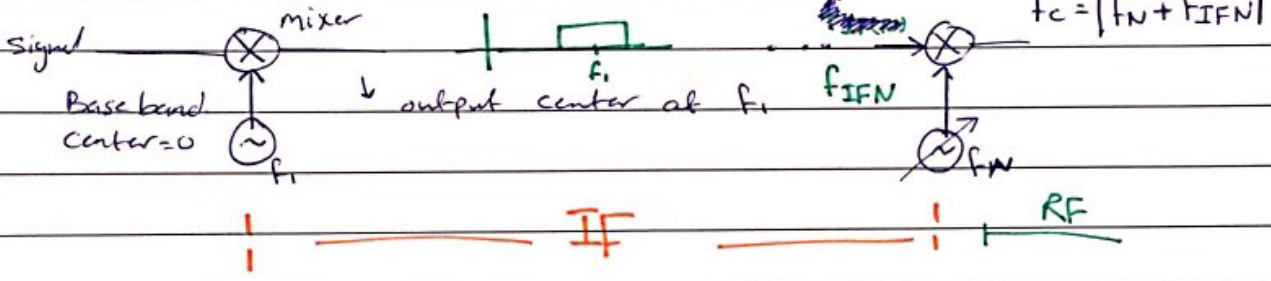
$\rightarrow$  clock speed ear  $\rightarrow$  50 Hz

$\rightarrow$  heat  $\rightarrow$  noise



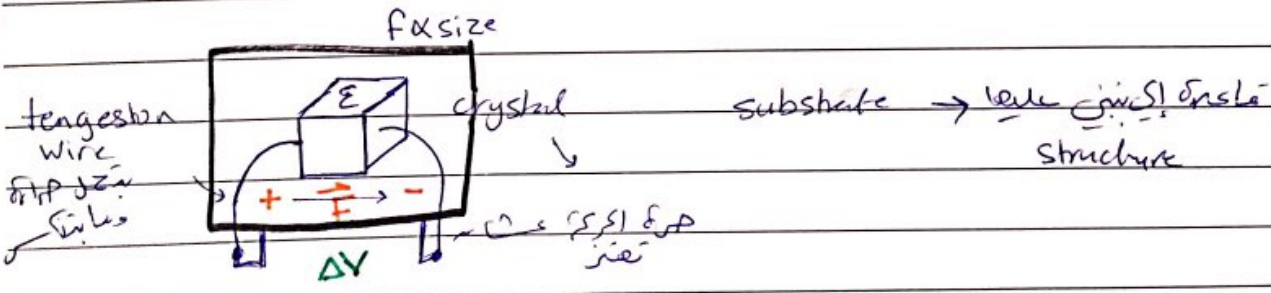


Modulator:



Phase locked loop

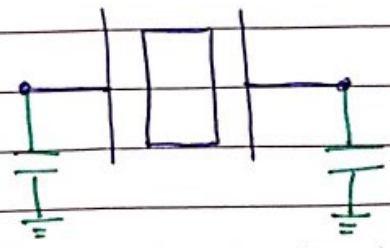
OSC with feedback → ~~oscillator~~. ① Stable due to temperature.  
↳ physical quantity



➔ damping → equivalent of Q ↓ → error. hence!

oscillation → ~~oscillation~~   
 current → AC current.

\* temperature compensation.  
2Cap ← to ~~compensate~~

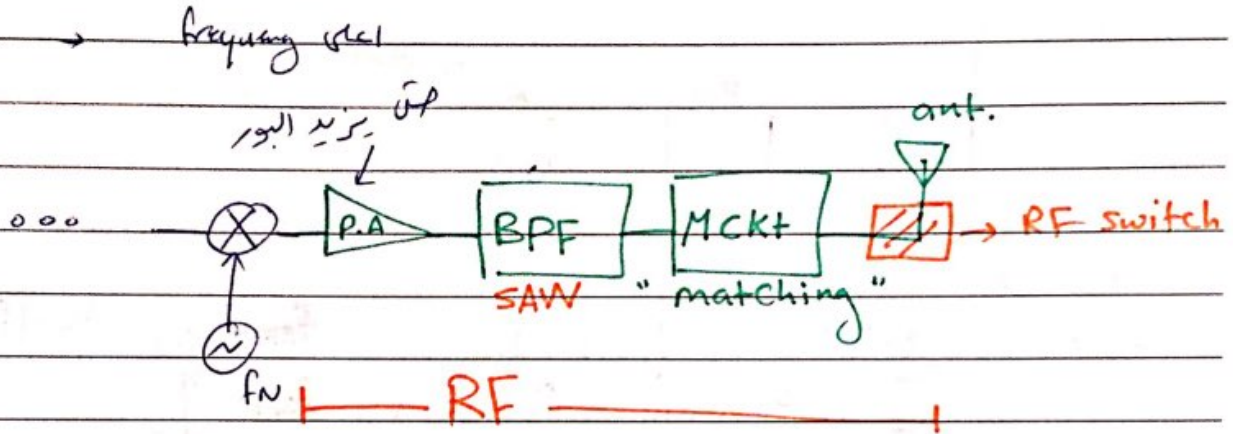


5

Crystal → . 160 ...

\* Junction temp

\* RF stage → تردد موجة الجانج التردد  
antenna



Harmonic lipap ← linear ~ 56 | si \*

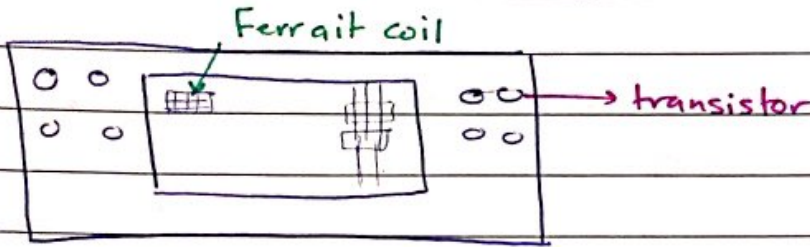
\* tunable Bandpass → big issue

\* matching ckt → directional coupler.  
↳ feed back system

\* Reverse direction → isolation. (self interference).

⇒ Magnetic memory :-

transistor → drivers → memory



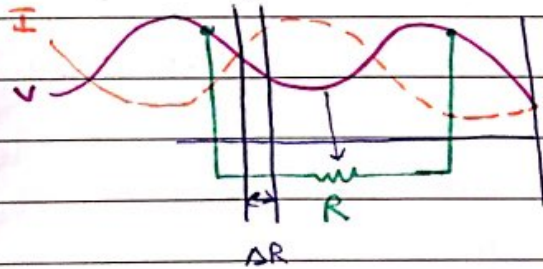
\* Power supply →  $f = 0$ .

⇒ RF → high frequency - on 1 KHZ not high freq.

⇒  $\lambda \gg$  Component  $\Rightarrow$  Component  $\neq$   $\lambda$  (not a lumped element)

⇒ lumped component →  $\lambda <$  Component.

standing wave.



↳ lumped element.

~~Handwritten scribbles and crossed-out text.~~

⇒ diode → nonlinear.

in high freq → different type of diode. (pin diode)  
 cost,  $L_0$ ,  $Q$  ←  $\mu s$  glass  $\rightarrow L_0$  → capacitance  $\mu b$



at low freq → component use as lumped ~~element~~ elements.

transistor is a switch

### HW #1:

How to use capacitance as inductor?!

↳ using stub

## Basic Components:

⇒ RF Modeling of Basic Component :-

### \* R :-

$$R = \frac{l}{\sigma S}$$

$S = \text{physical area}$   
 $\sigma = \text{conductivity}$

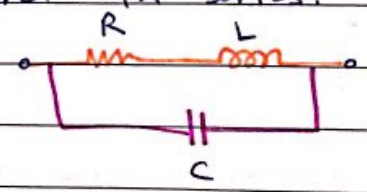
$R, L, C$   
 $\sigma, \mu, \epsilon$

↳ not in series

$C \Rightarrow \text{drop voltage} \rightarrow \text{electric field (+, -)}$   
(capacitance)

$$C = \frac{\epsilon S}{d}$$

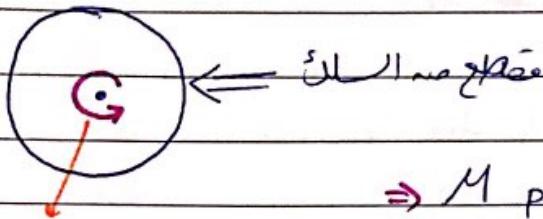
$$L = \frac{\mu l n}{S}$$



⇒ graphene ⇒ shield JFET

→ use a super conductor





magnetic field

⇒  $M$  permeability → كل شيء يتحرك في اتجاه

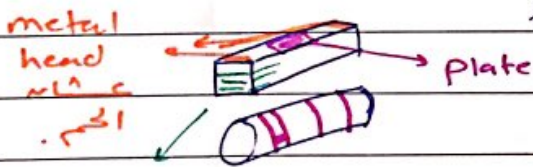
⇒ ferro magnetic material →  $M_r$  high

⇒ dia magnetic material → لا يتحرك مثل الماء

⇒ Inductance  $\Rightarrow$  تخزين التيار  $\Rightarrow$  اذا قضيت التيار  
Capacitance  $\Rightarrow$  تخزين الجهد



▷  $R$  \* كل شيء يتسبب في  $R$  material block of material.



trinch  $\Rightarrow$  spiral. leads

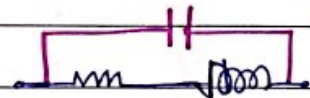
6-8 layers

Low freq.

high freq.

$R \rightarrow LC$   $\Rightarrow$   $R$

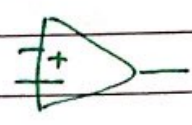
$R$



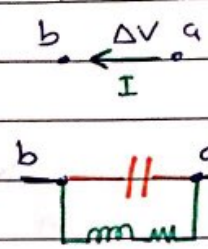
Power dissipation  $\leftarrow R$   $\Rightarrow$   $P$  \*  $R$

~~Capacitors Using Inductance~~

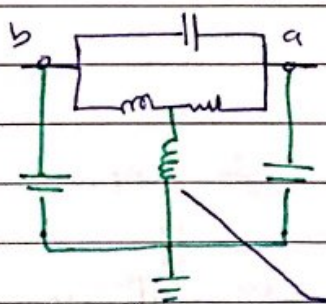
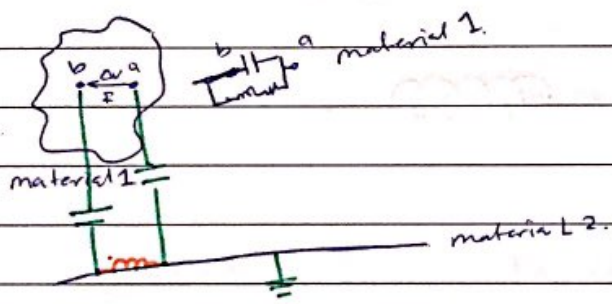
H.W. we use 2 op-amp to change the phase shift and use capacitance as inductance.



Capacitance  $\leftarrow \frac{\Delta V}{I}$  is  
 Inductor  $\leftarrow \frac{I}{\Delta V}$  is



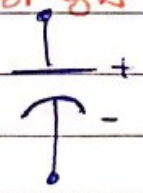
\* L in series with R.



mutual inductance between 2 material.

اذا كان في R في طرفه على لول اوله من قوه c و I ولازم اعزل  
 \* اذا كان في L اعزل لول لايم ← في Count it

\* Capacitor 8.1



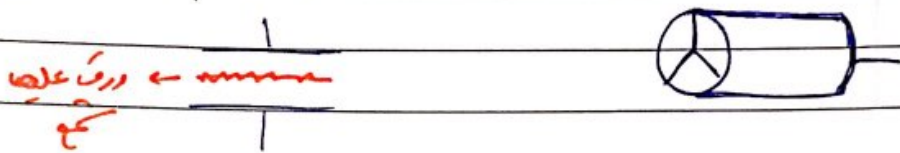
$ES \quad \uparrow C \rightarrow \uparrow E$

« في لول بين 2 parallel plate »

have weak point.

$\uparrow I \rightarrow I^2 R \uparrow \rightarrow \text{temp} \uparrow \rightarrow C$

power supply circuit  $\rightarrow$  use these capacitor. connect in parallel.



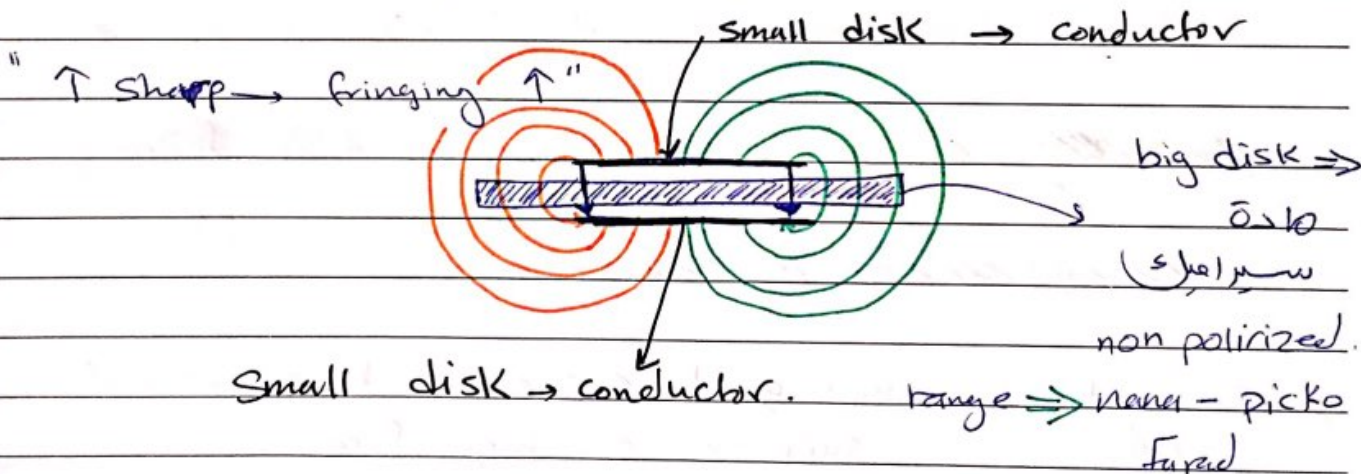
$E \uparrow \rightarrow$  more free electrons.

↓  
electric field  
↓  
electric field

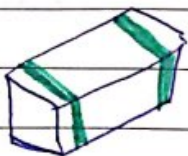
different btw Battery and Capacitor  $\Rightarrow E$

$\uparrow$  Voltage  $\rightarrow$   $\uparrow$  electric field strength  $\rightarrow$   $\uparrow$  force

- Capacitor ckt use  $\rightarrow$  not stored energy.
- $\rightarrow$  implement filter.
- $\rightarrow$  transfer function btw input and output
- $\rightarrow$  non polarized capacitor.

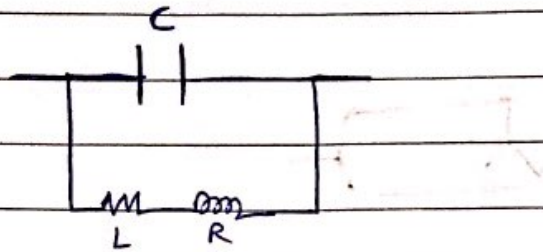


Survive ~~more~~ months

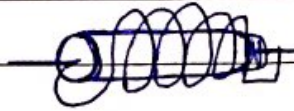


size  $\Rightarrow$  1.2 cm  $\rightarrow$  1mm  
range



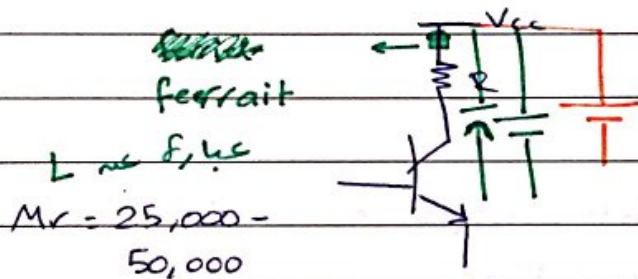


right rod  
M ↑



↑  $M_r$  → Compress the size

transistor work on 1G.



high freq. is  $\infty$  impedance of  $\mu p i$  \*

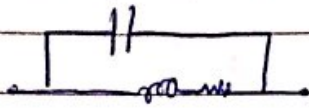
~~electrolytic capacitor~~ capacitor ~~to suppress~~ at high frequency

~~to suppress~~ spark

\* electro light  $\rightarrow$  not good capacitor to shunt out.   
 vide suppress on high freq.

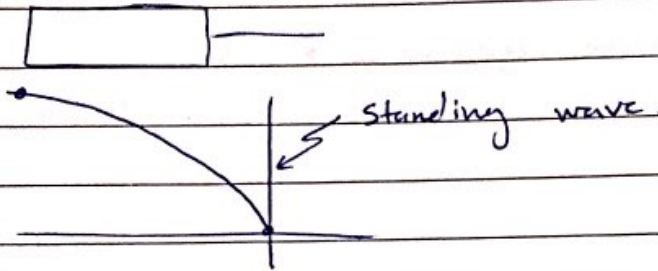
non polarized capacitor.

non polarized capacitor.

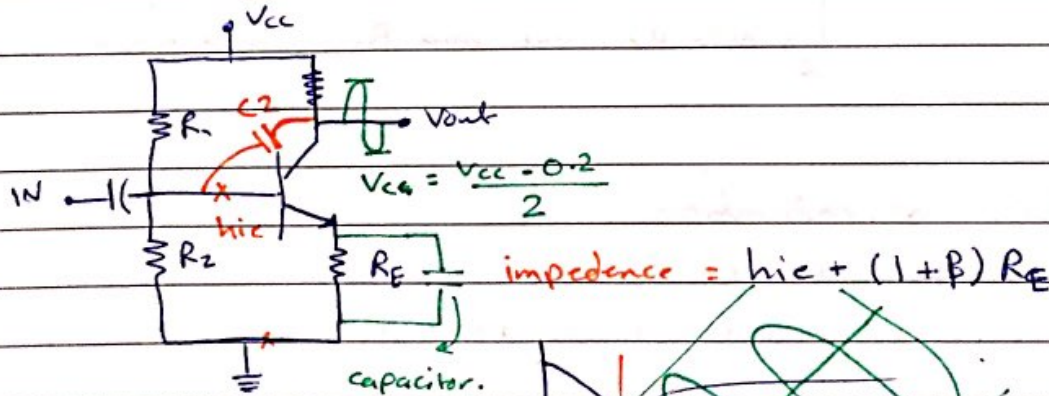
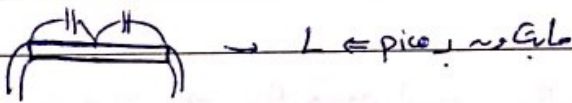


$\lambda = 3m$

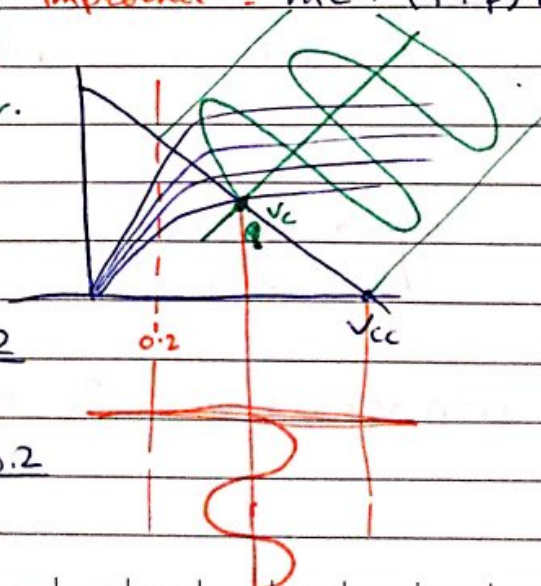
every  $\lambda/2 \rightarrow$  inverts



if current or voltage no ref.  $\rightarrow$  get in circuit



$Q = \frac{1}{3} V_{cc}$



$V_{cc} - I_c R_c = \frac{V_{cc} - 0.2}{2}$

$V_{cc} - (\beta I_b) R_c = \frac{V_{cc} - 0.2}{2}$

$$\text{Gain} = \frac{-h_{fe} R_c}{h_{ie} + (1+h_{fe})R_c} \quad (h_{fe} = \beta)$$

for AC

Find H module for transistor ?! ← HW2 \*

shunt capacitor → increase gain →  $R_c = 0$ .  
on  $R_E$

$$G = \frac{-h_{fe} R_c}{h_{ie}}$$

Sweep → freq (from  $f_i \rightarrow f_c$ )  
→ value

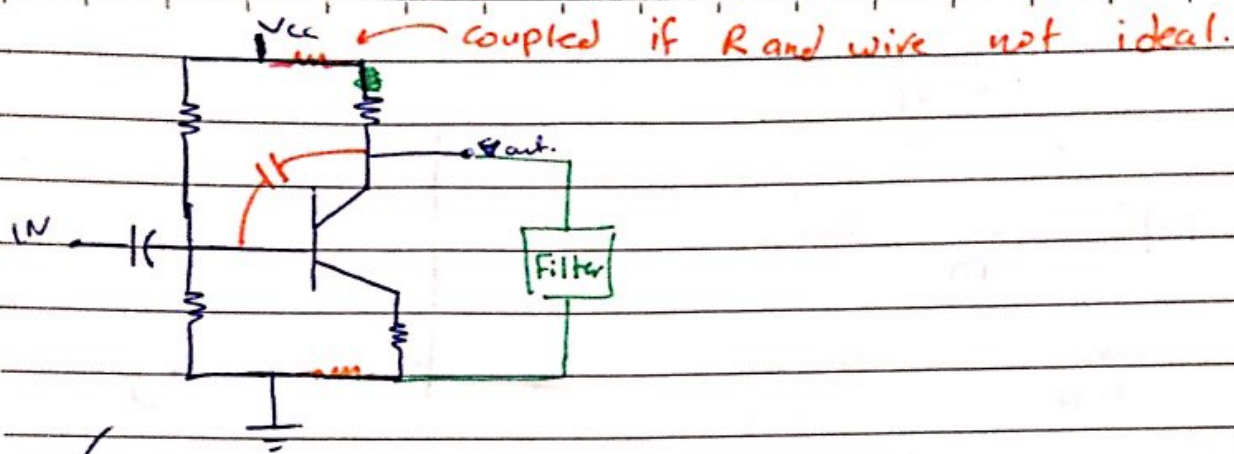
extrem cases. 1 → min  $R_c$  and max  $R_c \rightarrow$  min gain.  
2 → min  $R_E$  and max  $R_c \rightarrow$  max gain.

Inductor → radiation

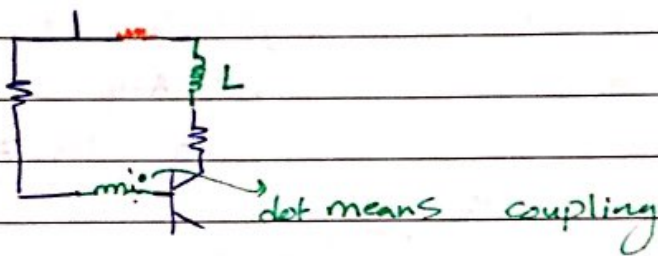
mutual inductance → \*  
cap → signal → induct → signal → \*

Capacitor 2 → path.  
→ oscillation.

filter ⇒ response between  $f_i$  and  $f_c$ .



to isolate  $V_{cc} \Rightarrow$  use inductor  $L$

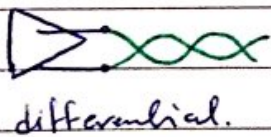
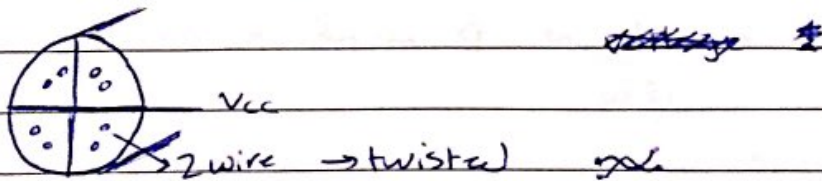


Inductors

↳ use under control environment

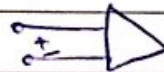
unshielded better than shielded in out door.

Ethernet cable.



differential.

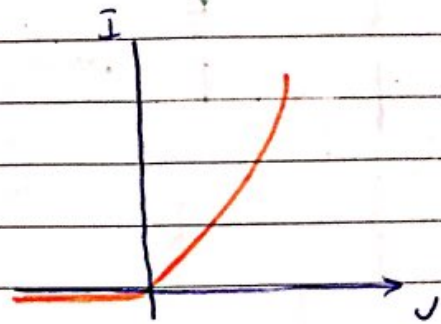
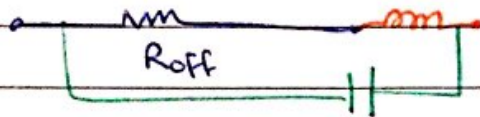
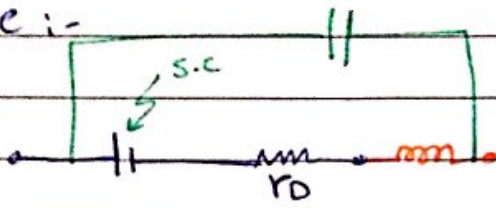
at Rx



limit for voltage  
Xserch Line driver ?!



\* Diode :-



سیرس N, P بی جلا ہے \*  
 سیرس سیرس سیرس سیرس

\* 30 Amp → 6mm - 10mm

$$\left[ \frac{30}{1.6} \right] = \sqrt{\frac{18.75}{\pi}}$$

current density → (A/mm<sup>2</sup>) ← AC current

radius = 2.4 mm

diameter = 5 mm

area =  $\pi r^2$

heat =  $i^2 R$

\* سیرس N, P بی جلا ہے سیرس سیرس سیرس سیرس

rated current 1A → IN 400 7 700 volt direction.  
 5 → use for power supply ckt  
 3

Peak volt = 380V

→ In Reverse :-

\* ↑ current → ↑ temperature → ↓ break down voltage  
 ↳ capacitor ↑

\* dont use in high freq → capacitor ↑ in Reverse. [16]

~~Inductance and capacitance~~

Inductance is related to  $I_{dc}$  \*  
 capacitance is related to drop volt

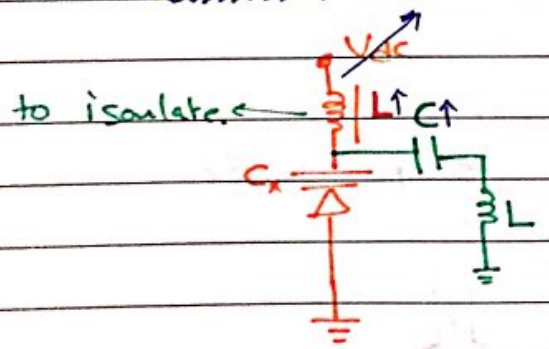
low current  $\rightarrow$  junction area small.

- $\Rightarrow$  diode IN448  $\Rightarrow$  use in communication.ckt
- $\rightarrow$  high freq = 1 GHz.
- $\rightarrow$  break down = 50-60V  
voltage
- $\rightarrow$   $I_{dc}$   $\rightarrow$   $C_j$

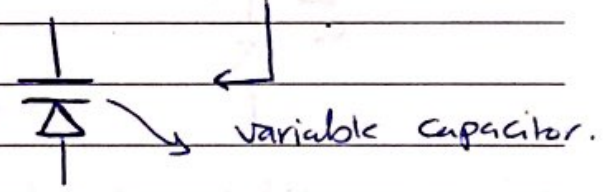
$\rightarrow$   $I_{dc}$   $\rightarrow$   $C_j \rightarrow$  diode not capacitor.  
 $\rightarrow$   $R_{eff} \uparrow$

In Reverse  $\rightarrow$   $R_{eff}$  كبيرة  $\rightarrow$   $C_j$  كبيرة

~~Inductance~~



Reverse bias. for this diode.  
 Volt = 15-30 V



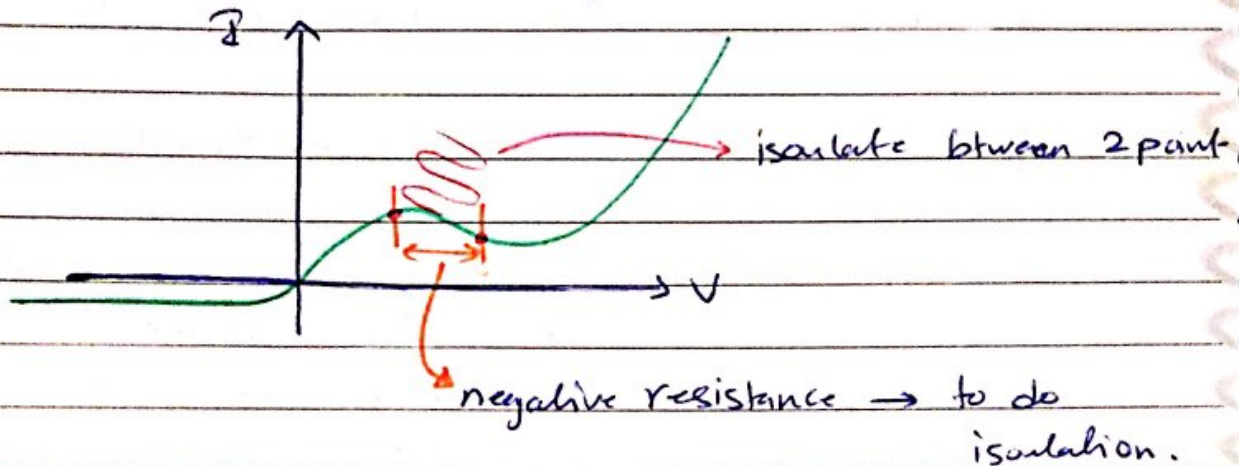
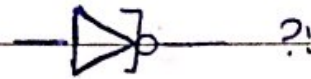
$C \Rightarrow$  to prevent dc volt in this path.

~~Inductance~~

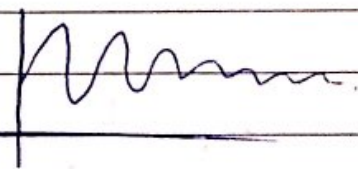
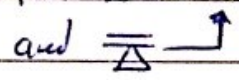
$L \rightarrow$  Resonance.

\*  $I_{dc}$   $\rightarrow$  doping  $\rightarrow$   $I_{dc}$

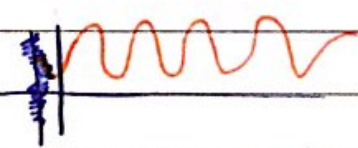
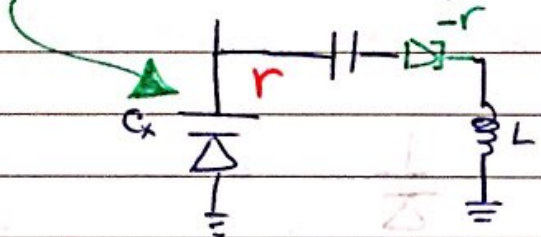
# \* Tunnel diode



in  $L \rightarrow$  internal resistance.

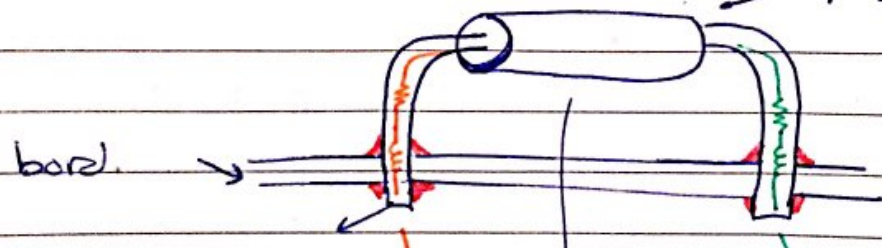


Resistance in loop = 0.  $\rightarrow$  ~~res~~



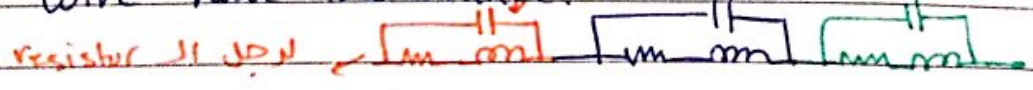
HW  $\rightarrow$  look like negative resistance impedance ckt.

Resistance.

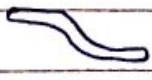


board.

wire have inductance.



legs  $\rightarrow$  smooth.



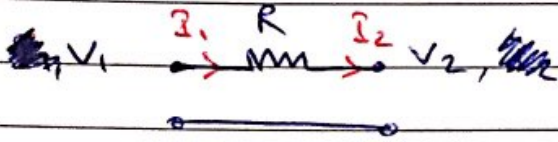
$L \rightarrow j\omega L$  (mutual inductance  $\angle$ )



$L \rightarrow j\omega L$   $\theta = 90^\circ$

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ I_2 \end{bmatrix}$$

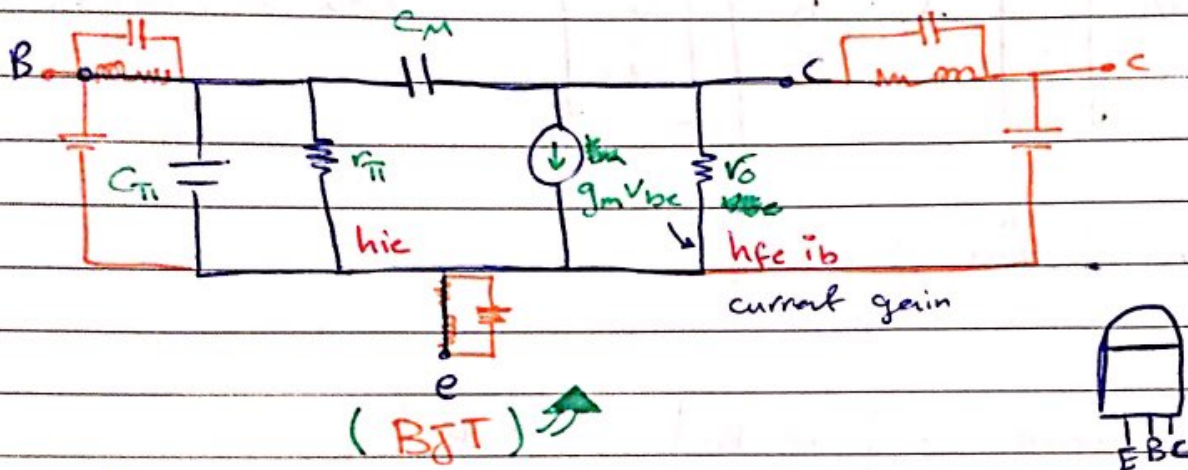
ABCD Model



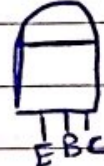
\* In series  $\rightarrow$   $\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & R \\ 0 & 1 \end{bmatrix}$

\* In parallel  $\rightarrow$   $\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ \frac{1}{R} & 1 \end{bmatrix}$

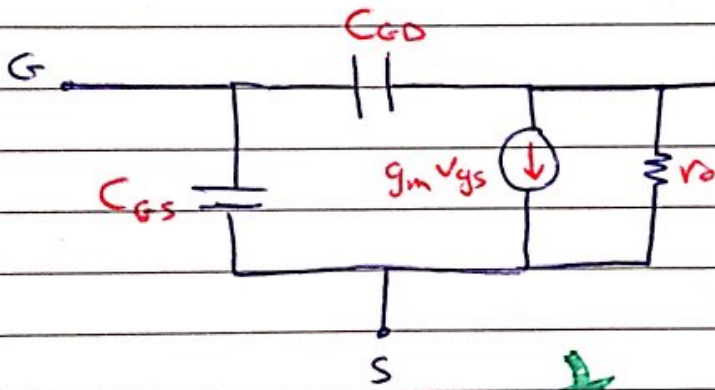
# H.F Transistor Model:-



(BJT)

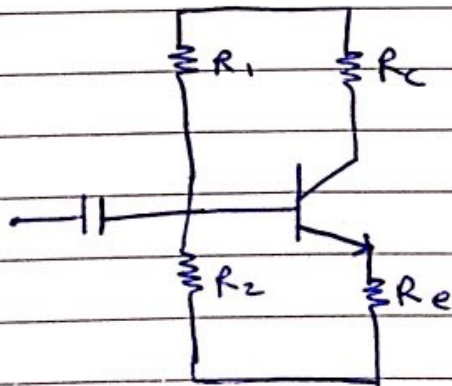


at low freq  $\Rightarrow$  (capacitors  $\Rightarrow$  open) \*  $g_m V_{be}$  current as a function of voltage.



(MOSFET)

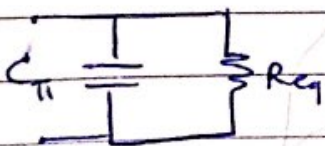
\*  $h_{fe} i_b \Rightarrow$  current as a function of ~~voltage~~ current.



DC Bias  $\Rightarrow$

$$V_c \approx \frac{1}{2} (V_{cc} - 0.2)$$

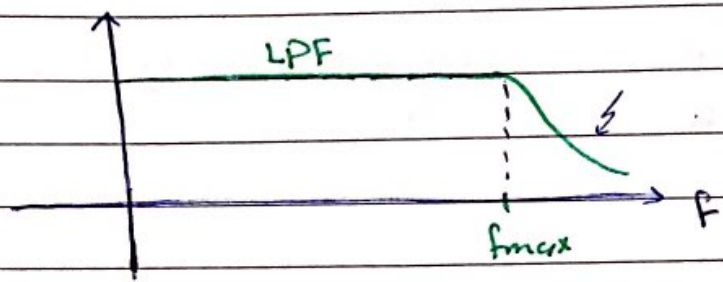
Saturation Voltage.



low side terminal  
ground terminal.

$\rightarrow$  low pass circuit.

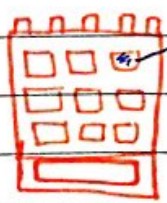
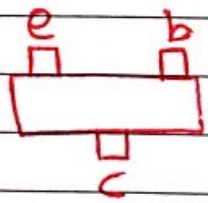
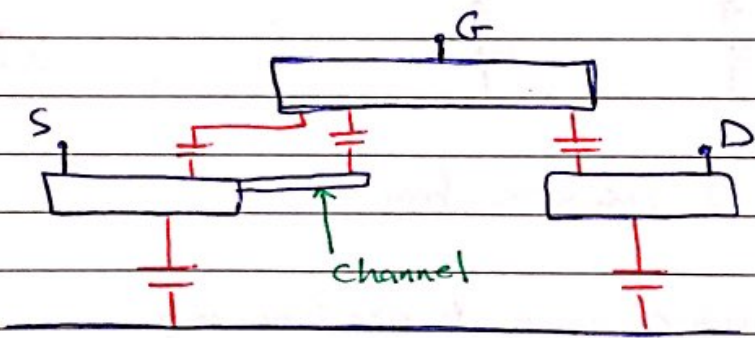
at low freq  $\rightarrow$  low pass filter.



the circuit can't amplify at high frequency.

$$g_m V_{be} = h_{fe} \cdot i_b = g_m i_b r_{\pi}$$

$$h_{fe} = r_{\pi} g_m$$



150K

stray capacitance  $\downarrow$  self inductance.  $\leftarrow$   $r_{ol} \ll r_{os}; G_{os}$

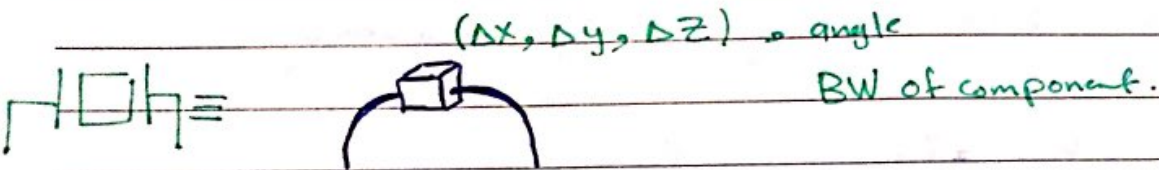
30 mill btw 2 leg  
1 mill = 1/1000 Inch



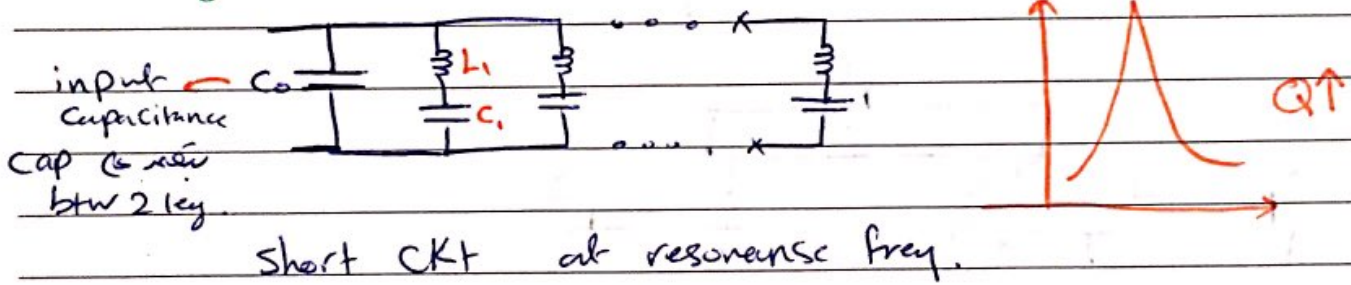
## Home work 2:

what are the characteristics of gallium arsenide transistor ?!

### \* Crystal s.d

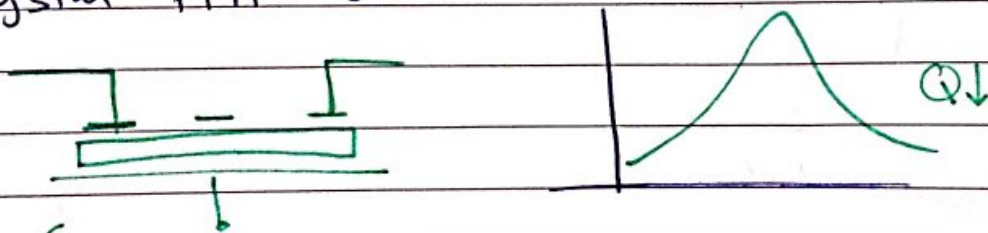


using as oscillator :-

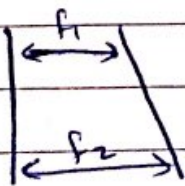


as reference oscillator → use at one frequency.

### \* Crystal Filter s.d



as Band Pass filter. ( $Q \downarrow$ ) not sharp.



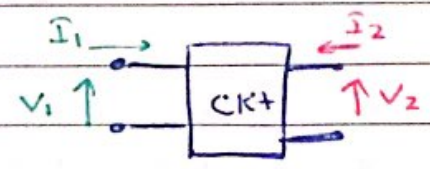
Quid Draw equivalent high freq model. ?!

equi model  $\leftarrow \dots I, C, R$  is not

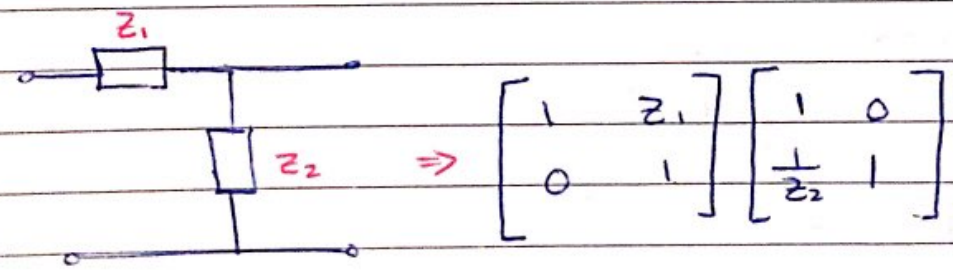
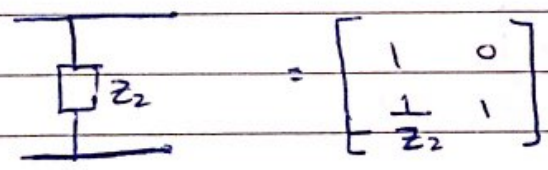
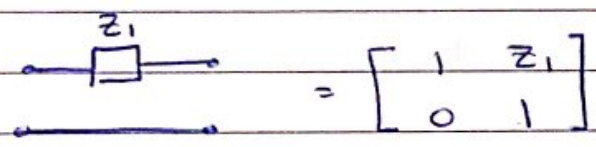
\* High freq  $\rightarrow$  Lowfreq  $\Rightarrow$  Cap/Ind circuit

2-port network.

$$Z = \begin{bmatrix} A & B \\ C & D \end{bmatrix}$$



$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = Z \begin{bmatrix} V_2 \\ I_2 \end{bmatrix}$$



$$= \begin{bmatrix} 1 + \frac{Z_1}{Z_2} & Z_1 \\ \frac{1}{Z_2} & 1 \end{bmatrix}$$

$$A \cdot B \neq B \cdot A$$



$$\text{transfer function} = \frac{1}{A}$$

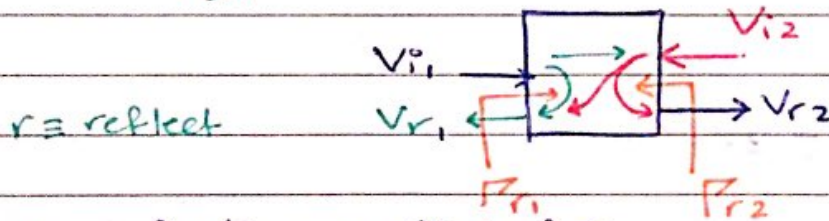
$$V_1 = AV_2 + B I_2$$

$$I_1 = C V_2 + D I_2$$

$$\frac{V_1}{I_1} = \left( \frac{AV_2 + B I_2}{C V_2 + D I_2} \right) / I_2$$

$$\frac{V_1}{I_1} = \frac{A Z_0 + B}{C Z_0 + D}$$

→ V (incident wave.)  
E, H  
V, I



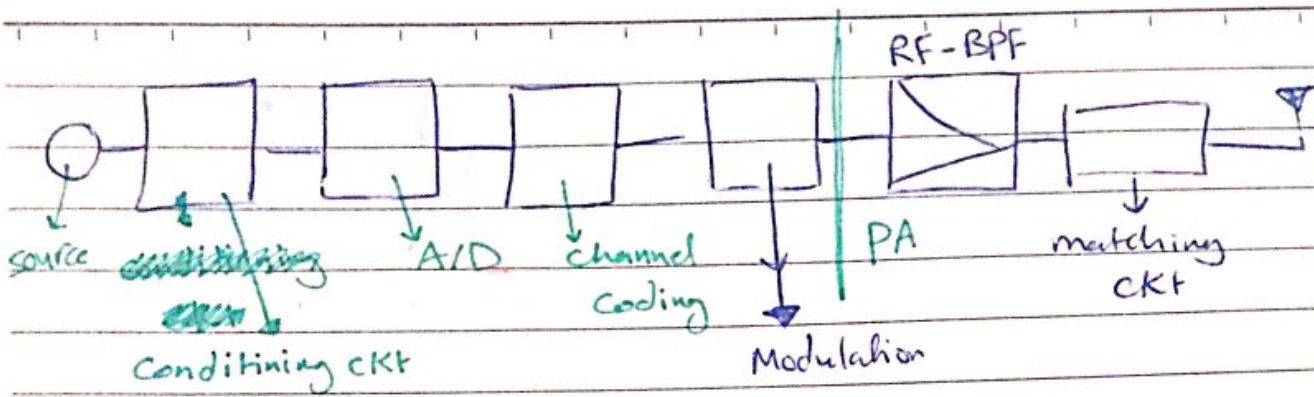
\* reflection coefficient  $\Gamma$

$$\Gamma_{r1} = \frac{V_{r1}}{V_{i1}}$$

$$\Gamma_{r2} = \frac{V_{r2}}{V_{i2}}$$

$$\Gamma = \frac{Z_2 - Z_1}{Z_2 + Z_1}$$

PA = power amplifier → (انتقال قوت الی انتاج) 0.5m ↓



## S Matrix

$$S = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}$$

$$\begin{bmatrix} V_{r1} \\ V_{r2} \end{bmatrix} = S \begin{bmatrix} V_{i1} \\ V_{i2} \end{bmatrix}$$

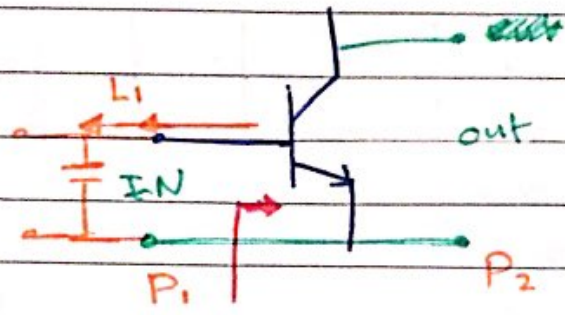
$$V_{r1} = S_{11} V_{i1} + S_{12} V_{i2}$$

$$V_{r2} = S_{21} V_{i1} + S_{22} V_{i2}$$

→  $S_{22}$  output reflection coefficient at  $V_{i1} = 0$ .

**Ex** AT-41511 npn transistor from HP.  
at 1 GHz.

$$S = \begin{bmatrix} 0.4 \angle -149^\circ & 0.073 \angle 43^\circ \\ 5.189 \angle 89^\circ & 0.49 \angle -39^\circ \end{bmatrix}$$



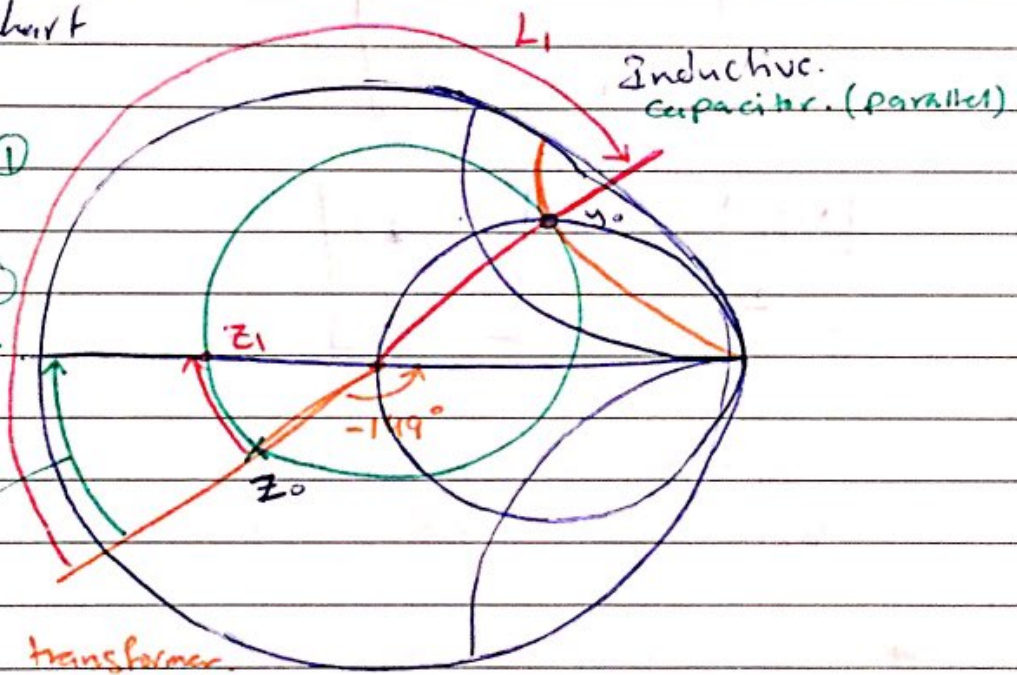
$$\Gamma = 0.4 \angle -119^\circ$$

matching  $\lambda/4$  &  $L$  or  $C$  or  $\dots$

$$\Gamma = 0.4 = ?!$$

Smith chart

←  $\Gamma_{\text{in}}$  ←  $\Gamma_{\text{out}}$  (1)  
 Smith chart  
 ←  $\Gamma_{\text{in}}$  ←  $\Gamma_{\text{out}}$  (2)  
 input impedance

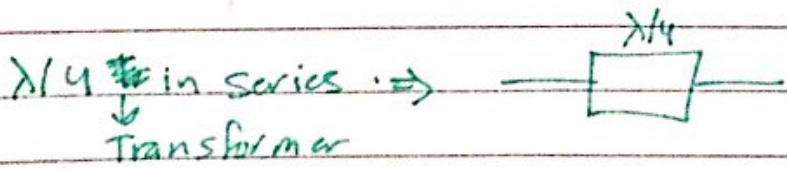


real part. → transformer matching

\* Parallel matching → parallel comp  $\left\langle \begin{matrix} C \\ RL \end{matrix} \right.$

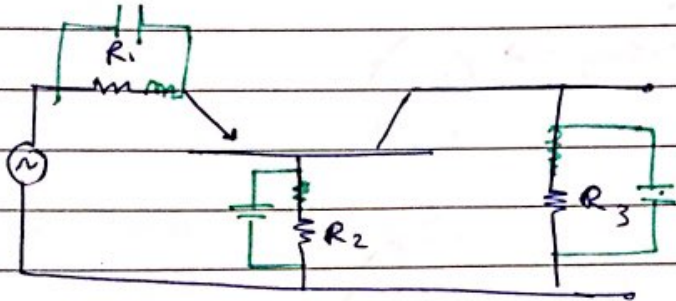
network analyzer → use to meter the S parameter.

$$Z_{Tr} = \sqrt{Z_0 Z_1}$$

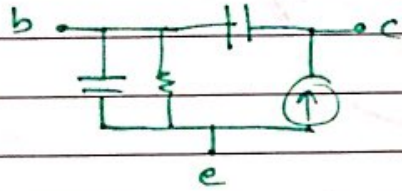


Quiz 1

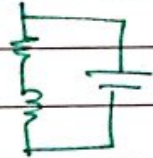
Draw the high freq model for the following CKT.



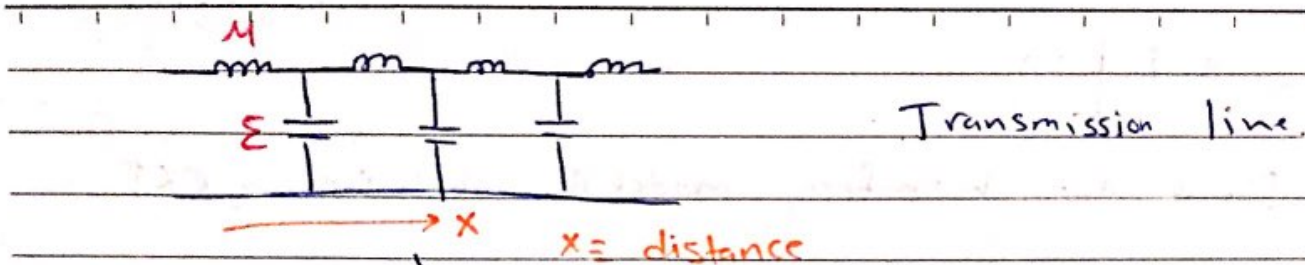
Solution :-



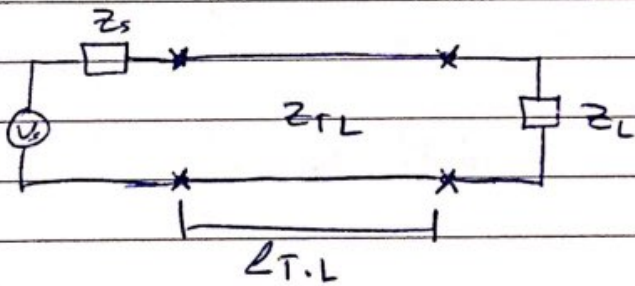
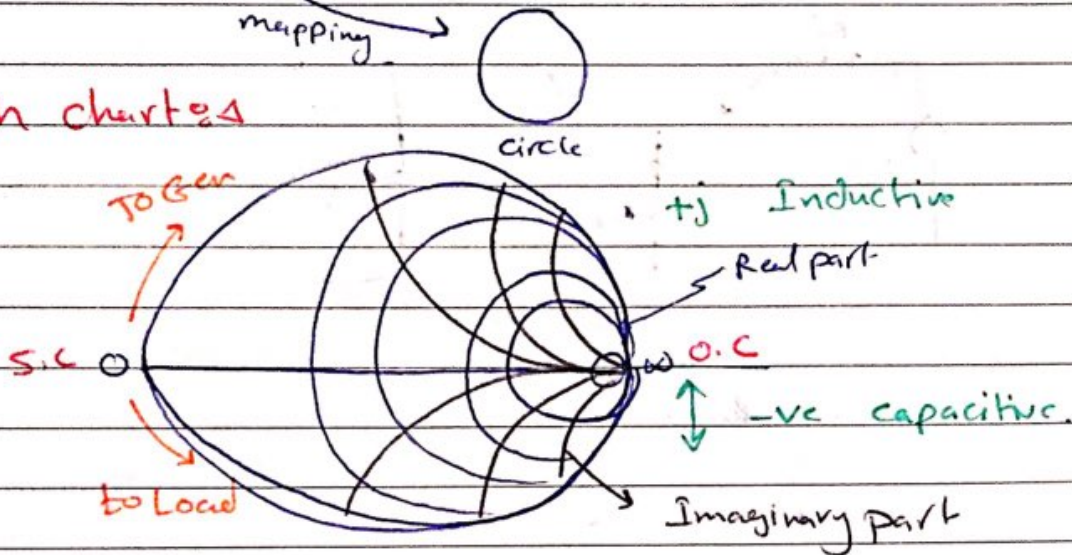
for transistor.



for R.



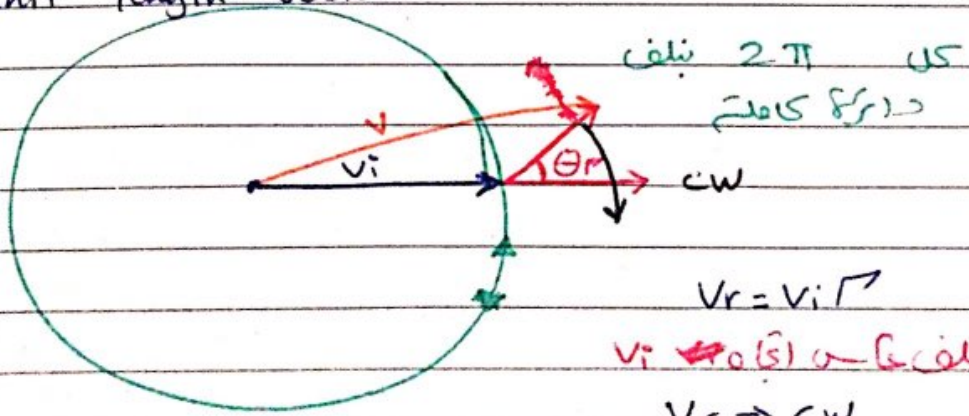
\* Smith chart



$\rightarrow V_i$  (V incident)

$\leftarrow V_r$  (V reflected)

as unit length vector.

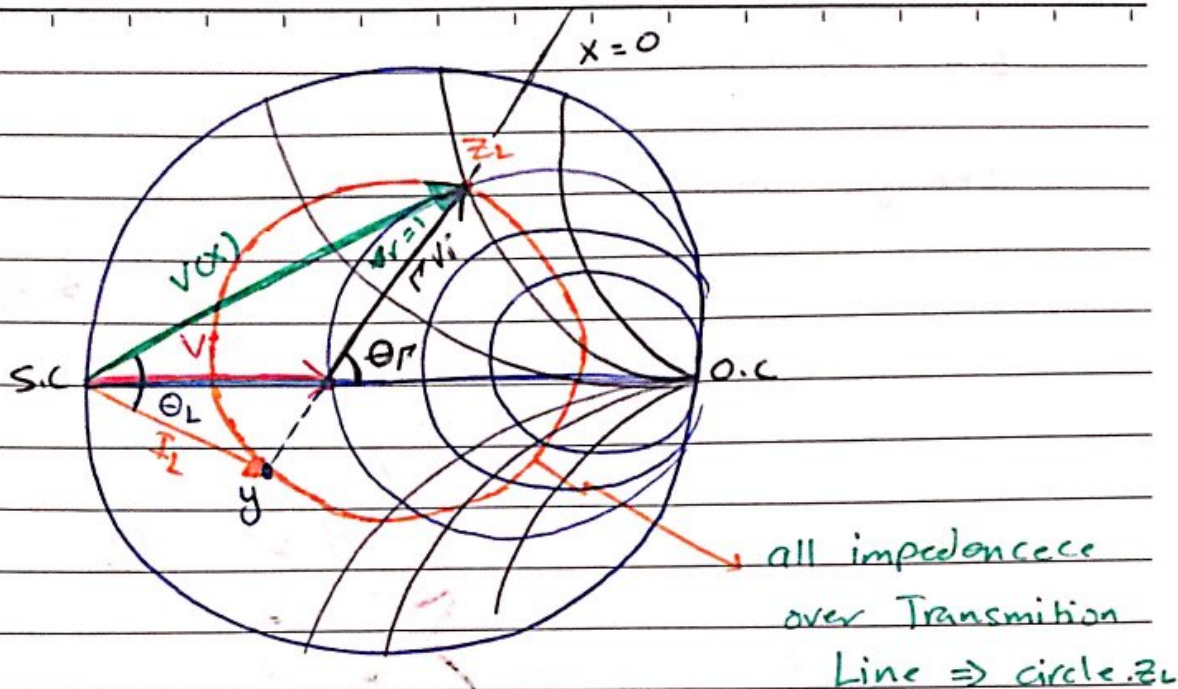


$V_r = V_i \Gamma$

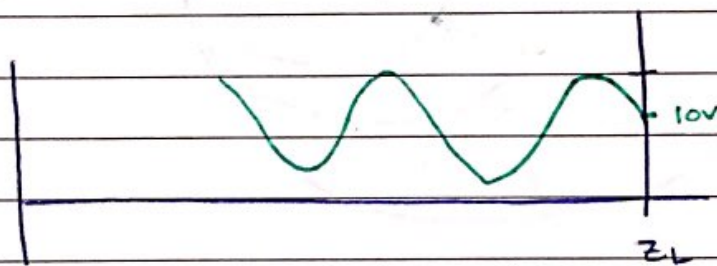
$V_i \rightarrow \text{clockwise}$

$V_r \Rightarrow \text{CW}$

$V_i \Rightarrow \text{CCW}$



~~XXXXXXXXXX~~ ~~XXXXXXXXXX~~ ~~XXXXXXXXXX~~ ~~XXXXXX~~



at center  $\rightarrow (1 + j0) \rightarrow$  (matching point)

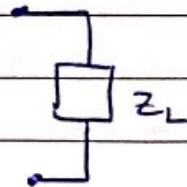
$$Z_L = a + jb$$

$$y = \frac{1}{Z} = \alpha - j\beta \text{ (in parallel)}$$

Ex:  $Z_L = 5 + j10$

$$y_1 = \frac{1}{5 + j10} =$$

$$= 0.04 - j0.08$$



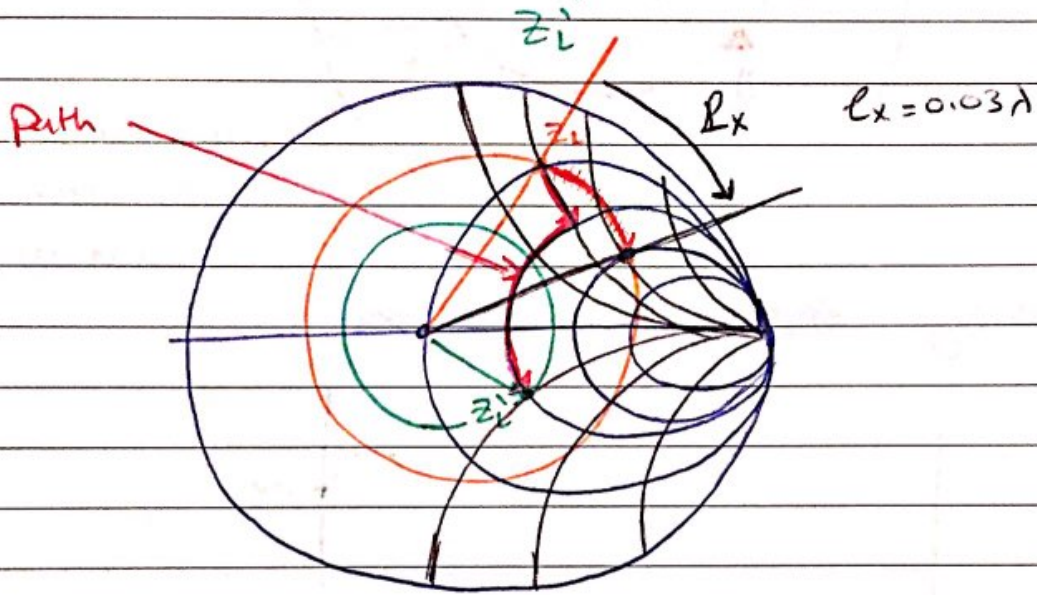
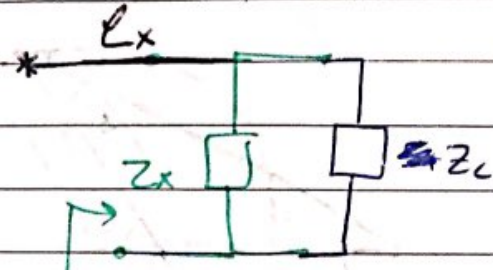
$$Z_L = 4 + j10 \text{ } \underline{5V}$$

$$Z_2 = 4 + j10$$

$$y_2 = 0.034 - j0.086$$

$$\Delta Y = Y_2 - Y_1$$

change impedance

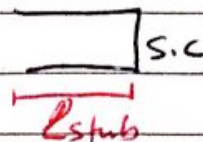
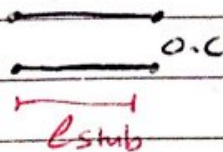


**Ex**  $Z_1 = 0.5 + j0.1$

$Z_2 = 0.4 + j0.1$

$R \rightarrow R \uparrow \rightarrow$  in series. add Resistor  
 $R \rightarrow R \downarrow \rightarrow$  in parallel. add Resistor.

Stub  $\rightarrow$  there's NO R (سبب لا يغير  $R$ )

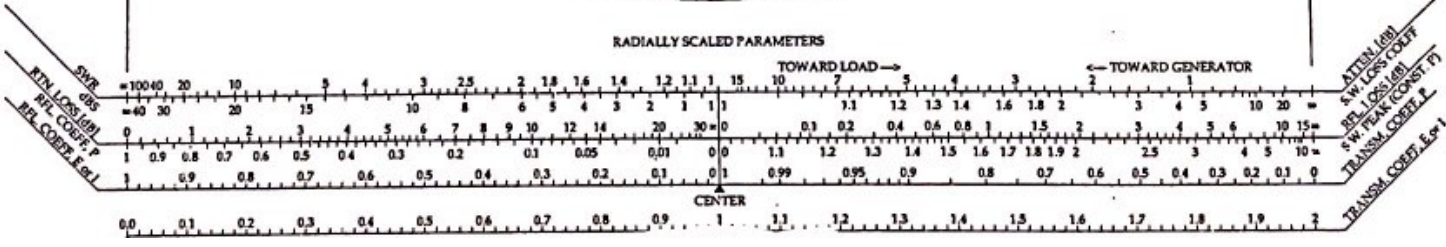
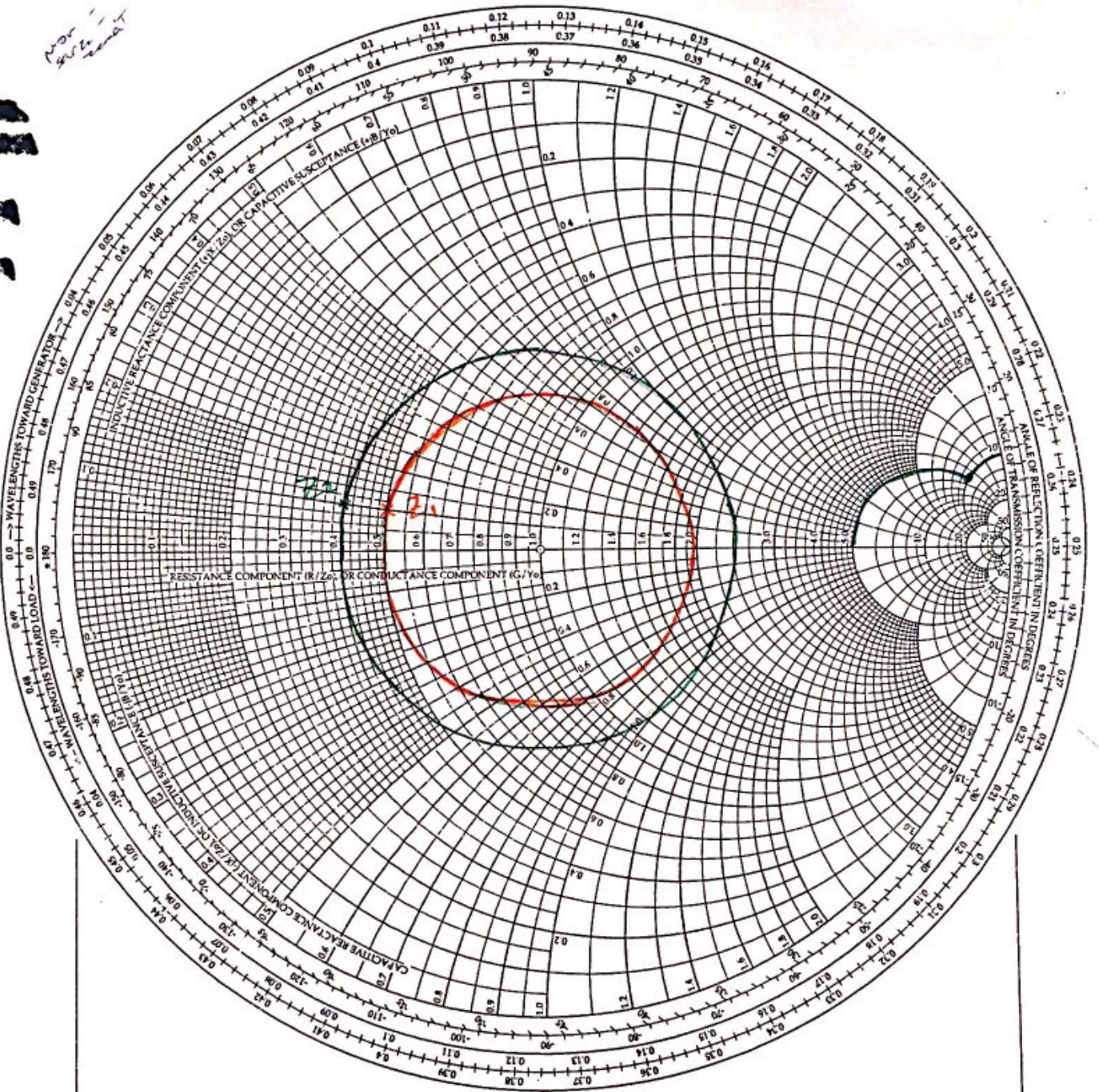


\* frequency  $\Rightarrow$  constant  $\Rightarrow \lambda$  constant.

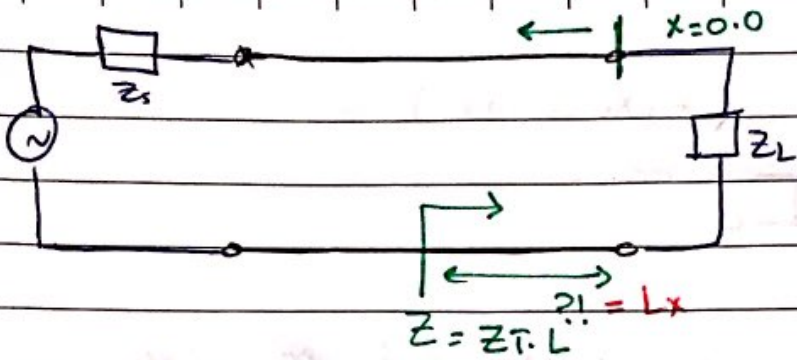
# The Complete Smith Chart

## Black Magic Design

*Handwritten note:*  
Not  
scale  
unit





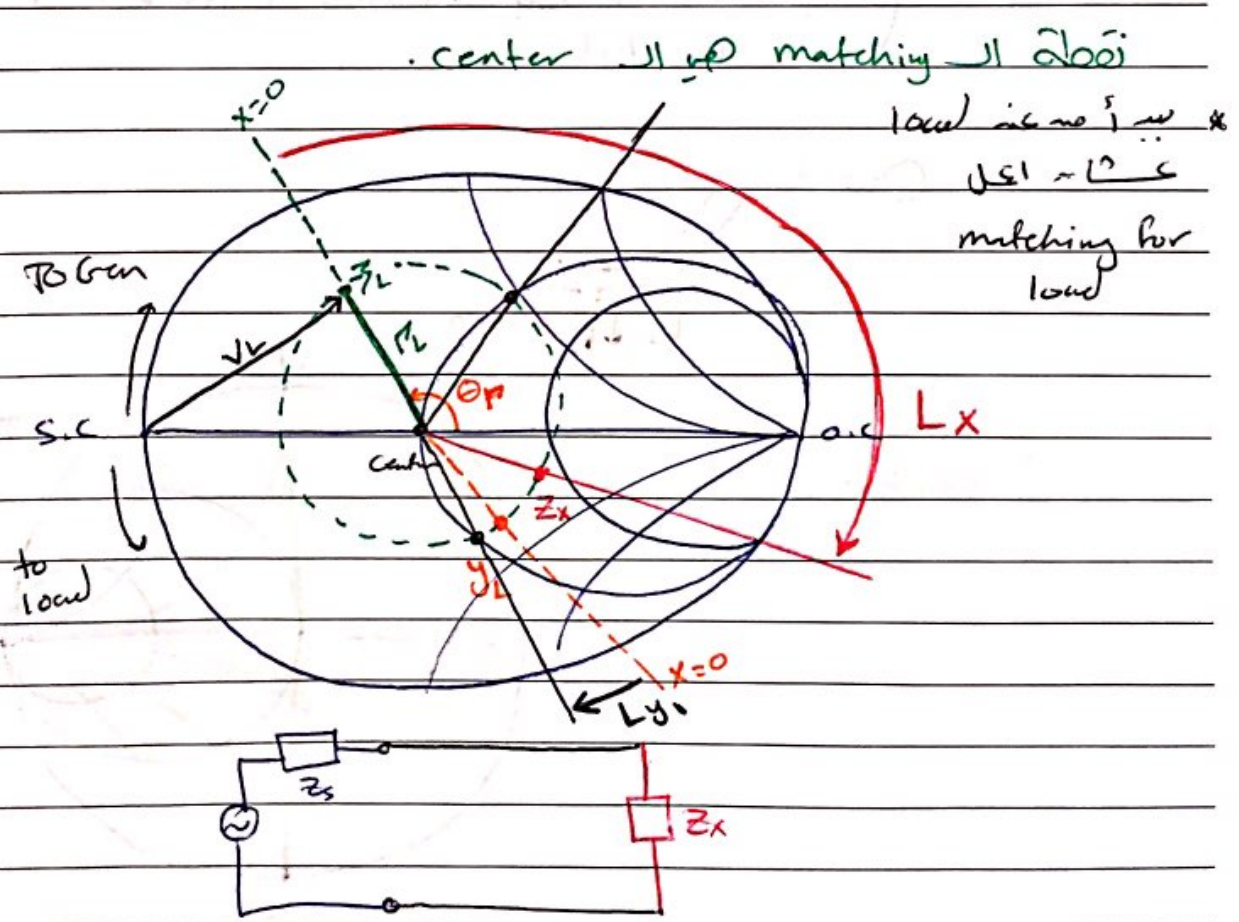


== Llm Clm

$$Z = \sqrt{\frac{L}{C}}$$

$$V(t) = A \cos(\omega t - \beta z)$$

$$Z_{T.L} = 50 \Omega$$



① Stub matching ( $+jX_s$  >  $-jX_c$ ):

Stub means  $\begin{bmatrix} L \\ C \end{bmatrix}$  or

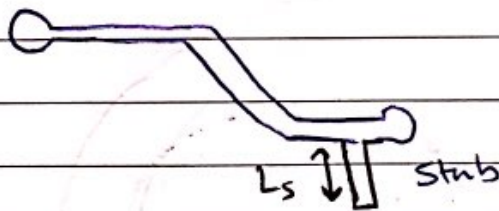
- Series capacitor → DC path. ~~is~~ like
- inductor in parallel → short ~~at~~ ~~port~~ ~~path~~ path.

$$\Rightarrow Y_{L_1} = 1 - jY_x$$

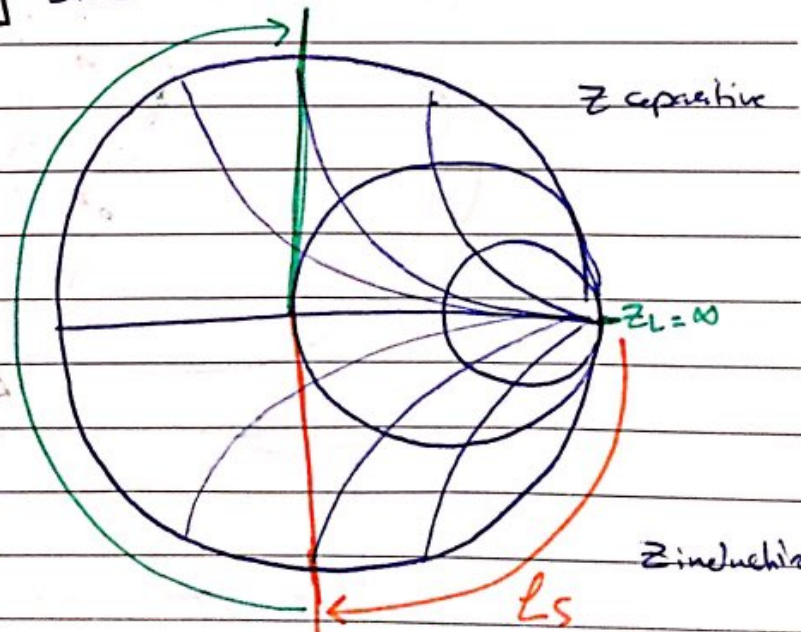
Stub →  $+jY_x$  → (capacitor)

capacitor in parallel → O.C DC (DC is  $\hat{L}$  like) Path

(capacitor in ~~cap~~ ~~port~~ ~~is~~ ~~parallel~~ ~~is~~ ~~parallel~~) \*



$$Z_{\text{stub}} = \frac{1}{Y_{\text{stub}}}$$



32

Ex

$$Z_L = 100 + j80$$

$$\lambda = 1 \text{ cm}$$

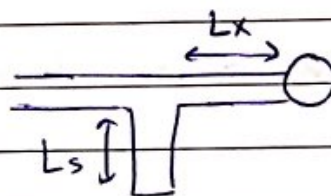
$$l_x = 0.215 \lambda$$

$$jy_x = +j1.3 \rightarrow y \text{ for load.}$$

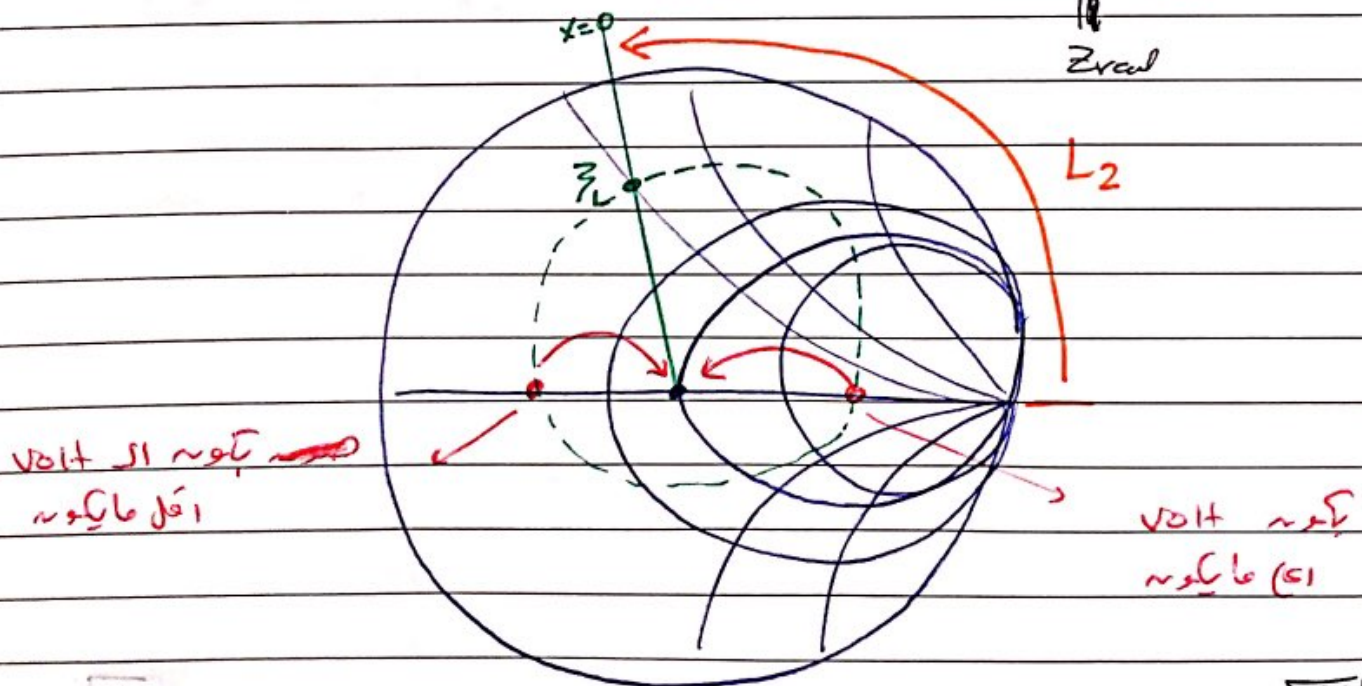
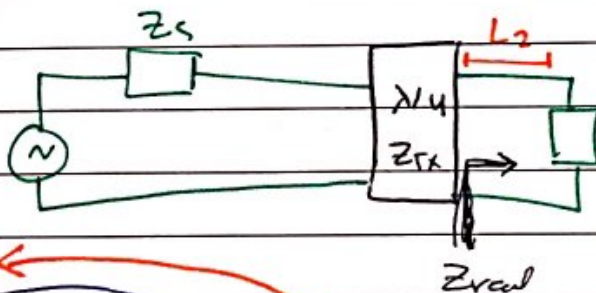
$$\text{for stub} \rightarrow y_s = -j1.3 \rightarrow Z_s = +j0.77$$

O.C stub

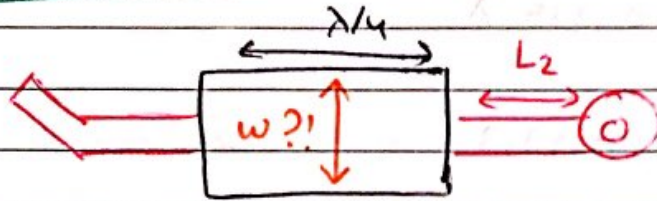
$$l_s = 0.25\lambda + 0.105\lambda = 0.355\lambda$$



\*  $\lambda/4$  Transformer:-



$$Z_{TX} = \sqrt{Z_{read} \times Z_{T.L}}$$



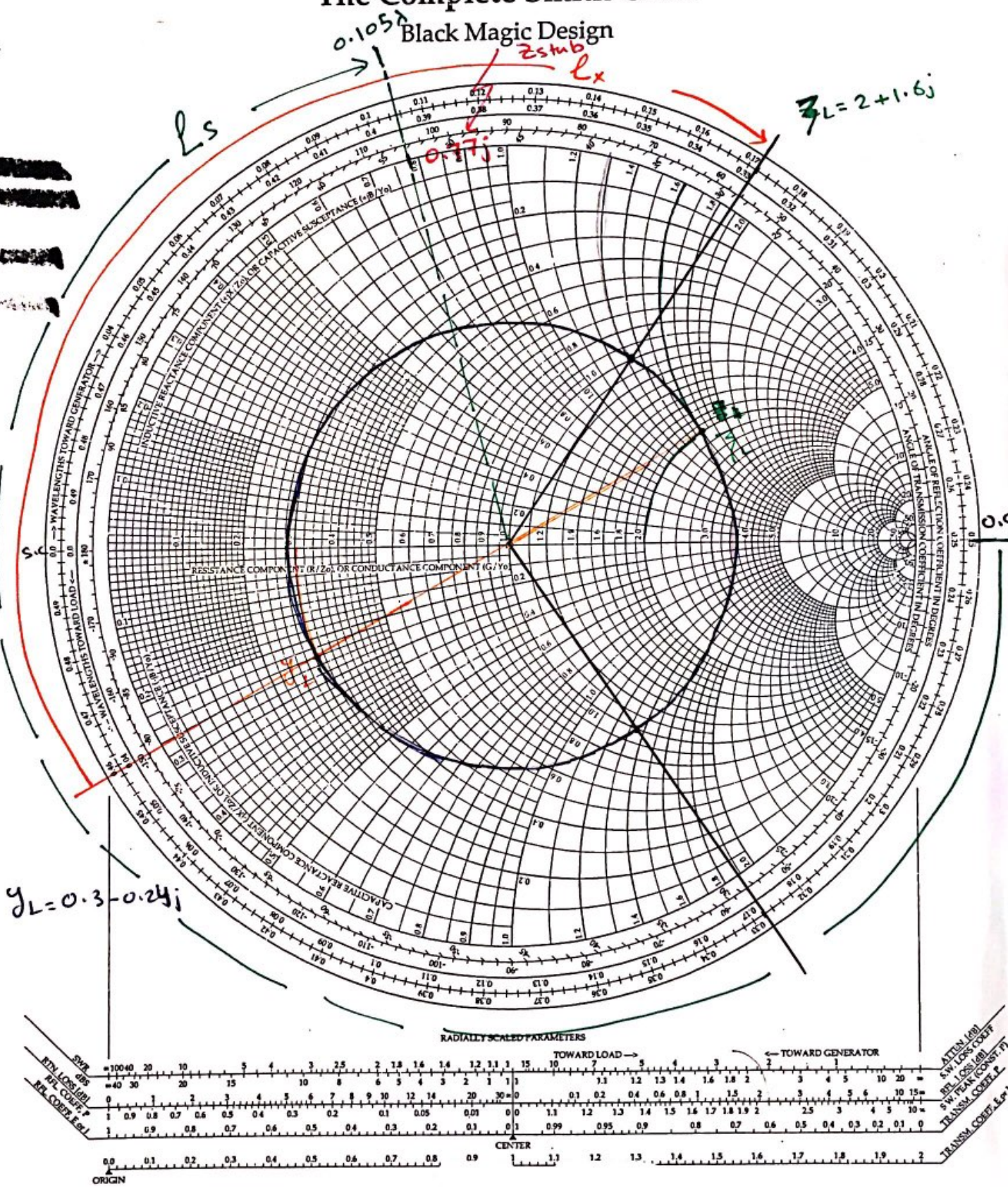
$w \equiv$  width

• trac  $\rightarrow$   $\lambda/4$   $\rightarrow$   $\lambda/4$   $\rightarrow$   $\lambda/4$

$\lambda/4$  ~~transform~~  $\rightarrow$  transform the impedance.

# The Complete Smith Chart

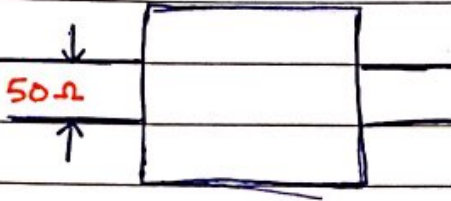
Black Magic Design



HFSS:-

⇒ read chapter 2, read  $\frac{1}{4}$  transformer.

λ/4



1m inside IC

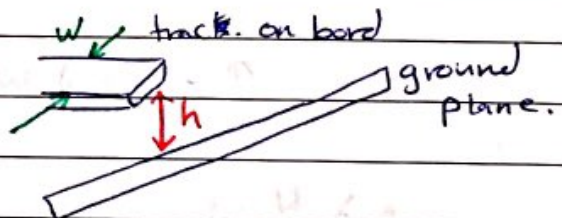
3m outside

For Micro-strip:-

$$Z_0 = \frac{Z_0}{T.L} \ln \left( 8 \frac{h}{w} + \frac{w}{4h} \right)$$

 ~~$\epsilon_{eff}$~~ 

$$FR4 \Rightarrow \epsilon_r = 4.4 - 4.6$$



$$\epsilon_{eff} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left[ \sqrt{1 + \frac{12h}{w}} + 0.04 \left( \frac{1 - w/h}{h} \right)^2 \right]$$

\*  $H \Rightarrow$   $\frac{1}{4} \lambda \Rightarrow H = 1.5$  ~~mm~~  $\frac{1}{4} \lambda$ ,  $w \rightarrow$  متغير

$$H \text{ layer} = \frac{1.5}{4}$$

$$Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 120\pi = 377 \Omega$$

Find  $Z_{T.L}$  using numerical method.

$$H = 1.5$$

**Ex**  $w = 5 \text{ mm}$ ,  $H = 1.5 \text{ mm}$   
 $\epsilon_r = 4.4$

$$\epsilon_{\text{eff}} = 6.563$$

$$Z_{T.L} = 27.48 \Omega$$

\* Home work 2  $\rightarrow$  on matlab  
(50 =  $Z_{T.L}$ ) gibet  $w$   $\rightarrow$   $\epsilon_r$  is  $\epsilon_r$

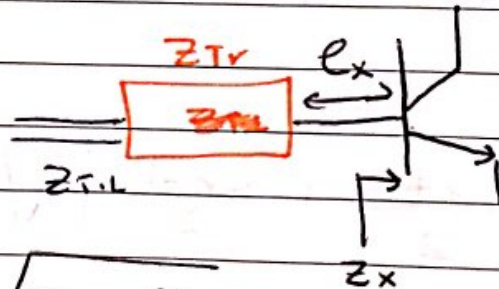
**2**  $w = 3 \text{ mm}$  ?!

$$\epsilon_{\text{eff}} = 7.2377$$

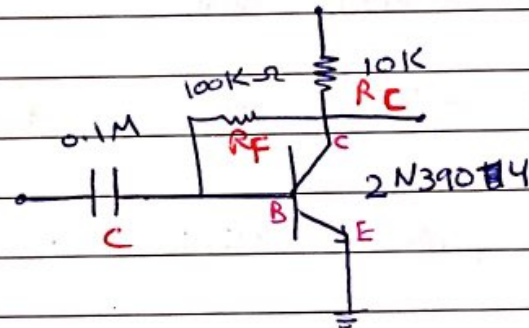
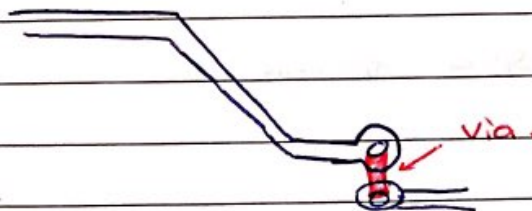
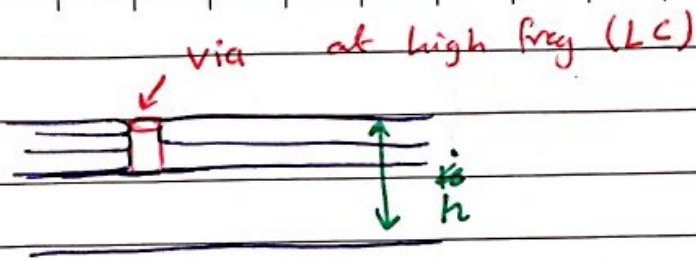
$$Z_{T.L} = 35.227 \Omega$$

$\uparrow Z \rightarrow \downarrow w$

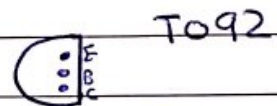
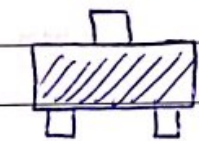
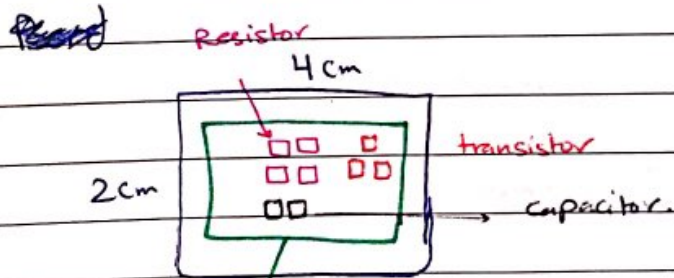
$\lambda/4 \rightarrow$



$$Z_{Tr} = \sqrt{Z_x \cdot Z_{TL}}$$



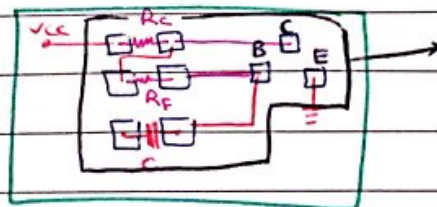
printed CKT Board. :



4 layers.

Keep in region *مناطق التردد العالية*

Routing =>



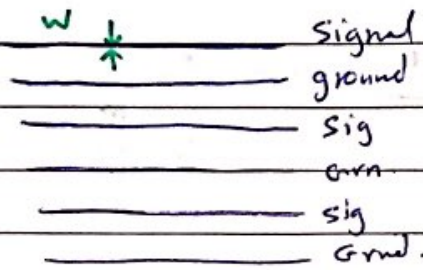
تجنب الارتفاع (الطبقات) at high freq

\* Area : ground track بين الـ plan

" بين الـ track في ground plane "



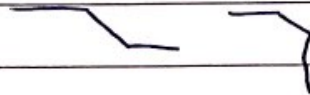
center to center =  $2w$



↑ wire → ↑ speed through it

rule ①  $2w$

② No sharp edge.



$90^\circ \rightarrow \uparrow$  inductance.



\* track path → horizontal or vertical best path.

delay TL →  $\sqrt{LC}$

2 point

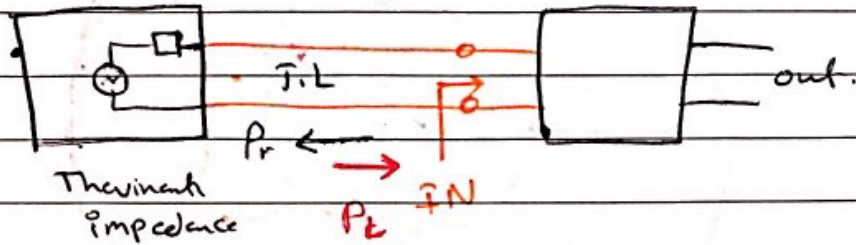
speed →  $\frac{1}{\sqrt{LC}} = 4$  meter per sec.

$\sqrt{LC}$

↑  
per meter    per meter.

\* Mid in 4/4 week

2 port Network:-



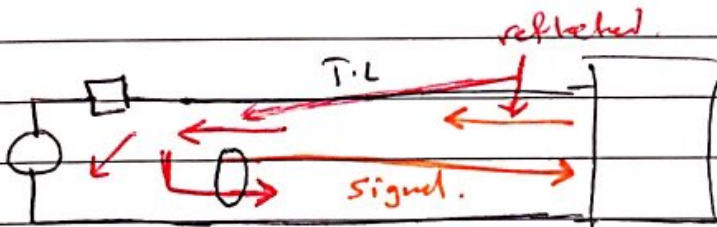
for wide band  $\rightarrow$  must do sweep.

narrow band.  $\rightarrow$  cos (wot)

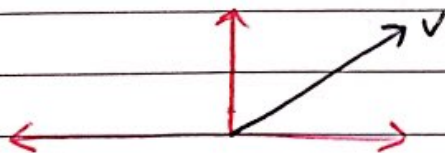
$$* \frac{\Delta f}{f_0} = \begin{cases} \ll 1 \rightarrow \text{narrow band} \\ \sim 1 \rightarrow \text{wide band} \end{cases}$$

\* narrow band  $\rightarrow$  only  $f_0$

\* wide band  $\rightarrow$  must sweep analysis.



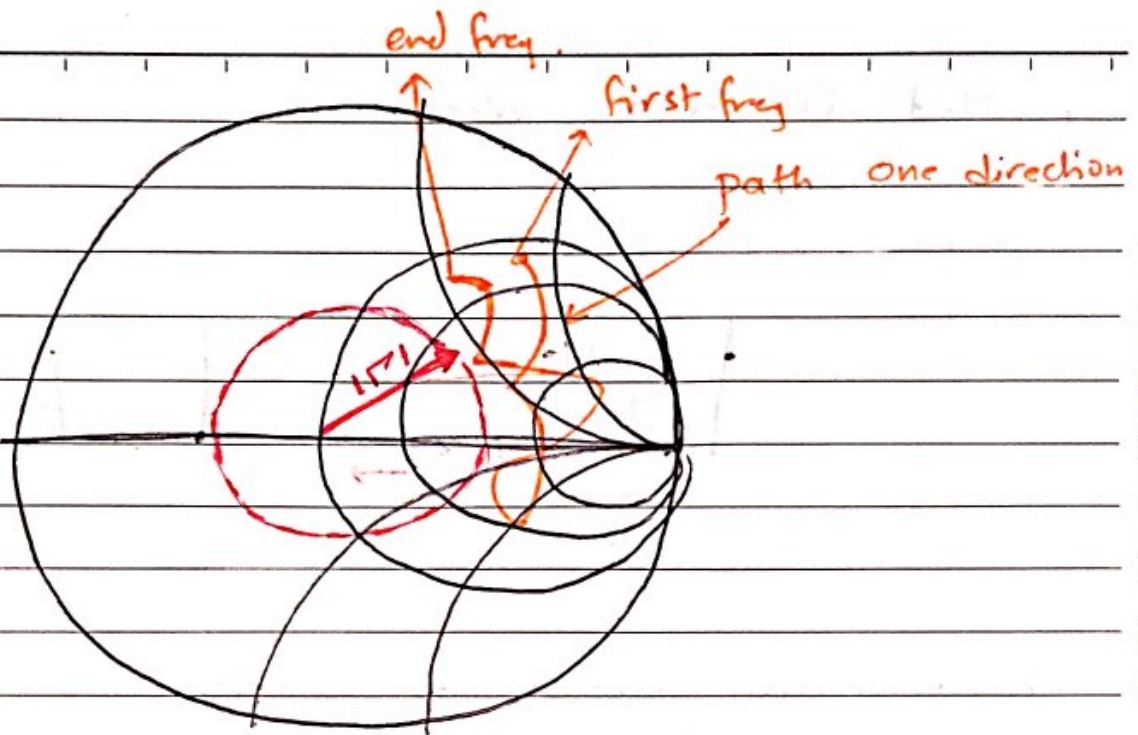
$P_r \Rightarrow$  nulling (fading).  
(180°  $\phi$  is sep. signal in circuit)



S-parameter :-

$S_{11} \rightarrow$  reflection coefficient.

Smith chart:-



$$\Rightarrow P_t = \frac{V_{in}^2}{Z_{i.L}} \Rightarrow \text{transmitted}$$

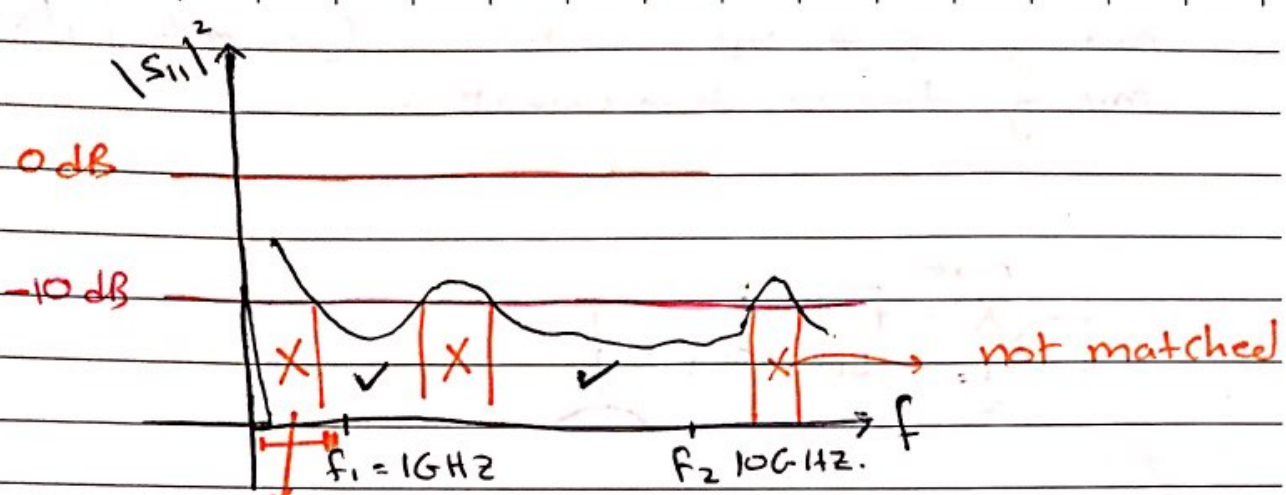
$$\Rightarrow P_r = \frac{|\Gamma|^2 V_{in}^2}{Z_{i.L}} \Rightarrow \text{reflected}$$

$$P_r = |\Gamma|^2 \cdot P_t$$

$$\text{Power loss \%} = \frac{P_r}{P_t} = |\Gamma|^2 \quad \text{unitless in dB}$$

$$\downarrow \text{Loss} = 20 \text{ Log}(S_{11})$$

Return



range (null)  $S_{11} = 1 \rightarrow 0 \text{ dB}$

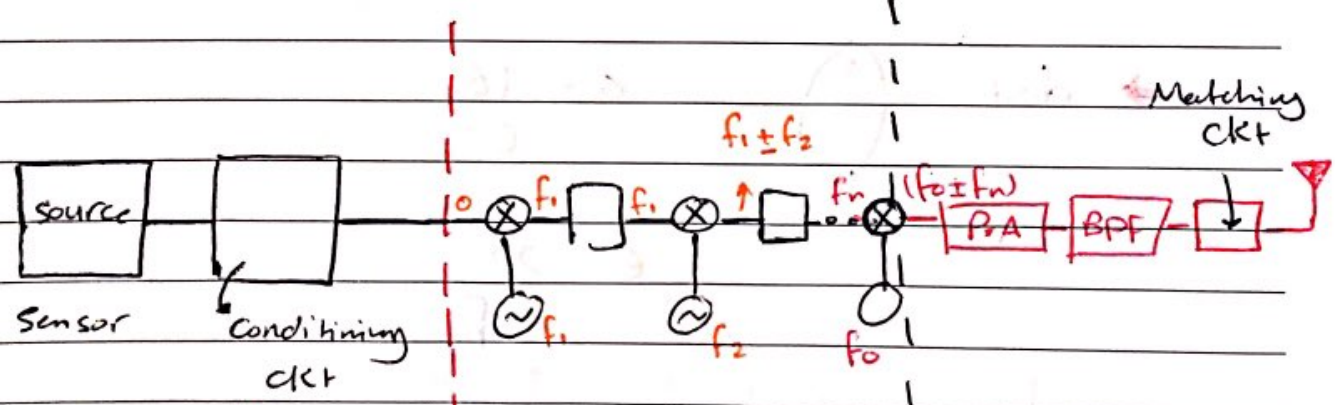
$S_{11} = 1 \rightarrow 0 \text{ dB}$

matched جا ڏيکاري ٿو  $S_{11}$  ڦيرڻ لاءِ

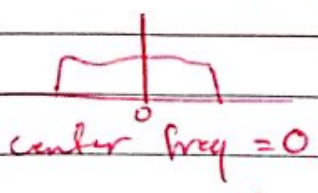
\* Solution in narrow band  $\Rightarrow$  add stub or double stub.

radiation pattern  $\Rightarrow$  space جي ڊيگري (ڊب) ۾ ڊيگري

return loss  $< -10 \text{ dB}$   $\Rightarrow$  for design



Base band side  
(A.F) Audio Frey stage



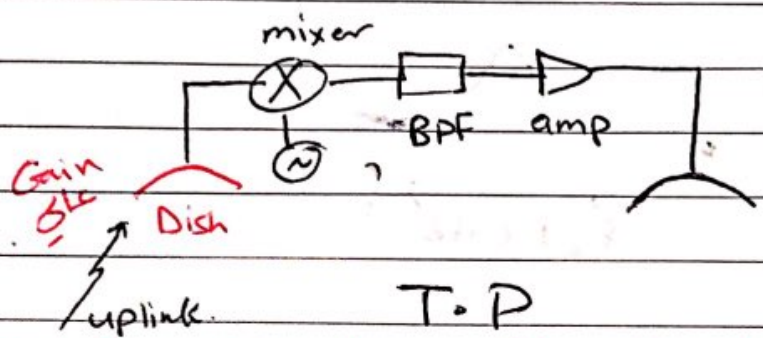
I.F  
Intermedia.

R.F

Tx  $\rightarrow$

$\leftarrow$  Rx

mixing up  $\rightarrow$  up converter. (Low  $\rightarrow$  high), (Tx  $\rightarrow$  Rx)  
 mixing down  $\rightarrow$  down converter.

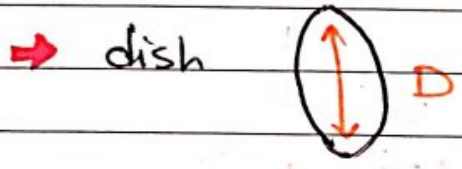


down converter.

Gain  $\propto \frac{1}{r^2}$   
 free space loss  
 $\propto \frac{1}{r^2}$

$$L = \frac{\lambda^2}{4\pi r^2}$$

$$L = \frac{c^2}{4\pi f^2 r^2} \Rightarrow f \uparrow \rightarrow L \uparrow$$

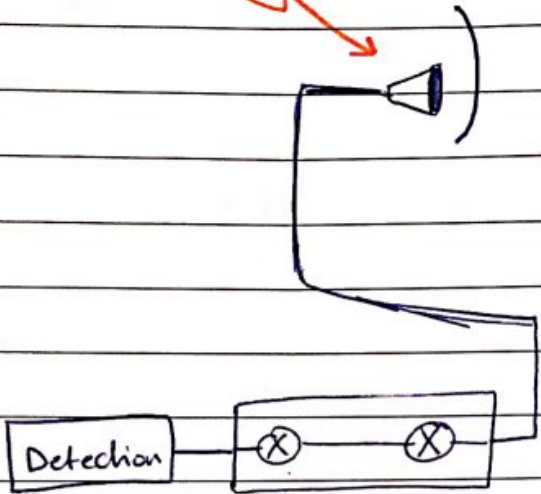


$$G = \frac{16}{\theta^2}$$

$$\theta = \frac{22}{D \cdot f}$$

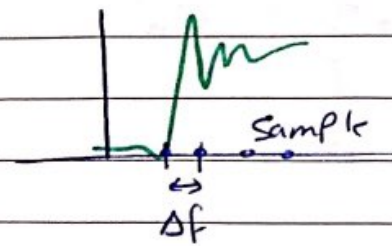
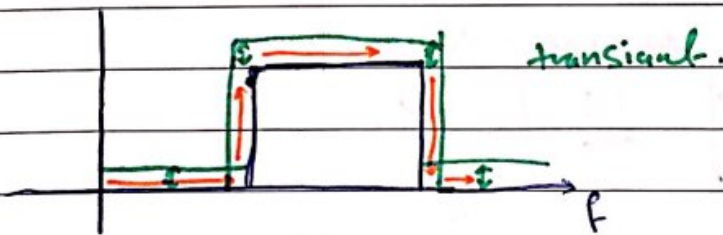
$D = 5\lambda$  best than  $D = 4\lambda$   
 $L \rightarrow$  gain  $\uparrow$

12G#



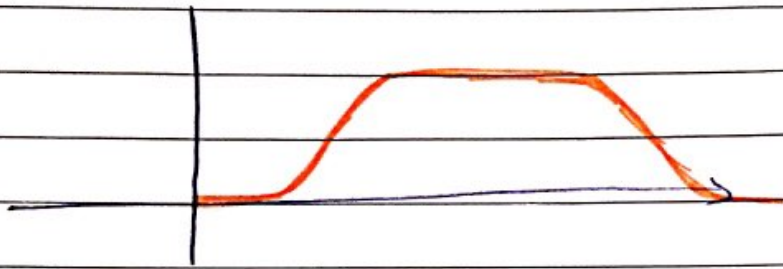
$\rightarrow$  output filter =  $\sum_{j=0}^{J+1} w_j x(t - \tau_j)$   
 $w = \text{weight}$   $\downarrow$  delays

OR out =  $\sum_{j=0}^{J+1} \alpha_j x(t - \tau_j)$



\* Back to analog  
 $\rightarrow$  ripple.

$\Delta f = \frac{f_s}{N} \rightarrow \text{frequency resolution.}$



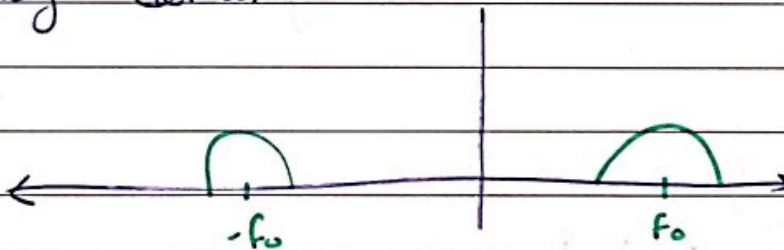
Modulation

$$z = v_1(t) \cdot v_2(t)$$

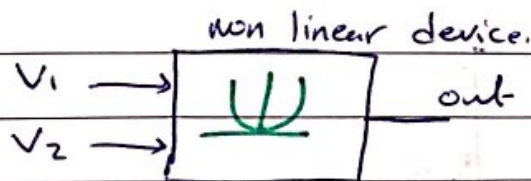
$$v_2(t) = 2 \cos(\omega_0 t)$$

$$z = 2 v_1(t) \cos(\omega_0 t)$$

frequency domain.



~~Impulse~~



$$\text{out} = \sum_{i=0}^N \alpha_i v_{in}^i$$

$N \equiv$  order of the ~~polynomial~~ polynomial.

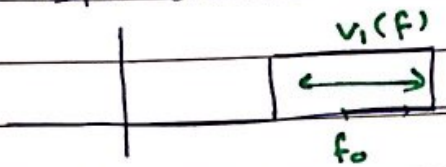
if  $N=2 \Rightarrow$

$$\text{out} = \alpha_0 + \alpha_1(v_1 + v_2) + \alpha_2(v_1 + v_2)^2$$

$$\text{out} = \alpha_0 + \alpha_1 V_1 + \alpha_1 V_2 + \alpha_2 V_1^2 + \alpha_2 V_2^2 + \underbrace{2\alpha_2 V_1 V_2}_{\text{modulation}}$$

base band

⇒ BPF at  $f_0$ .



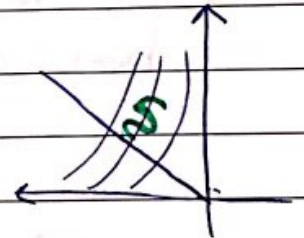
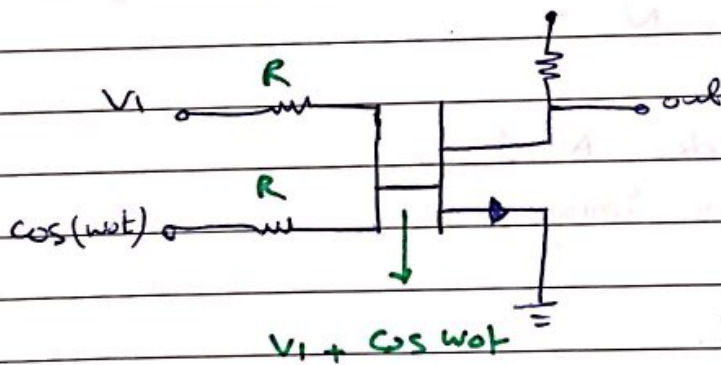
$$V_1(f) \neq 0$$

$$\Downarrow 2\alpha_2 V_1 \cos(\omega_0 t) + \alpha_1 \cos(\omega_0 t).$$

if  $\alpha_1 \approx 0$

$$\text{out} = 2\alpha_2 V_1 \cos(\omega_0 t).$$

FET Transistor relation btw input, output ~~square~~ square.



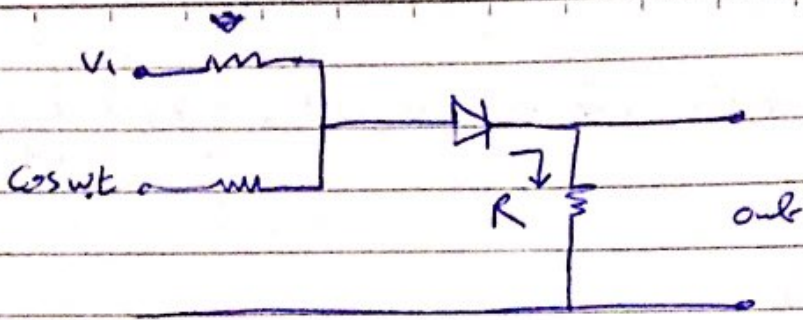
$$\text{out} = K V_{in}^2$$

if  $N=3 \Rightarrow$

$$\text{out} = \alpha_0 + \alpha_1 V_1 + \alpha_1 V_2 + \alpha_2 V_1^2 + \alpha_2 V_2^2 + 2\alpha_2 V_1 V_2 + \alpha_3 (V_1 + V_2)^3$$

$$\Downarrow V_1^2 V_2 \Rightarrow V_1^2 \cos \omega_0 t.$$





Diode relation exponential.

order  $N$

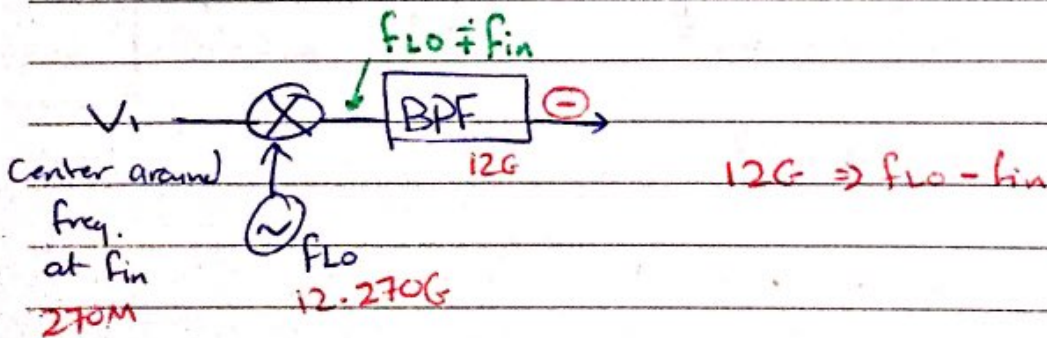
image freq  $\equiv f_I$

$$f_I = \frac{f_0}{n} \pm m \frac{f_{IF}}{n}$$

~~( $f_0 = f_c$ )~~

$n, m = 1, 2, \dots, N.$

⇒ Ideal mixer order  $N=1$   
best case one image.



## \* Filters

→ types

1] LPF

2] HPF

3] BPF

4] Notch Filter

5] Band reject filter

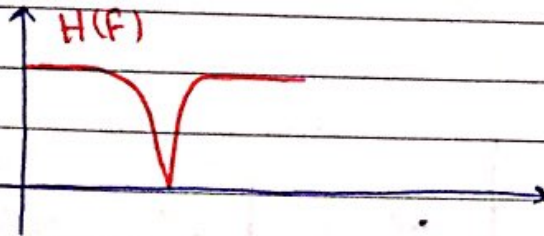
6] General filter.

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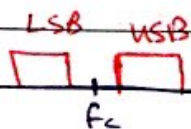
$\lambda \uparrow \rightarrow$  Shrink :

**Filter:-**

\* Notch Filter  $\rightarrow$  jeso notch is Signal 11 jee



in freq domain.



Pilot carrier.

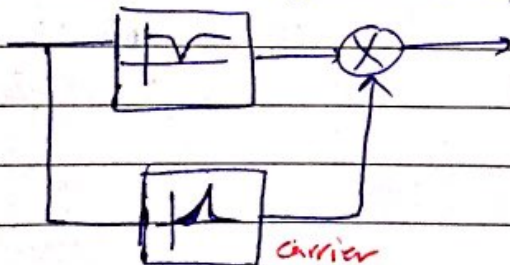
USB = upper side Band.

LSB = lower " "

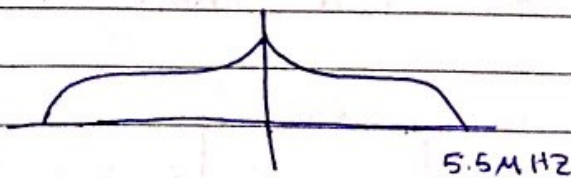
use in Synchronization Signal.

: Audio Signal DC level,

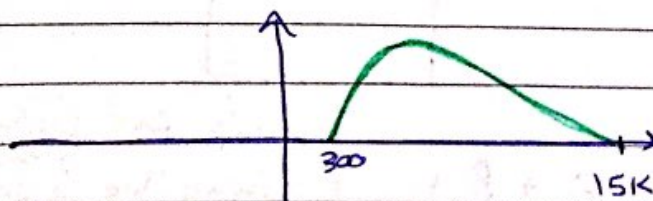
Video 11 jee to Signal.



video signal  
DC level



Audio signal

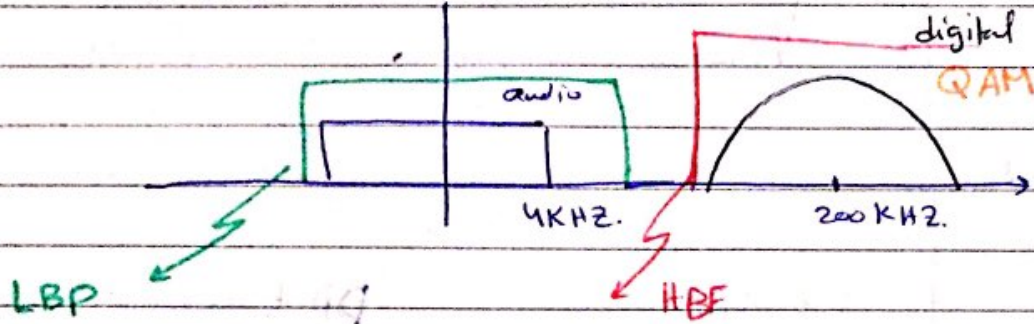


# HW 3:

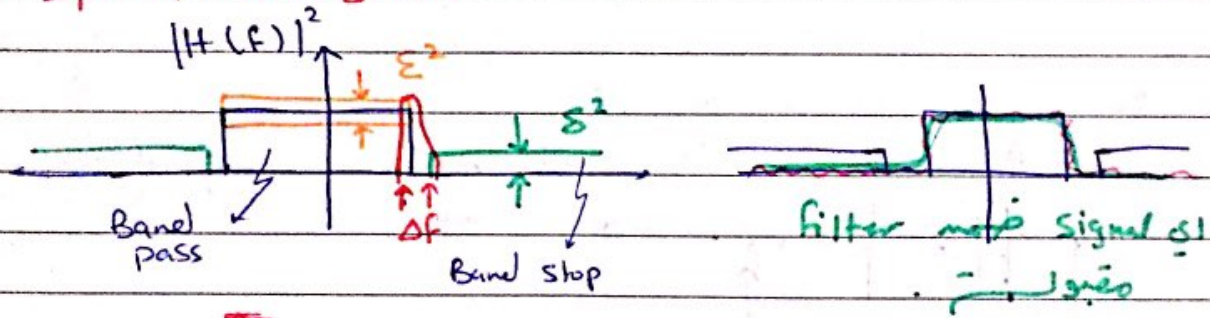
DC restoration ckt.

↳ coil peak detector.

~~Block~~ DC restoration ← DC block ← block ← coil ← Signal.  
 Cap.



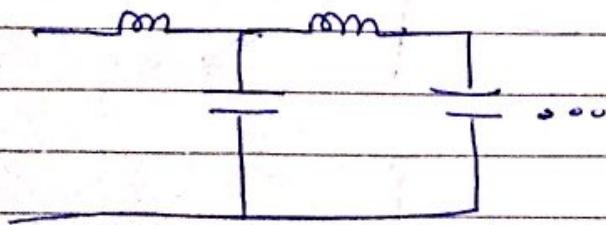
## \* Specifications 84



~~Transfer Function~~

$$H(f) = \frac{f^2 - 3}{5 + 2f - 4f^4}$$

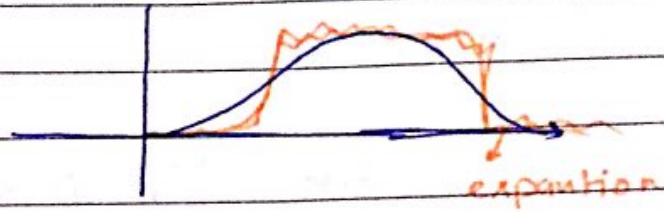
not ideal → distortion (10% جوابه)



$$\left( \alpha f + \frac{\beta}{f} \right) \begin{cases} \text{low freq} \rightarrow \delta \text{ جوابه} \\ \text{high freq} \rightarrow \epsilon \text{ جوابه} \end{cases}$$

$$H(f) = \frac{1}{\left(\alpha f + \frac{B}{f}\right)}$$

Band pass filter.

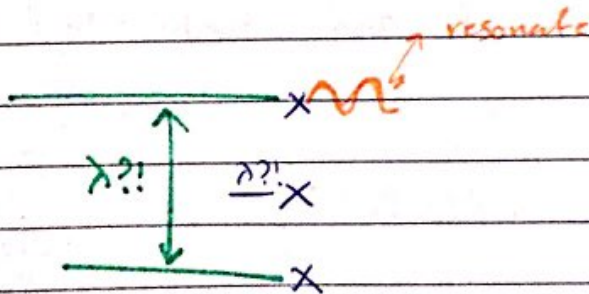


Transformation from Low pass  $\rightarrow$  Band pass.

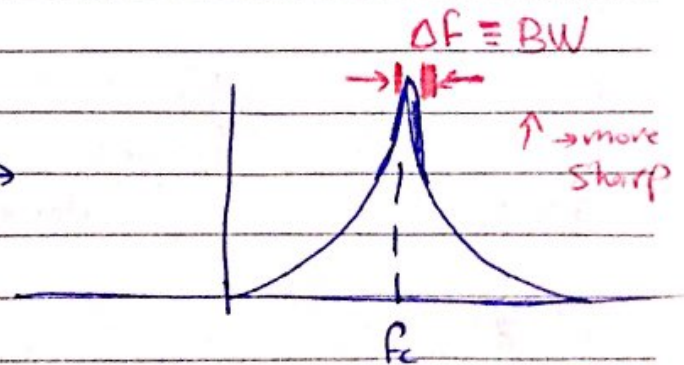
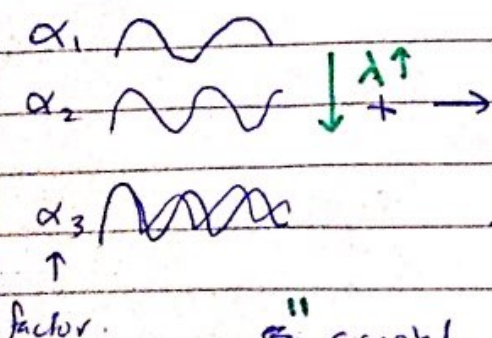
$$H(f) = \frac{1}{\left(\left(\alpha f\right)^n + \left(\frac{B}{f}\right)^m\right)}$$

Inverse  $\rightarrow$  Band stop.

L & C  $\rightarrow$  harmonic.



resonant at amplitude  $(\omega)$   
 view  $\rightarrow$



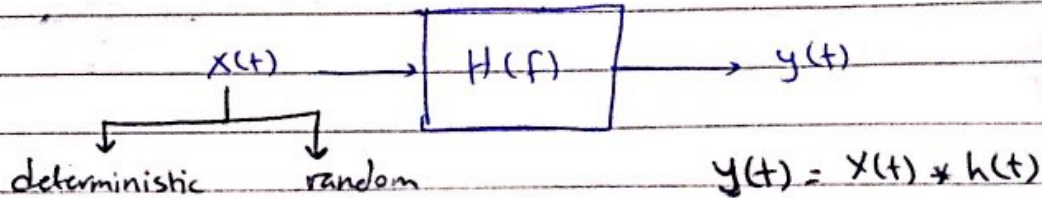
factor. "crystal stable at frequency"

491

## Filters

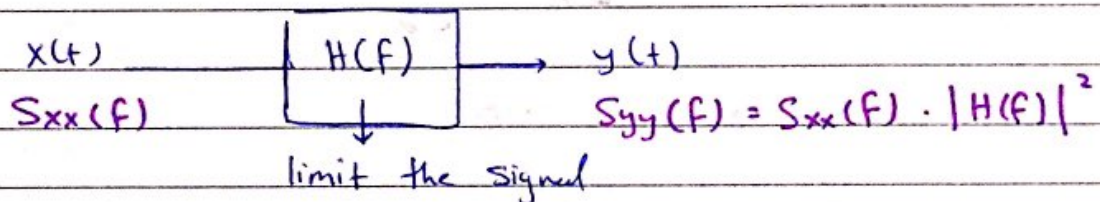
any filter can be determined as:

$$H(f) = ?$$



**Histogram** :- avg of the signal after apply F.T

for random  $x(t)$  &



\* we need  $H(f)$  causal and stable to represent the signal

$$H(f) = \sum_{n=0}^{N-1} \frac{A_n}{a_n + j b_n} \quad (\text{RC filter})$$

\* Another representation for  $H(f)$  is

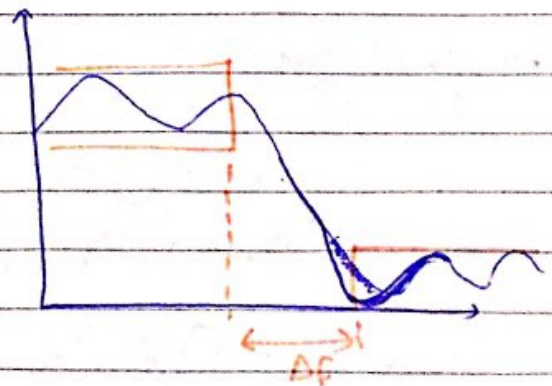
**FIR** :-

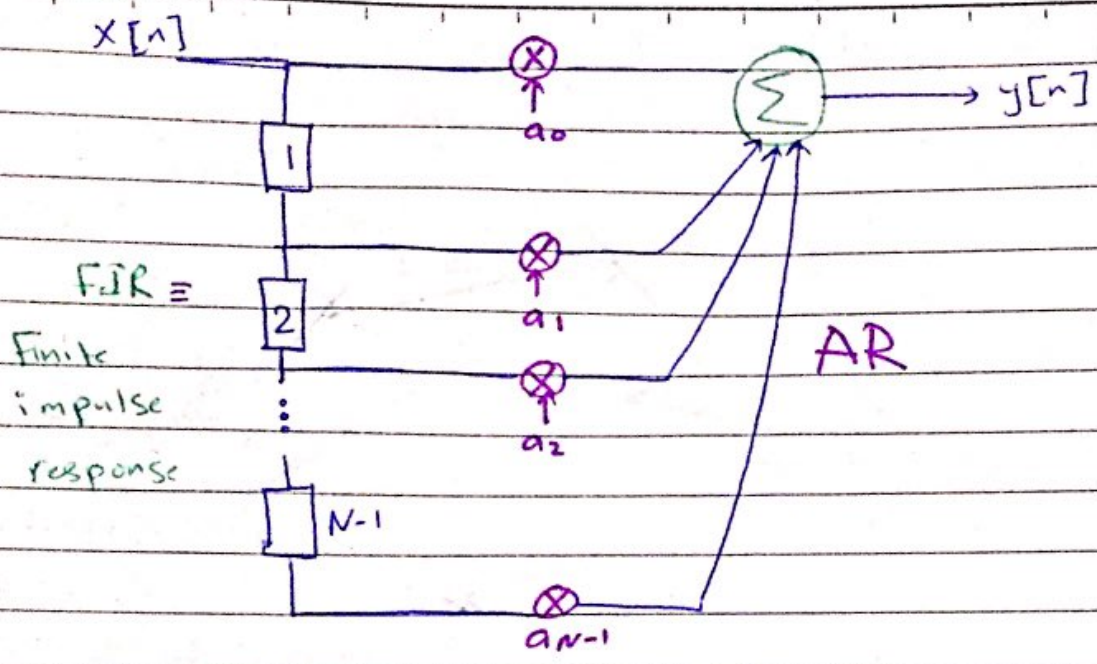
$$H_1(z) = \sum_{n=0}^{N-1} a_n z^{-n}$$

↳ delay in time domain

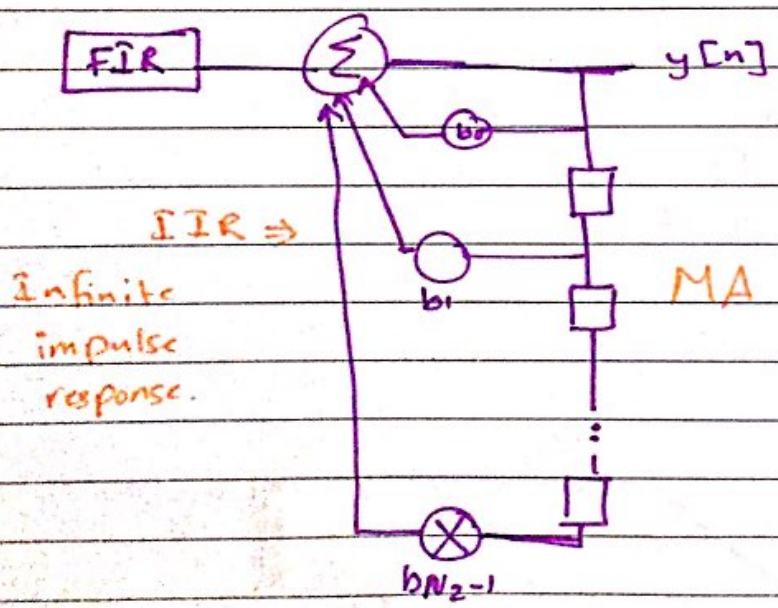
**IIR** :-

$$H_2(z) = \sum_{n=0}^{N-1} \frac{1}{1 + b_n z^{-n}}$$





Arma model:  
 $H_1(z), H_2(z)$



⇒ AR(10) used for voice signal  $[N_1=10]$

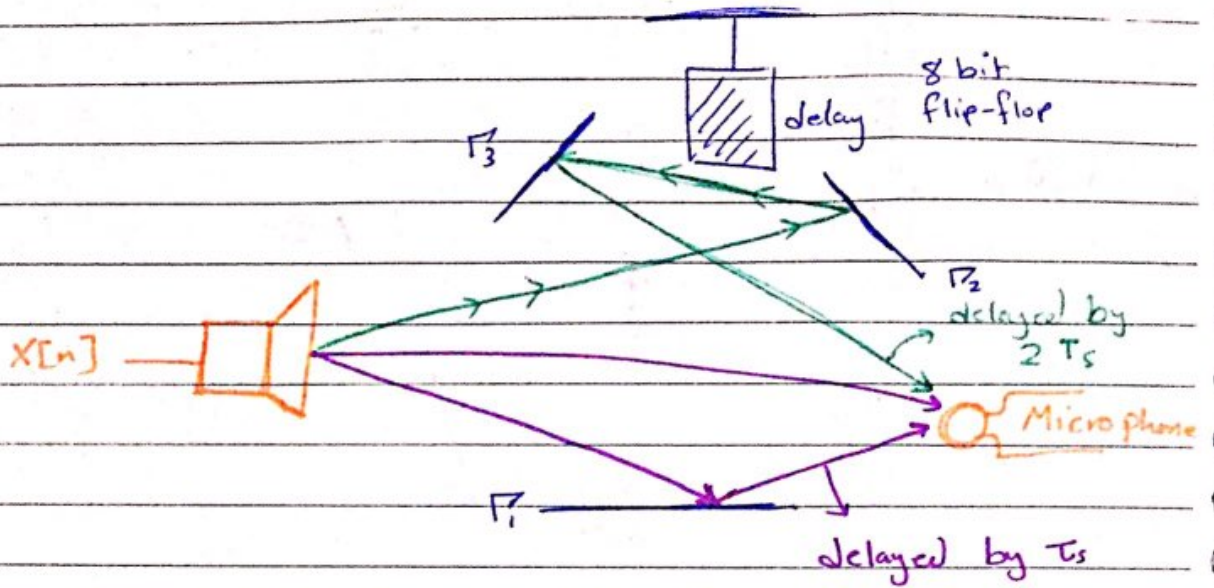
⇒ To determine  $N$  :

- 1) determine the order of the signal
- 2) how much we fit the actual shape.

$X[n]$  must be sampled and quantized to say that  $X[n]$  digital

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if  $x[n]$  is only sampled then its discrete



$$\text{out} = x[n] + a_1 x[n-1] + a_2 x[n-2]$$

$$a_1 = \Gamma_1, \quad a_2 = \Gamma_2 \cdot \Gamma_3$$

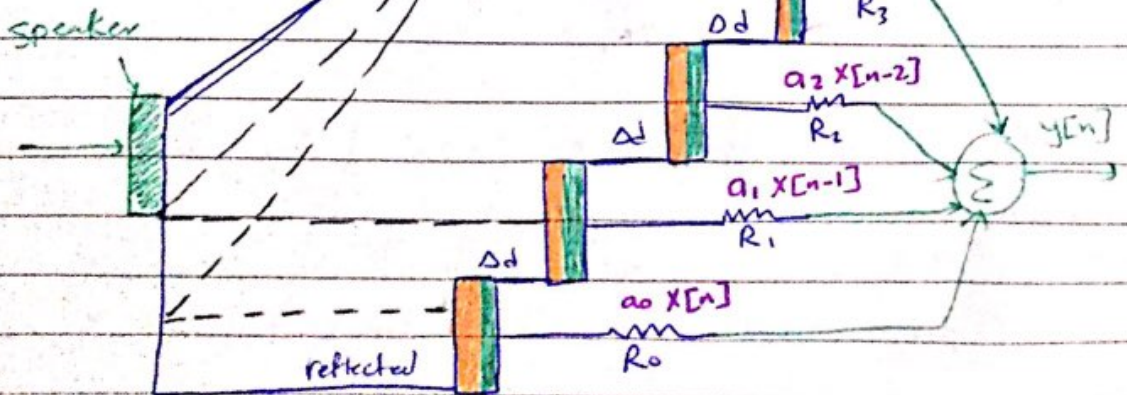
assume  $T_s = 1 \mu s$

$$\Delta d = M_s \cdot T_s$$

$$M_s = 20.3 \sqrt{f}$$

Ex  $\Rightarrow \Delta d = 1000, 1 \mu$   
 $= 1 \text{ mm}$

### SAW Filter

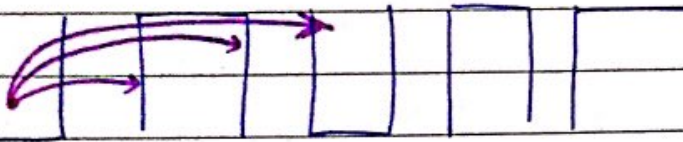


designed as an echo canceller

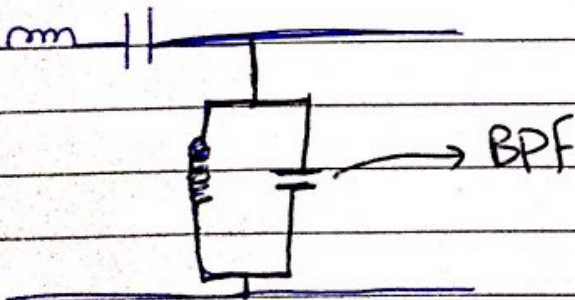
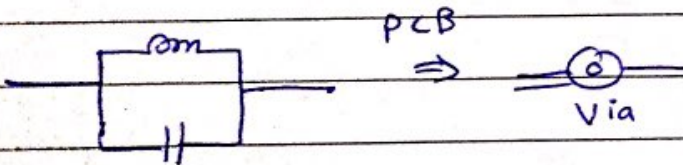
$$\text{let } h[n] = a x[n] + b x[n-1] + c x[n-2] + \dots$$

$$\text{then } h(z) = a z^0 + b z^{-1} + c z^{-2} + \dots$$

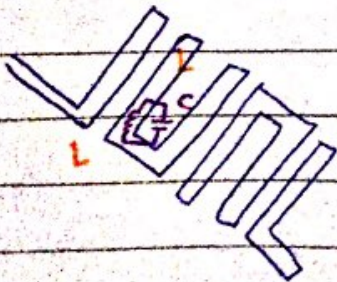
## Delayed EM wave



$$\sum_{i=0}^{I-1} \alpha_i x(t - \tau_i)$$



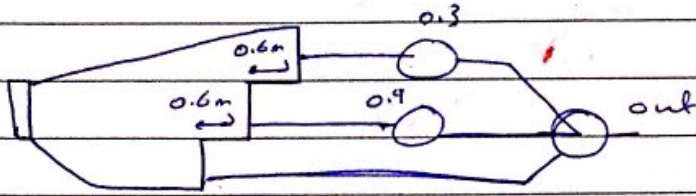
we need delay and sum



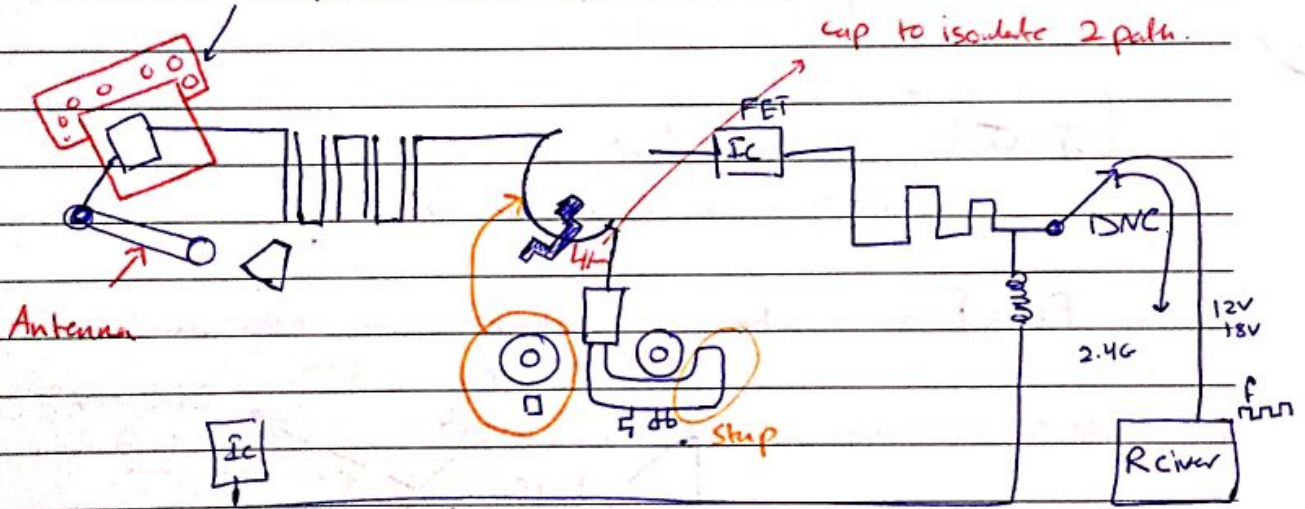


QUIZ 28

Design a SAW Filter with  $H(z) = 1 + 0.9z^{-1} + 0.3z^{-2}$   
if speed of sound is 600m/s.



amplifier for transistor.



stop → oscillator

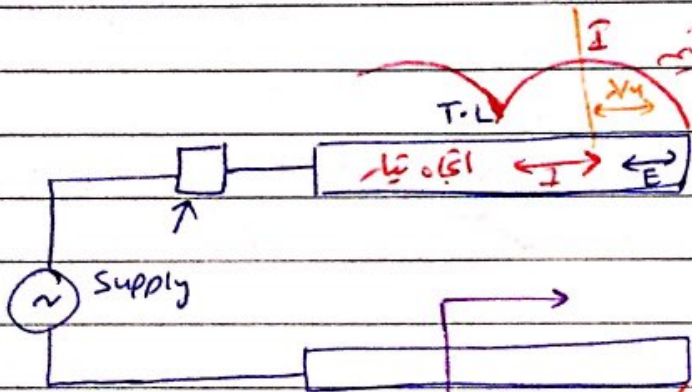
stubs → RF ic Transistor.

$$\lambda F = u$$

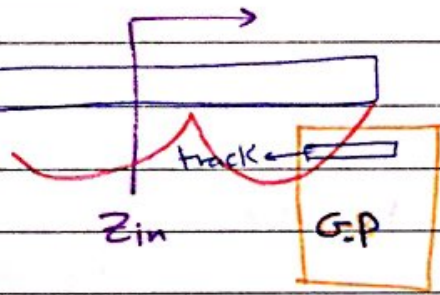
$$u = \frac{c}{\sqrt{\mu_r \epsilon_r}}$$

$$\lambda_{116} = 21.4 \text{ mm} \rightarrow \lambda/4 \rightarrow 5.35 \text{ mm}$$

$$\lambda_{126} = 25 \text{ mm} \rightarrow \lambda/4 \rightarrow 6.25 \text{ mm}$$



Standing wave.



G.P. = Ground Plane.

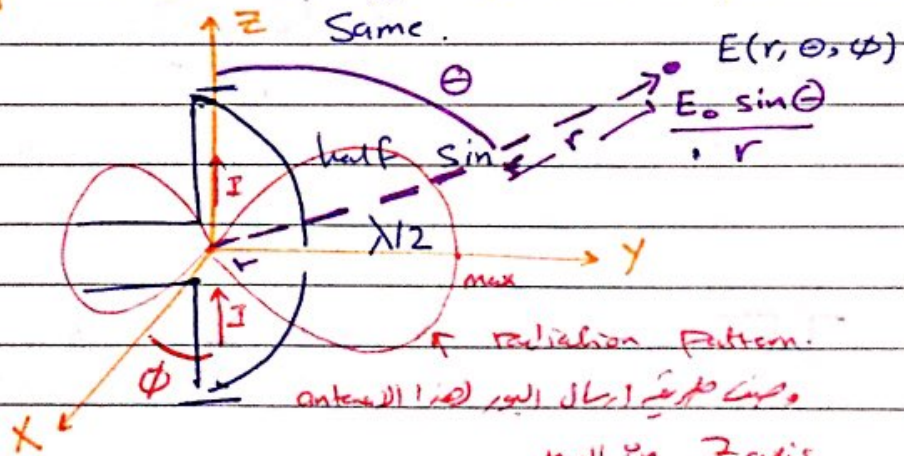
↳ reflection of track.

$$\Rightarrow \boxed{J = \sigma E} \quad \text{Ohm's law.}$$

$$\Rightarrow \boxed{E_{t1} = E_{t2}}$$

because voltage across two parallel the same.

Dipole :



current half sine  $\rightarrow E \sin$

\*  $\sin \theta =$  radiation pattern

Power Density  $\equiv P_r(r, \theta, \phi)$

$$\Rightarrow \boxed{P_r(r, \theta, \phi) = P_0 \frac{\sin^2(\theta)}{r^2}}$$

$$\boxed{P_0 = E_0^2}$$

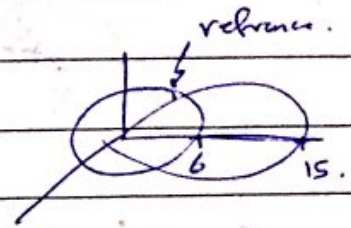
[55]

gain  $\Rightarrow$  max realization.

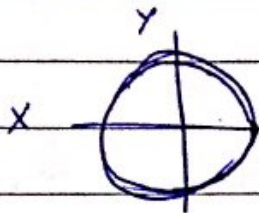
$\hookrightarrow$  ~~maximization~~

if antenna  $\rightarrow$  radiation circle

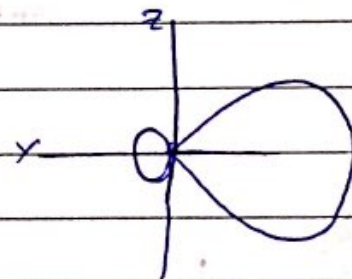
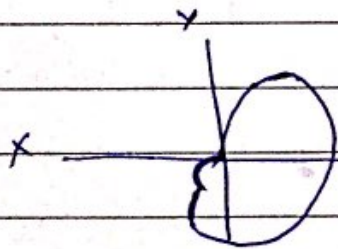
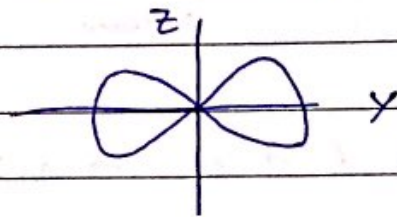
$$\text{gain} = \frac{15}{6}$$



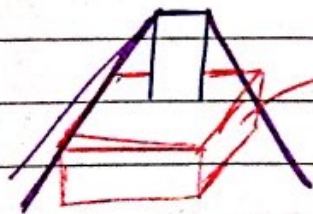
Horizontal.



Vertical radiation pattern.

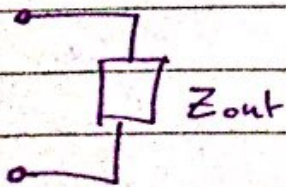


mono pole.



کیرنا GP سے بی بی ازل  
نظا بنو و سے برا اظلا مابن و و GP

input impedance  $\rightarrow$  o.c  $\rightarrow$   $\infty = Z$



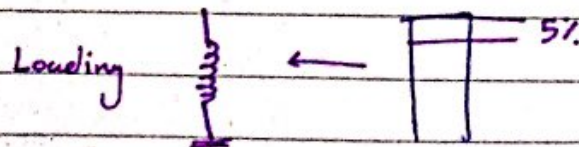
$$\text{dipole} = 53 - j72$$

$$= R_{rad} - X_{stored}$$

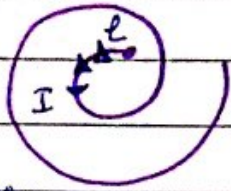
$\hookrightarrow$  radiated resistor

$\rightarrow$  stored Energy

(Loading antenna) 5% antenna 1 vea lea jela sy



# Spiral

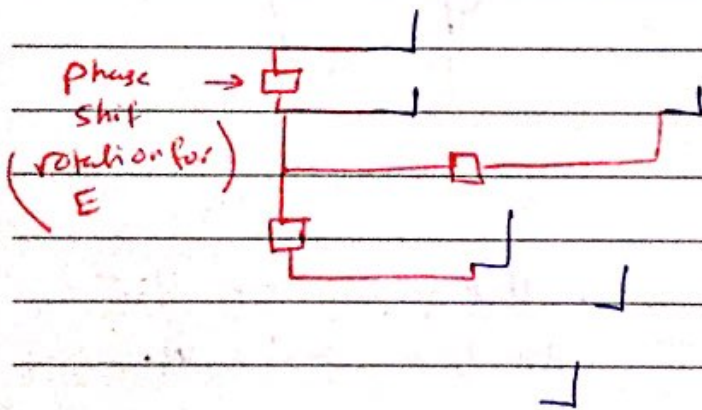


$$E = \sum_{i=0}^{\infty} \vec{E}_i = \int \vec{E}_i dl$$

length of antenna.  $\leftarrow L$

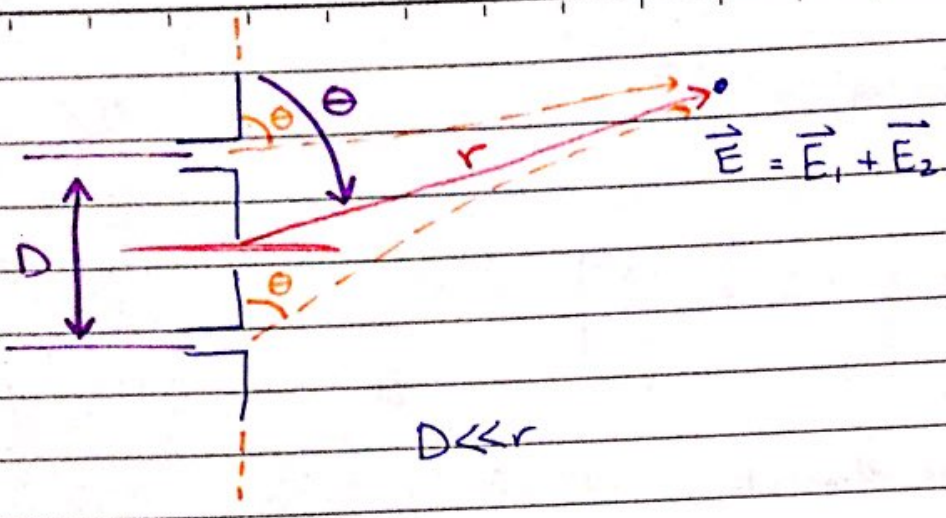
→ typical size →  $\lambda/2, \lambda/4$

\* array of antenna  $\lambda/4, \lambda/2$



can.

you ↑ control radiation pattern by control the phase shift.



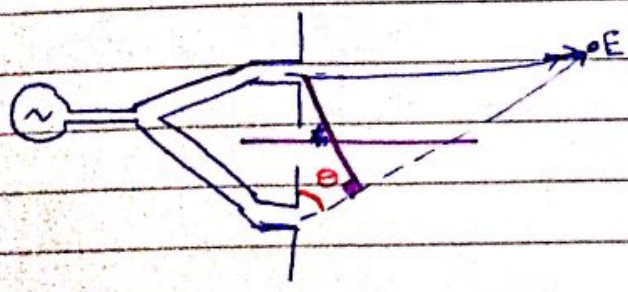
NFC  $\Rightarrow$  coupling induction.  
look like a transformer

$$\vec{E}_1 = \frac{E_{01}}{r} \sin \theta$$

$$\vec{E}_2 = \frac{E_{02}}{r} \sin \theta$$

if 2 signal coherent  $\rightarrow E_{01}, E_{02} \Rightarrow$  constant.  
depend on dimension.

function generator.



$$\Delta d = D \cos \theta$$

$$\Delta \theta = \Delta d \frac{2\pi}{\lambda} = \frac{2\pi D}{\lambda} \cos \theta$$

$$\vec{E}_2 = \frac{E_{01}}{r} \sin(\theta) e^{-j\Delta\theta}$$

$$\vec{E} = \underbrace{\frac{E_{01}}{r} \sin\theta}_{\text{R.P of one element.}} \underbrace{\left[ 1 + e^{-j\Delta\theta} \right]}_{\text{A.F}}$$

R.P of one element.  $\hookrightarrow$  A.F = Array Factor

RP = Radiation Pattern.

AF  $\Rightarrow$  amplitude of electric field.

$$AF = 1 + e^{-j \frac{2\pi D}{\lambda} \cos\theta}$$

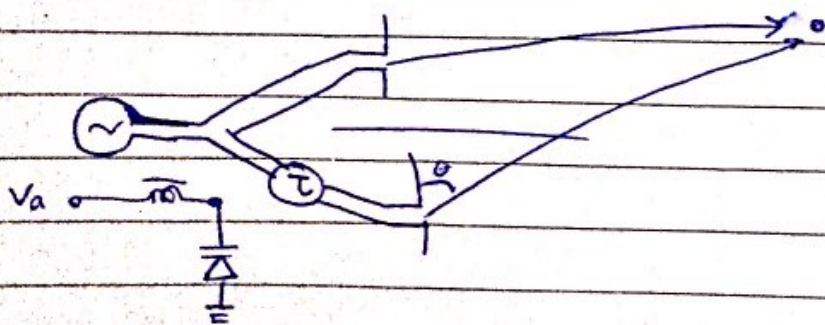
2 elements in  $\vec{r}$  direction  $\vec{r}_1$  &  $\vec{r}_2$  \*

\* correlation coefficient we assume = 0

2 ~~antennas~~  $\rightarrow$  are independent  
antennas  $\rightarrow$  antenna.

$\rightarrow$   $\uparrow$  correlation  $\rightarrow$   $\downarrow$  AF.

[2] add delay :-



$$\Delta\Theta_{new} = \frac{2\pi D}{\lambda} \cos\theta + \frac{2\pi \tau}{T}$$

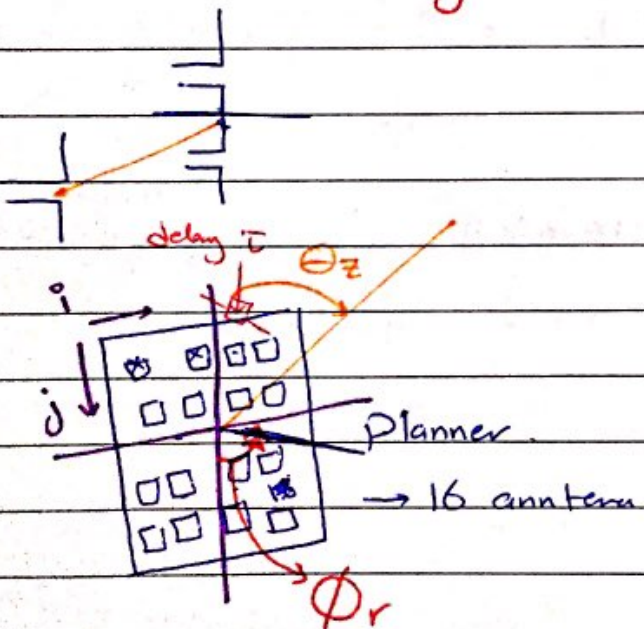
$$AF = 1 + e^{j2\pi \left( \frac{\tau}{T} - \frac{D}{\lambda} \cos\theta \right)}$$

maximize ~~in~~ when  $\frac{\tau}{T} = \frac{D}{\lambda} \cos\theta$

$\uparrow \tau \rightarrow \max \theta \uparrow$

$\rightarrow$  Changing  $\tau \rightarrow$  can maximize  $\theta$ .

\* 2 dimensional array :-



$$AF = 1 + e^{j2\pi \left( \frac{\tau}{T} - \frac{D}{\lambda} \cos\theta \right)}$$

$$= e^{-j\pi \left( \frac{\tau}{T} - \frac{D}{\lambda} \cos\theta \right)} + e^{j\pi \left( \frac{\tau}{T} - \frac{D}{\lambda} \cos\theta \right)}$$

$$= 2 \cos \left( \frac{\tau}{T} - \frac{D}{\lambda} \cos\theta \right)$$

$$AF = 2 \sum_i^{I/2} \sum_j^{J/2} \cos \left( \frac{T_{ij}}{T} - \frac{d_{ij} \cos \theta}{\lambda} - \frac{d_{ji} \cos \phi}{\lambda} \right)$$

Maximum  $\cos(0) = 1$

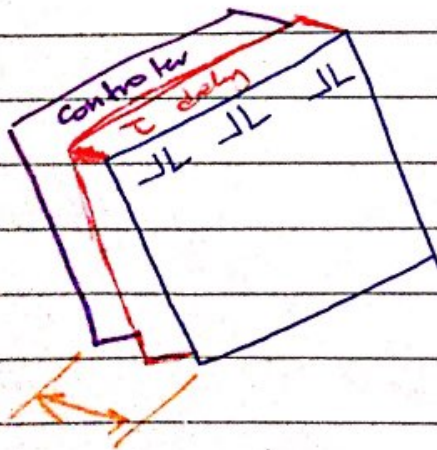
$$\frac{T_{ij}}{T} = \frac{d_{ij} \cos \theta}{\lambda} + \frac{d_{ji} \cos \phi}{\lambda}$$

$$d_{ij} = d_{ji} = \lambda/2$$

$$\frac{T_{ij}}{T} = \frac{i}{2} \cos \theta + \frac{j}{2} \cos \phi$$

$$i \rightarrow i/2 \rightarrow 2 \cos \text{ etc } \dots$$

$$\text{Max} = I * J$$



Smart Antenna  
Beam Stearing  
forming.

short antenna → patch antenna



# \*Patch Antennas 84

18/4 WED



$$R_{\Omega} = \frac{L}{\sqrt{2} \delta \pi \alpha}$$

$\delta \equiv$  skin depth

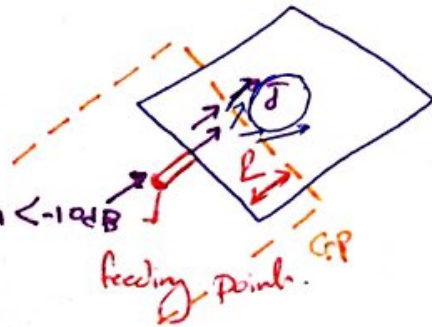
## ⇒ Web antenna

- Small antennas with respect to
- low gain
- ~~omni~~ omni-directional ⇒ radiation pattern.  
X-y → circle.

feeding point



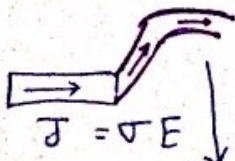
Skinner 50 Ω impedance



overlap  
 $L \Rightarrow$  distance btw G.P and patch antenna.

input signal → matching

\* Ground Plane → to support radiation  
↳ to control the BW of antenna.



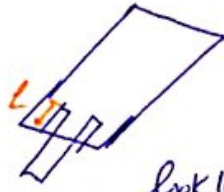
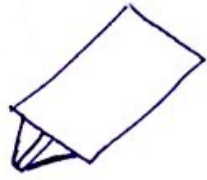
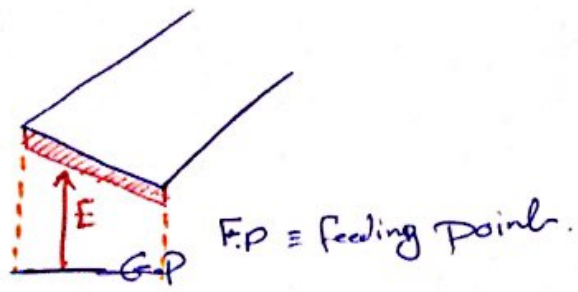
$\vec{J} = \sigma \vec{E}$

$\sum \vec{E}$

total  $\vec{E}$

$$\vec{E} = \frac{\int d\vec{J}(r, \theta, \phi)}{\epsilon_0}$$

line integrat.

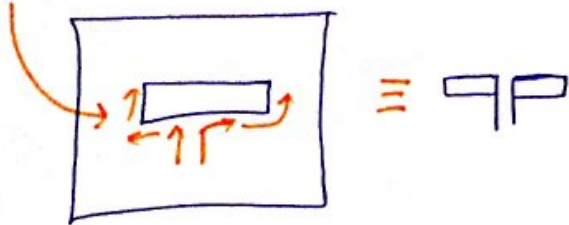


look like stub



curved stub

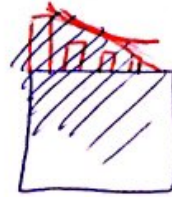
current.



\* tapering  $\Rightarrow$

- $\rightarrow$  increase operation of Antenna.
- $\rightarrow$  " BW.

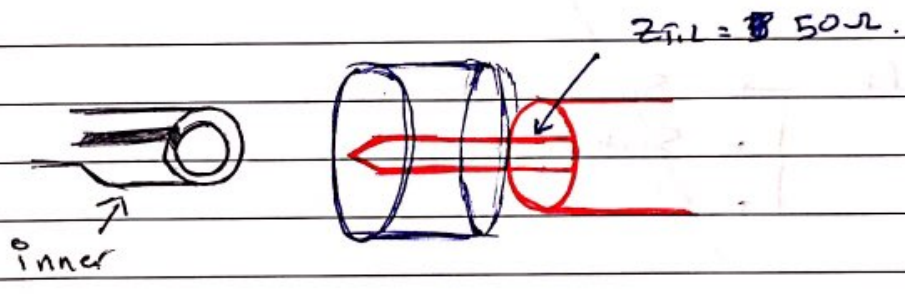
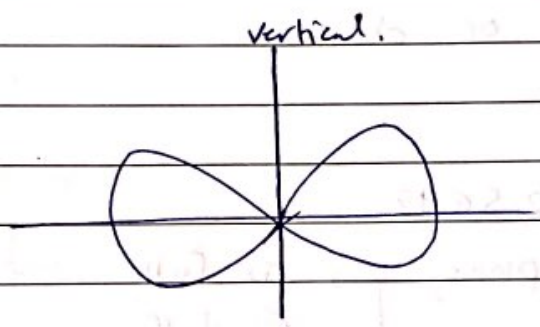
~~XXXXXXXXXX~~



**QUIZ 3**

Draw the V-shape radiation pattern for a  $\lambda/4$  monopole antenna.

Solo

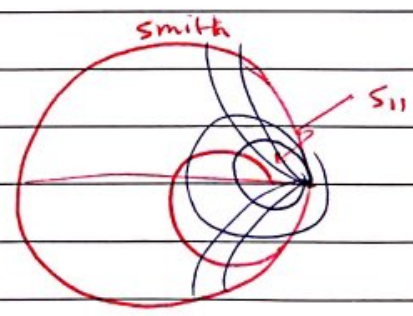


\* Diode 1N4007

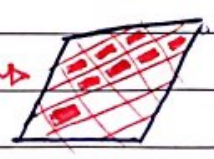
N-type

بند عرضی از  $z=0$  به  $z=l$  ← BAND width  
 (cm)  $0.1 = l$   $\lambda/10$   
 ← convert to.

وینا با  $z=0$  و  $z=l$  است، بنابراین هم  $z=0$  و  $z=l$  اول و آخر است  
 ← BW



current distribution in ground plane →



Search → GPS Receiver antenna

# Project :

Design a patch antenna using ADK in HFSS  
freq = 2.5 GHz

نرسم اسكل داخل ال Patch antenna

↳ change X for ground plane  
→ X full  
↳ X half.

result  
→ S<sub>11</sub>  
→ smith chart  
→ اكي قبليه ال denoub.

30/4 \* التالى الالين

**QUIZ 4**

What are the effect of ground plane on the patch antenna ?!

Sol: Control the BW

- a patch antenna in the x-y plane with full G.P does the R.P exist in the -ve z-direction ?! why ?!

Sol: Yes → if thin → current distribution on patch antenna  
No → thick.

↓  
shielding

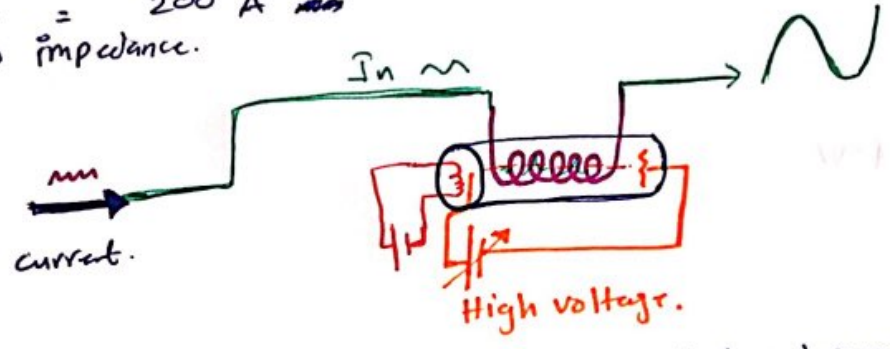
Q ↓ → BW ↑

↳ **R** in the path of circuit → losses.  
I<sup>2</sup>R → Noise.

↳ **L** → coupling effect

TWT : Troubling wave ~~transmission~~ tube.

$\frac{10KW}{50} \rightarrow \text{impedance} = 200 \text{ A}$

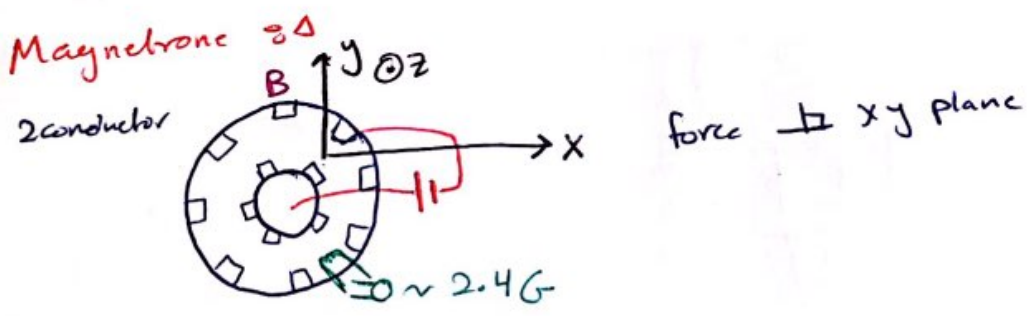


change high voltage  $\rightarrow$  to change electron beam  $\rightarrow$  current

\* Coherent with  $\downarrow$  signal external

TWT  $\Rightarrow$  use electric force to modulate the current using input signal.

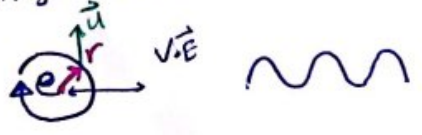
for High oscillator  $\Rightarrow$  we use Magnetron



for transition for electric field out  $\odot$

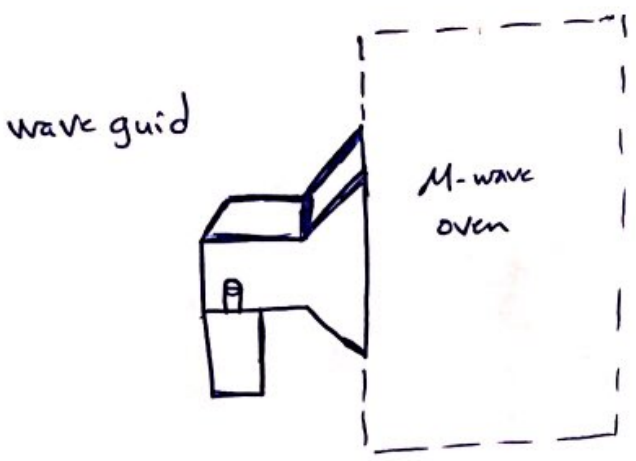
if connect volt  $\rightarrow$  electric field  $\rightarrow$  edges  $\rightarrow$   $\downarrow$  B magnetic field  $\rightarrow$

Voltage difference  $\rightarrow$  reduce magnetic field.

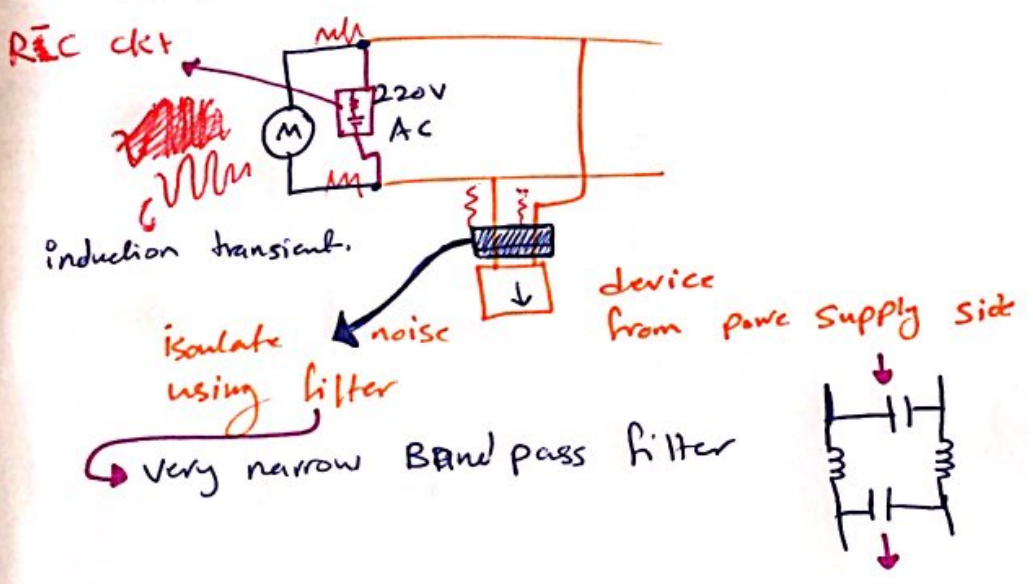


$\uparrow$  voltage  $\rightarrow$   $\uparrow$  force  $\rightarrow$  ~~wave~~

can select the frequency → ~~mechanical~~ tuning



- electro magnetic compatibility → 8
- ↳ matching btw input, output.
- ↳ power lines

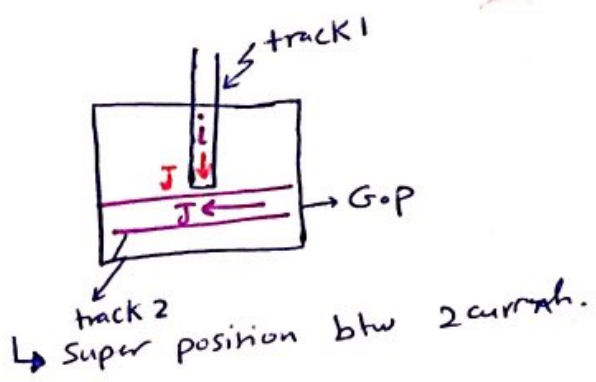


Shielding → size device  
 → device کی سائز اور کیمیا

- ① electric → current لا بہن لگای
- ② magnetic

EMI:4

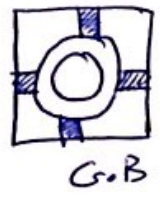
- Radiation
- Coupling
- G.L  $\equiv$  ground Loop



Via  $\rightarrow$  parallel LC circuit



via  $\rightarrow$  Ground plane  $\rightarrow$  not continuous connection with ground plane.



to create

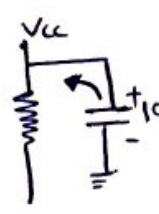
Via in power supply have 2 effect  $\rightarrow$  thermal effect.

G.L  $\rightarrow$  more than one voltage.

Qo  $\rightarrow$  0V  $\rightarrow$  dual polarity amplifier circuit.

Low Drop Out  $\equiv$  LDO regulator.  
input 3.7  $\rightarrow$  output 3.3

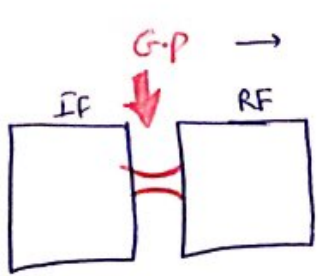
IC  $\rightarrow$  C = 100nF



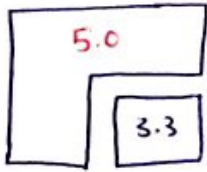
tanck  
sabit  $\rightarrow$  2k $\Omega$  LC

$\rightarrow$  result (no enough current to drive it)

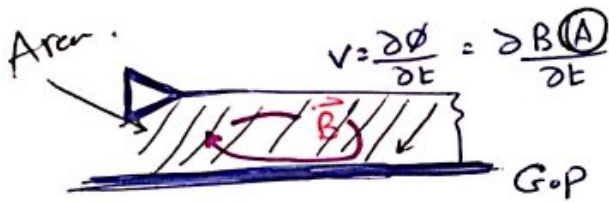




~ 12  $\mu$ s  
G.L is re



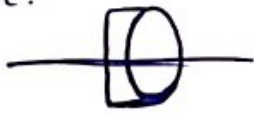
Coupling  $\rightarrow$  2 current have 2 magnetic field.  $\rightarrow$  induce voltage at point.



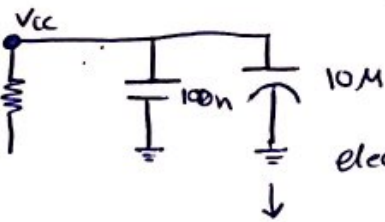
\* ~~increased voltage~~

$\rightarrow$  Area  $\downarrow$   $\rightarrow$  induced voltage  $\downarrow$

Ferrite.



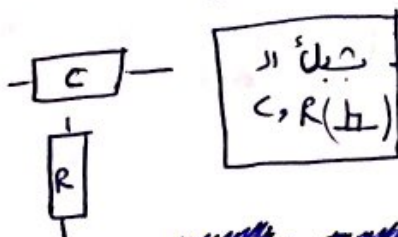
$M_r > 15K$



electro light  $\rightarrow$  charge  $\downarrow$

Slow variation)  $\downarrow$   $\downarrow$  for voltage.

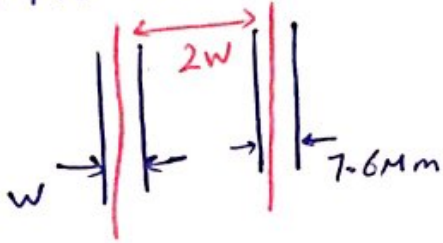
Ms  $\rightarrow$  long time



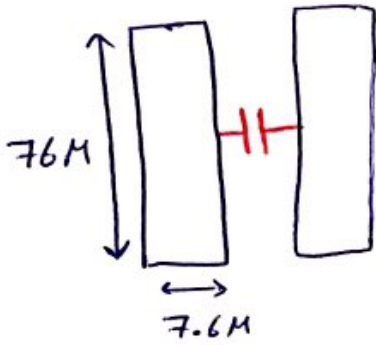
thermal coupling  $\sim$   $\sim$   $\sim$

~~smaller~~

WTW rule  $\Rightarrow$

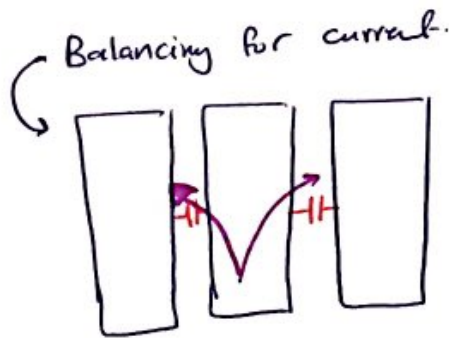


high  $\rightarrow$  30 mile  $\approx$  76M.



Capacitance  $\uparrow$   
high  $\gg$  width.

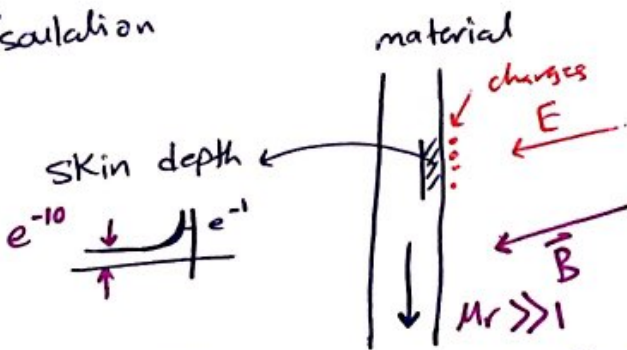
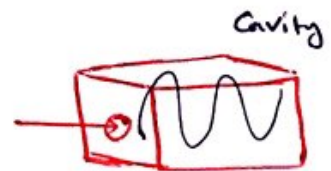
Guide for electron  $\rightarrow$  track



### Radiation:-

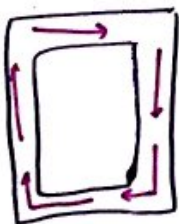
have regulation for radiation.

- $\rightarrow$  external  $\neq$
  - $\rightarrow$  internal =
- isulation



IL  $\rightarrow$  Insertion loss

log S21



$\mu_r \gg 1$   
 $\sigma \uparrow$

$IL \geq 40\text{dB}$

$\rightarrow$  (iron) best material

**Quiz 5**

a PCB track with loop area with the ground =  $10\text{mm}^2$   
 Find the external magnetic field that induces a 15 Volt  
 at the terminal at  $f = 1\text{GHz}$ .

Sol:-

$$V_{mf} = -N \frac{d\phi}{dt}$$

$N = 1 \rightarrow$  one loop

$$V = A \cdot \text{area} \cdot \omega$$

$$15 = A * 10 \times 10^{-6} * 2\pi * 10^9$$

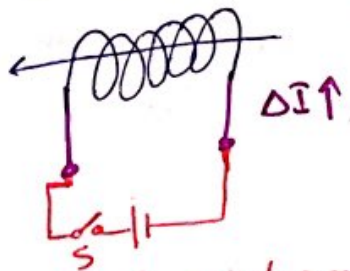
$$A = 238.7 \text{ MT}$$

worst case  $\rightarrow$  Maximum  
 cos  $\rightarrow$   $\frac{E_{mf}}{E_{\text{loop}}} \sim \frac{L^2}{r^2}$

$A = 238 \text{ MT}$

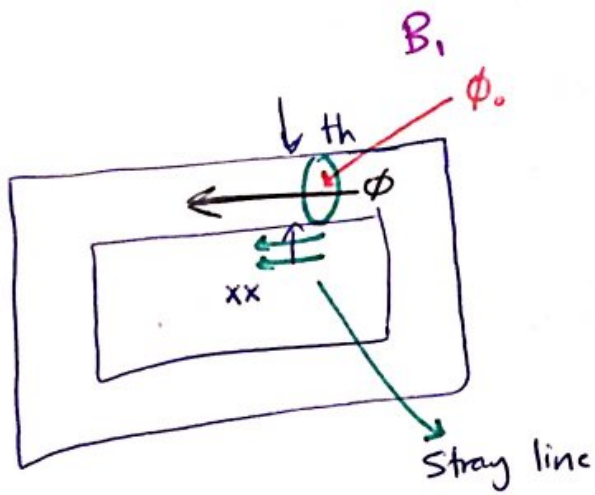
$\sim d^{-8}$  as a function of distance.

~~...~~  
 \* **Durty bumps**  
 $B = \mu I n$



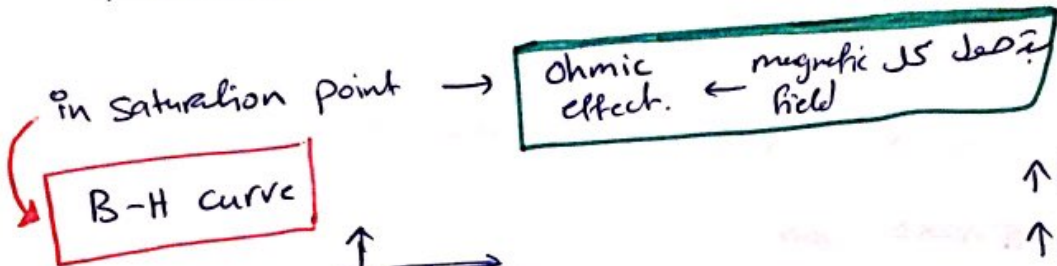
closed switch  $\rightarrow$  magnetic field impulse.

\* magnetic field  $\rightarrow$  current  $\rightarrow$  electrons or proton.

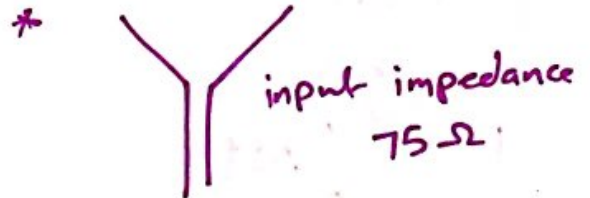
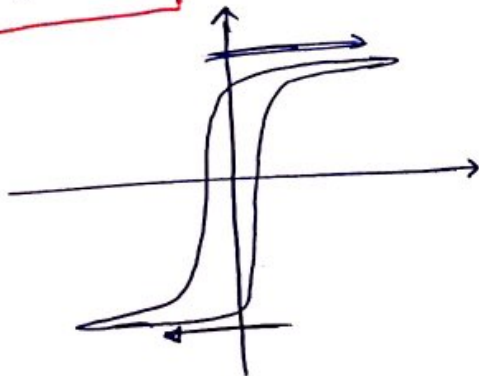


th = thickness

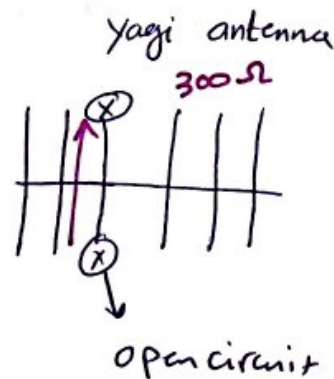
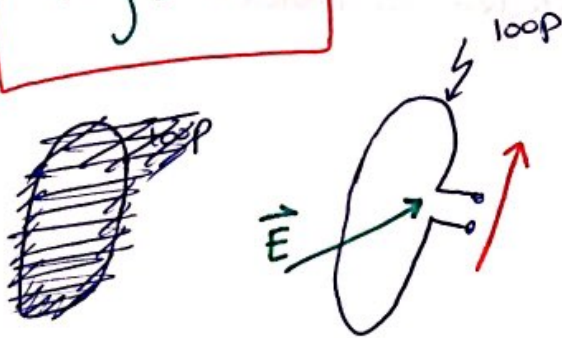
thickness  $\uparrow$   $\rightarrow$  cross section Area  $\uparrow$



$\uparrow$  freq  $\rightarrow$   $\uparrow$  T (تردد)  
 $\uparrow$  Area  $\rightarrow$   $\uparrow$  T



$$V = \int E \cdot dl$$



THE END