



Measurements

Summer017

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Measurements

5/6/2017

Overview :-

- 1] statistical measurements (mean, variance)
helpful for control & planning
ex. voltage of house to monitor drop
ex. controlling home devices like fridge, microwave...
- 2] effective sample : how many readings needed
& for how long to get gaussian curve 
- 3] state estimation, since measurement for all houses is costly & objected to error due to communication or meas. devices
- 4] meters (voltmeters, ameters) whether analog/digital
in terms of design & possible errors
- wattmeter measures energy watt/hour
- all meters will change to smart meters
- 5] bridges ex. temperature transducer \rightarrow voltage
- 6] earthing systems

Grading :-

First. 20%

Second 30%

Final 50%

Bonus Project 5% \rightarrow Labview, transducer

6/6/2017

Characteristics of Measurement Instruments &

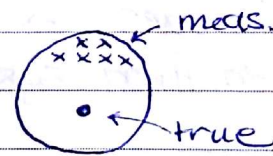
- Accuracy: how close is the measured value to the true value

$$\overset{\text{meas.}}{x} \text{ --- } \overset{\text{true}}{x}$$
 $\pm x\%$ tolerance/inaccuracy \rightarrow the smaller the better
 \hookrightarrow percentage % of the measured/full scale

[Ex] a voltmeter measured 10V, accuracy 10%, full scale, range is 0-15V, find true value??
 sol: true value = $10 \pm (10\% \cdot 15) = 8.5 - 11.5$ V

- * analog meas. devices work thru torque of current
- * digital meas. devices work thru A/D converters
 sampling, quantization ...

- Precision: reproduce ability in the measurements shown
 we note low accuracy & high precision



?? what's the metric used to describe low/high

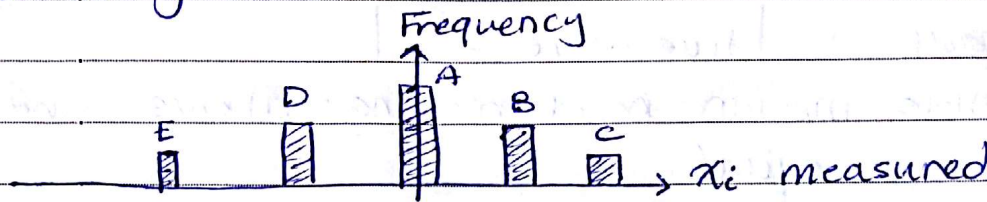
Precision \rightarrow mean (from min to max) $\left| \begin{array}{ccc} \text{min} & \text{mean} & \text{max} \end{array} \right.$
 \rightarrow standard deviation σ $\left| \begin{array}{ccc} \text{نطاق القراءات عن بعد} & & \end{array} \right.$

$$\sigma^2 = E[(x - \bar{x})^2]$$

variance \downarrow expectation \downarrow mean value
 mean القراءات عن بعد \downarrow (integration)

$$\bar{x} = E[x] = \frac{1}{N} \sum_{i=1}^N x_i$$

* Histogram:



to get the mean:

$$\bar{x} = \sum_{i=1}^N x_i * Pr(x_i)$$

where $Pr(x_i) = \text{Freq} / \# \text{ total measurements}$

to get standard deviation:

$$\sigma^2 = \sum_{i=1}^N (x_i - \bar{x})^2 * Pr(x_i)$$

assume uniform

$$\sigma^2 = \frac{1}{N} \sum_{i=1}^N (x_i - \bar{x})^2$$

* comparison btwn (mean & standard deviation):

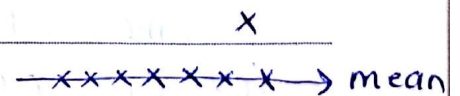
if 1 million readings were taken, & only 2 readings were far from mean

mean metric → conservative

low precision

takes highest

& lowest only



σ metric → high precision
considers their probabilities



Accuracy → | true value - \bar{x} |

percentile, median: no of readings above and below are equal

*note: accuracy cares about true value while precision cares about mean value.

⊠ Resolution: detection of small changes that could happen, minimum step change that can be captured

⊠ Ex] a digital voltmeter A/D uses 12-bits how much is the resolution knowing that the full scale is 5 V ??

sol levels = $2^{12} = 4096$

resolution = $5/2^{12} = 1.221 \times 10^{-3}$

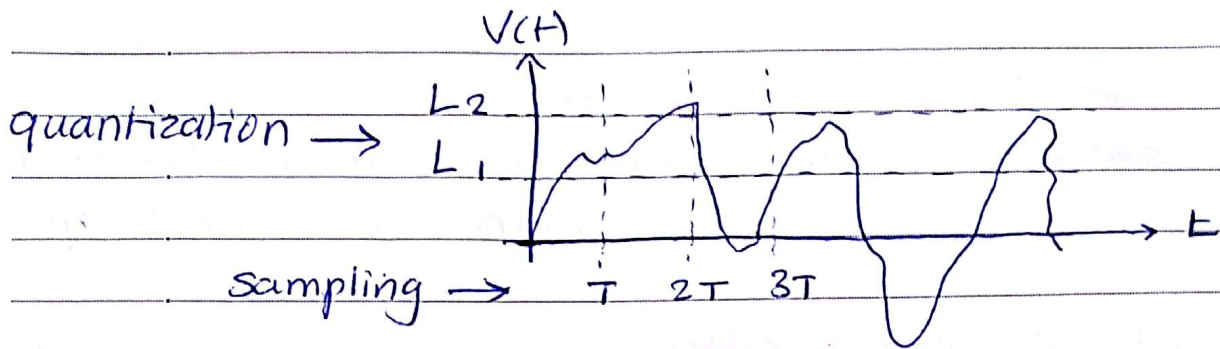
*remember (A/D): analog → sample → quantization → Encoder → bits

assume 2 bits → we have 4 encoded levels

(00) L₁ (01) L₂ (10) L₃ (11) L₄

of Levels = $2^{\text{\# of bits}}$

the closer the levels to each other, the higher the resolution



$$\text{step size/resolution} = \text{full scale} / \# \text{ of levels}$$

Sensitivity: how does change in input change the output

$$\text{Sensitivity} = \Delta \text{output} / \Delta \text{input}$$

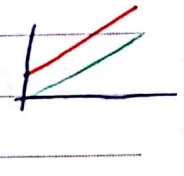
ex. $C = \frac{\epsilon A}{d}$ how does C change when A & d change??

Error Definition & Types :-

- 1] systematic errors: cause is known, can be eliminated
- 2] random errors: cause is unknown, use probability

* systematic errors offsets:

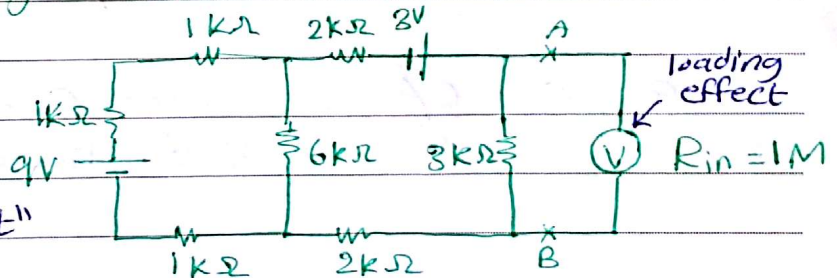
- ↳ constant (like zero offset: shift starts @ zero)
- ↳ % reading like scale offset



slide 8 **Ex** in the ckt shown find:

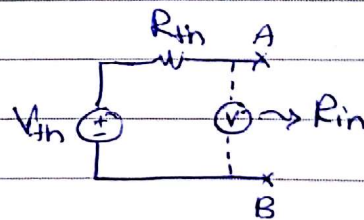
- 1] error in the measurement
- 2] $R_{volt\ meter\ (in)}$ that will give error smaller than 1%.

here we have systematic error due to "loading effect"



sol find true value

- 1] $R_{th} = 2k\Omega$
- ↳ ideal/no error/expected $R_{in} = \infty$
- ↳ measured $R_{in} = 1M$



$V_{expected} = V_{th}$

$V_{measured} = V_{th} * \frac{1M}{1M + 2k}$

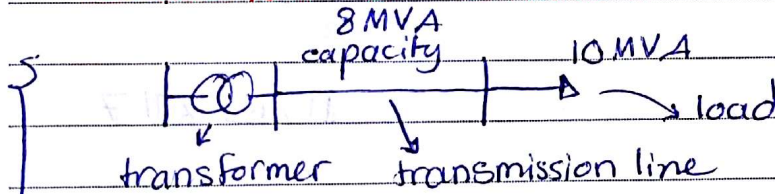
* types of errors \rightarrow relative
 \rightarrow absolute

$$\text{error \%} = \frac{V_{th} - 0.998 V_{th}}{V_{th}} \times 100\% = 0.2\%$$

$$\textcircled{2} \quad \frac{V_{th} - (R_{in}/R_{in} + 2k) V_{th}}{V_{th}} \times 100\% \leq 0.1\%$$

$$R_{in} \gg 198 \text{ k}\Omega$$

Reduction of Errors :-

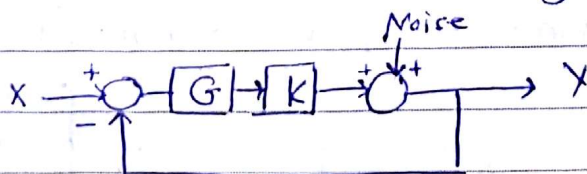


Active Network Management (ANM)

* increase in demand \rightarrow Reinforce Network
 add transformers, TL ...
 costly & takes time
 \rightarrow ANM
 control room to control
 2 MVA out of 10 MVA

here we note the importance of measurement in decision making & safety of network.

Negative Feedback: the target is to minimize error




transfer function:

$$y = (x - y)GK + N$$

$$y(1 + GK) = xGK + N$$

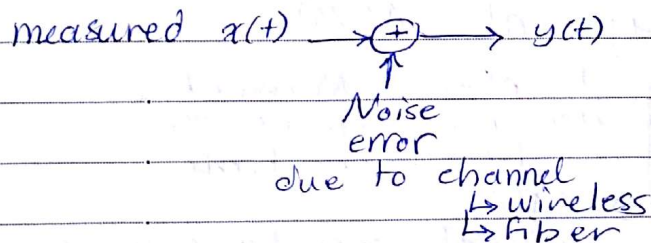
$$y = x \frac{GK}{1 + GK} + \frac{N}{1 + GK}$$

here we reduced effect of Noise by dividing it on gain

* assume noise is white gaussian 

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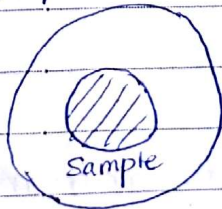
* Random Errors :-



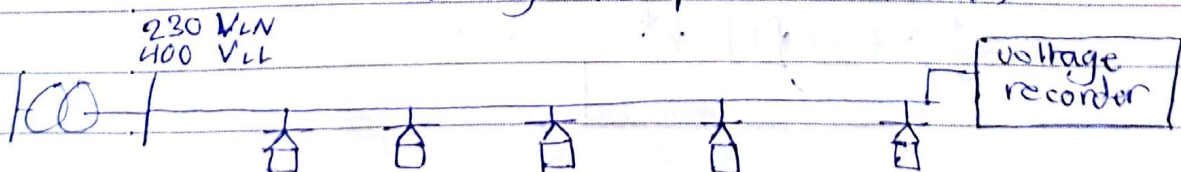
use probability calculate
↳ BER
↳ symbol error rate

* when the sample is small its hard to get gaussian curve

population



ex: when trying to reinforce a power grid, we cant take measurements for all the houses, we take a sample (preferably at the end during the peak demand)



from sample (\bar{X} mean, σ^2 variance) where $X \rightarrow$ voltage
 $\alpha \triangleq$ standard mean error (expansion for all population)

$\alpha = \frac{\sigma}{\sqrt{n}}$ \rightarrow standard deviation
 \rightarrow number of readings

X ?? which range of reading to choose?

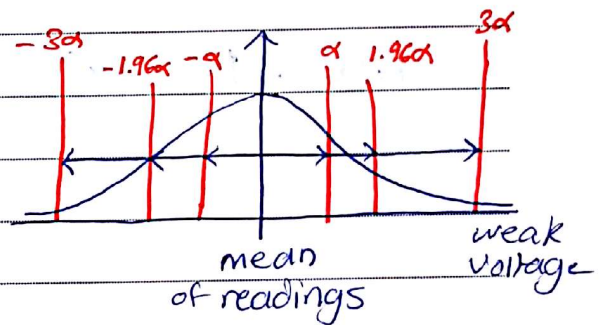
confidence level:

mean $\pm \alpha \rightarrow 68\%$

mean $\pm 1.96\alpha \rightarrow 95\%$

mean $\pm 3\alpha \rightarrow 99.7\%$

memorize these numbers



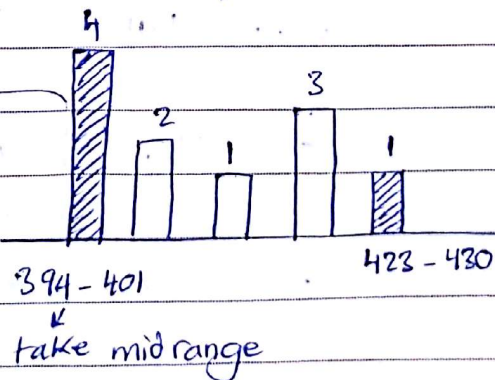
* confidence level: if you're 100% sure about your readings we take the biggest range ($\pm 3\alpha$)

* now we want to know if we need to reinforce the network based on readings:

-6% voltage drop $\leq V \leq$ +10% voltage rise
 $215 \leq 230 \leq 253$

* if given a histogram to find \bar{X} & σ^2

$\frac{294 + 401}{2} \times \left(\frac{4}{11}\right)$



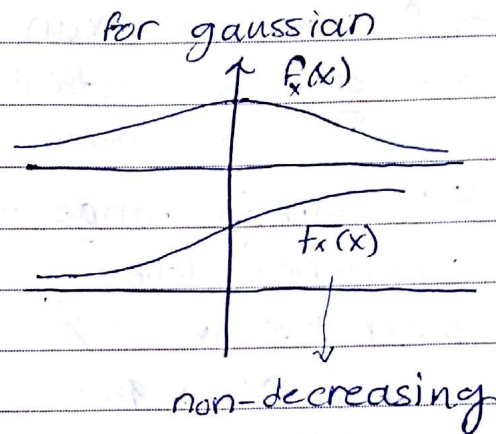
Cumulative Distribution Function CDF

$f_x(x)$ pdf

$F_x(x)$ cdf

$$F_x(x) = \int_{-\infty}^x f_x(x) dx$$

$$F_x(x_0) = \Pr(x \leq x_0)$$



12/6/2017

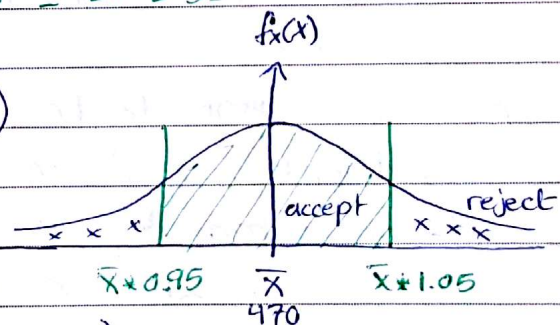
[Ex] 10,000 resistors, $R = 470 \Omega$, tolerance = $\pm 5\%$

Sample $\rightarrow \bar{x} = 470 \Omega$, $\sigma = 23.5 \Omega$

$$\Pr(\text{accepted}) = \Pr(0.95\bar{x} < x < 1.05\bar{x})$$

$$= \int_{0.95\bar{x}}^{1.05\bar{x}} f_x(x) dx$$

↳ from table



$$= \Pr(x < 1.05\bar{x}) - \Pr(x < 0.95\bar{x})$$

$$= F_x(1.05\bar{x}) - F_x(0.95\bar{x})$$

$$= F_z\left(\frac{1.05\bar{x} - \bar{x}}{\sigma}\right) - F_z\left(\frac{0.95\bar{x} - \bar{x}}{\sigma}\right)$$

$$= F_z(1) - F_z(-1) \rightarrow -ve$$

$$= F_z(1) - (1 - F_z(1))$$

$$= 2F_z(1) - 1 = 0.68$$

$$\Pr(\text{rejected}) = 1 - 0.68 = 0.32$$

$$\# \text{ of rejected} = 10,000 * 0.32 = 3200$$

t-test
chi-square

* remember to use table:

$$F_x(x_0) = F_z\left(\frac{x_0 - \bar{x}}{\sigma}\right)$$

[Ex] 10 readings from a voltmeter, express voltage reading as a range with 95.4%.

$$X = \{ \dots \}$$

$$\text{find mean } \bar{X} = \frac{1}{10} \sum X = 35.93 \Omega$$

$$\sigma^2 = \frac{1}{N} \sum (x_i - \bar{x})^2 = 0.365$$

$$\alpha = \frac{\sigma}{\sqrt{n}} = 0.115$$

$$\text{confidence level} = 95.4\% \rightarrow \bar{x} \pm 2\alpha = 35.95 \pm 2(0.115)$$

Aggregation of Errors

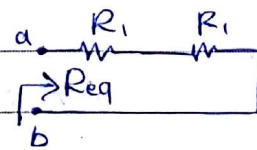
* to measure variable of interest as function of other variables.

* to find R_{eq} → measure terminals a & b

→ find R_1 and R_2

$$R_{eq} = R_1 + R_2$$

error error error



Error → limiting error (max, min)
→ most likely error

addition:

$$u = v + w \quad \text{where error: } v \pm m\%, w \pm n\%$$

↳ limiting error

$$u = (v+w) \pm (m\% \cdot v + n\% \cdot w) \quad \rightarrow \text{error is absolute}$$

$$\text{Ex } v = 10V \quad e = \pm 10\%, \quad w = 5V \quad e = \pm 10\%$$

$y = v + w$, what's the limiting error

$$\text{max } y \rightarrow (10 + 10\% \cdot 10) + (5 + 10\% \cdot 5) = 16.5V$$

$$\text{min } y \rightarrow (10 - 10\% \cdot 10) + (5 - 10\% \cdot 5) = 13.5$$

$$\text{error} = \pm (10\% \cdot 10 + 10\% \cdot 5) = \pm 1.5$$

$$y = 15 \pm 1.5$$

multiplication

$$u = v \cdot w$$

↳ limiting error

$$u = v \cdot w (1 \pm e) \quad \rightarrow \text{error is percentage}$$

$$= v \cdot w (1 \pm (m+n))$$

if we have $f = f(v_1, v_2, v_3, \dots, v_n) \rightarrow$ complicated
use partial derivatives

$$\text{Ex } F = \frac{EAd}{e}, \text{ variables } (A, d, e)$$

$$\Delta F = \Delta A \cdot \frac{\partial F}{\partial A} + \Delta d \cdot \frac{\partial F}{\partial d} + \Delta e \cdot \frac{\partial F}{\partial e}$$

$$= \Delta A \cdot \frac{F}{A} + \Delta d \cdot \frac{F}{d} + \Delta e \cdot \frac{F}{e}$$

$$\left| \frac{\Delta F}{F} \right|_{\text{max}} = \frac{|\Delta A|}{A} + \frac{|\Delta e|}{e} + \frac{|\Delta d|}{d} \quad \left| \frac{\Delta F}{F} \right|_{\text{min}} = -\frac{\Delta A}{A} - \frac{\Delta e}{e} - \frac{\Delta d}{d}$$

13/6/2017

Probable Values

$$R_1 = 10 \Omega \pm 10\% \quad 9 \Omega \leq R_1 \leq 11 \Omega$$

$$R_2 = 10 \Omega \pm 10\% \quad 9 \Omega \leq R_2 \leq 11 \Omega$$

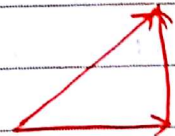
↳ Limiting error (assuming $R = R_1 + R_2$)

$$R_{\max} = 22 \Omega \quad R_{\min} = 18 \Omega$$

↳ Probable error

$$R_1 + R_2 \pm e$$

$$20 \pm \sqrt{1^2 + 1^2} = 20 \pm \sqrt{2}$$



[Ex] Find Req of most likely error

	R_1	R_2
Req	220Ω $\pm 2\%$	330Ω $\pm 2\%$

$$Req = R_1 + R_2 \pm e$$

$$= 550 \pm \sqrt{(220 \times 0.02)^2 + (330 \times 0.02)^2}$$

$$= 550 \pm 7.93 \Omega \rightarrow \text{actual error}$$

$$= 550 \pm 1.44\% \times 550 \Omega \rightarrow \text{relative error}$$

$$\downarrow 7.93/550$$

[Ex] $P = VI$ find most likely error if

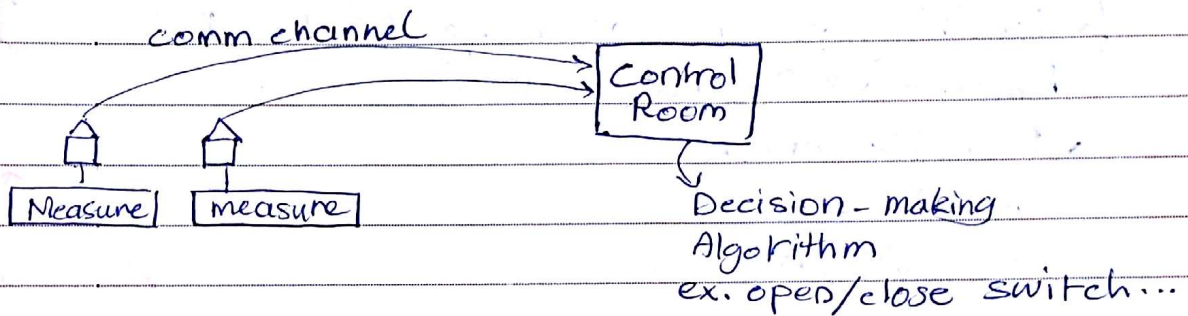
$$V = \pm 1\% \quad I = \pm 2\%$$

$$P = VI (1 \pm e\%)$$

$$e\% = \sqrt{(0.01)^2 + (0.02)^2}$$

State Estimation (not in the slides)

assume the power transmission network :-



* What's wrong with these measurements?

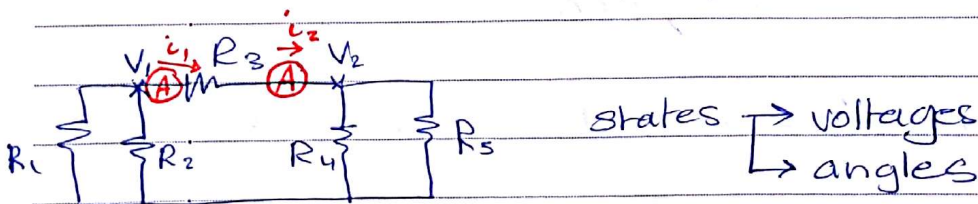
- errors in readings

ex. assume reading for power consumption of a house was 200kW (too large)

usually it ranges (5-10kW)

- high cost, number of readings is limited

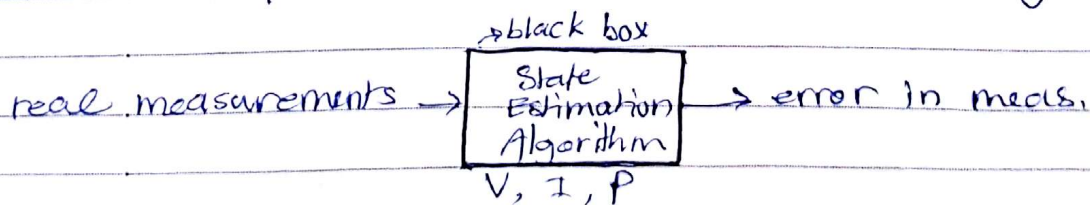
ex. only measure at end of T.L. 



which current (i_1 or i_2) is the correct one?

by estimating V_1 & V_2 we can calculate i

between V_1 & V_2 then decide which reading is correct



* Measurements \rightarrow Real
 \rightarrow Pseudo (historical)

* Black box function:-

$$\text{Min} \sum_{i=1}^m \frac{[Z_i - h_i(x)]^2}{\sigma_i^2}$$

where Z_i : measurements
 $h(x)$: model
 x : system state
 e : error
 m : # of measurements

$$Z_i = h_i(x) + e$$

steps \rightarrow find x (the states)
 \rightarrow find model $h(x)$

ex. $v_1 \xrightarrow{R} \textcircled{A} \xrightarrow{v_2}$

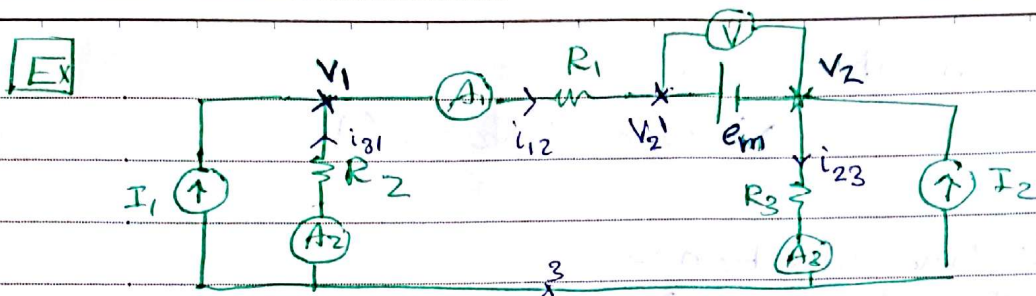
states: v_1, v_2

model: $\textcircled{A} = v_1 - v_2 / R$



* almost like when we know that a reading outside straight line of $V-I$ of resistor was an error

- ① system model : measurements = $h(\text{states})$
- ② sum squared error : write the summation
- ②ⁱ solution : hard, using matrices
- ③ find errors in measurements



where $R_1 = R_2 = R_3 = 1 \Omega$

known: states V_1, V_2, e_m

measurements $A_1 = 1A$ $A_2 = -3.2A$

$A_3 = 0.8A$ $V = 1.1V$

system model

$$\begin{bmatrix} 1 & -1 & -1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & -1 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ e_m \end{bmatrix} = \begin{bmatrix} A_1 \\ A_2 \\ A_3 \\ V \end{bmatrix} = \begin{bmatrix} 1 \\ -3.2 \\ 0.8 \\ 1.1 \end{bmatrix}$$

\downarrow $h_i(x)$ \downarrow states \downarrow measured

* note that the measured readings have error

(check using KVL or KCL)

$$-3.2 + 1 + 1.1 + 0.8 = -0.3 \neq 0$$

* to get the matrix $h_i(x)$:

$Z_i = h(x) + e \rightarrow$ purpose: write with respect to states

$$\textcircled{A_2} \quad i_{31} = \frac{V_1}{R_2} = V_1 = -3.2$$

$$\textcircled{A_3} \quad i_{23} = \frac{V_2}{R_3} = V_2 = 0.8$$

$$\textcircled{V} \quad V = e_m$$

14/6/2017

* note that we have 4 equations & 3 unknowns
thus we will not get a solution.
solution (states)

$$\begin{bmatrix} 1 \\ -3.2 \\ 0.8 \\ 1.1 \end{bmatrix} - \begin{bmatrix} 1 & -1 & -1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ e_m \end{bmatrix}$$

measured - model = error

$$\hookrightarrow Z_i - h(x) = e$$

Min (error)² → minimum square error

$$\text{Min} \left\{ (1 - V_1 + V_2 + e_m)^2 + (-3.2 - V_1)^2 + (1.1 - e_m)^2 + (0.8 - V_2)^2 \right\}$$

$$X = \begin{bmatrix} 3.125 \\ 0.875 \\ 1.175 \end{bmatrix} \begin{matrix} \rightarrow V_1 \\ \rightarrow V_2 \\ \rightarrow e_m \end{matrix} \quad \leftarrow \text{الحل المطلوب}$$

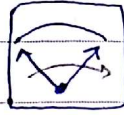
$$\text{error} = \begin{bmatrix} 1 \\ -3.2 \\ 0.8 \\ 1.1 \end{bmatrix} - \begin{bmatrix} 1 & -1 & -1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 3.125 \\ 0.875 \\ 1.175 \end{bmatrix}$$

Meters :-

DC Meter

Analog "Galvanometer"

↳ Ammeter
↳ Voltmeter



FULL scale

* calibration: to decide what is the full scale

AC Meter



Digital Voltmeter

15/6/2017

* Analog DC Meter

Permanent Magnet Moving Coil (PMMC)

* Full scale pointer \rightarrow internal resistance R_m
 $\rightarrow I_m$: full scale deflection current usually small $\approx 1\text{mA}$

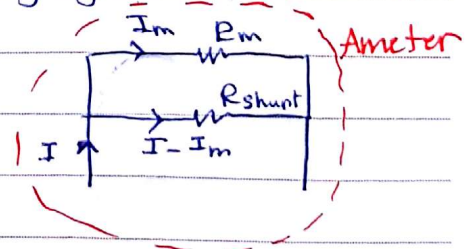
How to measure large current using galvanometer ??

we add resistance in parallel to increase the scale

$$I_m R_m = (I - I_m) R_{\text{shunt}}$$

$$R_{\text{shunt}} = \frac{I_m R_m}{I - I_m}$$

$$R_{\text{shunt}} = \frac{R_m}{\frac{I}{I_m} - 1}$$



[Ex] find R_{shunt} to measure 10mA using 1mA meter with internal resistance $R_m = 100\Omega$

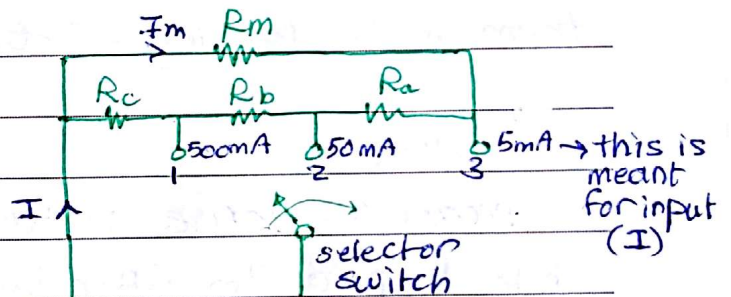
sol: $R_{shunt} = \frac{100}{\frac{10m}{1m} - 1} = 11.11\Omega$

* Multiple Range Ammeter

[Ex] $I_m = 50\mu A$

$R_m = 2400\Omega$

3 ranges $\left\{ \begin{array}{l} 5mA \\ 50mA \\ 500mA \end{array} \right\}$



sol: 5mA is when switch closes at position 3

↳ biggest shunt resistance

* $I_m R_m = (I - I_m)(R_a + R_b + R_c)$

$50\mu \times 2400 = (5m - 50\mu)(R_a + R_b + R_c) \dots \text{--- 1}$

at position 2 we read 50mA

* $(R_c + R_b)(I - I_m) = I_m(R_m + R_a)$

$(R_c + R_b)(50m - 50\mu) = 50\mu(2400 + R_a) \dots \text{--- 2}$

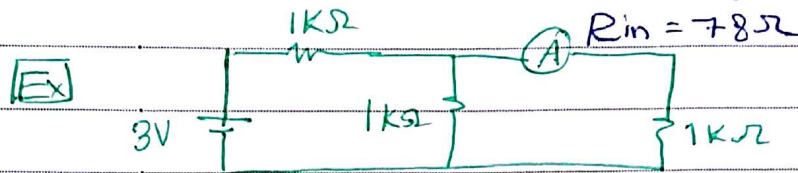
at position 1 we read 500mA

* $(I - I_m)R_c = I_m(R_m + R_a + R_b)$

$(500m - 50\mu) = 50\mu(2400 + R_a + R_b) \dots \text{--- 3}$

3 unknowns: $R_c = 2.18\Omega$ $R_b = 9\Omega$ $R_a = 21.81\Omega$

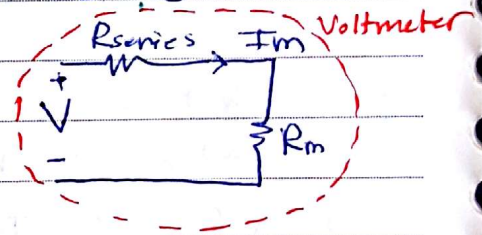
* Ammeter loading effect \rightarrow due to internal resistance
 what is the effect when adding R_{shunt} ?



sol:
 using current division solve once with 78Ω
 and then without it, the difference between
 them is the loading effect.

* DC Voltmeter

to measure large voltage we add R_{series}
 while keeping I_m within limits



Ex measure voltage = 10V

$R_m = 650\Omega$ $I_m = 1mA$

what's the suitable R_{series} ?

sol: $-10V + I_m R_{series} + I_m (650\Omega) = 0$

$R_{series} = 9.85k\Omega$

* for multi-range voltmeter we add selector switch
 of many resistances

* note: we might have ammeter & voltmeter
 in the same circuit.

* Sensitivity of Analog Meters

an ammeter measuring $50\mu\text{A}$ is more sensitive than that measuring 1mA .

$$S = 1 / I_{\text{FSD}} \Omega/\text{V}$$

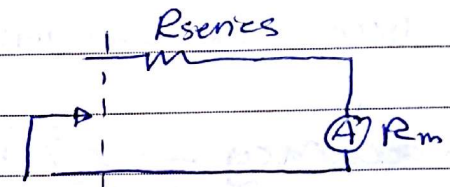
FSD: full scale deflection

$I_{\text{FSD}} \downarrow$ Sensitivity \uparrow

$$R_{\text{series}} = S * \text{Range} - R_m$$

↳ for voltmeter

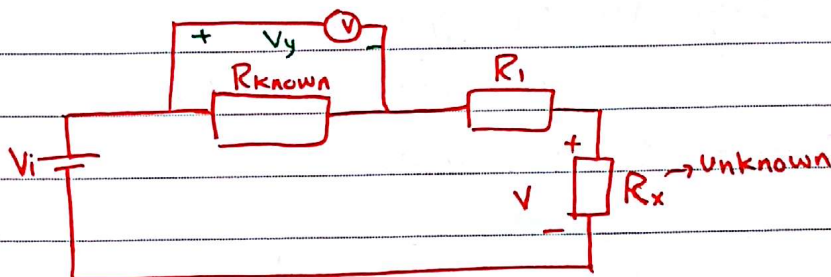
$$R_{\text{in}} = \frac{1}{I_{\text{FSD}}} * \text{Range}$$



20/6

* Ohmmeter \rightarrow Analogue
(Galvanometer)

$$R = \frac{V}{i}$$

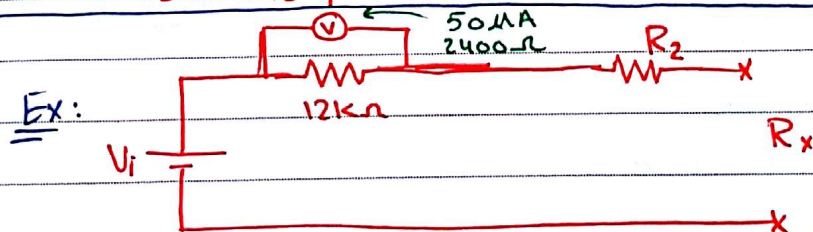


~~$R = \frac{V}{i}$~~
- Reverse Scaling - Non-linear

R_x large \rightarrow R_x small
"Short circuit"

$$V_y = V_i \cdot \frac{R_{known}}{R_i + R_x + R_{known}}$$

* The Relationship between them is not linear.



Desired $\Rightarrow R_x = 0$ (Full-Scale)

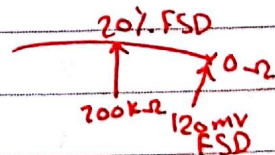
$R_x = 200k\Omega$ (20% Full Scale)

find R_2, V_i ??

~~50 uA~~ * FSD 50 uA $\xrightarrow{2400\Omega}$ ~~50 uA~~

$$V(FSD) = 2400 \cdot 50\mu A = 120mV = 0.12V$$

$$20\% V(FSD) = 0.024V$$



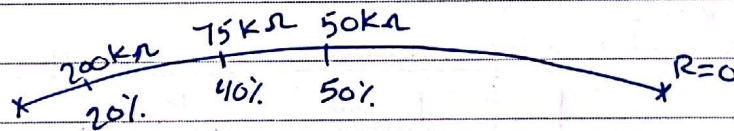
$$V_y = V_i \frac{(12k // 2.4k)}{(12k // 2.4k) + R_2 + R_x}$$

@ $R_x = 0 \Rightarrow$ FSD $\Rightarrow V_y = 0.12$

$$0.12 = \frac{V_i (12k // 2.4k)}{(12k // 2.4k) + R_2} \quad \text{①}$$

@ $R_x = 200k \Omega \Rightarrow 20\% \text{ FSD} \Rightarrow V_y = 0.024$

$$0.024 = \frac{V_i (12k // 2.4k)}{(12k // 2.4k) + R_2 + 200k} \quad \text{②}$$



- Reverse
- Non-linear.

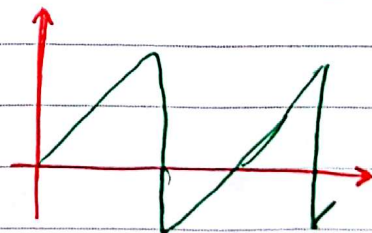
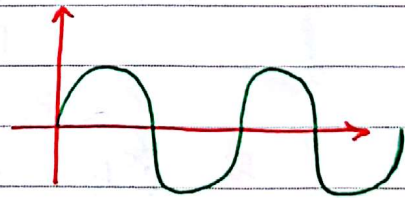
* AC Voltmeter "Analogue"

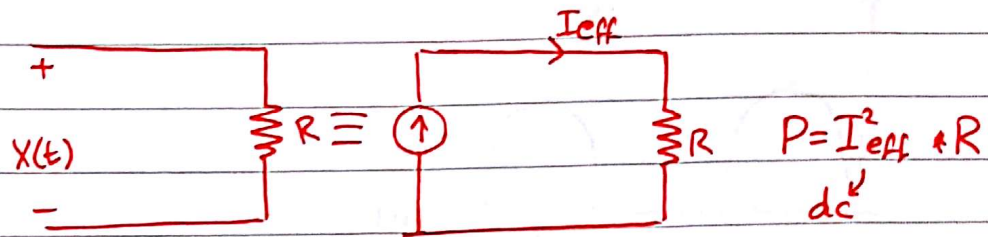
$$V_{RMS} = \sqrt{\frac{1}{T} \int_T V^2(t) dt}$$

RMS \equiv Effective

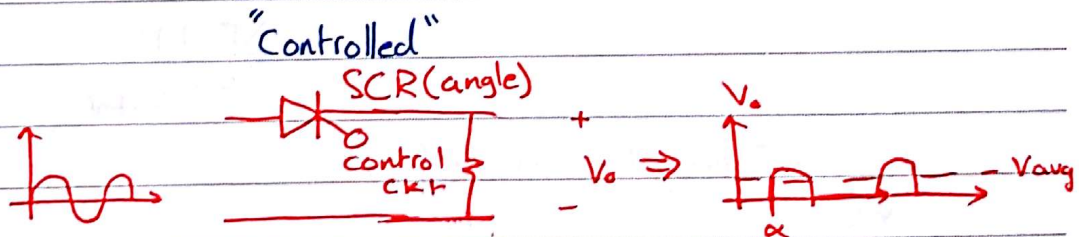
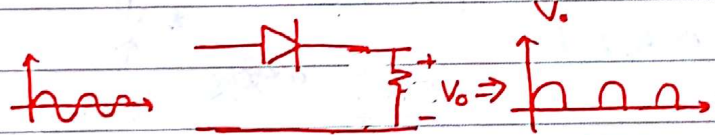
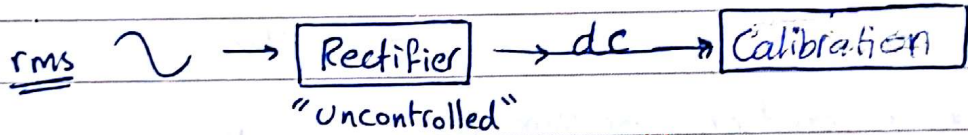
$$V_{avg} = \frac{1}{T} \int V^2(t) dt \Rightarrow \boxed{\frac{1}{2} \frac{V_m^2}{R} = \frac{1}{2} I_m^2 R}$$

Power

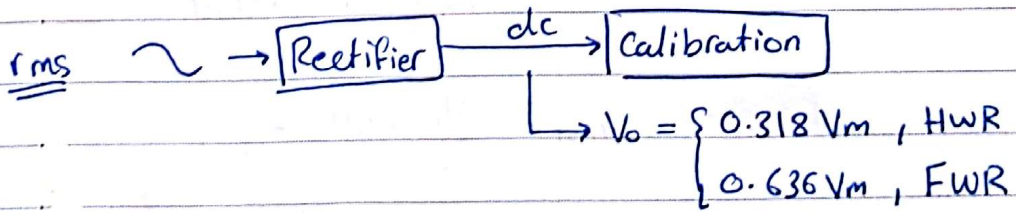


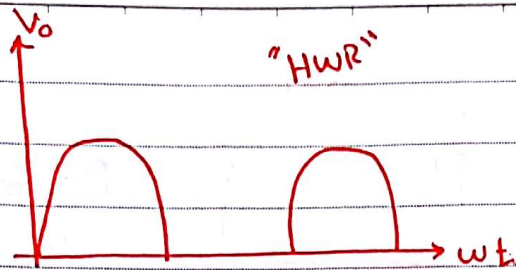


Pure AC Signal $\Rightarrow I_{rms} = \frac{I_m}{\sqrt{2}} = 0.707 I_m$
 ↳ for Sinusoidals.



Pure AC $\Rightarrow V_{rms} = 0.707 V_m$





Galvanometer (average) $\rightarrow V_o = \frac{1}{T} \int_0^T X(t) dt$

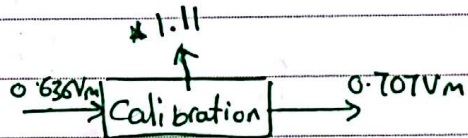
$$= \frac{1}{2\pi} \int_0^\pi V_m \sin \theta d\theta$$

$$= 0.318 V_m$$

* Calibration for pure AC

$$V_o = 0.636 V_m$$

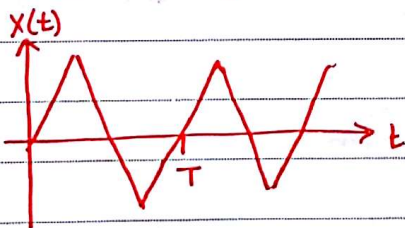
FWR



$$V_{rms} = 0.707 V_m \rightarrow \text{Desired}$$

SF = 1.11
 ↙
 Safe factor

* For Triangular wave form



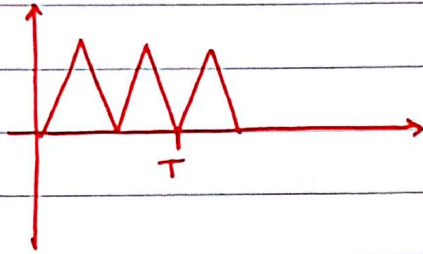
$$V_{rms} = \frac{V_m}{\sqrt{3}}$$

$$V_{avg} = \frac{1}{T} \int_0^T X(t) dt = \frac{V_m}{2}$$

$$\text{Error} = \frac{\frac{V_m}{2} * 1.11 - \frac{V_m}{\sqrt{3}}}{\frac{V_m}{\sqrt{3}}} * 100\%$$

$$\text{Error} = -3.81\%$$

V_{avg} for FWR Triangular waveform



22/6/2017

Digital Meter:-

* $4\frac{1}{2}$ digit display \rightarrow 4 digits display from 0~9
 \rightarrow 1 digit displays only 0/1

ex. 19,999 \rightarrow $4\frac{1}{2}$ digits maximum value

* $4\frac{3}{4}$ digits \rightarrow 4 digits from 0~9
 \rightarrow 1 digit from 0~3

here maximum value (count) = 39,999

* accuracy \rightarrow $\pm \% * \text{Full-scale}$ (analog)
 \rightarrow (digital) $\pm \% * \text{reading} \pm X \text{ counts}$

ex. 1.99 ± 2 :

accuracy = $1\% * 1.99 \pm 2 * 0.01$ \rightarrow LSD weight

ex. 1.999 ± 2 :

accuracy = $1\% * 1.999 \pm 2 * 0.001$

\rightarrow go to LSD
 Least Significant Digit
 LSD * X

* counts: when we increase the range, LSD weight will increase (resolution decreases)

ex. $3\frac{1}{2}$ digits

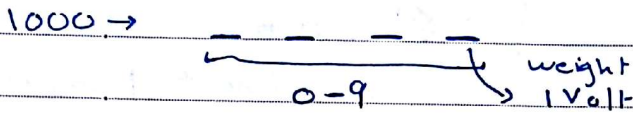
200 V 2 0 0 | LSD = $10^0 = 1 \text{ V}$
0.1

20 V 2 0 . 0 | LSD = 0.1 V

2 V 2 . 0 0 | LSD = 0.01 V \rightarrow highest resolution
 biggest # of digits
 after (.)

Digital Multimeter - Counts

4 digits Multi meter



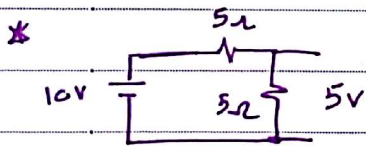
Digital Multimeter - Range

Digital

reading 001.8

Accuracy 5% ± 1 count

error 5% reading ± 1 count ⇒ 5% reading ± 0.1 count

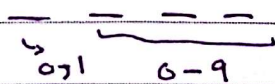


* error range 10V

* error range 100V (bigger error)



3 1/2



Range 10V → 0.01 count

Range 100V → 0.1 Count

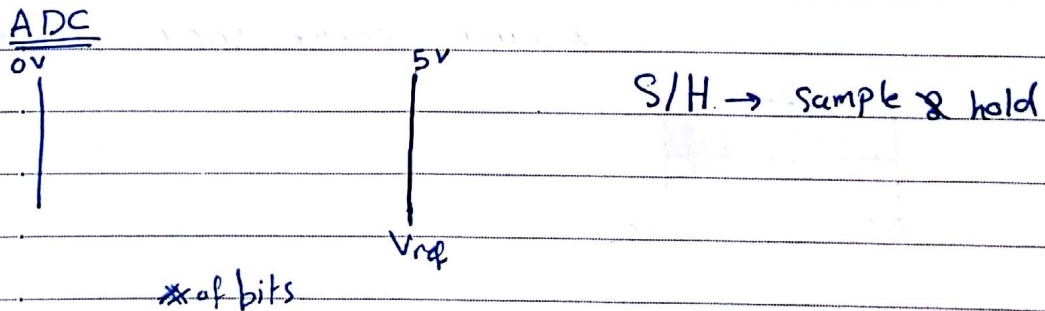
Range 20V → 0.1 count

Analogue \rightarrow 5% of Full Scale.

Digital \rightarrow 5% of Reading.

Ex: Analogue	Digital
Scale \rightarrow 25V	
Accuracy \rightarrow 2%	0.6% reading \pm 1 counts
error = 2% \times 25 = \pm 0.5V	$\frac{0.6}{100} \times 20 \pm 1 \times 0.1$
error = $\frac{0.5}{20} = 2.5\%$	$3\frac{1}{2} \rightarrow \underline{25}$
	25 V Full Scale
	error = 0.12 ± 0.1
	=

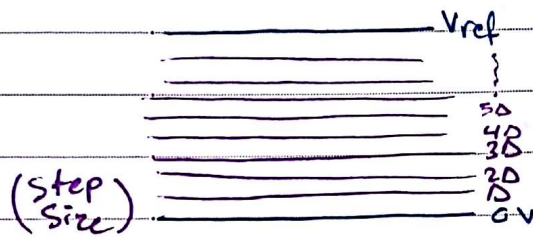
* Analogue to Digital Converter



each Sample \rightarrow n bits

3 bits \rightarrow 8 levels

n bits \rightarrow * of levels = 2^n



$$\Delta = \frac{V_{ref}}{2^n}$$

3 bits
 011
 010
 001
 000

~~error =~~

$$\text{Quantization Error} = \frac{\Delta}{2}$$

$$\text{Quantization Error} = \frac{V_{ref}}{2^{n+1}}$$

$$\text{Quantization Error} \% = \frac{V_{ref}}{2^{n+1} * V_{ref}} * 100\% = \frac{1}{2^{n+1}} * 100\%$$

$$QE \% = \frac{\Delta / 2}{V_{ref}}$$

Ex 8 bit
 Signal → ADC → level 80 , find Step Size??
 800-1500 mV level 150

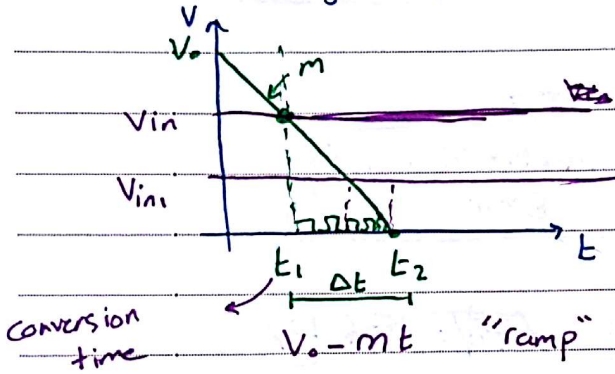
800 mV → level 80 (80 Δ)

1500 mV → level 150

$$800 \text{ mV} = 80 \Delta \rightarrow \Delta = 10 \text{ mV}$$

* Ramp-Type Digital Voltmeter

"Voltage to time conversion"



$$V_0 - m t_1 = V_{in}$$

$$V_0 - m t_2 = 0$$

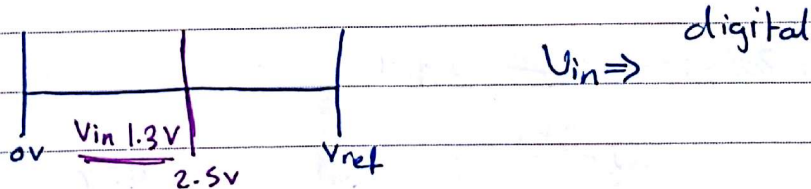
$$-m(t_2 - t_1) = -V_{in}$$

$$t_2 - t_1 = \Delta t = \frac{V_{in}}{m}$$

$$V_{in} = m \Delta t$$

→ counter

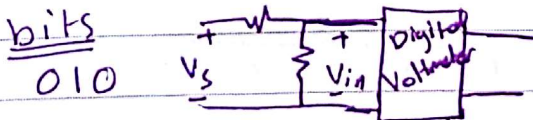
* Successive Approximation Digital Voltmeter



$$\text{Compare } V_{in} \text{ with } 2.5V \Rightarrow V_{in} < 2.5V \Rightarrow 0$$

$$\text{// } V_{in} \text{ with } 1.25V \Rightarrow V_{in} > 1.25V \Rightarrow 1$$

$$\text{// } V_{in} \text{ with } 2.$$

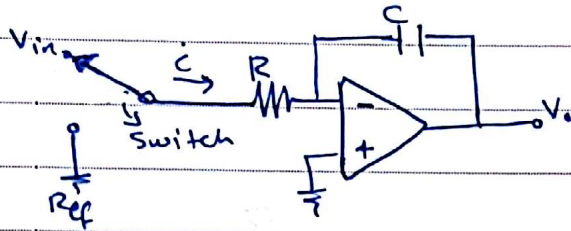


$$\text{Step Size} = \frac{5}{8} = \frac{V_{ref}}{2^n}$$

$$V_{in} = \frac{5}{8} \times 2 = \frac{5}{4} = 1.25$$

Voltmeter

* Dual Slope Digital Voltmeter



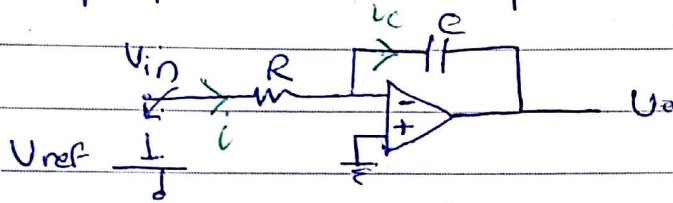
$$i = \frac{V_{in}}{R}$$

$$\frac{1}{C} \int i dt + V_o = 0 \Rightarrow V_o = -\frac{1}{RC} \int V_{in} dt$$

2/7/2017

Dual-Slope Digital Voltmeter → 8rd type

↳ purpose: reads input



$$i = V_{in}/R$$

$$V_c = \int i dt + V_{initial}$$

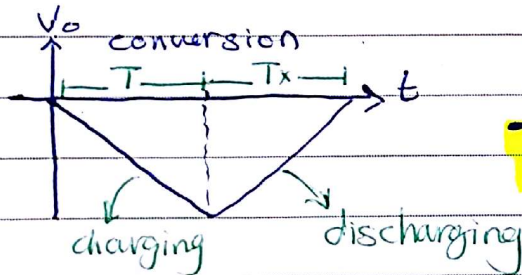
$$\frac{1}{C} \int i dt + V_o = 0$$

$$V_o = -\frac{1}{RC} V_{in} * T$$

(unknown) $V_{in} \Rightarrow T$ (known)

(known) $V_{ref} \Rightarrow T_x$ (unknown)

$$\text{Conversion Time} = T + T_x$$



$$T_x = \frac{V_{in} T}{V_{ref}}$$

$$\text{slope} = -\frac{T}{RC}$$

*if V_{in} bigger needs more conversion time

[Ex] $R = 100 \text{ k}\Omega$ $C = 0.01 \mu\text{F}$ $T = 10 \text{ ms}$ $V_{ref} = 10 \text{ V}$

Find T_x & conversion time if $V_{in} = 6.8 \text{ V}$

sol $T_x = \frac{V_{in} * T}{V_{ref}} = 6.8 \text{ ms}$

conversion time = $6.8 + 10 = 16.8 \text{ ms}$

R, C are used when drawing

in the question: V_{in} (input voltage)

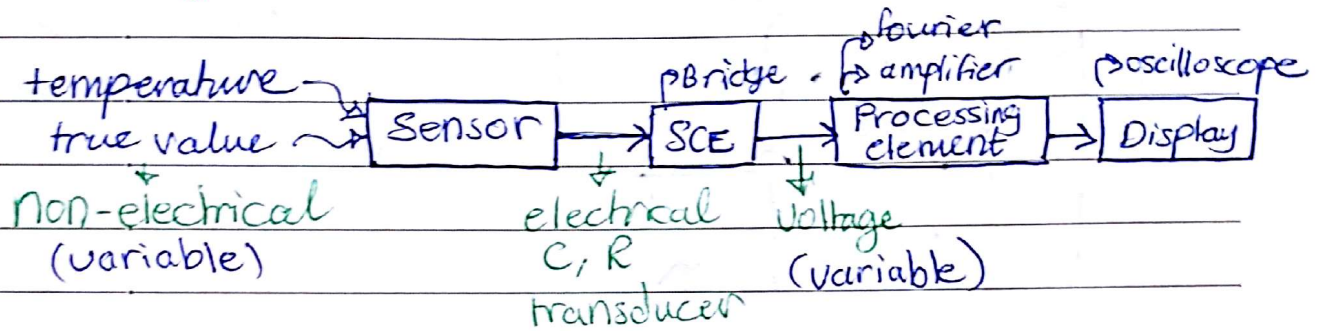
دائرة الجهد
الجهد V_{in}

V_{ref} (known voltage)

- how to check errors in energy & watt meters
- smart meters with internet & communication
- * wattmeter will be given at end of the semester.

* في سؤال على نظام الشرائح

Bridges

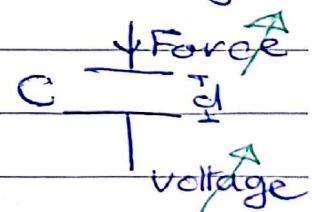


* Bridge: produce output in voltage form that changes as measured quantity changes

AC → R
 → C
 → L
 → f

DC → R

ex. when sensing capacitance, distance changes & bridge reads change in voltage

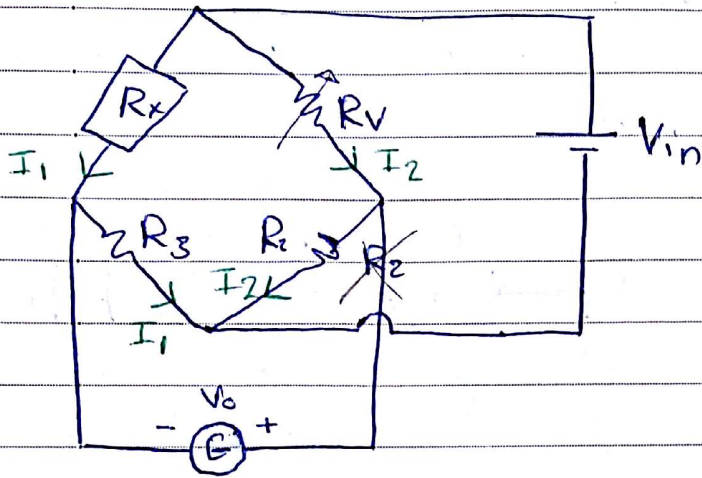


DC bridge → doesn't have different freq.
 wheat stone bridge

- Null method (Voltage = 0)
- Deflection method

$$\text{⊕ } V = f(R)$$

↳ function of resistance



ممكن موجه ال
 يتغير ابطع نرفنا
 من series وكيف
 توزيع ال current

$R_x \rightarrow$ from non-electrical
 $R_v \rightarrow$ variable resistance

Null $\rightarrow R_v \uparrow$ $V_o = 0$ (balanced) $R_1 R_x = R_3 R_v$
 set R_{in} of galvanometer $= \infty$ so $I_g = 0$

$$V_o = \frac{V_{in} \cdot R_x}{R_x + R_3} - \frac{V_{in} \cdot R_v}{R_v + R_2} \rightarrow \text{voltage division}$$

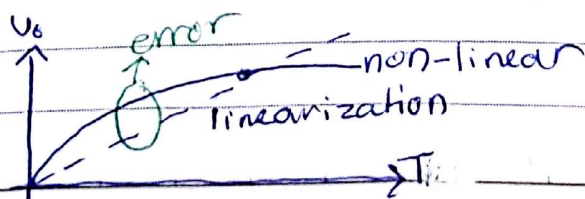
Ex a thermometer ($0 \rightarrow 50^\circ C$)

$$R = 500 \Omega @ 0^\circ C$$

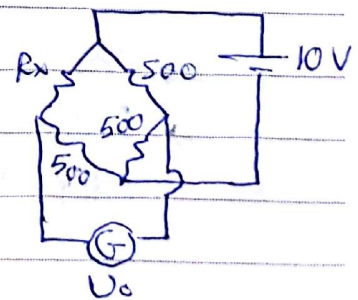
$$\Delta R = 4 \Omega / ^\circ C \quad V_{in} = 10V$$

$$R_1 = R_2 = R_3 = 500 \Omega \rightarrow \text{no variable } R$$

deflection ; purpose is to see relationship between R_x & V_o as R_x changes with temperature



$$V_o = f(R_x) \approx f(T)$$



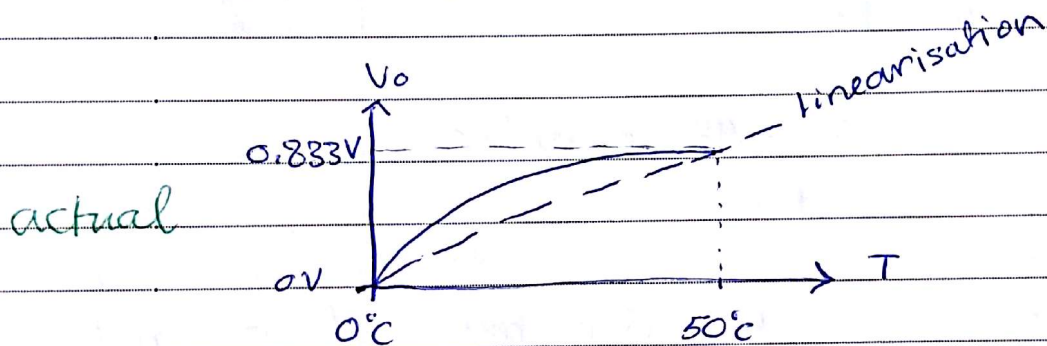
sol $0^\circ\text{C} \Rightarrow R_x = 500 \Omega$

$$U_o = U_{in} \left(\frac{R_x}{R_x + 500} - \frac{500}{1000} \right) = 0$$

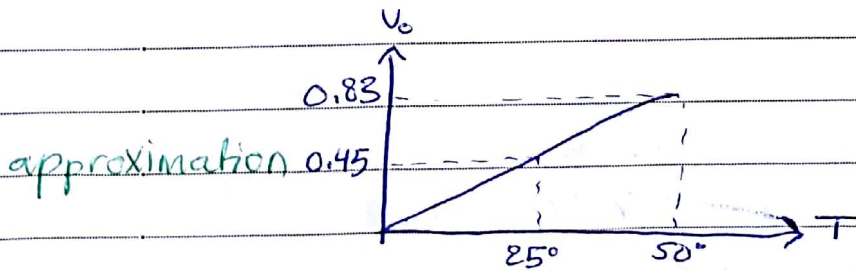
$50^\circ\text{C} \Rightarrow R_x = 500 + 4 \times 50 = 700 \Omega$

$$U_o = 10 \left(\frac{700}{700 + 500} - \frac{500}{1000} \right) = 0.833$$

note U_o & R_x are non-linearly related



linearisation: $U_o = \text{slope} * T = 0.016 * T$



actual: $R_x = 500 + 4T$

$$U_o = U_{in} \left(\frac{500 + 4T}{500 + 4T + 500} - \frac{500}{1000} \right) \text{ simplified}$$

approx: $U_o = 0.016 T$

error: actual - approx.

max error: $\frac{d}{dT} = 0$ (maximum value found)

3/7/2017

Project → note: may be included in final exam

- 1) Piezo Electrical tiles
- 2) Lab view (basics) + demonstration + example
- 3) Power Quality analyzer (harmonics)
- 4) Energy Meters (single & three phase)

group of 4-5 students

bonus 5 marks

↳ electro mech
↳ electronic
↳ smart

* slides

* presentation 30 - 45 minutes

* examples & maths

* simulation

presentations will be after material is finished
(maybe 11-12-13 / 7)

* search youtube: 3 min PhD UK

[Ex] same as previous example

a resistance thermometer ($0^{\circ} - 50^{\circ}\text{C}$)

$$R = 500 \Omega @ 0^{\circ}\text{C} \quad \Delta R = 4 \Omega/^{\circ}\text{C}$$

$$V_{in} = 10\text{V} \quad R_1 = R_2 = R_3 = 500 \Omega$$

$$\text{Bridge } U_o = V_{in} \left(\frac{R_x}{R_x + R_3} - \frac{R_1}{R_1 + R_2} \right)$$

$$R_x = 500 + 4T$$

$$\text{actual: } U_o = V_{in} \left(\frac{500 + 4T}{500 + 4T + 500} - \frac{500}{1000} \right)$$

approximation : linearization

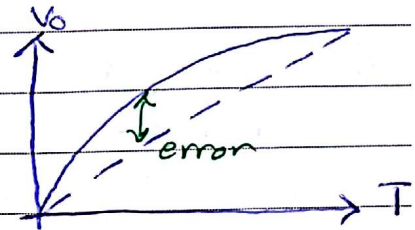
$$0^\circ\text{C} \rightarrow V_0 = 0 \text{ V}$$

$$50^\circ\text{C} \rightarrow V_0 = 0.833 \text{ V}$$

$$V_0 = 0.016 T$$

$$\text{error} = \underbrace{10 \times \left(\frac{125 + T}{250 + T} - 0.5 \right)}_{\text{actual}} - \underbrace{0.016 T}_{\text{approx}}$$

$$\text{max error } \frac{d(\text{error})}{dT} = 0$$



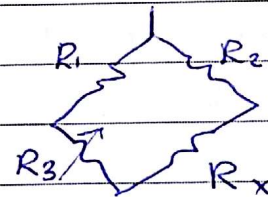
Ans: max error @ $T = 23.86^\circ\text{C}$ $e = 37.96 \text{ mV}$

* measurement errors

(Null, balanced) $V_0 = 0$

$$R_1 R_x = R_2 R_3$$

$$\Rightarrow R_x = \frac{R_2 R_3}{R_1}$$



where $R_2 = R_2 \pm \Delta R_2 \rightarrow$ tolerance

$$R_3 = R_3 \pm \Delta R_3$$

$$R_1 = R_1 \pm \Delta R_1$$

remember limiting error $\begin{cases} \rightarrow \text{max (take +)} \\ \rightarrow \text{min (take -)} \end{cases}$

$$R_x = \frac{(R_2 \pm \Delta R_2)(R_3 \pm \Delta R_3)}{R_1 \pm \Delta R_1}$$

approx. $\Delta R_2 + \Delta R_3 \approx 0$

$$R_x = \underbrace{R_3 R_2}_{\text{min}} \underbrace{\left(\frac{1 \pm \Delta R_1}{R_1} \pm \frac{\Delta R_2}{R_2} \pm \frac{\Delta R_3}{R_3} \right)}_{\text{nominal value without error}}$$

Range of R_x

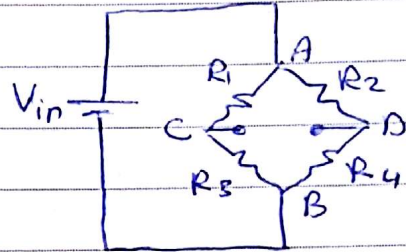
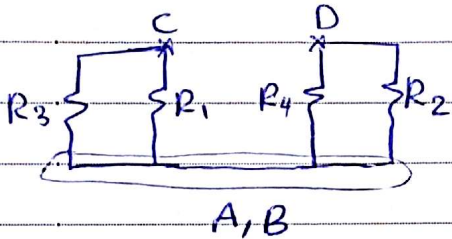
nominal value without error

Sensitivity of Galvanometer

For unbalanced wheatstone find thevinin equiv.

$$U_{th} = V_{in} \times \left(\frac{R_1}{R_1 + R_3} - \frac{R_2}{R_2 + R_4} \right)$$

$$R_{th} = (R_3 \parallel R_1) + (R_4 \parallel R_2)$$



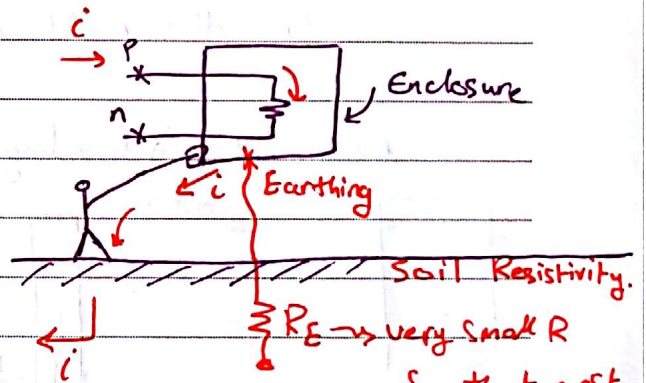
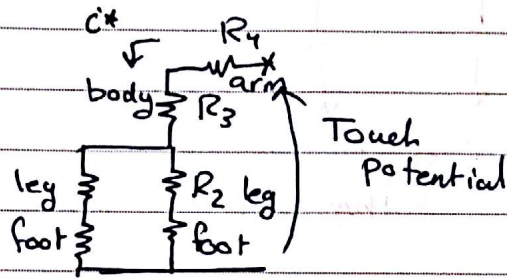
* note if it was current source instead of V_{in} we will get $(R_1 + R_3) \parallel (R_2 + R_4)$

! slides 126, 131 only the circuits & their names

Eartthing

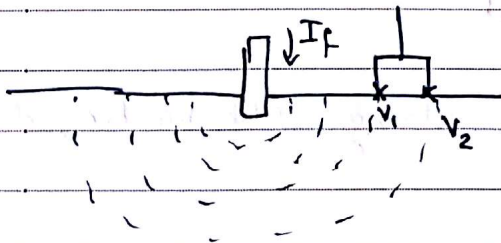
Touch Touch-estop Voltage

touch voltage

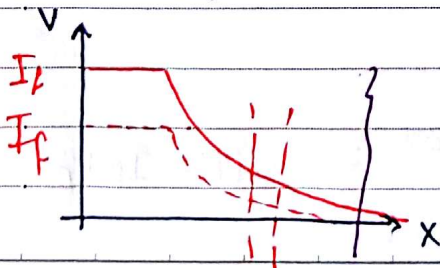


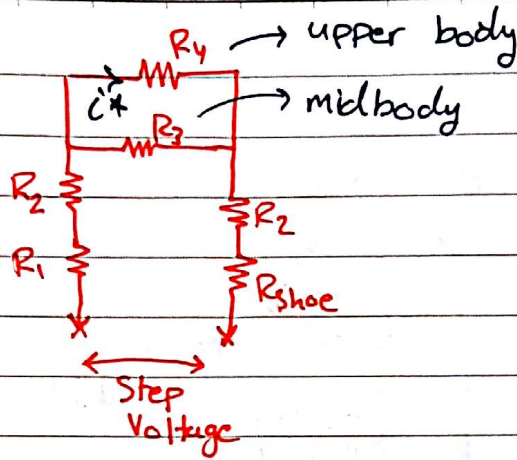
* Step Voltage

One leg has more Potential than the other which will produce current in your body.



this happens when a fault occur is P System.





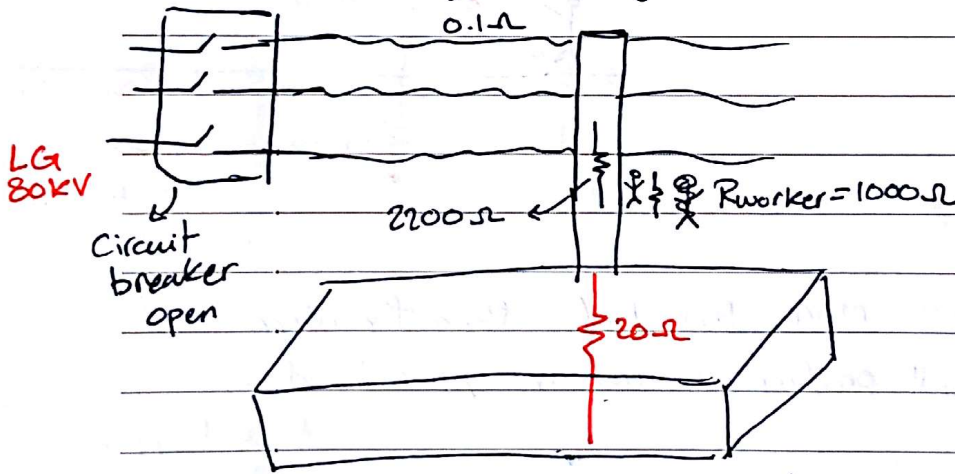
current, time
 ↓ fault ↓ protection system.

detects error
 clear the faulted part of the entire system by o.c the breaker.

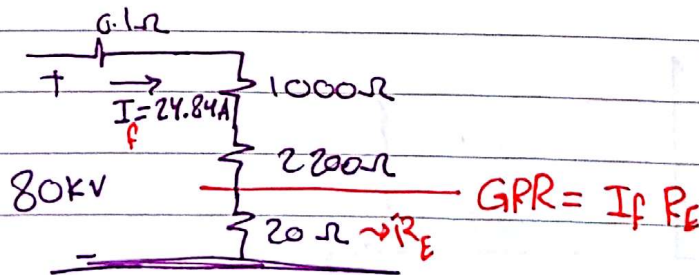
* if current fault is there for along time this might cause fires.

$$I^2 R t = \text{Energy}$$

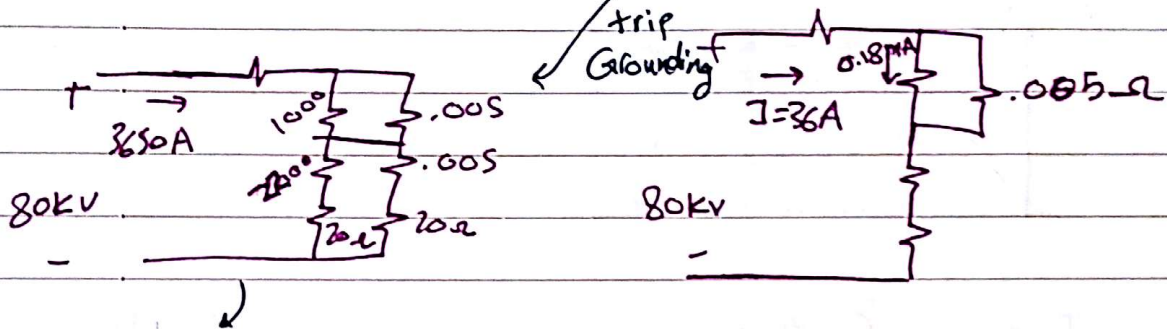
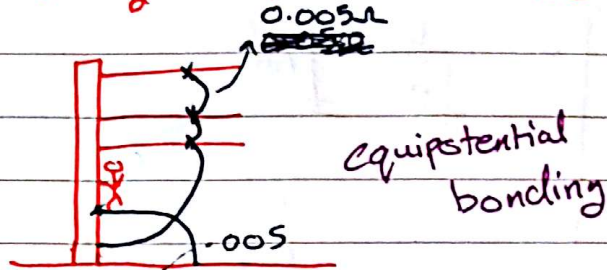
* Grounding & Bonding



A problem could occur by closing ckt breaker, due to lack of coordination.



Solution: by putting R parallel to the worker

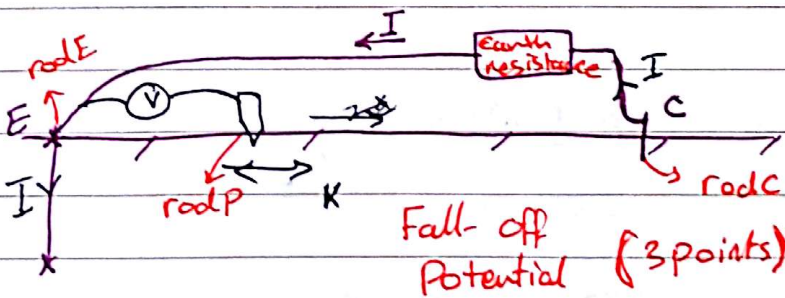


that is to increase I_p so that the protection system can detect it.

and by

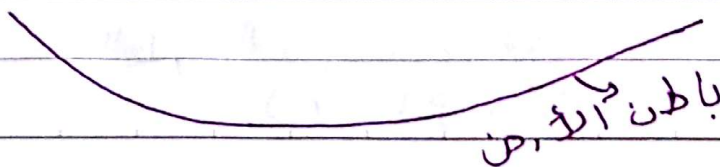
* Measurement of Earthing Earth Resistance

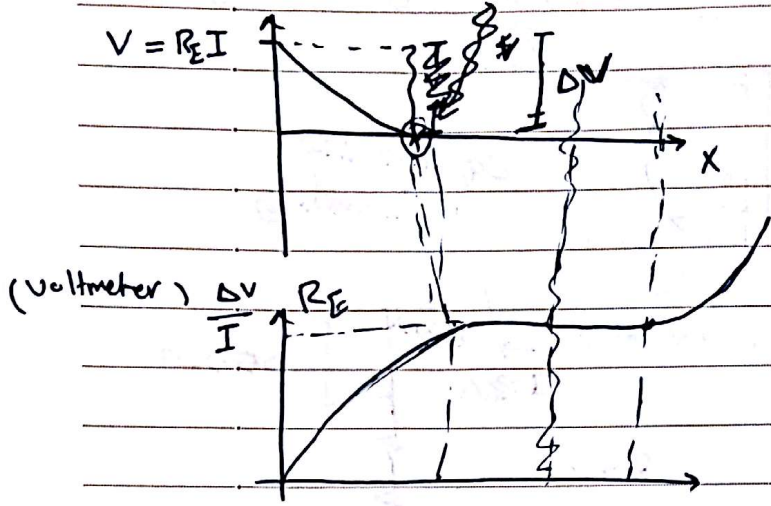
$$R_E = \frac{V}{I}$$



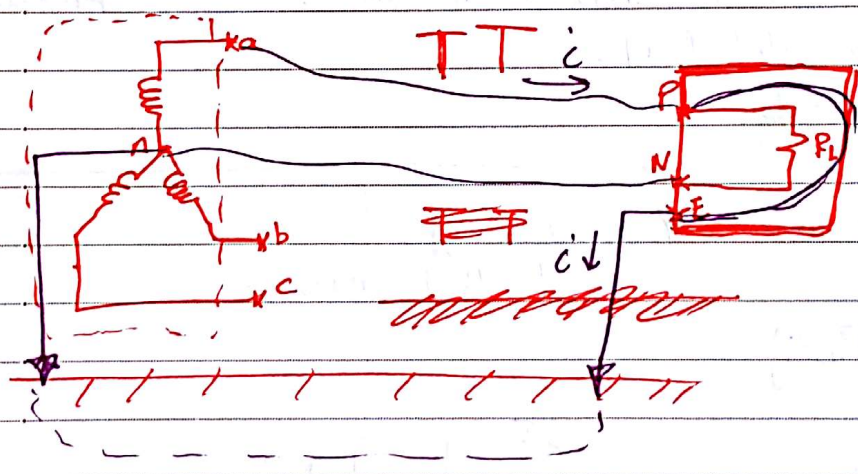
~~$$R_E = \frac{V}{I}$$~~

when $V = 0V$





* Types of Earthing System, for electricity Supplies.



Ground loop resistance

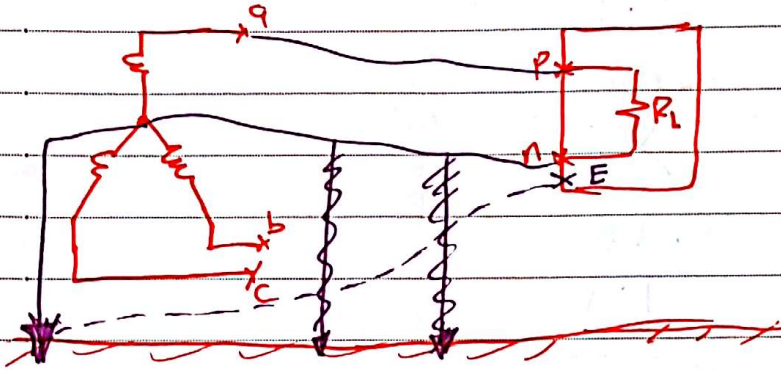
$$\approx 20 \Omega$$

$$I_{LG1} = \frac{230V}{20 \Omega} = 11.5 A$$

Small Current } MCB will not trip

التي التي يسبب الخلل بين ال current's
 بال n و P ال lines ؟

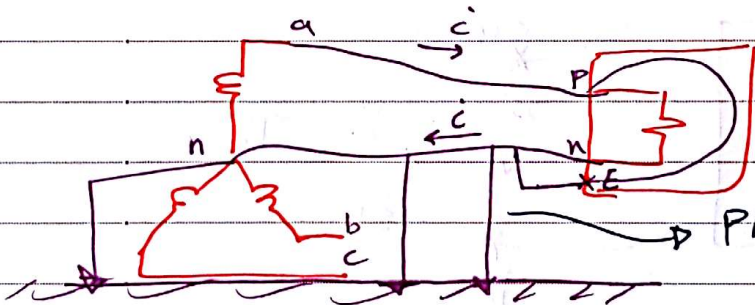
TN-S → separate



$$I_{LG} = \frac{230}{0.8\Omega} = 287.5A$$

The wire can be cut which is a problem because consumers will not have earthing system

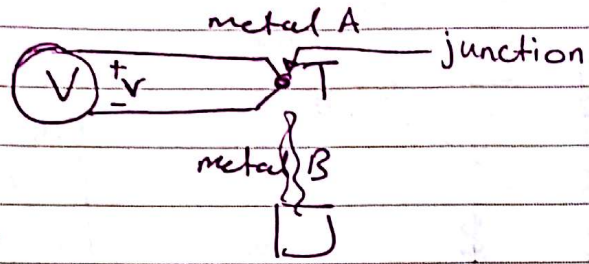
~~TN~~ TN-ES → combined
separate consumer



PME { Protective Multiple earthing }

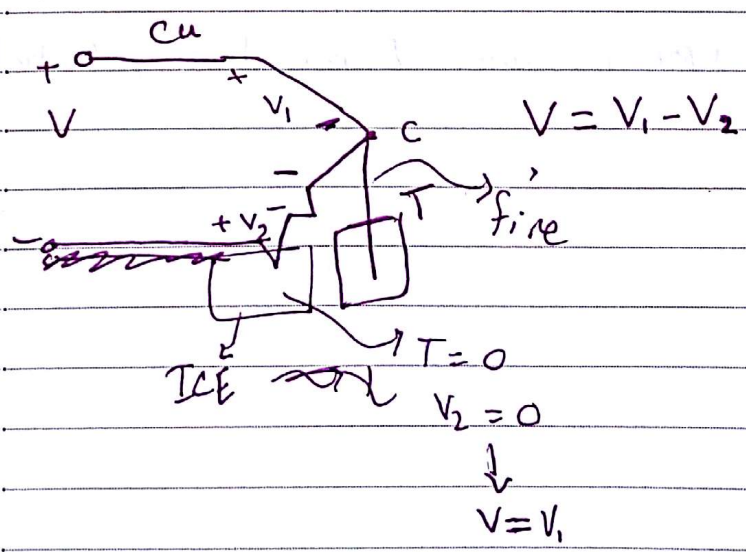
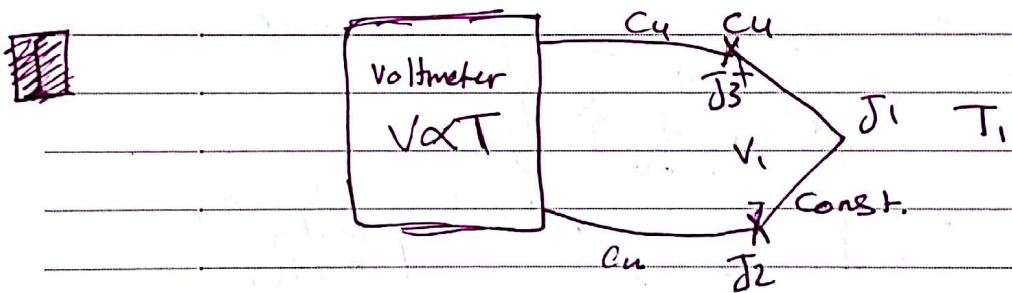
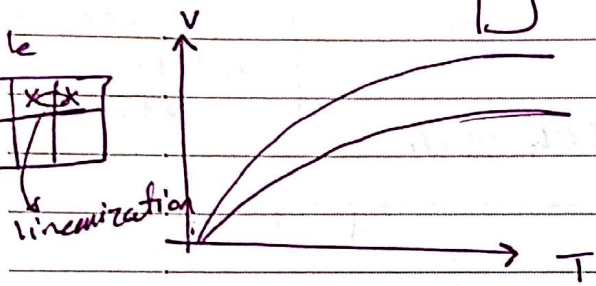
we do PME because E now has potential difference.

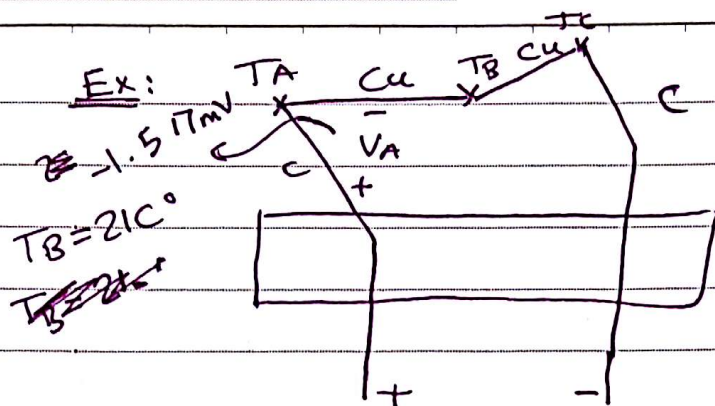
Thermo couple $\left\{ \begin{array}{l} \text{type J} \\ \text{type K} \\ \text{type T} \end{array} \right.$



table

T	K	x	x
V			





Cu-C $E_T = 2.05\text{mV}$

V_C ??
 V_B ??
 T_A ..
 T_C

T	
E	

$V_B = 0V$ (Cu-Cu)

~~$V_C = -E_T$~~

~~$-E_T - E_T + V_A + V_C = 0$~~

$V_C = E_T - V_A$

$= 3.567\text{mV}$

from Table

$T_A = 37.78^\circ\text{C}$

$T_C \rightarrow$ you need linearization