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Q # 1 (15)	Q # 2 (3)	Q # 3 (7)	GRADE
<u>13</u>	<u>2.5</u>	<u>7</u>	<u>22.5/25</u>

### Question # 1 (15 Points)

Select the correct answer of Questions (1.1-1.30) and fill it in the Table provided.

Q #	Q1	Q2	Q3	Q4	Q5	Q6	Q7	Q8	Q9	Q10
Ans	<u>a</u>	<u>b</u>	<u>a</u>	<u>d</u>	<u>a</u>	<u>c</u>	<u>d</u>	<u>b</u>	<u>d</u>	<u>b</u>
Q #	Q11	Q12	Q13	Q14	Q15	Q16	Q17	Q18	Q19	Q20
Ans	<u>c</u>	<u>c</u>	<u>b</u>	<u>c</u>	<u>c</u>	<u>b</u>	<u>d</u>	<u>d</u>	<u>a</u>	<u>c</u>
Q #	Q21	Q22	Q23	Q24	Q25	Q26	Q27	Q28	Q29	Q30
Ans	<u>d</u>	<u>d</u>	<u>a</u>	<u>d</u>	<u>a</u>	<u>a</u>	<u>b</u>	<u>c</u>	<u>b</u>	<u>a</u>

1.1 As load power factor of a synchronous generator becomes more lagging, the value of generated voltage  $E_a$  required to give rated terminal voltage ....

- a. increase      b. remains unchanged      c. decreases      d. varies with rotor speed

1.2 If the field of a synchronous generator is underexcited, the power factor will be ....

- a. lagging      b. leading      c. unity      d. more than unity

1.3 A synchronous generator connected to infinite bus-bars has at constant full-load, 100% excitation and unity pf. On decreasing the excitation only, the armature current will have ...

- a. leading PF with underexcitation      c. lagging PF with overexcitation  
b. leading PF with overexcitation      d. lagging PF with underexcitation

1.4 If the excitation of a synchronous generator is increased with the load remained unchanged, then ...

- a. the excitation voltage increases. ✓      c. the reactive power increases. ✓  
b. the maximum developed power increases. ✓      d. all of the above.

1.5 An alternator is delivering rated current at rated voltage and 0.8 PF lagging case. If it is required to deliver rated current at rated voltage and 0.8 PF lagging, the required excitation will be ....

- a. less.      b. more.      c. more or less.      d. the same.

1.6 As the speed of an alternator decreases ....

- a. the frequency remains constant but PF decreases      c. the frequency decreases  
b. the frequency increases      d. none of the above

$$I_{fs} = \frac{120}{P} \sqrt{f}$$



1.7 For successful connection of a synchronous generator to an infinite bus system (Grid) using three-lamp method, the following condition(s) must be satisfied:

- a. equal voltage magnitudes and phases of the running and incoming generators
- b. equal phase sequence of the running and incoming generators
- c. equal frequency of the running and incoming generators
- d. All of the above

1.8 When two alternators are running in parallel, their KW load share is changed by changing their ..... while their KVAR load share is changed by changing their .....

- a. excitation, driving torque
- b. driving torque, excitation
- c. excitation, excitation
- d. driving torque, driving torque

1.9 At a particular instant, an alternator is generating 80 MW at 0.8 power factor lagging. Now if the steam supply valve to the steam turbine is further closed and the excitation is not changed, .....

- a. the speed of the alternator will decrease but kW delivered will remain unchanged
- b. the speed of the alternator will decrease and kW delivered will also increase
- c. the speed of the alternator will remain unchanged but it will deliver less kVA
- d. the speed of the alternator will remain unchanged but it can meet less kW demand

1.10 Two alternators A and B are sharing a resistive load ( $pf=1$ ) equally. Now if the excitation of alternator A is decreased, .....

- a. alternator A will become lagging and alternator B will become leading
- b. alternator A will become leading and alternator B will become lagging
- c. both alternators will continue to operate on unity power factor
- d. both alternators will operate on leading power factor

1.11 When a generator designed for operation at  $f_1$  Hz is operated at  $f_2$  Hz, .....

- a. kVA rating can be upgraded to  $(60/50)$  of the rated value
- b. operating voltage must be derated to  $(50/60)^2$  of its original value
- c. operating voltage must be derated to  $(50/60)$  of its original value
- d. the generator will not take any load.

$$\frac{E_1}{E_2} = \frac{f_1}{f_2} = \frac{60}{50}$$

$$\therefore E_2 = \left(\frac{50}{60}\right) E_1$$

1.12 Two synchronous generators  $G_1$  and  $G_2$  are equally sharing the KVAR of the load while operating in parallel. Keeping the terminal voltage fixed in order to shift part of the KVAR load from  $G_1$  to  $G_2$ , ....

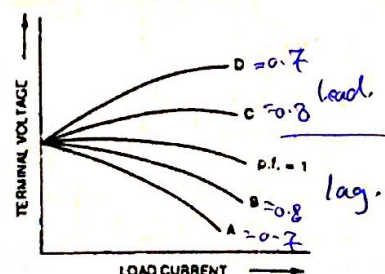
- a. the field current of  $G_1$  is lowered
- b. The field current of  $G_2$  is raised
- c. the field current of  $G_2$  is raised and of  $G_1$  is lowered.
- d. the field current of  $G_1$  is raised and of  $G_2$  lowered

1.13 The steady-state stability limit of a synchronous generator can be increased by ....

- a. an increase in its reactance
- b. an increase in the excitation of the machine
- c. a decrease in the moment of inertia of the machine
- d. an increase in the moment of inertia of the machine

1.14 Load characteristic curves for an alternator are shown. The curves are drawn for 0.9 PF lagging, 0.8 PF lagging, 0.8 PF leading and 0.7 PF leading. Which curve represents the characteristics for 0.8 PF lagging?

- a. curve A
- b. curve C
- c. curve B
- d. curve D





$$n_p = \frac{120}{8} \times 900 = 900 \Rightarrow f = 60 \text{ Hz}$$

$$E = 4.44 N \phi f K_w$$

$$s = \phi = \frac{E_{ph}}{4.44 N f K_w}$$

$$\phi = 4 \text{ mWb}$$

- 1.15 A 3-phase, 8-pole, 900-rpm, Y-connected synchronous generator has 120 turns per phase and a stator-winding factor  $K_w = 0.90$ . If a voltage of 200 V is measured across the machine terminals on no load, the flux per pole would be .... mWb.

a. 1.5      b. 8      c. 4      d. 20.8

- 1.16 A synchronous generator on open-circuit generates 400 V at 50 Hz when the field current is 4.0 A. Neglecting saturation, the open-circuit EMF when the frequency is 25 Hz and the field current is 6.0 A will be .... V.

a. 100      b. 300      c. 800      d. 600

$$\frac{E_1}{E_2} = \frac{f_1 I_{f1}}{f_2 I_{f2}}$$

$$E_2 = 300$$

- 1.17 A 50-Hz synchronous generator will run at the greatest possible speed if it is wound for ..... poles.

a. 8      b. 6      c. 4      d. 2

$$n_s = \frac{120}{P} f$$

$$\text{min.}$$

- 1.18 The effective voltage in one phase of an alternator having 480 turns per phase, frequency of 60 Hz and flux per pole of 20.8 mWb will be .... V.

a. 332.5      b. 665      c. 1330      d. 2660

$$E = 4.44 K_w N \phi f$$

$$E = 2660$$

- 1.19 The voltage regulation of a synchronous generator having 0.75 lagging pf load, no-load induced EMF voltage of 3000 V and rated terminal voltage of 2400 V is

a. +25.0%      b. -20.0%      c. +20.0%      d. -25.0%

$$VR = +25\%$$

- 1.20 A 50 kVA, 440 V, 3-phase, 50 Hz, Y-connected, alternator, has an armature resistance  $R_a$  of 0.25  $\Omega$ /phase and a synchronous reactance  $X_s$  of 3.2  $\Omega$ /phase. The % voltage regulation of the alternator at 1.0 PF is approximately .....%.

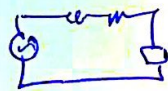
a. 55      b. 45      c. 35      d. 25

$$VR \approx 35\%$$

$$E_A = 593 \angle 7.8^\circ$$

$$E_A = V_t + I_a Z_s$$

$$I_A = \frac{50 \text{ kVA}}{\sqrt{3} (440)} = 65.6 \angle 0^\circ$$



- 1.21 A 3-phase  $\Delta$ -connected synchronous generator is tested in order to determine its effective armature resistance using DC resistance test. If the DC current and voltage results are  $I_{dc} = 40$  A and  $V_{dc} = 100$  V, the armature DC resistance  $R_{dc}$  will be ....  $\Omega$ .

a. 0.2      b. 0.9      c. 0.6      d. 0.66

$$R_{dc} = \frac{V}{I}$$

$$R_{dc} = 3.75 \Omega$$

- 1.22 If, in a 3-phase, Y-connected synchronous generator, a field current of 50 A produces a full-load armature current of 200 A on short-circuit and 1730 V on open circuit, then its synchronous reactance  $X_s$  is ....  $\Omega$

a. 0.4      b. 2.5      c. 0.6      d. 3.75

$$X_s = \frac{E_{oc}}{I_{sc}} = 4.99$$

$$X_s = 4.99 \Omega$$

- 1.23 A 10,000 kVA, 6600-V, 60-Hz, 3-Phase, Y-connected synchronous generator operates at full-load at a lagging PF of 0.8 and 80% efficiency. The real and reactive power delivered by the generator per phase is ..... kVA.

a. 8000 + j 6000      b. 2667 + j 2000      c. 2133 + j 1600      d. 6400 + j 4800

$$I_a = \frac{10 \text{ kVA}}{0.6 \text{ kV} \sqrt{3}} = 874.8 \text{ A} \angle -36.9^\circ$$

$$P = \sqrt{3} V_T I_a \cos \theta = 8000 \text{ kW}$$

$$Q = \sqrt{3} V_T I_a \sin \theta = 6000 \text{ kVAR}$$

$$S = 8000 + j 6000$$



1.24 A 3-phase Y-connected synchronous generator has a synchronous reactance  $X_s$  of  $4 \Omega$  per phase and a terminal voltage of 2300 V. The field current is adjusted so that the excitation voltage is 2300 V at a power angle  $\delta$  of  $15^\circ$ . The power developed power by the generator is ..... kW

- a. 1026.86      b. 3967.5      c. 1322.28      d. 342.23

$$P = \frac{3E_a V_t}{X_s} \sin \delta = \underline{342.3 \text{ kW}}$$

1.25 A 3-phase, 6600-V, Y-connected synchronous generator has  $X_s = 4 \Omega$  and its armature resistance  $R_a$  is negligible. If the induced voltage is adjusted to 8000 V at 0.8 PF lagging, the maximum power developed  $P_d$  is ..... MW.

- a. 13.2      b. 19.8      c. 6.6      d. 15.84

$$P_d = \frac{3E_a V_t}{X_s} \sin 90^\circ = \underline{13.2 \text{ MW}}$$

Questions 1.26 to 1.28 refer to the following data:

A 2300 V, 60-Hz, 3-phase, synchronous generator has a synchronous reactance  $X_s$  of  $4 \Omega$  per phase and a negligible armature resistance  $R_a$ . The field current is adjusted so that the excitation voltage is 2300 V at an angle  $\delta$  of  $30^\circ$ .

1.26 The total output real Power  $P$  delivered is ..... kW.

- a. 661.25      b. 1983.8      c. 1322.5      d. 2645

$$I_a = \frac{E - V_t}{X_s} = \underline{171.8 / 15^\circ} \quad P = 3V_t I_a \cos \theta \quad P = \underline{661.1 \text{ kW}}$$

1.27 The total output reactive Power  $Q$  delivered is ..... kVAR.

- a. -59.1      b. -177.2      c. 1145.3      d. 381.8

$$Q = \underline{-177.14 \text{ kVAR}}$$

1.28 The power factor is .....

- a. 0.5 lagging      b. 0.866 lagging      c. 0.966 leading      d. 0.866 leading

$$PF = \cos 15^\circ = \underline{0.966 \text{ leading}}$$

Questions 1.29 to 1.30 refer to the following data:

A 3-phase, 50 Hz, 6600 V, alternator is rated at 6000 kW at 0.8 PF and a full load efficiency of 90%.

1.29 kVA is rating of the alternator is ... kVA.

- a. 4800      b. 7500      c. 6667      d. 5400

$$I = 656.1 \text{ A}$$

1.30 The input power to the alternator is ... kW.

- a. 6667      b. 8333      c. 5400      d. 7500

$$E_a = \underline{6600}$$

$$S = \frac{P}{PF} = \underline{7500 \text{ kVA}}$$

$$P_{out} = 6000 \text{ kW}$$

$$\eta = \frac{P_{out}}{P_{in}} \Rightarrow P_{in} = \frac{6000 \text{ kW}}{0.9} = \underline{6667 \text{ kW}}$$



### Question # 2-a (1.5 Points)

A 750-kVA, 1380-V, 60-Hz,  $\Delta$ -connected 3-phase synchronous generator is tested in order to determine its voltage regulation. The results of these tests are:

Open-Circuit Test	Short-Circuit Test	DC-Resistance Test
$I_f = 17.5$ A	$I_f = 17.5$ A	$I_{dc} = 100$ A
$V_{Loc} = 1020$ V	$I_{sc} = 314$ A	$V_{dc} = 40$ V

Assume the effective armature resistance  $R_a = 1.5 \times R_{dc}$ , find

2.a.1	the armature resistance, $R_a$	$R_a =$	$0.6 \Omega$
2.a.2	the synchronous impedance, $Z_s$	$Z_s =$	$5.626 \Omega$
2.a.3	the synchronous impedance, $X_s$	$X_s =$	$5.594 \Omega$

$$R_a = \frac{3}{2} \frac{V_{dc}}{I_{dc}} = \frac{3}{2} \left( \frac{40}{100} \right) \Rightarrow R_a = 0.6 \Omega$$

$$Z_s = \frac{E_{oc}}{I_{sc}} = \frac{1020}{\frac{314}{\sqrt{3}}} = 5.626 \Omega$$

$$Z_s = \sqrt{R_a^2 + X_s^2}$$

$$\Rightarrow X_s = \sqrt{(5.626)^2 - 0.6^2}$$

$$\Rightarrow X_s = 5.594 \Omega$$

### Question # 2-b (1.5 Points)

A 2300 V, 60-Hz, 3-phase, synchronous generator has a synchronous reactance  $X_s$  of  $4 \Omega$  per phase and a negligible armature resistance  $R_a$ . The field current is adjusted so that the excitation voltage is 2300 V at a power angle  $\delta$  of  $30^\circ$ .

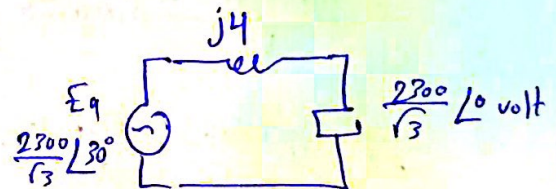
2.b.1	The total output real Power delivered $P_{out}$	$P_{out} =$	$661.25$ kW
2.b.2	The total output reactive Power delivered $Q_{out}$	$Q_{out} =$	$-177.18$ kVAR
2.b.3	The generator operating power factor	$Pf =$	$0.9659$ lag lead

$$\begin{aligned} P_{out} &= P_d = \frac{3 V_t E_a \sin \delta}{X_s} \\ &= \frac{V_t E_a \sin \delta}{X_s} \\ &= \frac{(2300)(2300)}{4} \sin 30^\circ \end{aligned}$$

$$P_{out} = 661.25 \text{ kW}$$

$$\begin{aligned} Q_{out} &= \frac{3 V_t}{X_s} [E_a \cos \delta - V_t] \\ &= \frac{(2300)(2300)}{4} \cos 30^\circ - \frac{2300^2}{4} \end{aligned}$$

$$Q_{out} = -177.18 \text{ kVAR}$$



$$P = 3 V_t I_a \cos \theta$$

$$I_a = \frac{E_a - V_t}{j X_s} = 171.8 \angle 15^\circ$$

$$Pf = \cos 15^\circ = 0.9659$$

Leading.



### Question # 3 (7 Points)

Two identical 3-ph, Y-connected alternators (A and B) are connected in parallel and deliver a total load of 2.5 MW at 11 kV and a power factor of 0.866 lagging. Each generator has a per phase synchronous reactance  $X_s = 10 \Omega$  and a negligible armature resistance. The induced voltage ( $E_A$ ) and the power angle ( $\delta_A$ ) of generator A are adjusted to 12.5 kV and  $6.26^\circ$ , respectively. Determine for generators A and B the following:

a.	The magnitude of the load current $ I_L $	$ I_L  =$	151.5	A
b.	the real output power $P_A$ and $P_B$	$P_A =$ $P_B =$	1.5 1	MW
c.	the armature current phasors $I_A$ and $I_B$	$I_A =$ $I_B =$	113.9 $\angle -46.3^\circ$ 52.9 $\angle 7.2^\circ$	A
d.	the power factor $PF_A$ and $PF_B$ and indicate lead or lag	$PF_A =$ $PF_B =$	0.6904 lagging 0.9921 leading	lag lead
e.	the reactive output power $Q_A$ and $Q_B$	$Q_A =$ $Q_B =$	+1.569 -126.32	MVAR kVAR
f.	the magnitude of the induced phase voltage $ E_B $ and the angle ( $\delta_B$ )	$ E_B  =$ $\angle \delta =$	6.306 4.77	kV <sub>LN</sub> °
g.	the percentage voltage regulation of generators A and B,	$\%VR_A =$ $\%VR_B =$	13.6 -0.91	% %

a)  $I_L = \frac{P_{\text{tot}}}{\sqrt{3} V_L \text{pf}} = \frac{2500 \text{ kW}}{0.866 \sqrt{3} \times 11 \text{ kV}} = 151.5 \angle -30^\circ$

b)  $P_A = 3 \frac{V_t E_A}{X_s} \sin \delta$   
 $= \frac{11 \text{ kV} \times 12.5 \text{ kV}}{10} \sin 6.26^\circ \Rightarrow P_A = 1.5 \text{ MW}$

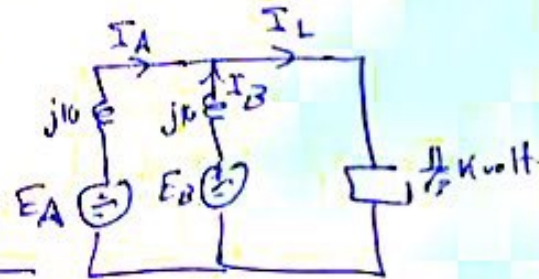
c)  $I_A = \frac{E_A - V_t}{jX_s} = \frac{\frac{12.5 \text{ kV}}{\sqrt{3}} \angle 6.26^\circ - \frac{11 \text{ kV}}{\sqrt{3}} \angle 0^\circ}{10 \angle 90^\circ} \Rightarrow I_A = 113.9 \angle -46.3^\circ \text{ A}$

$I_L = I_A + I_B \Rightarrow I_B = I_L - I_A \Rightarrow I_B = 52.9 \angle 7.2^\circ \text{ A}$

d)  $PF_A = \cos(46.3^\circ) = 0.6904 \text{ lag}$   
 $PF_B = \cos(7.2^\circ) = 0.9921 \text{ lead}$

e)  $Q_A = 3 V_t I_A \sin \theta$   
 $= \sqrt{3} V_t I_A \sin \theta_A = 1.569 \text{ MVAR}$

$Q_B = \sqrt{3} V_t I_B \sin \theta_B = -126.32 \text{ kVAR}$



$\Rightarrow P_B = P_L - P_A = 1 \text{ MW}$

f)  $E_B = V_t \angle 0^\circ + I_B jX_s$   
 $\Rightarrow E_{B \text{ phase}} = 6306.4 \angle 4.8^\circ \text{ V}_{\text{LN}}$

g)  $|E_B|_{\text{LL}} = 10.9 \text{ kV}_{\text{LL}}$   
 $VR_A = \frac{12.5 - 11}{11} \times 100\% = 13.6\%$   
 $VR_B = \frac{10.9 - 11}{11} \times 100\% = -0.91\%$