

Student Name [REDACTED]

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Serial #: 80

* Q # 1 (5)	Q # 2 (5)	Q # 3 (7)	Q # 4 (13)	GRADE
5	8	4	12.5	22 / 30

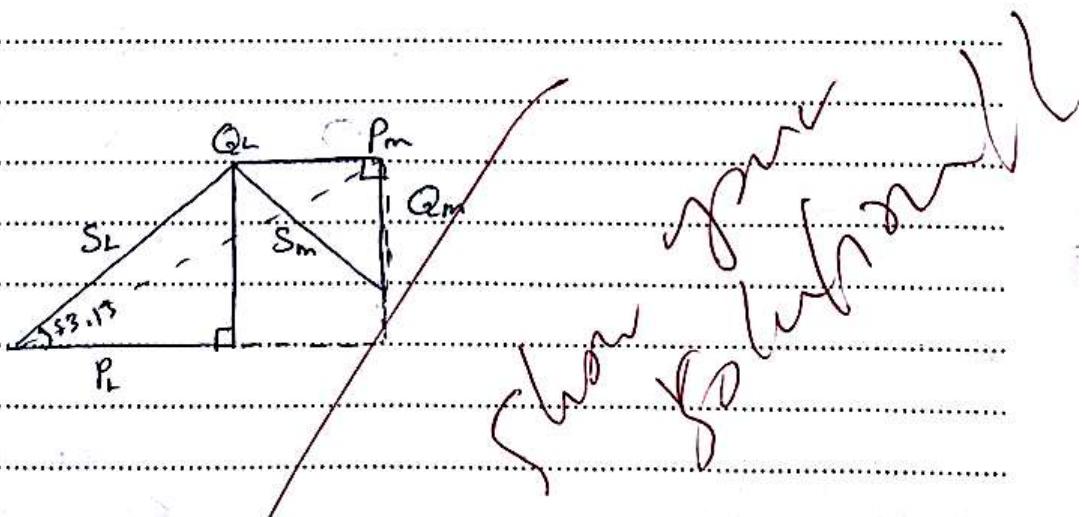
Question # 1 (5 marks) ABET Outcome h Assessment SHOW YOUR CALCULATIONS

A 3-phase, load of an industrial plant takes a total power of 240 kW at a PF of 0.6 lagging from a 220-V supply. An additional motor load of 200 hp must be added to the plant. If a synchronous motor operating at 0.8 PF leading and having an efficiency of 90% is added in parallel with the load. (pf correction)

Part I: Determine:

a.	the reactive power Q_L and the magnitude of the load current $ I_L $, taken by the load.	$Q_L = 320$ kVAR
		$ I_L = 1049.7$ A
b.	the motor's real power, P_m , and reactive power, Q_m , and the magnitude of the motor current, I_m taken by the motor.	$P_m = 165.7$ kW
		$Q_m = 124.3$ kVAR
		$ I_m = 543.8$ A
c.	the system total real power, P_s , and reactive power, Q_s , and the magnitude of the line current, I_s supplied by the power supply.	$P_s = 405.7$ kW
		$Q_s = 195.7$ kVAR
		$ I_s = 1182.98$ A
d.	e. the overall (combined) system power factor, $PF_{overall}$.	$PF_{overall} = 0.9$ lag

Part II: Draw the power triangles for the load, motor and system.



(Q1)

$$Q_L = P_L \tan(\cos^{-1} 0.6) = 320 \text{ KVAR (absorbed)}$$

$$|I_L| = \frac{P_L / \text{pf}}{\sqrt{3} \cdot V_{LL}} = \frac{240 \text{ kV} / 0.6}{\sqrt{3} \times 220} = 1049.72 \text{ A}$$

$$P_a = 200 \times 746 = 149200 \text{ W}$$

$$P_m = P_m = \frac{P_{\text{out}}}{\eta} = \frac{149200}{0.9} = 165.7 \text{ kW}$$

$$Q_m = P_m \tan(\cos^{-1} 0.8) = 124.3 \text{ KVAR (supplied, capacitive)}$$

$$|I_m| = \frac{P_m}{\sqrt{3} \cdot V_{LL} \cdot \text{pf}} = \frac{165.7 \text{ k}}{\sqrt{3} \times 220 \times 0.8} = 543.8$$

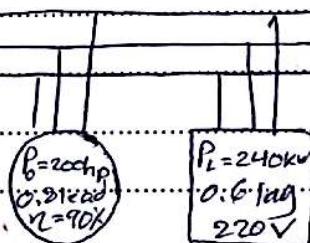
$$P_s = P_m + P_L = 165.7 \text{ k} + 240 \text{ k} = 405.7 \text{ kW}$$

$$Q_s = Q_m + Q_L = -124.3 \text{ k} + 320 \text{ k} = 195.7 \text{ KVAR}$$

$$\text{pf}_{\text{overall}} \rightarrow \tan^{-1}\left(\frac{Q_s}{P_s}\right) = 25.7 \quad \text{pf}_s = \cos(25.7) = 0.9$$

$$|I_s| = \frac{P_s / \text{pf}}{\sqrt{3} \cdot V_{LL}} = \frac{405.7 \text{ k} / 0.9}{\sqrt{3} \times 220} = 1182.98$$

$$|I_s| = |I_m| + |I_L| = 1049.72 + 543.8 = 1593.52$$



$$303.4 \text{ k} = 3 \times V_t \times E_a \Rightarrow E_a = \frac{303.4 \text{ k} \times 8}{3 \times \frac{4160}{\sqrt{3}}} = 336.8 \text{ V}$$

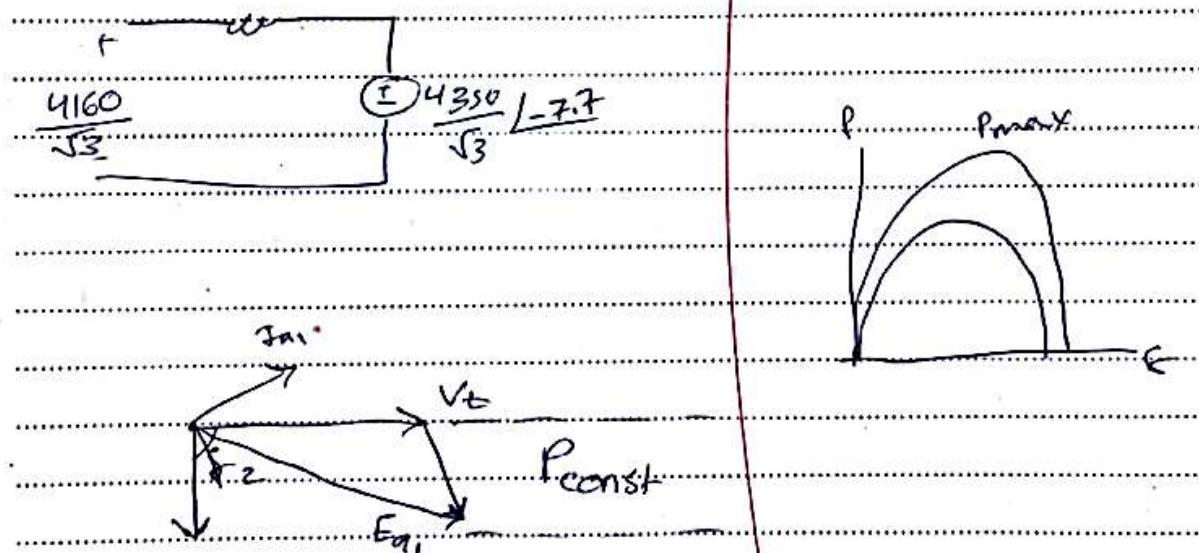
~~$\theta = 90^\circ$~~

$$\Rightarrow E_{\text{all}} = \sqrt{3} \times 336.8 = 583.46$$

$$I_a = \frac{\frac{4160}{\sqrt{3}} - 336.8}{j8} \approx 303.15 \angle -82^\circ$$

$$\rho_f = \cos(82) = 0.139$$

$$Q = \sqrt{3} \times 4160 \times 303.15 \sin(82) = -2163.0$$



Question # 2 (5 marks)SHOW YOUR CALCULATIONS

1 hp = 746 W

A 440-V, 60-Hz, 6-pole, 3-ph, Δ -connected synchronous motor draws a line current $I_L = 86.6$ A on full-load with rotational losses $P_{rot} = 3$ kW. The field current is adjusted to obtain an open-circuit voltage E_a equal to 440 V. The synchronous reactance $X_s = 5 \Omega$ per phase and the winding resistance is negligible. Draw the phasor diagram and determine:

a.	the torque angle δ	$\delta = 90^\circ$
b.	the power factor PF	$PF = 0.707$ lag
c.	the power input P_{in}	$P_{in} = 116.16$ kW
d.	the output power P_{out}	$P_{out} = 113.16$ kW
e.	the net output torque T_{out}	$T_{out} = 900.52$ Nm

$$V_L = 440 \text{ V} \quad f = 60 \text{ Hz} \quad \Delta\text{-con.} \quad I_L = 86.6 \text{ A} \quad P_{rot} = 3 \text{ kW}$$

$$E_{a_{LL}} = 440 \text{ V} \quad X_s = 5 \Omega \quad R_a \approx 0.0 \quad P = G$$

$$P_{dev} = P_{in} = \sqrt{3} \cdot V_L \cdot I_L \cdot \cos \theta$$

$$E_A \sin \delta = I_A \cdot X_s \cos \theta$$

$$P_{in} = \frac{3 V_L E_a \sin \delta}{X_s}$$

$$\text{full load} \Rightarrow \delta = 90^\circ$$

$$E_A \sin \delta = I_A \cdot X_s \cos \theta$$

$$440 \cdot 1 = \frac{86.6 \cdot 5 \cdot \cos \theta}{\sqrt{3}} \rightarrow \cos \theta = 1.76 ??$$

$$P_{in} = P_{max} = \frac{3 V_L E_a}{X_s} = \frac{3 \cdot 440 \cdot 440}{5} = 116.16 \text{ kW}$$

$$P_{in} = \frac{3 V_L I_A \cos \theta}{X_s} \Rightarrow \cos \theta = \frac{116.16}{3 \cdot 440 \cdot \frac{86.6}{\sqrt{3}}} = 1.76 ??$$

$$P_{out} = P_{in} - P_{rot} = 116.16 \text{ kW} - 3 \text{ kW} = 113.16 \text{ kW}$$

$$T_{out} = \frac{P_{out}}{W_s} = \frac{113.16 \text{ kW}}{125.66} = 900.52 \text{ Nm}$$

$$W_s = \frac{2\pi \cdot 120 \cdot 60}{60} = \frac{2\pi \cdot 1200}{60} = 125.66 \text{ rad/s}$$

$$I_A = \frac{V_L \cos \theta - E_a \sin \theta}{X_s} = \frac{129.2}{45}$$

Question # 3 (7 marks)

A 208-V Y-connected synchronous motor is drawing 50 A at unity power factor from a 208-V power system. The field current flowing under these conditions is 2.7 A. Its synchronous reactance X_s is 1.6Ω .

Part I: Assume a linear O.C. characteristic, draw the phasor diagram for this condition and find

a.	the magnitude of the induced phase voltage E_a and torque angle δ .	$E_a = 144.29$ V
b.	the steady-state stability power limit.	$P_{max} = 32.5$ kW

Part II: If the field current is adjusted to make the motor operate at 0.80 PF leading, determine.

c.	the magnitude of the new armature current I_a , induced phase voltage E_a and field current I_f .	$ I_a = 112.7$ A
d.	the new torque angle in part(c)	$E_a = 270.16$ V
		$I_f = 1.44$ A

$$V_L = 208V \quad I_L = 50A \quad pf = 1 \quad I_f = 2.7A \quad X_s = 1.6 \Omega$$

(I) $\vec{E}_a = V_t - jI_a X_s = 208/10 - 50/10 \cdot (j1.6)$

$$= 144.29 / -33.6$$

$$P_{max} = \frac{3 \times \frac{208}{\sqrt{3}} \times 144.29}{1.6} = 32.5 \text{ kW}$$

(II) $pf = 0.8 \text{ leading} \Rightarrow \theta = 36.86^\circ$

$$I_{q1} = 50 \rightarrow pf_1 = 1$$

$$I_{q2} = ? \rightarrow pf_2 = 0.8$$

$$P = \frac{3 \times \frac{208}{\sqrt{3}} \times E_a \sin \theta}{1.6} = 32.5 \text{ kW}$$

$$\rightarrow 32.5K = 3 \times V_t \times I_a \cos \theta \Rightarrow I_a = \frac{32.5K}{3 \times \frac{208}{\sqrt{3}} \times 0.8} = 112.76 \text{ A}$$

$$\vec{E}_a = V_t - jI_a X_s = 208 - (j1.6) \times 112.76 / 36.9 = 270.16 / -32.27$$

$$E_{A1} I_{F1} = E_{A2} I_{F2} \Rightarrow I_{F2} = \frac{E_{A1} \times I_{F1}}{E_{A2}} = \frac{144.29 \times 2.7}{270.16} = 1.44 ??$$

Question # 4 (13 marks)**SHOW YOUR CALCULATIONS**

A three-phase, 4160-V, Y-connected, cylindrical-rotor synchronous motor has a synchronous reactance of 8Ω per phase and a negligible armature resistance. The combined rotational losses (friction and windage plus core loss) amount to 5 kW. The highest excitation voltage possible is 4350 V. The motor delivers an output of 400 hp to a mechanical load connected to its shaft.

Part I: If the field current is increased to give the maximum excitation voltage, find:

a.	the power developed by the motor P_d .	$P_d = 303.4$ kW
b.	the torque angle δ .	$\delta = 7.7^\circ$
c.	the magnitude of the motor's armature current I_a and PF.	$I_a = 43.4 / 14.5$ A
d.	the motor efficiency η_m .	$\eta_m = 98.3\%$
e.	the maximum developed power P_{max} at the above excitation voltage.	$P_{max} = 2.262$ MW

Part II: If the field current is reduced without changing the load, find: (const power)

f.	the new maximum developed power P_{max} which the motor will remain in synchronism (stable operation).	$P_{max} = 303.4$ kW
g.	the magnitude of the smallest excitation phase voltage E_a and torque angle δ	$E_a = 583.5$ V
h.	the magnitude of the armature current I_a and PF at the smallest excitation voltage of part (g).	$I_a = 203.15 / 82$ A
i.	the reactive power Q absorbed/supplied by the motor.	$Q = 2163.0$ MVAR

Draw the equivalent circuit, phasor and power angle-curve diagrams to illustrate your solution.

$$P_{out} = 400 \text{ hp} = 298.4 \text{ kW}$$

$$V_L = 4160, X_S = 8 \Omega, R_a = 0, \text{Eff. loss} = 5 \text{ kW}, E_A = 4350$$

$$(I) P_{dev} = P_{in} = P_{out} + \text{losses} = 298.4 \text{ kW} + 5 \text{ kW} = 303.4 \text{ kW}$$

$$303.4 \text{ kW} = 3 \times \frac{4160}{\sqrt{3}} \times 4350 / \sqrt{3} \sin \delta \Rightarrow \sin \delta = 0.13 \Rightarrow \delta = 7.7^\circ$$

$$I_a = \frac{4160 / \sqrt{3}}{8} - \frac{4350 / \sqrt{3}}{14.5} = 43.4 / 14.5 \quad \text{pf} = \cos(14.5) = 0.96$$

$$\eta = \frac{P_{out}}{P_{in}} = \frac{298.4}{303.4} \times 100\% = 98.3\%$$

$$P_{max} = \frac{4160 \times 4350}{8} = 2.262 \text{ MW}$$

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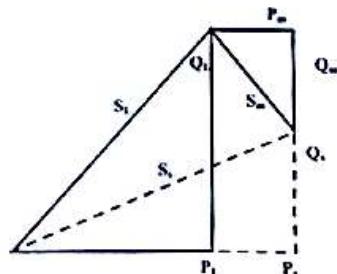
Question # 1 ⁵ (20 marks) ABET Outcome h Assessment SHOW YOUR CALCULATIONS

A 3-phase, load of an industrial plant takes a total power of 240 kW at a PF of 0.6 lagging from a 220-V supply. An additional motor load of 200 hp must be added to the plant. If a synchronous motor operating at 0.8 PF leading and having an efficiency of 90% is added in parallel with the load.

Part I: Determine:

a.	the reactive power Q_L and the magnitude of the load current $ I_L $, taken by the load.	$Q_L = 320$ kVAR $ I_L = 1049.7$ A
b.	the motor's real power, P_m , and reactive power, Q_m , and the magnitude of the motor current, I_m taken by the motor.	$P_m = 165.8$ kW $Q_m = 124.3$ kVAR $ I_m = 543.8$ A
c.	the system total real power, P_s , and reactive power, Q_s , and the magnitude of the line current, I_s supplied by the power supply.	$P_s = 405.8$ kW $Q_s = 195.6$ kVAR $ I_s = 1182.5$ A
d.	e. the overall (combined) system power factor, $PF_{overall}$.	$PF_{overall} = 0.900$ lag

Part II: Draw the power triangles for the load, motor and system.



1 hp = 746 W

Question # 2 (5 marks)

SHOW YOUR CALCULATIONS

A 440-V, 60-Hz, 6-pole, Δ-connected synchronous motor draws a line current $I_L = 86.6 \text{ A}$ on full-load with rotational losses $P_{rot} = 3 \text{ kW}$. The field current is adjusted to obtain an open-circuit voltage E_a equal to 440 V. The synchronous reactance $X_s = 5 \Omega$ per phase and the winding resistance is negligible. Draw the phasor diagram and determine:

a.	the torque angle δ	$\delta = 33^\circ$
b.	the power factor PF	$PF = 0.96$ lag
c.	the power input P_{in}	$P_{in} = 63.36 \text{ kW}$
d.	the output power P_{out}	$P_{out} = 60.36 \text{ kW}$
e.	the net output torque T_{out}	$T_{out} = 480.3 \text{ Nm}$

Solution

$$I_a = \frac{I_L}{\sqrt{3}} = \frac{86.6}{\sqrt{3}} = 50 \text{ A}$$

$$\bar{V}_t = \bar{E}_a + j\bar{I}_a X_s \Rightarrow \bar{I}_a = \frac{\bar{V}_t - \bar{E}_a}{jX_s}$$

$$|\bar{I}_a|^2 = \frac{|\bar{V}_t|^2 + |\bar{E}_a|^2 - 2|\bar{V}_t||\bar{E}_a|\cos\delta}{X_s^2} \Rightarrow 50^2 = \frac{440^2 + 440^2 - 2 \times 440 \times 440 \cos\delta}{5^2} \Rightarrow \delta = 33^\circ$$

$$\bar{I}_a = \frac{\bar{V}_t - \bar{E}_a}{jX_s} = \bar{I}_a = \frac{440\angle 0^\circ - 440\angle -33^\circ}{5\angle 90^\circ} \Rightarrow \bar{I}_a = 50\angle -16.5^\circ \text{ A}$$

$$PF = \cos(16.5^\circ) = 0.959 \text{ lag}$$

$$P_{in} = \sqrt{3}V_t I_L \cos\theta = \sqrt{3} \times 440 \times 86.6 \times 0.959 = 63.36 \text{ kW}$$

$$P_{out} = P_{in} - P_{rot} = (63.36 - 3) = 60.36 \text{ kW}$$

$$T_{out} = \frac{P_{out}}{\omega_s} = \frac{P_{out}}{\frac{2\pi N_s}{60}} = \frac{P_{out}}{\frac{2\pi}{60} \times \frac{120f}{P}} = \frac{60.36 \times 10^3}{\frac{2\pi}{60} \times \frac{120 \times 60}{6}} = \frac{60.36 \times 10^3}{125.7} \Rightarrow T_{out} = 480.3 \text{ Nm}$$

Question # 3 (11-Points)

A 208-V Y-connected synchronous motor is drawing 50 A at unity power factor from a 208-V power system. The field current flowing under these conditions is 2.7 A. Its synchronous reactance is 1.6Ω .

Part I: Assume a linear O.C. characteristic, draw the phasor diagram for this condition and find

a.	the magnitude of the induced phase voltage E_a and torque angle δ .	$E_a = 144$ V
b.	the steady-state stability power limit.	$\delta = -33.7^\circ$
		$P_{\max} = 32.4$ kW

Part II: If the field current is adjusted to make the motor operate at 0.80 PF leading, determine.

c.	the magnitude of the new armature current I_a , induced phase voltage E_a and field current I_f .	$I_a = 37$ A
d.	the new torque angle in part(c)	$E_a = 197$ V
		$I_f = 3.7$ A
		$\delta = -23.9^\circ$

Solution:

(a) The phase voltage of this motor is $V_s = 120$ V, and the armature current is $I_a = 50 \angle 0^\circ$ A

Therefore, the internal generated voltage is

$$E_a = V_s - R_a I_a - jX_a I_a$$

$$E_a = 120 \angle 0^\circ V - j(1.6 \Omega)(50 \angle 0^\circ A)$$

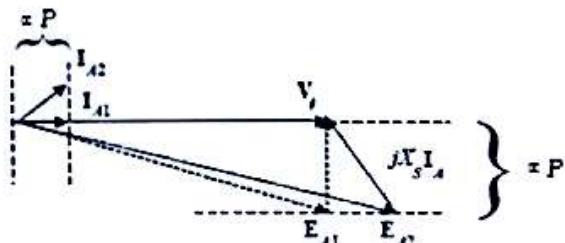
$$E_a = 144 \angle -33.7^\circ V$$

The torque angle δ of this machine is -33.7° .

The static stability power limit is given by

$$P_{\max} = \frac{3V_s E_a}{X_a} = \frac{3(120 V)(144 V)}{(1.6 \Omega)} = 32.4 \text{ kW}$$

A phasor diagram of the motor operating at a power factor of 0.78 leading is shown below.



Since the power supplied by the motor is constant, the quantity $I_a \cos \theta$, which is directly proportional to power, must be constant. Therefore,

$$I_{a2}(0.8) = (50 A)(1.00) \Rightarrow I_{a2} = 62.5 \angle 36.87^\circ A$$

The internal generated voltage required to produce this current would be

$$E_{a2} = V_s - R_a I_{a2} - jX_a I_{a2}$$

$$E_{a2} = 120 \angle 0^\circ V - j(1.6 \Omega)(62.50 \angle 36.87^\circ A)$$

$$E_{a2} = 197 \angle -23.9^\circ V$$

The internal generated voltage E_a is directly proportional to the field flux, and we have assumed in this problem that the flux is directly proportional to the field current. Therefore, the required field current is

$$I_{f2} = \frac{E_{a2}}{E_{a1}} I_{f1} = \frac{197 V}{144 V} (2.7 A) = 3.70 A$$

The new torque angle δ of this machine is -23.9° .

Question # 6 13 marks

SHOW YOUR CALCULATIONS

A three-phase, 4160-V, Y-connected, cylindrical-rotor synchronous motor has a synchronous reactance of 8Ω per phase and a negligible armature resistance. The combined rotational losses (friction and windage plus core loss) amount to 5 kW. The highest excitation voltage possible is 4350 V. The motor delivers an output of 400 hp to a mechanical load connected to its shaft.

Part I: If the field current is increased to give the maximum excitation voltage, find:

a.	the power developed by the motor P_d .	$P_d = 303.08$ kW
b.	the torque angle δ	$\delta = -7.7^\circ$
c.	the magnitude of the motor's armature current I_a and PF.	$I_a = 43.5$ A $PF = 0.968$ lead
d.	the motor efficiency η_m .	$\eta_m = 98.4\%$
e.	the maximum developed power P_{max} at the above excitation voltage.	$P_{max} = 2.262$ MW

Part II: If the field current is reduced without changing the load, find:

f.	the new maximum developed power P_{max} which the motor will remain in synchronism (stable operation).	$P_{max} = 303.08$ kW
g.	the magnitude of the smallest excitation phase voltage E_a and torque angle δ	$E_a = 583.5$ V $\delta = -90^\circ$
h.	the magnitude of the armature current I_a and PF at the smallest excitation voltage of part (g).	$I_a = 303.2$ A $PF = 0.1389$ lag
i.	the reactive power Q absorbed/supplied by the motor.	$Q = 2.164$ MVAR

Draw the equivalent circuit, phasor and power angle-curve diagrams to illustrate your solution.

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