

Student Name: _____

$\mu_0 = 4\pi \times 10^{-7} \text{ H/m}$

Question	1	2	3	4	5	6	7	8
Answer	c	a	b	c	d	b	b	d
Question	9	10	11	12	13	14	15	
Answer	b	d	c	a	b	d	d	

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SHOW YOUR CALCULATIONS

Question # 1 (15 points)

Select the correct answer for each of the following statements and fill it in the table.

1.1 A transformer transforms:

- a. the frequency.
- b. the power at constant frequency.
- c. the voltage at constant power.
- d. both the power and the voltage.

1.2 When conducting the no-load and short circuit tests for single-phase transformers, it is not recommended to:

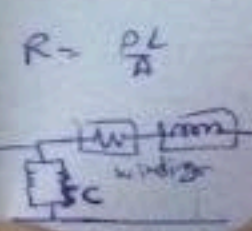
- a. Apply the rated voltage during SC test.
- b. Apply the rated voltage during OC test.
- c. Apply the rated current during SC test.
- d. None of the above.

1.3 In single phase transformers, what type of losses always exist regardless of the load:

- a. Copper losses.
- b. Core losses.
- c. (a) and (b)
- d. None of the above.

1.4 Eddy current losses can be reduced by

- a. using high quality magnetic material.
- b. using light weigh magnetic material.
- c. using thin magnetic material.
- d. using heavy weigh magnetic material.



1.5 Short circuit test is conducted in transformers to find:

- a. winding resistance
- b. winding leakage reactance
- c. core resistance
- d. winding inductance

1.6 The rated primary and secondary currents of a 20 kVA, 1200/120 V single-phase transformer. If this transformer delivers a load of 12 kW at PF = 0.8 lagging are A and A.

- a. $I_{1(rated)} = 10$
 $I_{2(rated)} = 100$
- b. $I_{1(rated)} = 12.5$
 $I_{2(rated)} = 125$
- c. $I_{1(rated)} = 16.7$
 $I_{2(rated)} = 167$
- d. $I_{1(rated)} = 13.4$
 $I_{2(rated)} = 134$

1.7 A magnetic circuit has eddy-current loss $P_e = 1000 \text{ W}$ and hysteresis loss $P_h = 800 \text{ W}$ at rated voltage and rated frequency. If the frequency is reduced by 20% while the flux density remains constant, the eddy-current loss P_e and hysteresis loss P_h become W and W.

$P_e = k_e f^2 B_m^2$
 $P_h = k_h f B_m$

- a. $P_e = 640$,
 $P_h = 640$
- b. $P_e = 200$,
 $P_h = 160$
- c. $P_e = 400$,
 $P_h = 160$
- d. $P_e = 800$,
 $P_h = 640$

$\frac{f_2}{f_1} = 0.2$

$\frac{P_{e2}}{P_{e1}} = \left(\frac{f_2}{f_1}\right)^2$

$\frac{P_{h2}}{P_{h1}} = 0.2$

$P_{e2} = 0.2 \times 1000$

$\frac{P_{h2}}{P_{h1}} = \frac{f_2}{f_1}$

$P_{h2} = 0.2 \times 800$

1.11 A single-phase transformer has 400 primary turns and 800 secondary turns. The net cross-sectional area of the core is 40 cm^2 . If the primary winding is connected to a 60 Hz supply at 60 V. The maximum value of the core flux density, B_m is ... T.

- a. $B_m = 2.8$ b. $B_m = 0.7$ c. $B_m = 1.4$ d. $B_m = 5.6$

$$V_p = N_p \frac{d\phi}{dt}$$

$$\phi = \frac{1}{N_p} \int V_p dt$$

$$\phi = \frac{1}{400} \times \int 60 \cos(2\pi \times 60 t) dt$$

$$\phi = \frac{1}{400} \times \frac{60}{2\pi \times 60} \sin(2\pi \times 60 t)$$

$$\phi = \frac{0.15}{400} \sin(2\pi \times 60 t)$$

$$\phi = 3.75 \times 10^{-4} \sin(2\pi \times 60 t)$$

$$\frac{\phi}{A} = \frac{3.75 \times 10^{-4}}{40 \times 10^{-4}} = 0.9375 \text{ T}$$

1.12 How many turns must the primary and the secondary windings of a 220/110-V, 50-Hz ideal transformer have if the core flux is not allowed to exceed 5 mWb ?

- a. $N_p = 198, N_s = 99$ b. $N_p = 220, N_s = 110$ c. $N_p = 40, N_s = 20$ d. $N_p = 2, N_s = 1$

$$V_p = N_p \frac{d\phi}{dt}$$

$$\phi = \frac{1}{N_p} \int V_p dt$$

$$5 \times 10^{-3} = \frac{220}{2\pi \times 50 \times N_p}$$

$$N_p = \frac{220}{2\pi \times 50 \times 5 \times 10^{-3}} = 198$$

$$N_s = \frac{220}{110} \times 198 = 396$$

1.13 A 1.2-kVA, 240/120-V, 400 Hz transformer is desired to be used at a frequency of 50 Hz. The kVA rating of the transformer under reduced frequency would be:

- a. 9.6 kVA b. 0.15 kVA c. 76.8 kVA d. 1.92 kVA

$$\frac{S_2}{S_1} = \frac{f_2}{f_1}$$

$$S_2 = S_1 \times \frac{f_2}{f_1} = 1.2 \times \frac{50}{400} = 0.15 \text{ kVA}$$

1.14 A single-phase transformer has 180 and 45 turns, respectively, on its primary and secondary windings. The corresponding resistances are $R_1 = 0.242 \Omega$ and $R_2 = 0.076 \Omega$, respectively. The equivalent resistance R'_{eq} referred to the primary is ... Ω .

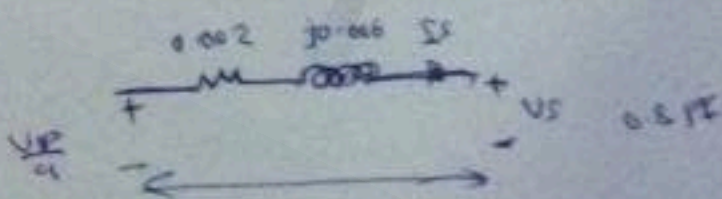
- a. $R'_{eq} = 0.55$ b. $R'_{eq} = 0.32$ c. $R'_{eq} = 0.14$ d. $R'_{eq} = 1.46$

$$a = \frac{180}{45} = 4$$

$$R'_{eq} = R_1 + a^2 R_2 = 0.242 + 4^2 \times 0.076 = 1.46 \Omega$$

1.15 A 500-kVA, 2300/230-V transformer has a series impedance referred to the secondary $Z'_{eq} = 0.002 + j0.006 \Omega$. The percentage voltage regulation when the transformer is delivering its rated load at 0.8 PF lagging is:

- a. %VR = 2.05% b. %VR = 4.97% c. %VR = -3.26% d. None of these



$$\frac{V_p}{V_s} = \frac{0.002 + j0.006 \sqrt{1779.1}}{230} \times 230 = 2391.2$$

$S = VI$

$P = VI \cos \phi$

$$I_s = \frac{500 \times 10^3 \times 0.8}{230} = 1739.1 \angle -36.87^\circ$$

2391.2

239.1

$$\%VR = \frac{239.1 - 230}{230} \times 100 = 3.91\%$$

$N_p = 400$ $A = 40 \times 10^{-4}$
 $N_s = 800$ $V_p = 600$ $f_1 = 60$

1.11 A single-phase transformer has 400 primary turns and 800 secondary turns. The net iron cross sectional area of the core is 40 cm^2 . If the primary winding is connected to a 60 Hz supply at 600 V. The maximum value of the core flux density, B_m is ... T.

- a. $B_m = 2.8$ b. $B_m = 0.7$ c. $B_m = 1.4$ d. $B_m = 5.6$

$V_p = N_p \frac{d\phi}{dt}$
 $\phi = \frac{1}{N} \int V dt$
 $\phi = \frac{1}{400} \times \int 600 \cos(2\pi \times 60 t) dt$
 $\phi = \frac{1}{400} \times \frac{600}{2\pi \times 60} \sin(2\pi \times 60 t)$
 $\phi = \frac{1}{400} \times 600 \sin(2\pi \times 60 t)$
 $\phi = \frac{1.5}{400} \sin(2\pi \times 60 t)$
 $\phi = 3.75 \times 10^{-3} \sin(2\pi \times 60 t)$
 $\phi = 3.75 \times 10^{-3} \text{ Wb}$
 $\frac{\phi}{A} = B$

1.12 How many turns must the primary and the secondary windings of a 220/110-V, 50-Hz ideal transformer have if the core flux is not allowed to exceed 5 mWb ?

- a. $N_p = 198, N_s = 99$ b. $N_p = 220, N_s = 110$ c. $N_p = 40, N_s = 20$ d. $N_p = 2, N_s = 1$

$V_p = N_p \frac{d\phi}{dt}$
 $\phi = \frac{1}{N_p} \int V_p dt$
 $5 \times 10^{-3} = \frac{220}{2\pi \times 50 \times N_p}$
 $5 \times 10^{-3} = \frac{1}{N_p} \int V_p \cos(\omega t) dt$
 $5 \times 10^{-3} = \frac{1}{N_p} \times \frac{220}{\omega} \sin(\omega t)$
 $5 \times 10^{-3} = \frac{220}{N_p \times 2\pi \times 50}$

1.13 A 1.2-kVA, 240/120-V, 400 Hz transformer is desired to be used at a frequency of 50 Hz. The kVA rating of the transformer under reduced frequency would be:

- a. 9.6 kVA b. 0.15 kVA c. 76.8 kVA d. 1.92 kVA

$\frac{S_2}{S_1} = \frac{f_2}{f_1}$
 $N_p = 180$ $N_s = 45$ $\frac{180}{45}$

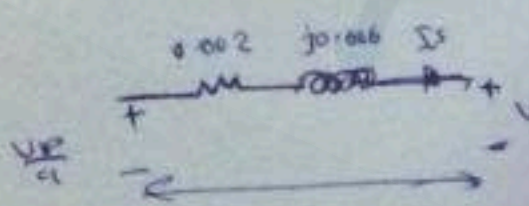
1.14 A single-phase transformer has 180 and 45 turns, respectively, on its primary and secondary windings. The corresponding resistances are $R_1 = 0.242 \Omega$ and $R_2 = 0.076 \Omega$, respectively. The equivalent resistance R'_{eq} referred to the primary is Ω .

- a. $R'_{eq} = 0.55$ b. $R'_{eq} = 0.32$ c. $R'_{eq} = 0.14$ d. $R'_{eq} = 1.46$

$a = \frac{180}{45} = 4$
 3.832
 1.916

1.15 A 500-kVA, 2300/230-V transformer has a series impedance referred to the secondary $Z'_{eq} = 0.002 + j0.006 \Omega$. The percentage voltage regulation when the transformer is delivering its rated load at 0.8 PF lagging is:

- a. %VR = 2.05% b. %VR = 4.97% c. %VR = -3.26% d. Non of these



$S = VI$
 $P = VI \cos \phi$

$I_s = \frac{500 \times 10^3 \times 0.8}{230}$
 $1739.1 \angle -36.87^\circ$
 $\frac{V_p}{a} = (0.002 + j0.006) \times (1739.1 \angle -36.87^\circ) + 230$
 2391.2
 239.1
 $VR = \frac{239.1 - 230}{230}$

$$L = 36 \times 10^{-2}$$

$$A = 3 \times 10^{-4}$$

$$N = 400$$

$$NI = \phi \cdot R$$

$$\frac{400 \times 1.4}{1.4 \times 10^{-3}} = 1.4 \times 10^{-3} \times R$$

$$R = 400 \times 10^3$$

$$R = \frac{L}{\mu A}$$

1.8 A ferromagnetic ring with a mean circumference $L_m = 36$ cm and a cross-sectional area $A_c = 3$ cm² is wound with 400 turns of wire as shown in Fig. 1. When the excitation current is 1.4 A, the flux is found to be $\phi = 1.4$ mWb. The relative permeability of the iron μ_r is

a. $\mu_r = 238732$

b. $\mu_r = 238.7$

c. $\mu_r = 0.2387$

d. $\mu_r = 2387$

$$\mu = \frac{L}{RA} = \frac{36 \times 10^{-2}}{400 \times 10^3 \times 3 \times 10^{-4}} = 3 \times 10^{-3}$$

$$\mu = \mu_r \mu_0$$

$$\mu_r = \frac{3 \times 10^{-3}}{\mu_0} = 2387$$

1.9 The solenoid shown in the Fig. 2 consists of a 500 turn coil on a uniformly sized core. The core has a cross-sectional area $A_c = 4$ cm². The length of the air gap is $l_g = 5$ mm long. If the reluctance of the core is negligible and the coil exciting current $I = 10$ A, the total magnetic flux ϕ that circulates in the core is mWb.

a. $\phi = 1.25$

b. $\phi = 0.50$

c. $\phi = 5$

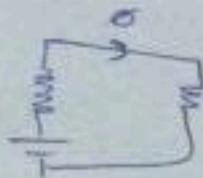
d. $\phi = 12.5$

$$N = 500$$

$$A = 4 \times 10^{-4}$$

$$l_g = 5 \times 10^{-3}$$

$$I = 10$$



$$NI = H_g l_g$$

$$H_g = \frac{5000}{5 \times 10^{-3}} = 1 \times 10^6$$

$$H_g \mu_0 = B$$

$$B = 1.256$$

1.10 A cast steel ring, as shown in Fig. 3 with B-H data as shown in Table 1, has a mean length of $L_m = 30$ cm and an air gap of $L_g = 2$ mm length. The number of ampere-turns (NI) required to produce a flux density $B = 0.6$ T in the air gap is ... At.

a. $NI = 1084$

b. $NI = 955$

c. $NI = 129$

d. $NI = 0.86$

Table 1: B-H data for Cast Steel

B (T)	0.4	0.6	0.8
H (At/m)	130	430	720

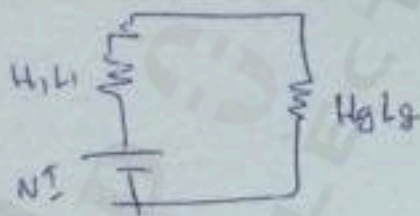
$$L = 30 \times 10^{-2}$$

$$L_g = 2 \times 10^{-3}$$

$$B_g = 0.6 \text{ T}$$

$$H_g = 430$$

$$L_g = 2 \times 10^{-3}$$



$$B \cdot A = \phi$$

$$\phi = 0.282$$

$$NI = H_1 L_1 + H_2 L_2$$

$$= \frac{430 \times 30 \times 10^{-2}}{100} + 430 \times 2 \times 10^{-3}$$



Fig. 1

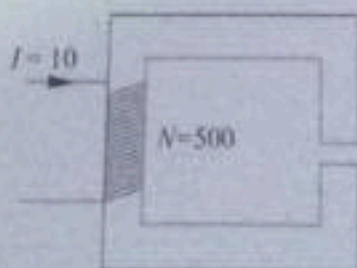


Fig. 2

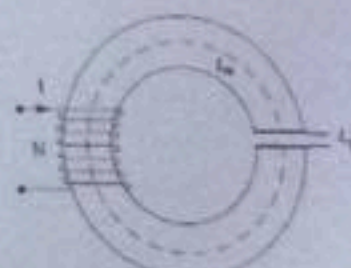


Fig. 3

$$\phi = 1.4$$

$$1.4 \times 10^{-3}$$