

\* Vectors:  $\vec{A}$  ( $\hat{A}$ )

in Cartesian (Rectangular) coordinates:

- a vector can be finite or infinite

\* Representing vectors:

1- long format: -

$$\vec{A} = A_x \underline{\hat{a}_x} + A_y \underline{\hat{a}_y} + A_z \underline{\hat{a}_z}$$

where:  $A_x, A_y, A_z$  are vector components.  
And  $\hat{a}_x, \hat{a}_y, \hat{a}_z$  are unit vectors.

2- short format: preferred to perform mathematical operations.

$\vec{A} = (A_x, A_y, A_z)$  - but always convert final answer to long format

Point  $(x, y, z)$  is different from a vector.

\* Magnitude of vector:

$$A = |\vec{A}| = \sqrt{A_x^2 + A_y^2 + A_z^2}$$

\* unit vectors in the direction of  $\vec{A}$ :

$$\vec{a}_A = \frac{\vec{A}}{|\vec{A}|} = \frac{A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z}{\sqrt{A_x^2 + A_y^2 + A_z^2}} = \hat{a}_A$$

\* Vector operations:  $\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$   
 $\vec{B} = B_x \hat{a}_x + B_y \hat{a}_y + B_z \hat{a}_z$

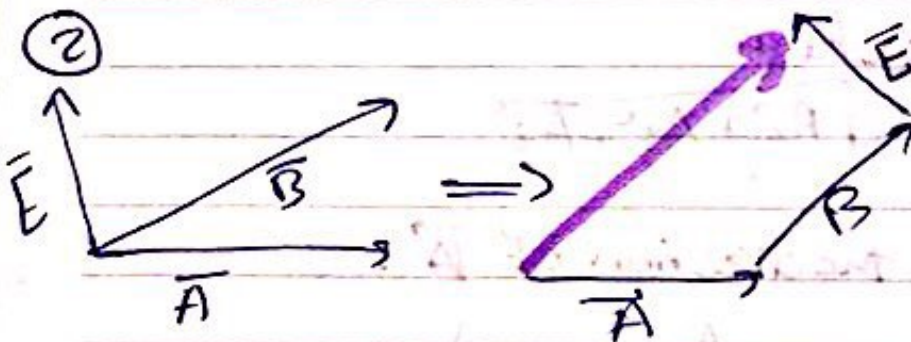
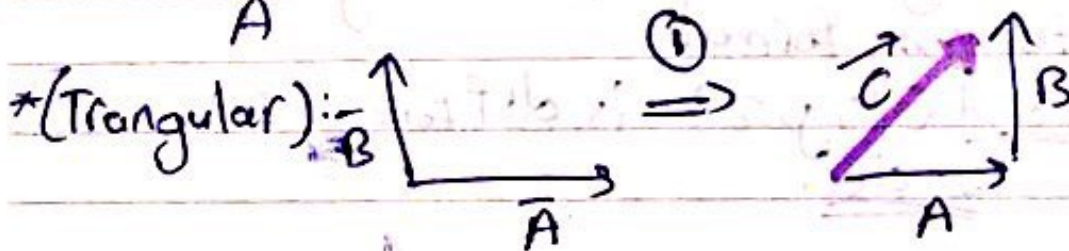
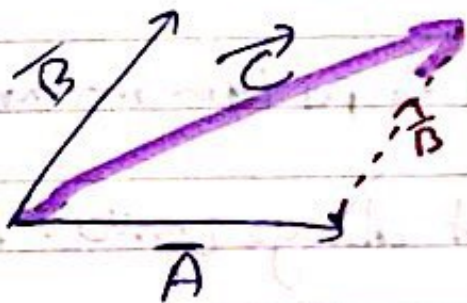
→ Addition & subtraction:

\*  $\vec{C} = \vec{A} + \vec{B} = (A_x + B_x) \hat{a}_x + (A_y + B_y) \hat{a}_y + (A_z + B_z) \hat{a}_z$

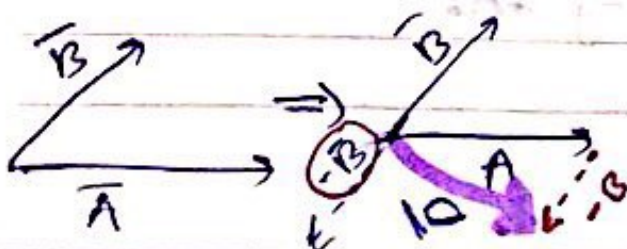
\*  $\vec{D} = \vec{A} - \vec{B} = (A_x - B_x) \hat{a}_x + (A_y - B_y) \hat{a}_y + (A_z - B_z) \hat{a}_z$

Graphically :-

\* (Parallelgram method):

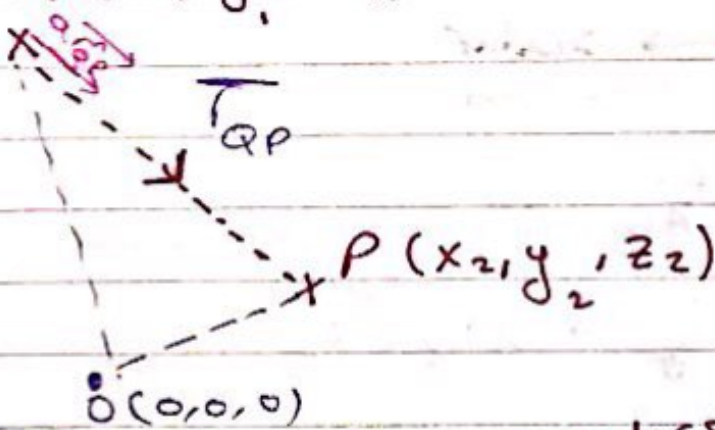


③  $\vec{D} = \vec{A} - \vec{B} = \vec{A} + (-\vec{B})$



\* Distance:

$$Q(x_1, y_1, z_1)$$



$$\vec{r}_{QP} = \vec{r}_P - \vec{r}_Q$$

vectors not points

$$= (x_2, y_2, z_2) - (x_1, y_1, z_1)$$

$$= (x_2 - x_1)\hat{a}_x + (y_2 - y_1)\hat{a}_y + (z_2 - z_1)\hat{a}_z$$

$$r_{QP} = |\vec{r}_{QP}| = \sqrt{(x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2}$$

$$\hat{a}_{r_{QP}} = \frac{\vec{r}_{QP}}{r_{QP}}$$

$$\vec{r}_{PQ} = -\vec{r}_{QP}$$

$$\hat{a}_{PQ} = -\hat{a}_{r_{QP}}$$

## \* Multiplication:

1) Dot product  $\rightarrow$  Scalar

$$\vec{A} \cdot \vec{B} = AB \cos \theta_{AB}$$

$$\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$$

$$\vec{B} = B_x \hat{a}_x + B_y \hat{a}_y + B_z \hat{a}_z$$

$$\hat{a}_x \cdot \hat{a}_x = (1)(1) \cos 0^\circ = 1$$

$$\hat{a}_x \cdot \hat{a}_y = (1)(1) \cos 90^\circ = 0$$

$$\vec{A} \cdot \vec{B} = A_x B_x + A_y B_y + A_z B_z$$

$$\theta_{AB} = \cos^{-1} \left( \frac{\vec{A} \cdot \vec{B}}{|\vec{A}| |\vec{B}|} \right)$$

$$\vec{A} \cdot \vec{B} = \vec{B} \cdot \vec{A}$$

$$\vec{A} \cdot (\vec{B} + \vec{C}) = \vec{A} \cdot \vec{B} + \vec{A} \cdot \vec{C}$$

$$\vec{A} \cdot \vec{A} = A^2$$

2) Cross product:

$$|\vec{A} \times \vec{B}| = AB \sin \theta_{AB}$$

$$\sin \theta_{AB} = \frac{|\vec{A} \times \vec{B}|}{AB}$$

$$\vec{A} \times \vec{B} = \begin{vmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$$

row  $\rightarrow$   $1+1$   $\leftarrow$  column

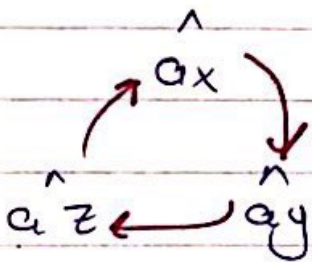
$$\vec{A} \times \vec{B} = (-1) (A_y B_z - A_z B_y) \hat{a}_x + (-1) (A_x B_z - A_z B_x) \hat{a}_y$$

$$+ (-1) (A_x B_y - A_y B_x) \hat{a}_z$$

$$\vec{A} \times \vec{B} \perp \vec{A} \text{ and } \vec{B}$$

$$|\hat{a}_x \times \hat{a}_x| = (1)(1) \sin(0) = \text{zero}$$

$$|\hat{a}_x \times \hat{a}_y| = (1)(1) \sin(90) = 1$$



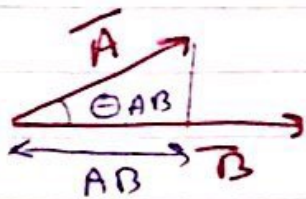
$$\hat{a}_x \times \hat{a}_z = -(1) \hat{a}_y$$

$$\hat{a}_z \times \hat{a}_x = + \hat{a}_y$$

$$\vec{A} \times \vec{B} = -\vec{B} \times \vec{A}$$

$$\vec{A} \times (\vec{B} + \vec{C}) = \vec{A} \times \vec{B} + \vec{A} \times \vec{C}$$

\* Component of a vector along another vector.



$A_B =$  scalar projection from A along B

$\overline{A_B} =$  vector " " " " " "

$$A_B = A \cos \theta_{AB}$$

$$\hat{a}_B = \frac{\overline{B}}{B}$$

$$\overline{A} \cdot \hat{a}_B = A \cos \theta_{AB}$$

$$* \overline{A} \cdot \hat{a}_B = A_B *$$

$$\overline{A_B} = A_B \hat{a}_B$$

$$\overline{A_B} = (\overline{A} \cdot \hat{a}_B) \hat{a}_B$$

↑  
scalar

\* Example: given  $\overline{A} = 3\hat{a}_x + 4\hat{a}_y + 1\hat{a}_z$   
 $\overline{B} = 2\hat{a}_y + 5\hat{a}_z$

Find: a) The angle between A and B

b)  $A_B$ ,  $\overline{A_B}$

a)

Sol.

$$\vec{A} \cdot \vec{B} = AB \cos \theta_{AB}$$

$$\vec{A} \cdot \vec{B} = 0 + 8 - 5 = 3$$

$$A = \sqrt{26}$$

$$B = \sqrt{29}$$

$$\Rightarrow \theta_{AB} = \cos^{-1} \left( \frac{3}{\sqrt{29} \cdot \sqrt{26}} \right)$$

try it using  $\sin^{-1} \left( \frac{|\vec{A} \times \vec{B}|}{AB} \right)$

b)  $A_B = \vec{A} \cdot \hat{a}_B$

$$\hat{a}_B = \frac{(0, 2, -5)}{\sqrt{29}}$$

$$A_B = \frac{8}{\sqrt{29}} - \frac{5}{\sqrt{29}} = \frac{3}{\sqrt{29}}$$

or  $A_B = A \cos \theta_{AB}$

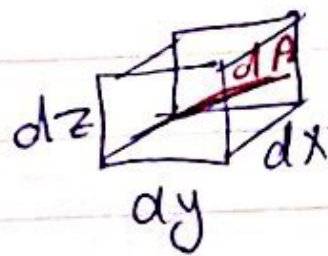
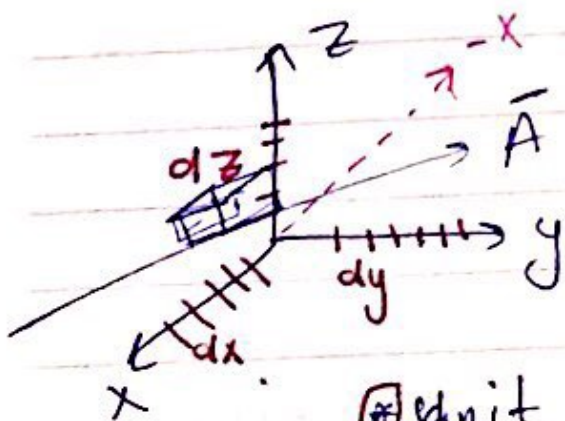
$$= \frac{\sqrt{26} \cdot 3}{\sqrt{29} \cdot \sqrt{26}}$$

$$\vec{A}_B = A_B \hat{a}_B = \frac{3}{\sqrt{26}} \cdot \frac{1}{\sqrt{29}} (0, 2, -5) = \frac{6}{29} \hat{a}_y - \frac{15}{29} \hat{a}_z$$

## CH. 2 Coordinate Systems:

### ① Cartesian coordinates (rectangular)

$$\left. \begin{aligned} -\infty < x < \infty \\ -\infty < y < \infty \\ -\infty < z < \infty \end{aligned} \right\} \rightarrow \text{3D object Infinite box.}$$



- ⊗ Unit vectors:  $\hat{a}_x, \hat{a}_y, \hat{a}_z$
- ⊗ Differential elements:  $dx, dy, dz$

⊗ Differential length ( $d\vec{l}$ ) → vector

$$d\vec{l} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

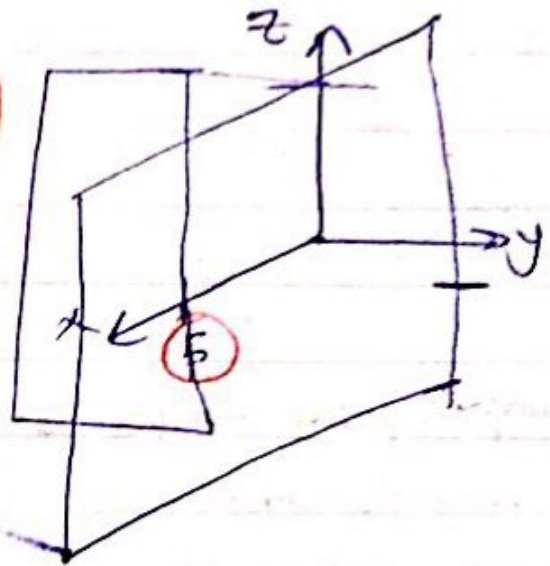


Differential volume.

$$dV = dx dy dz \quad \left. \vphantom{dV} \right\} \text{conserve order.}$$

→ 2D surfaces: - produced by fixing the value of one variable and varying the other two.

graph of  $x=5$



→ 1D segment → produced by fixing 2 variables

example: ①  $x=2, z=-2$

an infinite line parallel to the y-axis

②  $y=0, z=0$

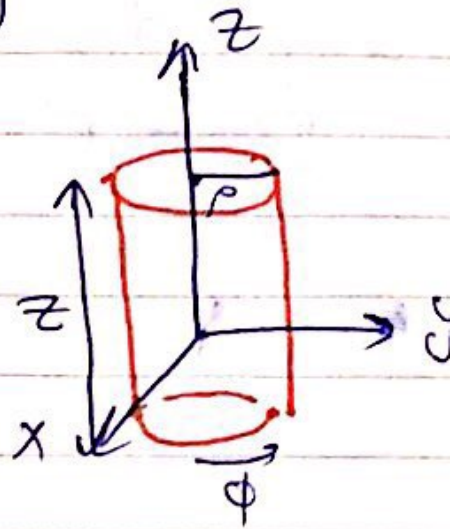
an infinite line that lies on the x-axis

→ points: produced by fixing 3 variables.

[2] Cylindrical coordinates:

→ parameters:  $\rho, \phi, z$

$$\rightarrow \begin{cases} 0 < \rho < \infty \\ 0 < \phi < 2\pi \\ -\infty < z < \infty \end{cases}$$



→ unit vectors:  $\hat{a}_\rho, \hat{a}_\phi, \hat{a}_z$

→ differential elements:  $d\rho, d\phi, dz$

→ differential length

$$d\ell = d\rho \hat{a}_\rho + \rho d\phi \hat{a}_\phi + dz \hat{a}_z$$

\* Differential Normal Surface Area:

$$\vec{ds} = r d\phi dz \hat{a}_\rho$$

$$\vec{ds}_{\text{top}} = r d\phi dr \hat{a}_z$$

$$\vec{ds}_{\text{bottom}} = r d\phi dr - \hat{a}_z$$

$$\vec{ds}_{\text{cut}} = r dz \hat{a}_\phi \quad \bigcirc$$

\* Volume: (scalar)  $\int \rho \, d\phi \, dz$

2D-Surfaces:-

produced by fixing one variable and varying the other two.

ex.  $\rho = 3 \rightarrow$  infinite hollow cylinder.

$\rho = 0 \rightarrow$  infinite line that is along the z axis.

1D-segment:-

$\rightarrow$  when the radius is zero, the angles no longer effect graph.

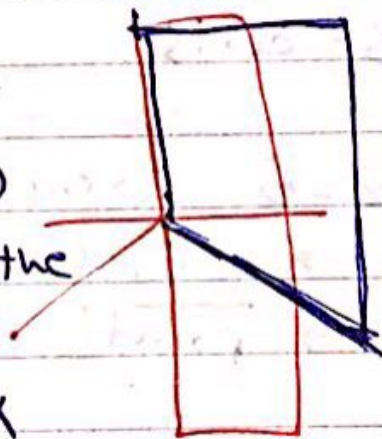
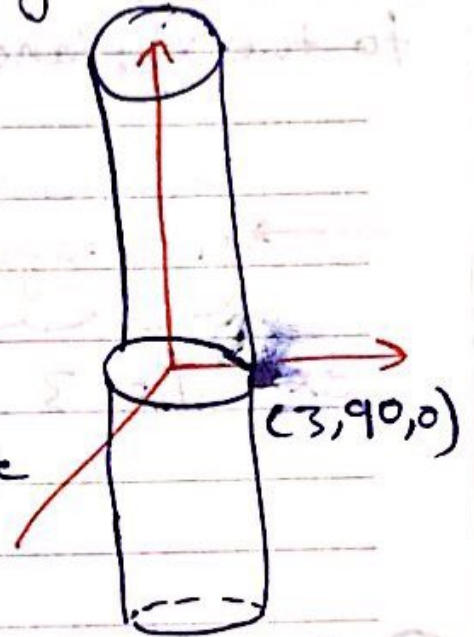
$\phi = \text{constant}$

\*  $\phi = 90$

$\rightarrow$  an infinite plane that lies along the positive yz-plane.

$\rightarrow$  the normal to the 2D surface is always along the fixed variable.

$\rightarrow \phi$  increases from x towards y in the counter clock wise direction. (normal will be with  $\phi$ 's movement).

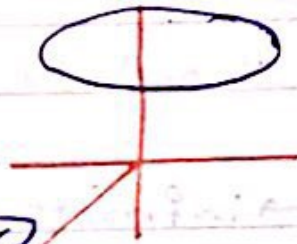


\*  $\phi = 45$   
 $\hookrightarrow$  an infinite plane perpendicular to the xy plane.

$z = \text{constant}$

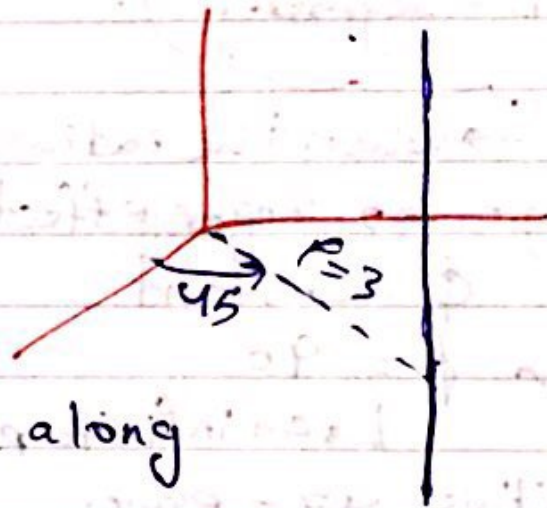
ex.  $z = 2$

infinite disk parallel to the xy plane  $\rightarrow$



$\rightarrow$  1-D segments

ex. ①  $\rho = 3, \phi = 45$



②  $\rho = 0, \phi = 70$

$\hookrightarrow$  an infinite line along the z-axis.

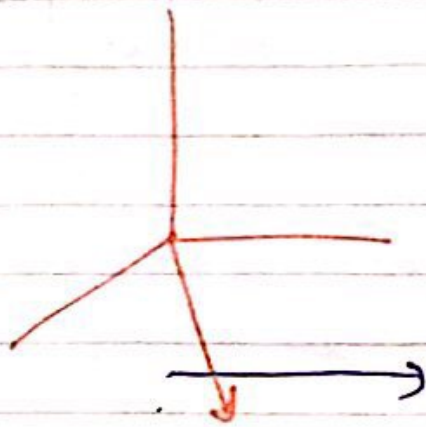
③  $\rho = 5, z = 5 \rightarrow$  circle parallel to the xy plane  
 if  $z = 0 \rightarrow$  a circle along the xy plane.  
 if  $\rho = 0 \rightarrow$  point (when  $\rho = 0$ )

④  $\phi = 45^\circ, z = 0 \rightarrow$  a (semi-infinite) line along the xy plane

$\phi = 90^\circ, z = ?$

$\Rightarrow$  continue.

⇒ semi-infinite line parallel to the xy plane.



### 3 Spherical Coordinates.

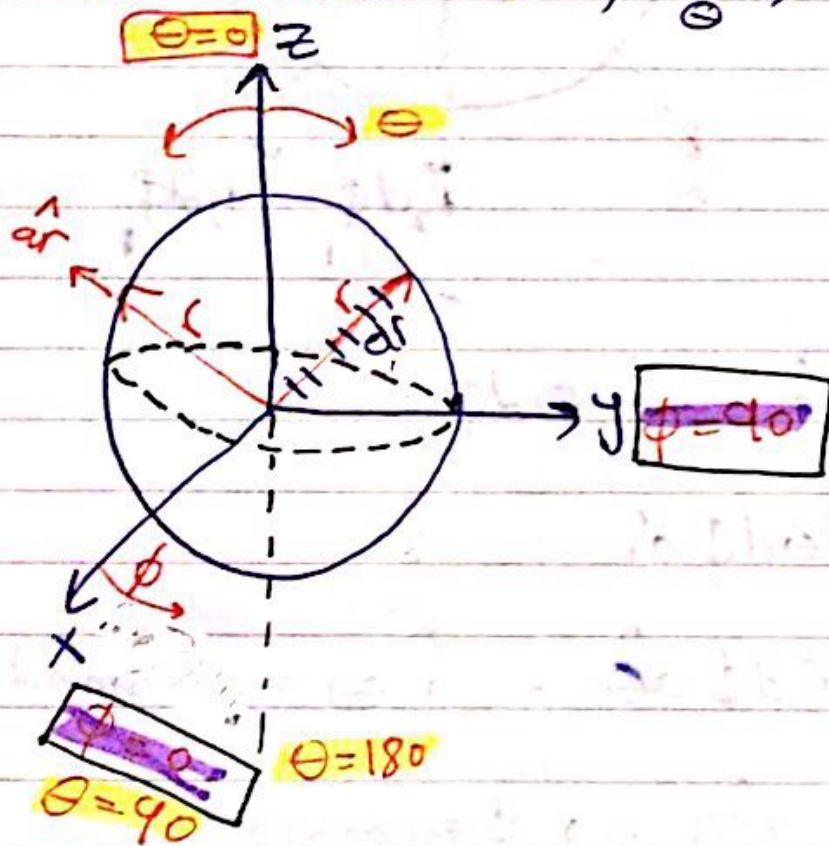
$$0 \leq r < \infty$$

$$0 \leq \theta \leq \pi$$

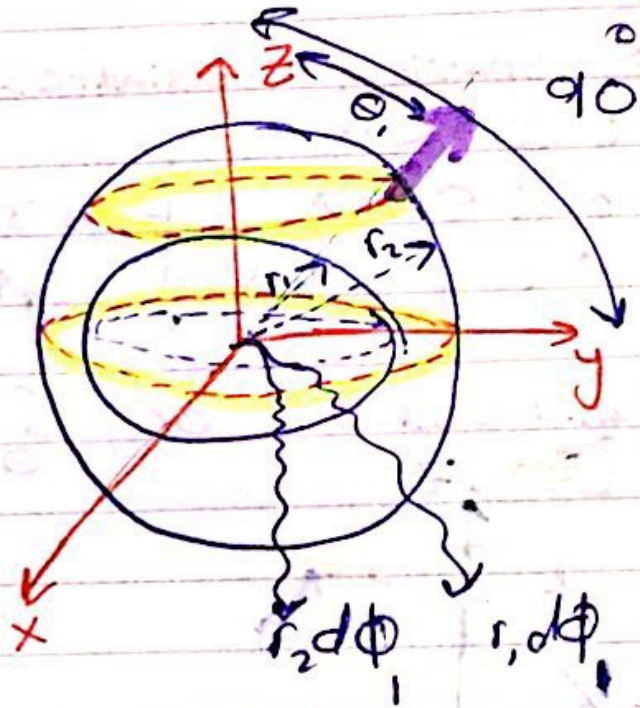
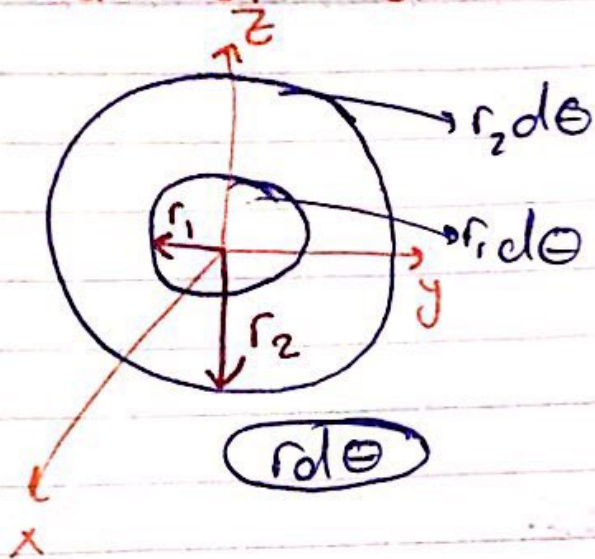
$$0 \leq \phi \leq 2\pi$$

} 3D object Inf. Solid Sphere.

\* unit vectors:  $\hat{a}_r$ ,  $\hat{a}_\theta$ ,  $\hat{a}_\phi$



\* differential elements:  $dr, r d\theta, r \sin \theta d\phi$



$$d\vec{l} = dr \hat{a}_r + r d\theta \hat{a}_\theta + r \sin \theta d\phi \hat{a}_\phi$$

$$d\vec{s} = r^2 \sin \theta d\theta d\phi \hat{a}_r$$

$$d\vec{s} = r \sin \theta dr d\phi \hat{a}_\theta \rightarrow \theta = \text{constant}$$

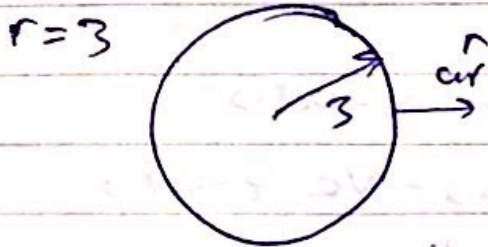
$$d\vec{s} = r dr d\theta \hat{a}_\theta \rightarrow \phi = \text{constant}$$

$$dV = r^2 \sin \theta dr d\theta d\phi \rightarrow \text{Vol} = \int_0^{2\pi} \int_0^\pi \int_0^r r^2 \sin \theta dr d\theta d\phi$$

# 2D Surfaces:

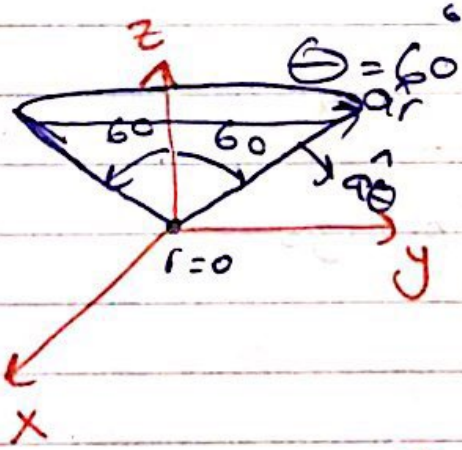
$r = \text{constant}$

$r = \text{any value} \neq \text{zero} \rightarrow \text{hollow sphere}$   
 $r = 0 \rightarrow \text{point.}$



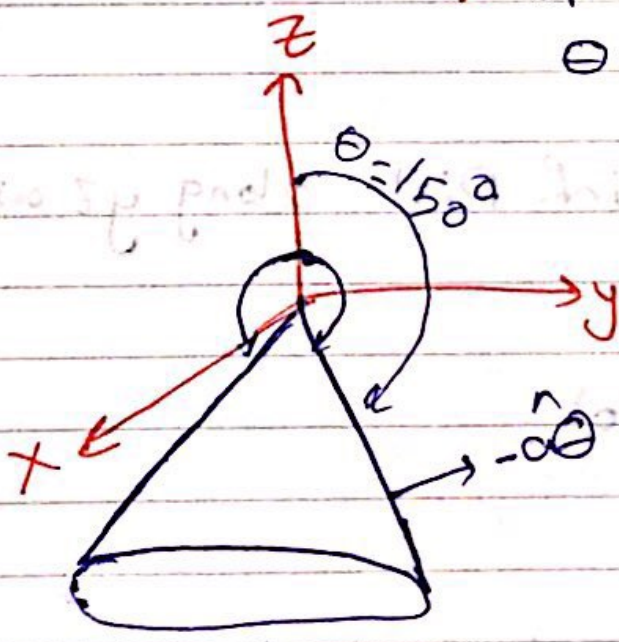
$\theta = \text{constant}$

\* if  $0 < \theta < 90^\circ$



inf. hollow cone

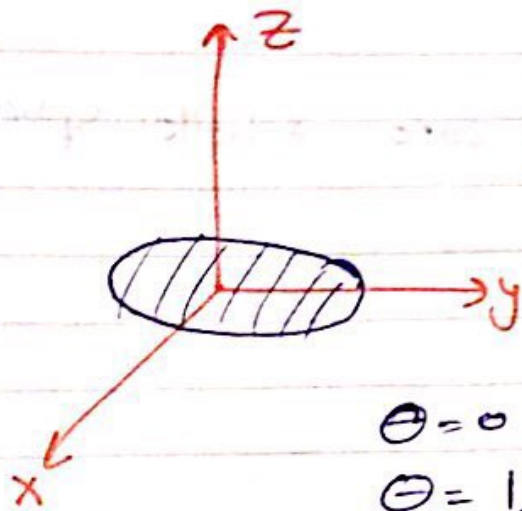
\* if  $90^\circ < \theta < 180^\circ$   
 $\theta = 150^\circ$



inf. hollow cone.

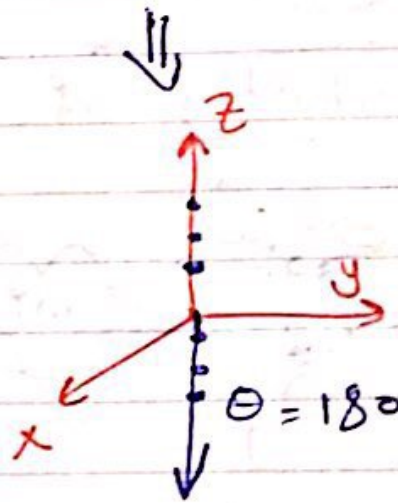


$\Theta = 90^\circ \rightarrow$  inf. Disc along xy plane



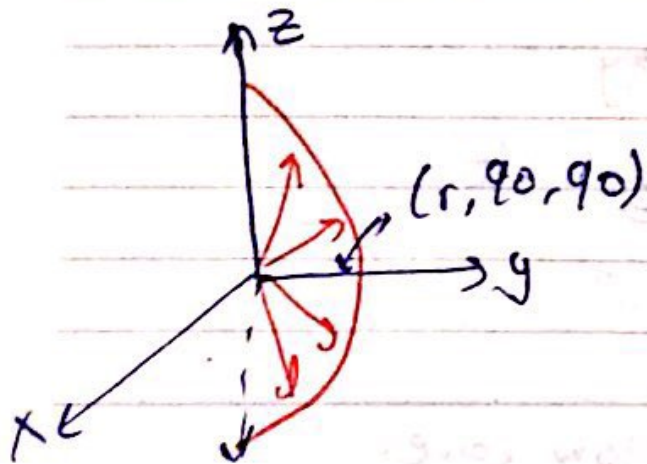
$\Theta = 0 \Rightarrow +ve$  z-axis

$\Theta = 180^\circ \Rightarrow -ve$  z-axis.



$\phi = \text{constant}$

$\Phi = 90^\circ \rightarrow$  semi inf. Disc along yz axis



∴ 1-D segment :

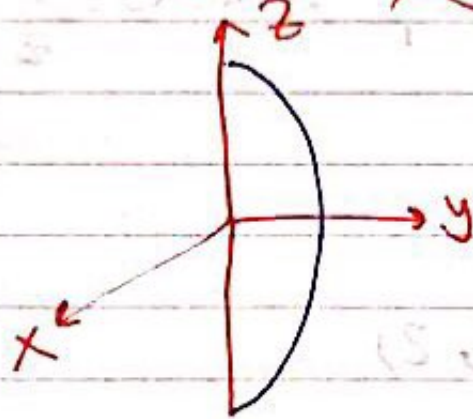
⊠  $r, \theta$  are constants

- ↳ circle (if  $r \neq 0$ )  
 $\theta = 0, 180$   
Parallel xy plane.
- ↳ circle along xy plane.  
if  $\theta = 90^\circ$   
 $r \neq 0$

⊠  $r, \phi$  are constants.

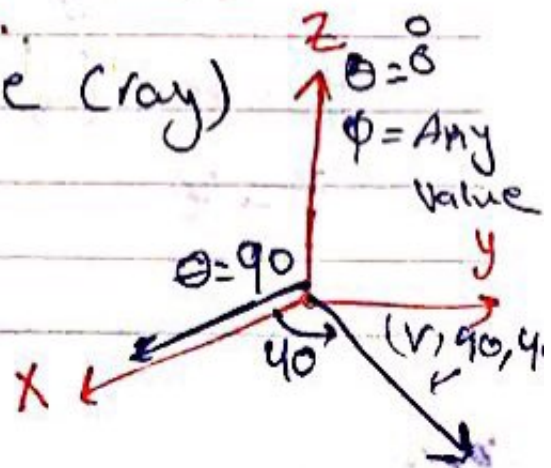
- ↳ half circle ( $r \neq 0$ )

$r = 3$  ,  $\phi = \frac{\pi}{2}$

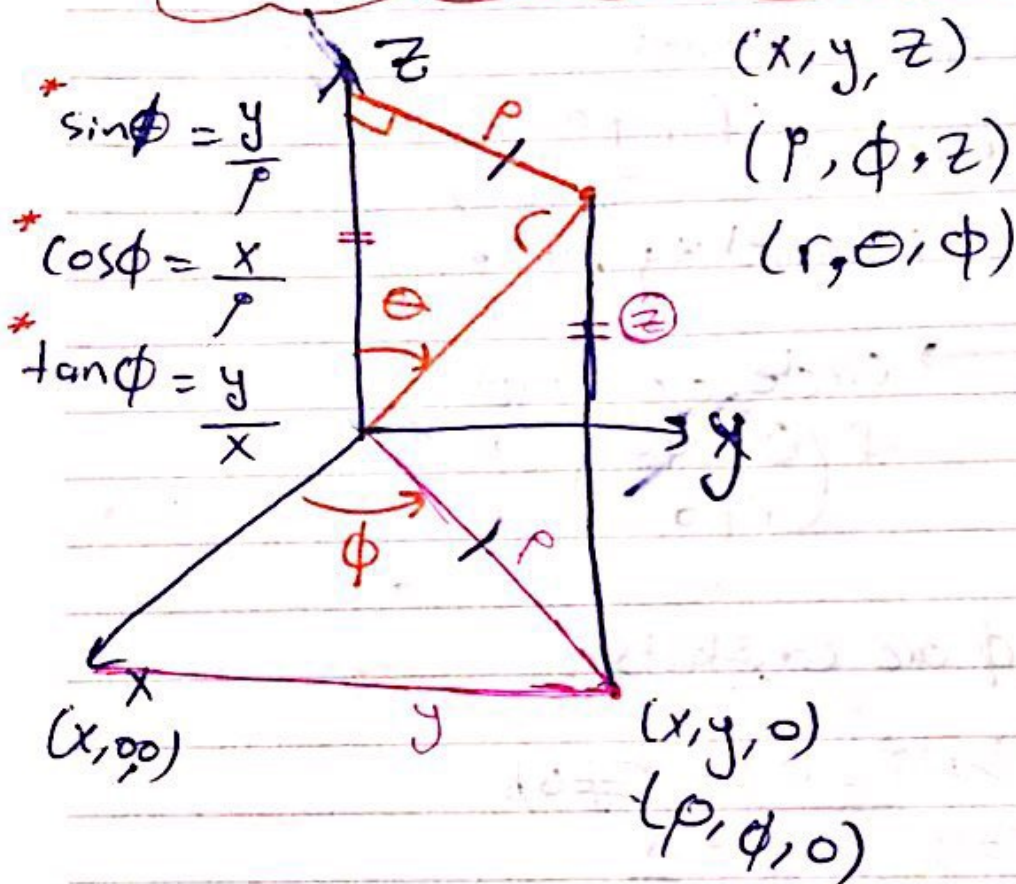


⊠  $\theta, \phi$  are constants.

- ↳ semi-inf line (ray)
- $\theta = 90^\circ$  ,  $\phi = 40$



\* Transformation between coordinates :-



\*  $\sin \phi = \frac{y}{\rho}$

\*  $\cos \phi = \frac{x}{\rho}$

\*  $\tan \phi = \frac{y}{x}$

\*  $\sin \theta = \frac{\rho}{r}$  , \*  $\cos \theta = \frac{z}{r}$  , \*  $\tan \theta = \frac{\rho}{z}$

\* { Cart  $\rightarrow$  Cyl. }

$(x, y, z) \rightarrow (\rho, \phi, z)$

$\rho = \sqrt{x^2 + y^2}$

$\phi = \tan^{-1}\left(\frac{y}{x}\right)$

$z = z$

(y)  $\rightarrow$  cart :-

$$x = \rho \cos \phi$$

$$y = \rho \sin \phi$$

$$z = z$$

cart  $\rightarrow$  sph.

$$(x, y, z) \rightarrow (r, \theta, \phi)$$

$$r = \sqrt{x^2 + y^2 + z^2}$$

$$\theta = \tan^{-1} \left( \frac{\sqrt{x^2 + y^2}}{z} \right)$$

$$\phi = \tan^{-1} \left( \frac{y}{x} \right)$$

sph  $\rightarrow$  cart.

$$x = r \sin \theta \cos \phi$$

$$y = r \sin \theta \sin \phi$$

$$z = r \cos \theta$$

cyl  $\rightarrow$  sph.

$$(\rho, \phi, z) \rightarrow (r, \theta, \phi)$$

$$r = \sqrt{\rho^2 + z^2}$$

$$\theta = \tan^{-1} \left( \frac{\rho}{z} \right)$$

$$\phi = \phi$$

sph  $\rightarrow$  cyl.

$$\rho = r \sin \theta$$

$$\phi = \phi$$

$$z = r \cos \theta$$

## \* Transformation of vectors.

Cart  $\rightleftharpoons$  cyl.

$$\begin{aligned} \text{Cart. } \vec{A} &= A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z \\ \text{Cyl. } \vec{A} &= A_\rho \hat{a}_\rho + A_\phi \hat{a}_\phi + A_z \hat{a}_z \end{aligned}$$

$$\begin{bmatrix} A_\rho \\ A_\phi \\ A_z \end{bmatrix}_{3 \times 1} = \begin{bmatrix} \cos\phi & \sin\phi & 0 \\ -\sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix}_{3 \times 3} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix}_{3 \times 1}$$

← given

$$\Rightarrow A_\rho = \cos\phi A_x + \sin\phi A_y$$

i.e.  $A_x = x^2 y$

replace any  $x, y$  by it's en.

$$x = \rho \cos\phi$$

$$y = \rho \sin\phi$$

$$x^2 y = (\rho \cos\phi)^2 (\rho \sin\phi)$$

\* transforming from cyl  $\rightarrow$  cart  
we replace each column with row in the matrix.

$$\begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} = \begin{bmatrix} \cos\phi & -\sin\phi & 0 \\ \sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A_\rho \\ A_\phi \\ A_z \end{bmatrix}$$

cart  $\rightleftharpoons$  sph.

cart.  $\vec{A} = A_x \hat{a}_x + A_y \hat{a}_y + A_z \hat{a}_z$

sph.  $\vec{A} = A_r \hat{a}_r + A_\theta \hat{a}_\theta + A_\phi \hat{a}_\phi$

$\begin{matrix} r \\ \theta \\ \phi \end{matrix}$   $\begin{bmatrix} A_r \\ A_\theta \\ A_\phi \end{bmatrix} = \begin{bmatrix} \sin\theta \cos\phi & \sin\theta \sin\phi & \cos\theta \\ \cos\theta \cos\phi & \cos\theta \sin\phi & -\sin\theta \\ -\sin\phi & \cos\phi & 0 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix}$

we can also use the matrix to get the unit vectors.

$\begin{bmatrix} \hat{a}_r \\ \hat{a}_\theta \\ \hat{a}_\phi \end{bmatrix} = \begin{bmatrix} \cos\theta \cos\phi \\ \cos\theta \sin\phi \\ -\sin\theta \end{bmatrix}$

→ replace any x, y, z by:-

$$x = r \sin\theta \cos\phi$$

$$y = r \sin\theta \sin\phi$$

$$z = r \cos\theta$$

ex.  $\hat{a}_\phi = -\sin\phi \hat{a}_x + \cos\phi \hat{a}_y$

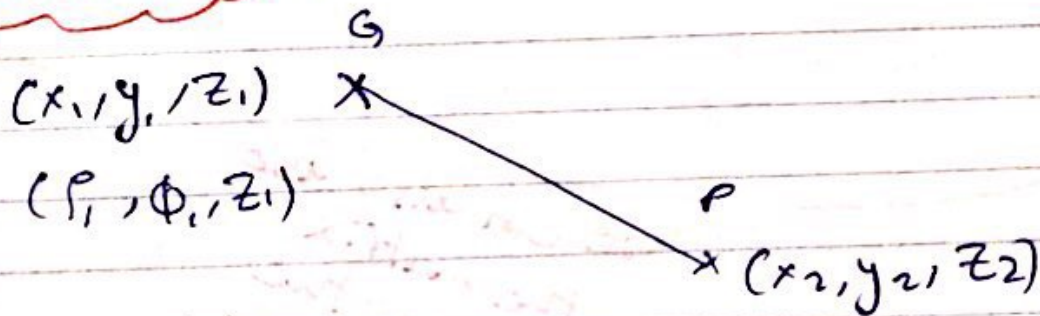
Cyl  $\rightleftharpoons$  sph  $\vec{A} = (A_\rho, A_\phi, A_z) \rightarrow \vec{A} = (A_r, A_\theta, A_\phi)$



$$\begin{bmatrix} Ar \\ A\theta \\ A\phi \end{bmatrix} = \begin{bmatrix} \sin\theta & 0 & \cos\theta \\ \cos\theta & 0 & -\sin\theta \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} Ap \\ A\phi \\ Az \end{bmatrix}$$

$$* \boxed{A\phi = A\phi}$$

\* Distance :-



$$\text{Cart} \Rightarrow d^2 = (x_2 - x_1)^2 + (y_2 - y_1)^2 + (z_2 - z_1)^2$$

$$d^2 = (r_1^2 + r_2^2 - 2r_1 r_2 \cos(\phi_2 - \phi_1) + (z_2 - z_1)^2)$$

$$\Rightarrow \text{if } \phi_1 = \phi_2 \Rightarrow (r_2 - r_1)^2 + (z_2 - z_1)^2$$

$$\cos(\phi_2 - \phi_1) = 1$$

\*CH.3

\*Integrals:

→ line integral →  $\int \vec{A} \cdot d\vec{L}$

$$\int_C \vec{A} \cdot d\vec{L} = \int_x A_x dx + \int_y A_y dy + \int_z A_z dz$$

$\vec{A} = A_x \hat{x} + A_y \hat{y} + A_z \hat{z}$   
 $d\vec{L} = dx \hat{x} + dy \hat{y} + dz \hat{z}$   
 any vector / cart / sph / cyl...  
 line integral

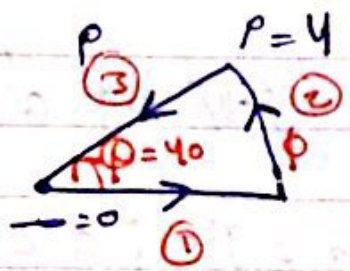
ex.  $\vec{A} = (A_x, A_y, A_z)$

$$d\vec{L} = dx \hat{x} + dy \hat{y} + dz \hat{z}$$

$$\vec{A} \cdot d\vec{L} = A_x dx + A_y dy + A_z dz$$

⇒ Closed line integral:

$$\oint_C \vec{A} \cdot d\vec{L}$$



$$\oint_C \vec{A} \cdot d\vec{L} = \oint_{L_1} \vec{A} \cdot d\vec{L}_1 + \oint_{L_2} \vec{A} \cdot d\vec{L}_2 + \oint_{L_3} \vec{A} \cdot d\vec{L}_3$$

$$dL_1 = d\rho \hat{\rho}$$

$$dL_2 = \rho d\phi \hat{\phi}$$

$$dL_3 = dL_1$$

\*  $dL$  is always +ve, direction of integration



→ Surface integral:

$$\int \vec{A} \cdot \vec{ds}$$

$$\int \int_A A_x dy dz$$

$$\vec{ds}_{\text{front}} = dy dz \hat{a}_x$$



$$\vec{A} \cdot \vec{ds}$$

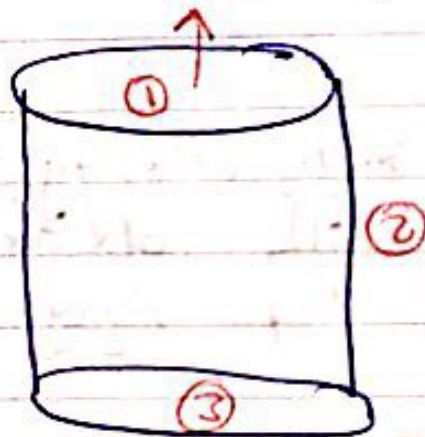
$$(A_x \hat{a}_x \cdot dy dz \hat{a}_x + (0) + (0))$$

→ closed surface integral:

$$\vec{A} = (A_\rho, A_\phi, A_z)$$

$$\oint \vec{A} \cdot \vec{ds}$$

$$= \oint_{S_1} \vec{A} \cdot \vec{ds}_1 + \int_{S_2} \vec{A} \cdot \vec{ds}_2 + \int_{S_3} \vec{A} \cdot \vec{ds}_3$$



$$\vec{ds}_1 = r d\phi dz \hat{a}_z$$

$$\vec{ds}_2 = r d\phi dz \hat{a}_\phi$$

$$\vec{ds}_3 = r d\phi dz \hat{a}_z$$

→ volume integral:  $dv$

$$\int_V |\vec{A}| dv \rightarrow \sqrt{A_x^2 + A_y^2 + A_z^2}$$

$$dv = r^2 \sin\theta dr d\theta d\phi$$

$$\int_r A dv = \int_0^{2\pi} \int_0^{\pi} \int_0^d A r^2 \sin \theta dr d\theta d\phi$$

\*\* Del operator  $\nabla \Rightarrow$  vector.

→ cart :-  $\nabla = \frac{\partial}{\partial x} \hat{a}_x + \frac{\partial}{\partial y} \hat{a}_y + \frac{\partial}{\partial z} \hat{a}_z$

→ cyl :-  $\nabla = \frac{\partial}{\partial \rho} \hat{a}_\rho + \frac{1}{\rho} \frac{\partial}{\partial \phi} \hat{a}_\phi + \frac{\partial}{\partial z} \hat{a}_z$

→ sph :-  $\nabla = \frac{\partial}{\partial r} \hat{a}_r + \frac{1}{r} \frac{\partial}{\partial \theta} \hat{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} \hat{a}_\phi$

\* uses:

1) Gradient: → vector

$$\nabla \psi = \text{Gradient of } \psi$$

$$\text{Cart } \nabla \psi = \frac{\partial \psi}{\partial x} \hat{a}_x + \frac{\partial \psi}{\partial y} \hat{a}_y + \frac{\partial \psi}{\partial z} \hat{a}_z$$

ex:-  $v = \rho^2 \cos \phi e^z$  → cyl

$$\nabla v = 2\rho \cos \phi e^z \hat{a}_\rho - \rho \sin \phi e^z \hat{a}_\phi + \rho^2 \cos \phi e^z \hat{a}_z$$

2) divergence → scalar:  $\nabla \cdot \vec{A} \rightarrow$  Divergence of A

\*\* cart:  $\left( \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right) \cdot (A_x, A_y, A_z)$

given

\* cyl:  $= \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho A_\rho) + \frac{1}{\rho} \frac{\partial A_\phi}{\partial \phi}$

\* sph:  $\nabla \cdot \vec{A} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta A_\theta) + \frac{1}{r \sin \theta} \frac{\partial A_\phi}{\partial \phi}$

[3] Curl  $\rightarrow$  vector.

$$\nabla \times \bar{A} \equiv \text{curl of } \bar{A}.$$

(given)

$$\text{in Cart: } \nabla \times \bar{A} = \begin{bmatrix} \hat{a}_x & \hat{a}_y & \hat{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{bmatrix}$$

$$\text{in Cyl: } \nabla \times \bar{A} = \frac{1}{\rho} \begin{bmatrix} \hat{a}_\rho & \rho \hat{a}_\phi & \hat{a}_z \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ A_\rho & A_\phi & A_z \end{bmatrix}$$

$$\text{in Sph: } \frac{1}{r^2 \sin \theta} \begin{bmatrix} \hat{a}_r & r \hat{a}_\theta & r \sin \theta \hat{a}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & r A_\theta & r \sin \theta A_\phi \end{bmatrix}$$

[4] Laplacian  $\Rightarrow$  scalar.

$$\nabla \cdot \nabla V \Rightarrow \nabla^2 V \Rightarrow \text{Laplacian of } V$$

$\rightarrow$  used later in chapter 6

\* Ch. 4 :-

:- electrostatics fields :-

→ to have a static electric field. the charge should be static (not moving,  $v=0$ )

\* types of charges :-

- 1) point charge  $Q$  or  $q$ .
- 2) line charge ( $\rho_L$ )
- 3) surface charge ( $\rho_S$ )
- 4) volume charge ( $\rho_V$ )
- 5) electric dipole.
- 6) polarized dielectric.

→ two main equations deal with electrostatics:

- 1) Coulomb's law → general
- 2) Gauss law → special case from Coulomb's law.

\*\* Coulomb's law :- (discovered by experiment).

$F = \text{force}$ .

$$\left. \begin{aligned} F &\propto Q_1, Q_2 \\ F &\propto \frac{1}{R^2} \end{aligned} \right\} \rightarrow F \propto \frac{Q_1 Q_2}{R^2}$$

$$\Rightarrow F = k \frac{Q_1 Q_2}{R^2}$$

$$\text{constant} = \frac{1}{4\pi\epsilon_0} \Rightarrow \text{depend on:}$$

- 1) channel used  
2) units used

ⓔ → free space permibility by  $= \frac{10^{-9}}{36\pi} = 8.853 \times 10^{-12} \text{ F/m}$

$$F = \frac{Q_1 Q_2}{4\pi\epsilon_0 R^2} \text{ N}$$

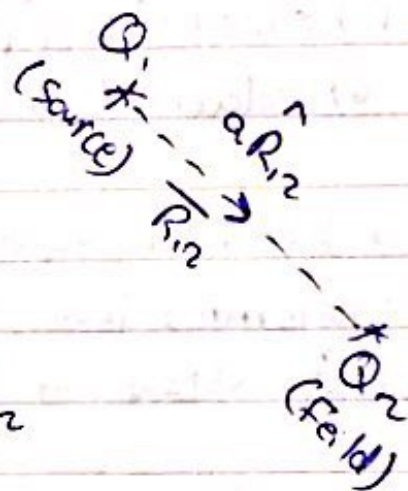
↳ magnitude only.

→ to determine the direction of the force the force on  $Q_2$  due to  $Q_1$  →  $\vec{F}_{12} = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} \hat{r}_{12}$   
↓  
vector

→ Distance = field - source

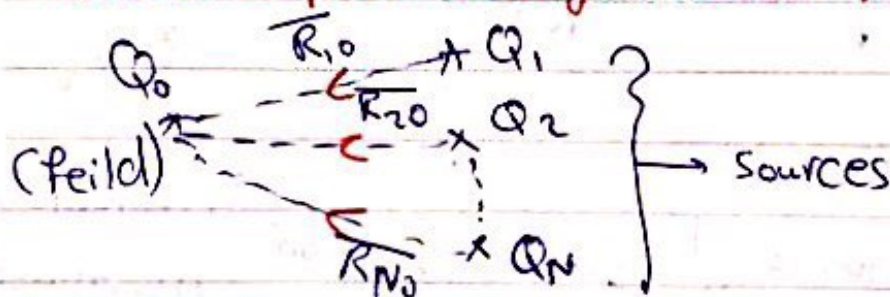
$$\begin{cases} \vec{F}_{12} = -\vec{F}_{21} \\ |\vec{F}_{12}| = |\vec{F}_{21}| \\ \rightarrow a\hat{R}_{12} = -a\hat{R}_{21} \end{cases}$$

→ we know:  $\frac{\vec{R}_{12}}{|R_{12}|} = \hat{r}_{12}$



$$F_{12} = \frac{Q_1 Q_2}{4\pi\epsilon_0 R_{12}^2} * \frac{\vec{R}_{12}}{R_{12}} = \frac{Q_1 Q_2 \vec{R}_{12}}{4\pi\epsilon_0 R_{12}^3}$$

\* force on point charge due to N charges:



The force on  $Q_0 = \vec{F} = \vec{F}_{10} + \vec{F}_{20} + \dots + \vec{F}_{N0}$

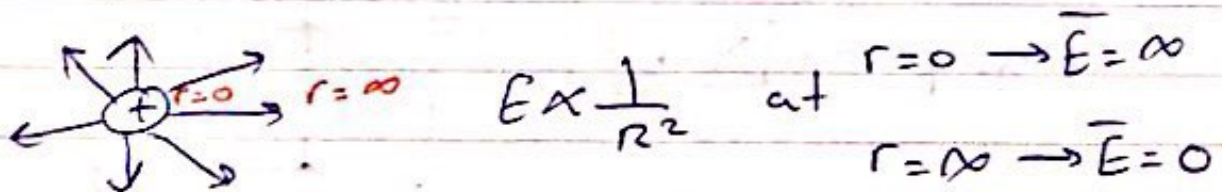
$$\rightarrow F = \frac{Q_1 Q_0 (\vec{r}_0 - \vec{r}_1)}{4\pi\epsilon_0 |\vec{r}_0 - \vec{r}_1|^3} + \frac{Q_0 Q_2 (\vec{r}_0 - \vec{r}_2)}{4\pi\epsilon_0 |\vec{r}_0 - \vec{r}_2|^3} + \dots + \frac{Q_0 Q_n (\vec{r}_0 - \vec{r}_n)}{4\pi\epsilon_0 |\vec{r}_0 - \vec{r}_n|^3}$$

$$\Rightarrow F = \frac{Q_0}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k (\vec{r}_0 - \vec{r}_k)}{|\vec{r}_0 - \vec{r}_k|^3}$$

\* Electric field Intensity :-

$$\vec{E} = \frac{\vec{F}}{Q_{\text{field}}} = \text{N/C or V/m}$$

→ Flux lines :-



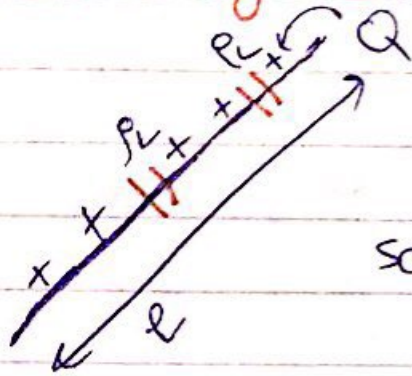
\* Example: point charges  $1\text{mC}$  and  $2\text{mC}$  located at  $(3, 2, -1)$  and  $(-1, -1, 4)$ . find  $\vec{F}$  and  $\vec{E}$  on a charge located at  $(0, 3, 1)$ .

$$F_1 = \frac{1 \times 10^{-3} \times 10 \times 10^{-9} (-3, 1, 2)}{4\pi \times \frac{10^{-9}}{36\pi} (16)^{\frac{3}{2}}} + F_2 \text{ field}$$

$\swarrow$   $S_1$  on field      $\nwarrow$  vector field

\* continuous charge distribution:

1) Line charge dist  $\rightarrow \rho_L$



$$Q = \int \rho_L dl$$

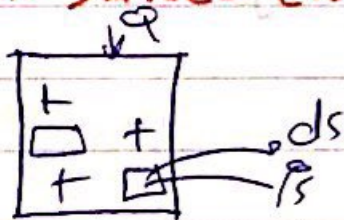
scalar                  scalar                  scalar

$$Q = \rho_L l$$

$$\rho_L = \frac{Q}{l}$$

$\rightarrow C/m$

2) Surface charge dist.



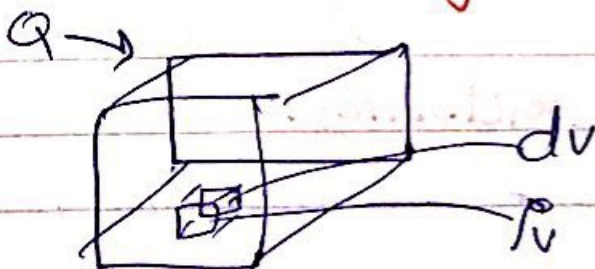
$$Q = \int \rho_s ds$$

$$Q = \rho_s S$$

$$\rho_s = \frac{Q}{S}$$

$\rightarrow C/m^2$

3) Volume charge dist.

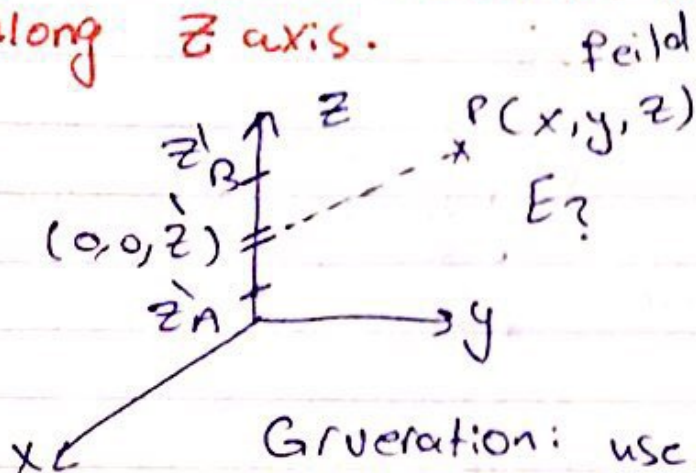


$$Q = \int \rho_v dv$$

$$\rho_v = \frac{Q}{\text{volume}}$$

$\rightarrow C/m^3$

E-field due to a finite line of charge along z axis.



Convention: use dashes to represent the source - and without dashes to represent the field.

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

$$\vec{E} = \int_l \frac{\rho_L dl}{4\pi\epsilon_0 r^2} \hat{a}_r \quad \rho = \sqrt{x^2 + y^2}$$

$$dl = dz$$

$$\vec{r} = x\hat{a}_x + y\hat{a}_y + (z - z')\hat{a}_z$$

$$r = \sqrt{x^2 + y^2 + (z - z')^2}$$

$$\vec{E} = \frac{\rho_L}{4\pi\epsilon_0} \int_{z_A}^{z_B} \frac{(x, y, z - z')}{[x^2 + y^2 + (z - z')^2]^{3/2}} dz$$

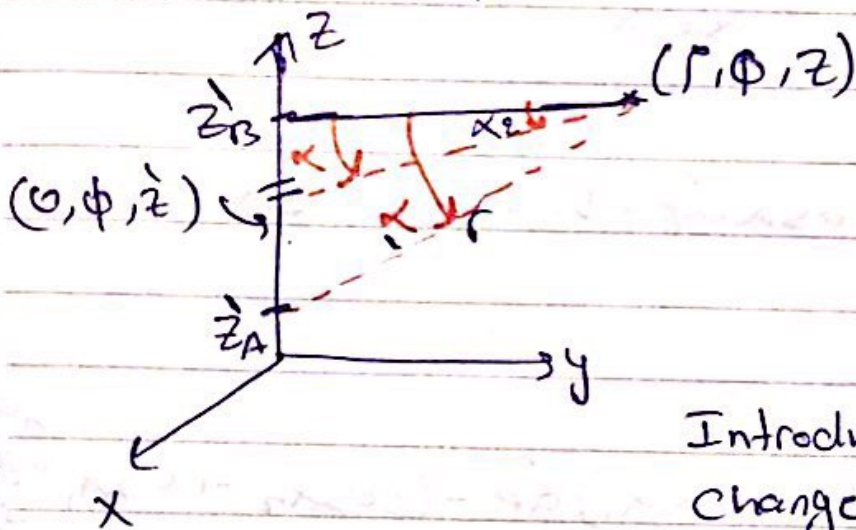
\* converting to cylindrical coordinates:

$$\vec{R} = \rho\hat{a}_\rho + (z - z')\hat{a}_z$$

$$r = R = \sqrt{\rho^2 + (z - z')^2}$$



$$\vec{E} = \frac{\rho_L}{4\pi} \int_{z_A}^{z_B} \frac{\rho \hat{a}_\rho + (z - z') \hat{a}_z}{[r^2 + (z - z')^2]^{\frac{3}{2}}} dz$$



Introduce angles  $\alpha, \alpha, \alpha$   
change from  $dz'$   $\rightarrow$   $d\alpha$

$$\sin \alpha = \frac{z - z'}{r}$$

$$\cos \alpha = \frac{\rho}{r}$$

$$\tan \alpha = \frac{z - z'}{\rho}$$

$$\Rightarrow z - z' = \rho \tan \alpha$$

$$-dz' = \rho \sec^2 \alpha d\alpha$$

$$\boxed{dz' = -\rho \sec^2 \alpha d\alpha}$$

$$\begin{aligned} r^2 &= \rho^2 + (z - z')^2 \\ &= \rho^2 + \rho^2 \tan^2 \alpha \\ &= \rho^2 \left( 1 + \frac{\sin^2 \alpha}{\cos^2 \alpha} \right) \end{aligned}$$

$$r = \rho \sec \alpha$$

$$r^3 = \rho^3 \sec^3 \alpha$$

$$* \rho = r \cos \alpha = \rho \sec \alpha \cos \alpha$$

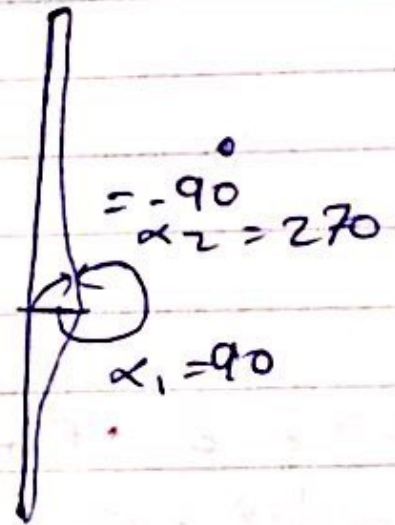
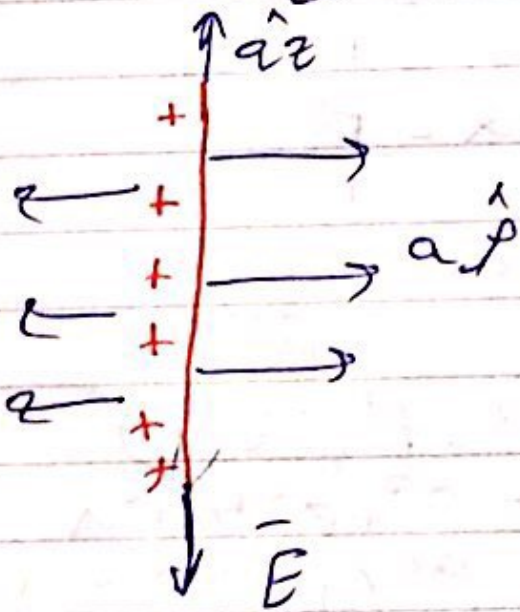
$$z - z' = r \sin \alpha = \rho \sec \alpha \sin \alpha$$

$\Rightarrow$

$$\vec{E} = \frac{\rho_L}{4\pi\epsilon_0} \int_{\alpha_1}^{\alpha_2} \frac{\rho \sec\alpha (\cos\alpha \hat{a}_\rho + \sin\alpha \hat{a}_z)}{\rho^3 \sec^3\alpha} (-\rho \sec^2\alpha) d\alpha$$

$$\vec{E} = -\frac{\rho_L}{4\pi\epsilon_0 \rho} \int_{\alpha_1}^{\alpha_2} (\cos\alpha \hat{a}_\rho + \sin\alpha \hat{a}_z) d\alpha$$

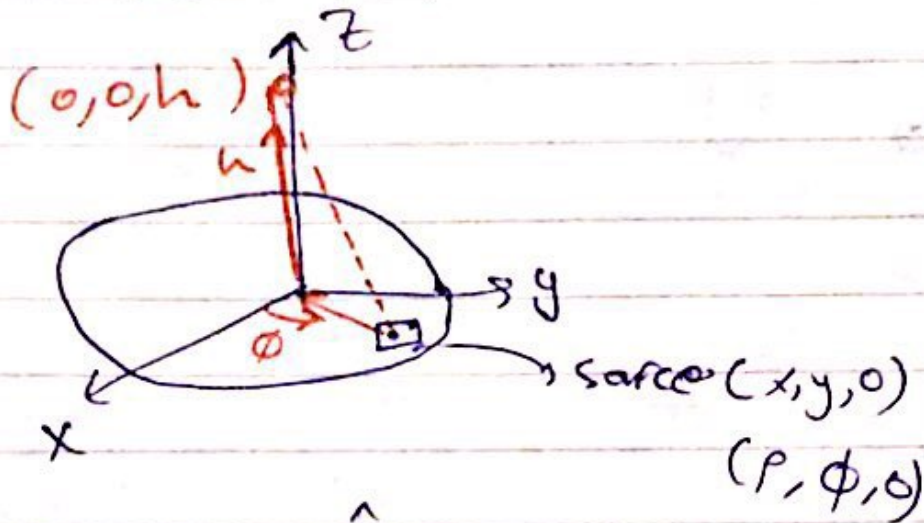
$$\Rightarrow -\frac{\rho_L}{4\pi\epsilon_0 \rho} \left[ (\sin\alpha_2 - \sin\alpha_1) \hat{a}_\rho - (\cos\alpha_2 - \cos\alpha_1) \hat{a}_z \right] \quad \text{V/m}$$



For Any inf. line

$$\vec{E} = \frac{\rho_L}{2\pi\epsilon_0 \rho} \hat{a}_\rho$$

Ex: for an inf. sheet of charge along xy plane.  
 Find  $\vec{E}$  at  $(0, 0, h)$  or  $(0, 0, -h)$ .



$$\vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r, \quad Q = \int_S \rho_s ds$$

$$\vec{E} = \int_S \frac{\rho_s ds \vec{r}}{4\pi\epsilon_0 r^2}$$

$$ds = dx dy \quad \text{carb.}$$

$$ds = \rho d\phi dz \quad \text{cyl.}$$

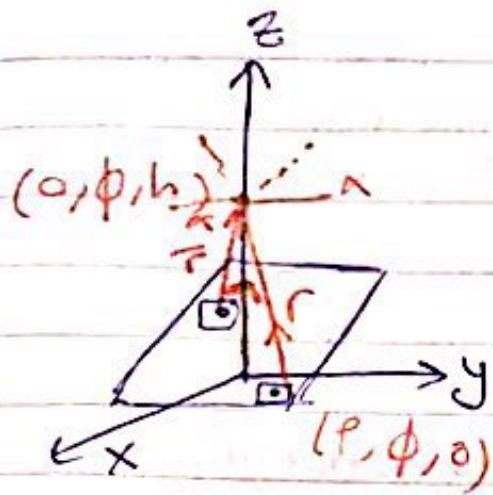
$$\vec{r} = -\rho a_\rho + h a_z$$

$$r = \sqrt{\rho^2 + h^2}$$

$$\vec{E} = \frac{\rho_s}{4\pi\epsilon_0} \int_0^{2\pi} \int_0^\infty \frac{-\rho a_\rho + h a_z}{[\rho^2 + h^2]^{3/2}} \rho d\rho d\phi$$

$\vec{E}$  - for inf. sheet along xy plane.





$$\vec{E} = \int_s \frac{\rho_s ds}{4\pi\epsilon_0 r^2} \hat{a}_r$$

$$\vec{r} = -\rho \hat{a}_\rho + h \hat{a}_z$$

$$r = \sqrt{\rho^2 + h^2}$$

$$ds = \rho d\rho d\phi$$

$$\vec{E} = \frac{\rho_s}{4\pi\epsilon_0} \int_0^{2\pi} \int_0^a \frac{(-\rho \hat{a}_\rho + h \hat{a}_z)}{[\rho^2 + h^2]^{\frac{3}{2}}} \rho d\rho d\phi$$

→ The  $\rho$ -component will be cancelled due to symmetry.

$$\vec{E} = \frac{\rho_s h}{2\epsilon_0} \int_0^{\infty} \frac{\rho d\rho}{\rho^2 + h^2}$$

let  $u = \rho^2 + h^2$   
 $du = 2\rho d\rho$   
 $\rho d\rho = \frac{du}{2}$

$$\vec{E} = \frac{\rho_s h}{2\epsilon_0} \int \frac{\frac{du}{2}}{u^{\frac{3}{2}}} \hat{a}_z$$

$$= \frac{-\rho_s h}{2\epsilon_0} \frac{1}{2} \frac{u^{-\frac{1}{2}}}{-\frac{1}{2}} \Big| \hat{a}_z$$

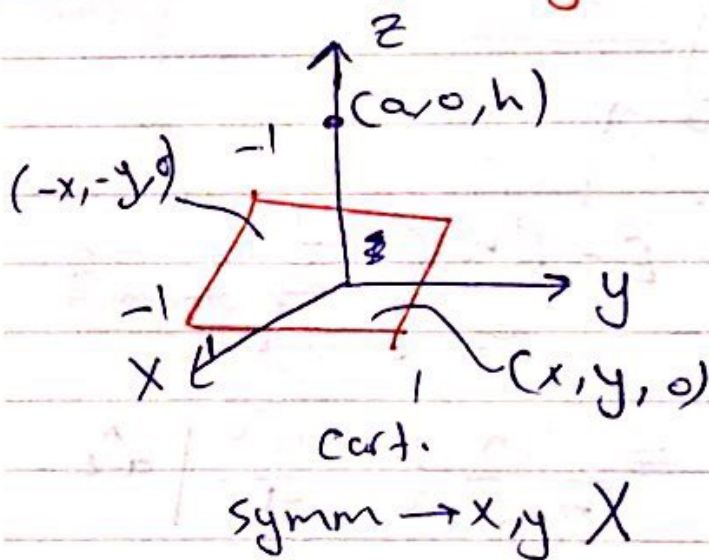
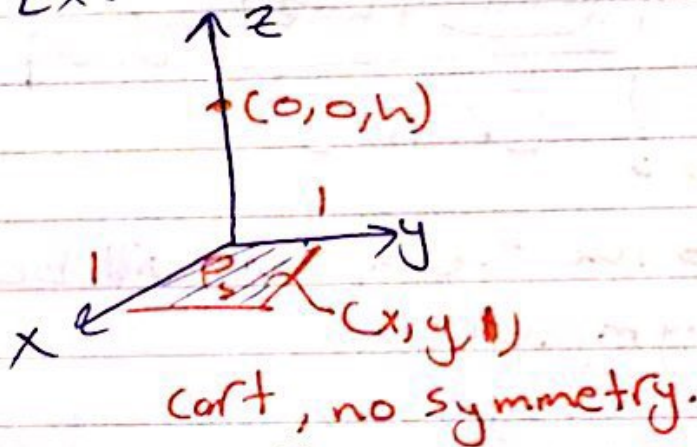
$$= \frac{-\rho_s h}{2\epsilon_0} \frac{1}{\sqrt{\rho^2 + h^2}} \Big|_0^{\infty} \hat{a}_z$$

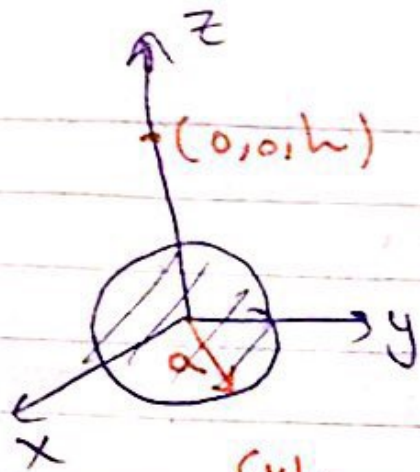
$$\bar{E} = -\frac{P_s h}{2\epsilon} \left[ 0 + \frac{1}{n} \right] \hat{a}_z$$

$$E = \frac{P_s}{2\epsilon} \hat{a}_z \quad v/h$$

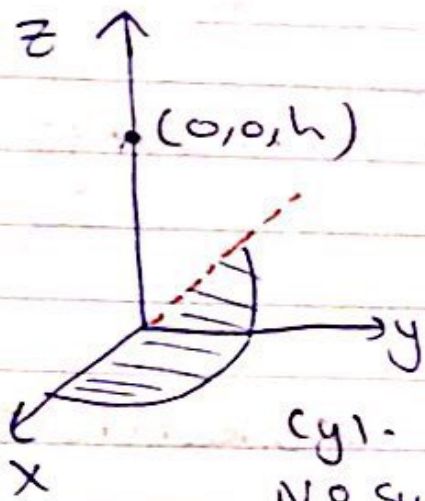
$$\bar{E} = \frac{P_s}{2\epsilon} \hat{a}_n \quad v/m \rightarrow \text{in general}$$

\* Ex.

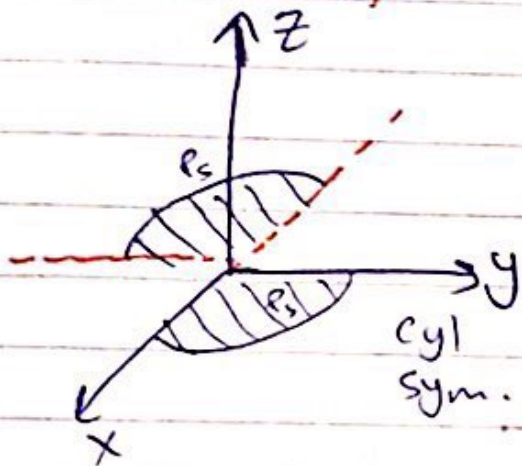




Cyl. Sym.

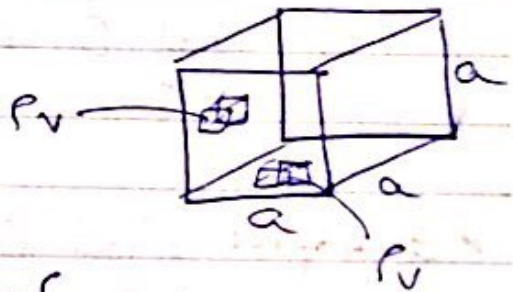


Cyl. No sym.



Cyl Sym.

E-field for a uniform volume.



$$Q = \int_V \rho_v dV$$

$$\Rightarrow \vec{E} = \int \frac{\rho_v dV}{4\pi\epsilon_0 r^2} \hat{r}$$

$$\vec{D} = \int \frac{\rho_v dV}{4\pi r^2} \hat{r}$$

\* Electric Flux Density ( $\vec{D}$ ):-

$$\vec{D} = \epsilon_0 \vec{E}$$

constitutive Relation

$$\vec{E} = \frac{\vec{D}}{\epsilon_0}$$

$$\frac{F}{m} \cdot \frac{V}{m} = \frac{C}{m^2}$$

- point charge  $\vec{E} = \frac{Q}{4\pi\epsilon \cdot r^2} \hat{a}_r$

$\vec{D} = \frac{Q}{4\pi r^2} \hat{a}_r$  (C/m<sup>2</sup>)

\* Electric flux (4)

or (4)  
\* scalar

$\Psi = \int_S \vec{D} \cdot d\vec{s} = Q$

or  $\Psi = \int_S \vec{E} \cdot d\vec{s} = \frac{Q}{\epsilon}$

field

\* Example: find  $\vec{D}$  at (4, 0, 3) if there is a point charge  $-5\pi$  mC at (4, 0, 0) and a line charge  $3\pi$  mC/m along y-axis

$\vec{D} = \vec{D}_Q + \vec{D}_P$

$\vec{D}_Q = \frac{Q\vec{r}}{4\pi r^3} = \frac{-5\pi \times 10^{-3} (3\hat{a}_z)}{4\pi (3)^3} = -0.138 \frac{\hat{a}_z}{\text{mC/m}^2}$

$\vec{D}_P = \frac{P_L}{2\pi P} \hat{a}_P = \frac{P_L \vec{P}}{2\pi P^2}$

$\vec{P} = (4, 0, 3) - (0, y, 0)$

↳ shortest distance (y=0)

$\vec{P} = (4, 0, 3)$

$P = 5$

$$\bar{P} = \frac{3\pi \times 10^{-3} (4, 0, 3)}{2\pi \times 25}$$

$$= 0.24 \hat{a}_x + 0.18 \hat{a}_z \text{ m/m}^2$$

$$\bar{D} = \bar{D}_q + \bar{P} = 240 \hat{a}_x + 42 \hat{a}_z \text{ N/C/m}^2$$

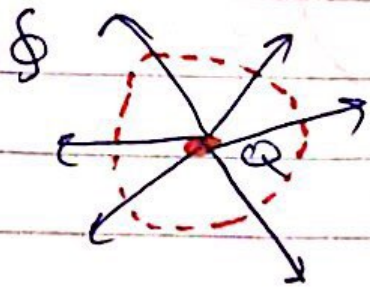
$$\bar{E} = \frac{\bar{D}}{\epsilon}$$



\* Gauss's law:-

$$\Phi = \oint \vec{D} \cdot d\vec{s} = Q_{\text{enclosed}} = Q$$

$\hookrightarrow \text{C/m}^2$



$$= \int_L \rho_L dL = \int_S \rho_S dS = \int_V \rho_V dV$$

$$\vec{D} = \frac{Q}{4\pi r^2} \hat{a}_r$$

$$S = 4\pi r^2$$

\* Electric flux (scalar)

$$\Phi = \oint \vec{D} \cdot d\vec{s}$$

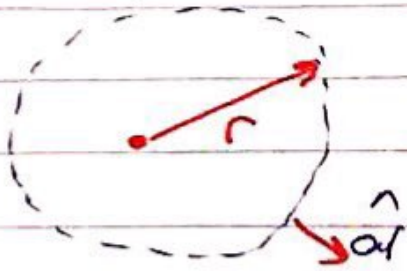
$$\oint \vec{D} \cdot d\vec{s} = \int_V \rho_V dV \Rightarrow \text{first Maxwell's eq. (in integral form).}$$

$$\nabla \cdot \vec{D} = \rho_V \Rightarrow \text{1st Maxwell's eq. int (differential form).}$$

## \* Application on Gauss's law:

① To find  $\vec{E}, \vec{P}$  due to a point charge.

$$\oint_S \vec{D} \cdot d\vec{s} = Q_{enc} = Q$$



$$\vec{D} = D r \hat{a}_r$$
$$d\vec{s} = r^2 \sin\theta d\theta d\phi \hat{a}_r$$

$$\int_0^{2\pi} \int_0^{2\pi} \sin\theta d\theta d\phi = 4\pi$$
$$\int_0^{2\pi} d\phi = 2\pi$$

$$\rightarrow D r (4\pi, 2) = Q$$

$$D = \frac{Q}{4\pi r^2}$$

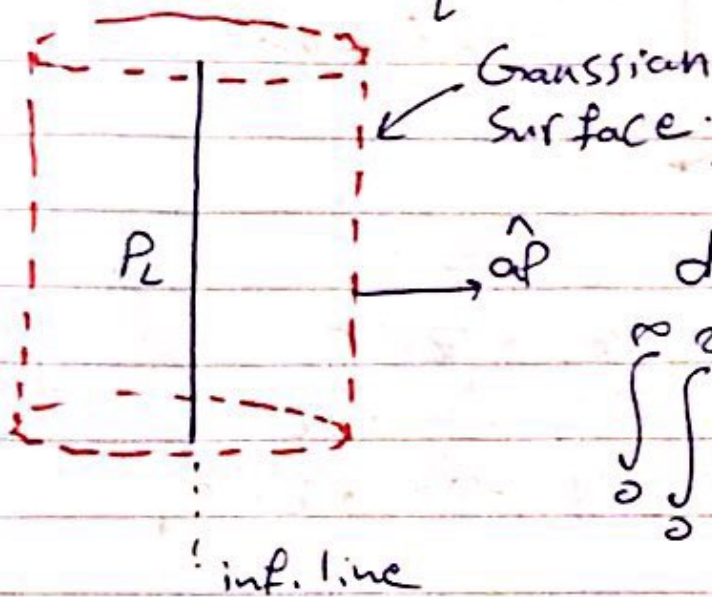
$$\vec{D} = \frac{Q}{4\pi r^2} r \hat{a}_r \text{ C/m}^2$$

$$\vec{E} = \frac{\vec{D}}{\epsilon_0}$$

$$\vec{E} = \frac{Q}{4\pi \epsilon_0 r^2} \hat{a}_r \text{ V/m}$$

\* 2) To find  $\vec{E}$  or  $\vec{D}$  due to an infinite line of charges.

$$\oint_S \vec{D} \cdot d\vec{s} = \int_L \rho_L dl$$



$$\vec{D} = \rho \rho \hat{a}_\rho$$

$$d\vec{s} = \rho d\phi dz \hat{a}_\rho$$

$$\int_0^\infty \int_0^{2\pi} \rho \rho \rho d\phi dz = \int_{-\infty}^\infty \rho_L dl$$

$$\int_{-L}^L \int_0^{2\pi} \rho \rho \rho d\phi dz = \int_{-L}^L \rho_L dl, \quad \boxed{L \rightarrow \infty}$$

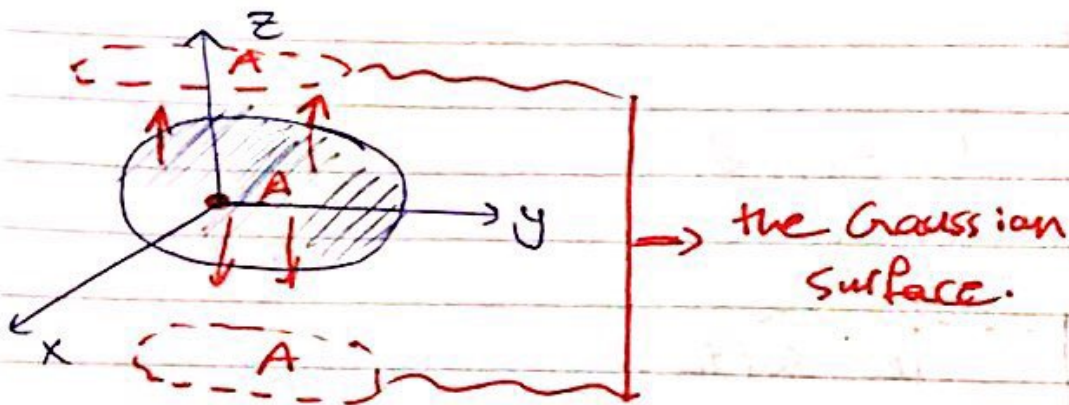
$$\rho \rho (2\pi) = \rho_L$$

$$\rho \rho = \frac{\rho_L}{2\pi \rho}$$

$$\vec{D} = \frac{\rho_L}{2\pi \rho} \hat{a}_\rho, \quad \vec{E} = \frac{\rho_L}{2\pi \epsilon_0 \rho} \hat{a}_\rho \text{ V/m}$$

$\text{C/m}^2$

3)  $\vec{E}$  or  $\vec{P}$  due to an inf. sheet.



$$\vec{D} = D_z(\hat{a}_z), \quad z > 0$$

$$D_z(-\hat{a}_z), \quad z < 0$$

$$d\vec{s}_{top} = \rho d\rho d\phi \hat{a}_z, \quad z > 0$$

$$d\vec{s}_{bot} = \rho d\rho d\phi (-\hat{a}_z), \quad z < 0$$

$$\int_{S_{top}} \vec{D} \cdot d\vec{s}_{top} + \int_{S_{bot}} \vec{D} \cdot d\vec{s}_{bot}$$

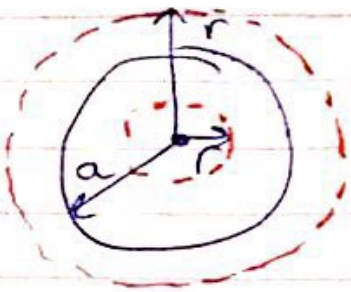
$$D_z A + D_z A = \rho_s A$$

$$D_z = \frac{\rho_s}{2}$$

$$\vec{D} = \frac{\rho_s}{2} \hat{a}_n \begin{cases} \hat{a}_z \\ -\hat{a}_z \end{cases}$$

$$\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{a}_n \quad \text{V/m}$$

4)  $\vec{E}$  or  $\vec{D}$  for a uniform volume charge dist. on a sphere of radius (a). (find  $\vec{E}$ ,  $\vec{P}$  everywhere)



for  $a < r < \infty$

$$\oint_S \vec{D} \cdot d\vec{s} = Q_{enc} = \int_V \rho_V dV$$

$$\vec{D} = D_r \hat{a}_r$$

$$\int_0^{2\pi} \int_0^\pi \int_0^r \rho_V r^2 \sin\theta d\theta d\phi dr = \int_0^{2\pi} \int_0^\pi \int_0^r \rho_V r^2 dr d\theta d\phi$$

$$D_r \cdot 4\pi r^2 = \rho_V \cdot 4\pi r^3$$

$$D_r = \frac{\rho_V r}{3} = \frac{\rho_V r a^3}{3} \text{ C/m}^2$$

$$\vec{E} = \frac{\rho_V r}{3\epsilon_0} \hat{a}_r$$

for  $a < r < \infty$

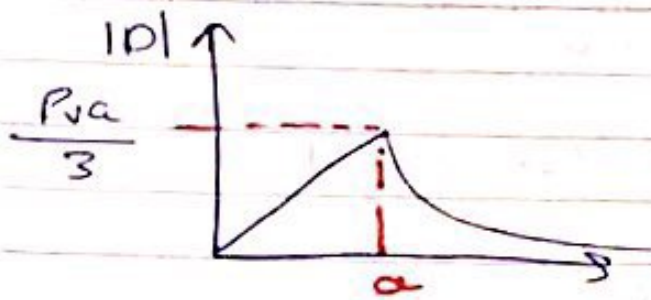
$$4\pi r^2 D_r = \int_0^{2\pi} \int_0^\pi \int_0^a \rho_V r^2 \sin\theta dr d\theta d\phi$$

$$+ \int_0^{2\pi} \int_0^\pi \int_0^r \rho_V r^2 \sin\theta dr d\theta d\phi$$

$$4\pi r^2 D_r = \rho_V \cdot 4\pi a^3$$

$$\vec{D} = \frac{\rho_V a^3}{3r^2} \hat{a}_r, a < r$$

$$\vec{E} = \frac{\rho_V a^3}{3\epsilon_0 r^2} \hat{a}_r, a < r$$



\* example: given  $\vec{D} = z P \cos^2 \phi \hat{a}_z \text{ C/m}^2$ ,  
 - calculate: a) The charge density at  $(1, \frac{\pi}{4}, 3)$   
 b) the total charge enclosed by the cylinder of radius 1m and  $-2 \leq z \leq 2$ m

Sol.

a)  $P_v \times$

$$P_s = \vec{D} \cdot \hat{a}_n$$

$$\checkmark P_v = \nabla \cdot \vec{D}$$

$$P_v = \nabla \cdot \vec{D} = \frac{\partial}{\partial z} D_z \Rightarrow P_v = P \cos^2 \phi \text{ C/m}^3$$

$$P_v \Big|_{(1, \frac{\pi}{4}, 3)} = 0.5 \text{ C/m}^3$$

$$b) Q = \int_V P_v dV$$

$$Q = \oint_S P_s dS = \oint_S \vec{D} \cdot \vec{dS}$$

$$= \int_V \nabla \cdot \vec{D} dV$$



$$Q = \int_V \rho_V dV$$

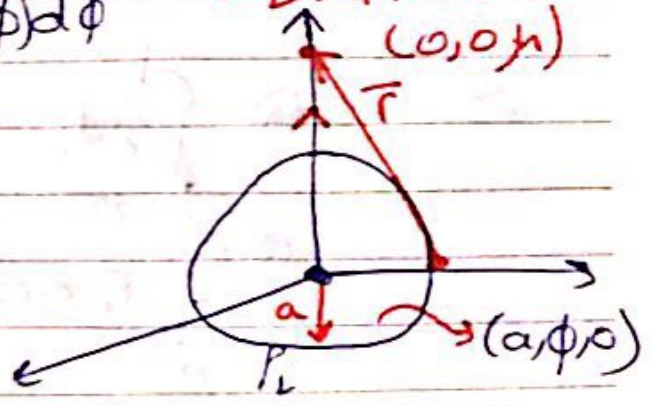
$$\rightarrow b) \quad Q = \int_{-2}^2 \int_0^{2\pi} \int_0^{2\pi} \rho \cos^2 \phi \rho d\rho d\phi dz$$

$$\left(\frac{1}{3}\right) (2-(-2)) \int_0^{2\pi} \cos^2 \phi d\phi$$

$$\Rightarrow \frac{4}{3} \int_0^{2\pi} \frac{1}{2} (1 + \cos 2\phi) d\phi$$

$$= \frac{4}{3} \pi C$$

\* Example (2)  
(0, 0, h)



a) Find  $\vec{E}$  at (0, 0, h)?

$$\vec{E} = \int_L \frac{\rho_L dL}{4\pi\epsilon_0} \vec{a}_r = \int \frac{\rho_L dL}{4\pi\epsilon_0 r^2} \cdot \frac{\vec{r}}{r}$$

~~①  $dL = \rho_L d\phi$~~

①  $dL = \rho_L d\phi = a d\phi$     ②  $\vec{r} = -a \hat{\phi} + h \hat{z}$   
 $r = \sqrt{a^2 + h^2}$

③  $\vec{E} = \frac{\rho_L}{4\pi\epsilon_0} \int_0^{2\pi} \frac{-a \hat{\phi} + h \hat{z}}{(a^2 + h^2)^{3/2}}$

$$\Rightarrow \vec{E} = \frac{\rho_L \cdot h \cdot a}{4\pi\epsilon_0 \cdot (a^2 + h^2)^{3/2}} \int_0^{2\pi} d\phi = 2\pi$$

$$\vec{E} = \frac{\rho_L h a}{2\epsilon_0 \cdot (a^2 + h^2)^{3/2}} \hat{z} \quad \text{V/m}$$



b) proof: if  $a \rightarrow 0$  then the  $\vec{E}$ -field will be as a point charge

\* 
$$E = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

Sol.  $Q = \int P_L dL$

$$Q = \int_0^{2\pi} P_L a d\phi$$

$$Q = 2\pi a P_L$$

$$P_L = \frac{Q}{2\pi a}$$

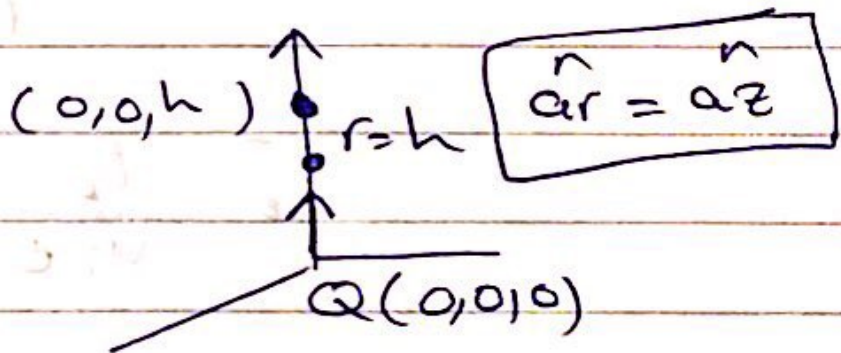
$$E = \frac{Q}{2\pi a} \frac{ha}{2\epsilon_0 (a^2+h^2)^{3/2}}$$

$$\vec{E} = \frac{Q}{4\pi\epsilon_0 h^2} \hat{a}_z$$



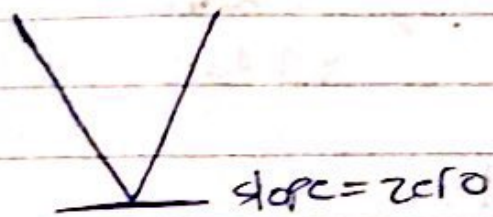
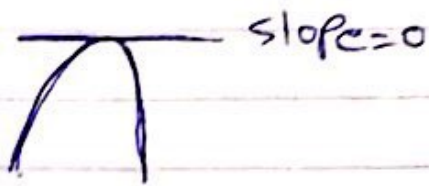
\* 
$$= \frac{Q}{4\pi\epsilon_0} \hat{a}_r$$

because  $r^2 = h^2$





c) determine the value of (h) to have max(E)



$$\frac{dE}{dh} = 0$$

$$\frac{d \cdot \frac{\rho_L h a a^2}{2E \cdot (a^2 + h^2)^{\frac{3}{2}}}}{dh} = \boxed{2c\sigma}$$

$$\frac{\rho_L a}{2E} \left( \frac{(a^2 + h^2)^{\frac{3}{2}} (1) - (h) (3) (a^2 + h^2)^{\frac{1}{2}} \times (2h)}{(a^2 + h^2)^3} \right)$$

$$\Rightarrow (a^2 + h^2)^{\frac{3}{2}} - 3h^2 (a^2 + h^2)^{\frac{1}{2}} = 0$$

$$(a^2 + h^2)^{\frac{1}{2}} (a^2 + h^2 - 3h^2) = 0$$

$$\downarrow$$

$\neq 0$

$$\downarrow$$
$$a^2 - 2h^2 = 0$$

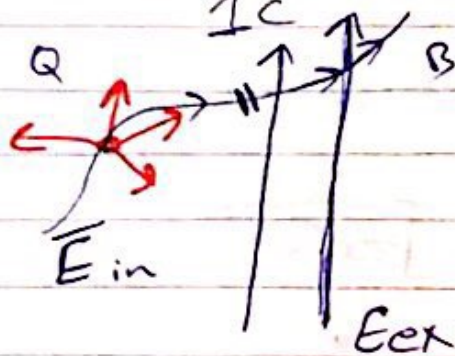
$$\hookrightarrow \boxed{h = \frac{+a}{\sqrt{2}} \text{ m}}$$

\* Electric potential:

(V)  $\rightarrow$  scalar

$$\text{Vol tage} = \frac{\text{work}}{\text{charge}}$$

$$1V = \frac{1J}{1C}$$



the work is done.

$$W = \vec{F} \cdot \vec{l} \text{ by } \vec{E}_{\text{ext}}$$

$$= - \int \vec{F} \cdot d\vec{l}, \vec{F} = Q\vec{E}$$

$$W = -Q \int \vec{E} \cdot d\vec{l}$$

$$V_{AB} = \frac{W}{Q} = - \int \vec{E} \cdot d\vec{l}$$

$$= V_B - V_A$$

\* if  $V_{AB}$  is +ve  $\rightarrow$  gain in potential

$$\int \vec{E} \cdot d\vec{l} \text{ is } -ve$$

The work is done by  $E_{\text{ext}}$ .

\* if  $V_{AB}$  is -ve  $\rightarrow$  drop in potential

$$\int \vec{E} \cdot d\vec{l} \text{ is +ve.}$$

$\rightarrow$  The work is done by the field itself.

\* V for a point charge:

$$V = - \int \vec{E} \cdot d\vec{l}, \quad \vec{E} = \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r$$

$d\vec{l} = dr \hat{a}_r$

$$V_{AB} = - \int_{r_A}^{r_B} \frac{Q}{4\pi\epsilon_0 r^2} dr$$

$$V_{AB} = \frac{Q}{4\pi\epsilon_0 r} \Big|_{r_A}^{r_B} = \frac{Q}{4\pi\epsilon_0 r_B} - \frac{Q}{4\pi\epsilon_0 r_A}$$

$\downarrow \qquad \qquad \downarrow$   
 $- V_B \qquad - V_A$

$$V = \frac{Q}{4\pi\epsilon_0 r} \text{ (V)}$$

\* for line charge  $\Rightarrow V = \int \frac{\rho_L dl}{4\pi\epsilon_0 r}$

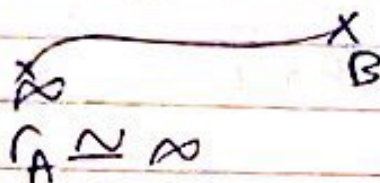
\* for surface charge  $\Rightarrow V = \int \frac{\rho_S ds}{4\pi\epsilon_0 r}$

\* for volume charge  $\Rightarrow V = \int_V \frac{\rho_v \, dv}{4\pi\epsilon_0 r}$

\* for point charges:

$$V = \frac{1}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k}{|\mathbf{r} - \mathbf{r}_k|} \quad (V)$$

- Assume point  $a$  is at  $\infty$



$$\begin{aligned} V_{AB} &= V_B - V_A \\ &= \frac{Q}{4\pi\epsilon_0 r_B} - \frac{Q}{4\pi\epsilon_0 r_A} \\ &= \frac{Q}{4\pi\epsilon_0 r_B} = V_B \end{aligned}$$

\* Example: Two point charges  $-4\mu\text{C}$  and  $5\mu\text{C}$  are located at  $(2, -1, 2)$  and  $(0, 4, -2)$

Find the potential at  $A(1, 0, 1)$

ref.  $\rightarrow V_\infty = 0$

$$* V_A = \frac{-4 \times 10^{-6}}{4\pi \times 10^{-9} \times \sqrt{(-1)^2 + 1^2 + (-2)^2}}$$

$$\oplus \frac{5 \times 10^{-6}}{4\pi \frac{10^{-9}}{36\pi} \sqrt{(1-4)^2 + 3^2}} \leftarrow \sqrt{26}$$

$$\Rightarrow V_A - V_{\infty} = V_A - \text{zero} = V_A$$

$$V_A = -5.872 \text{ kV}$$

\*Example: A point charge of  $5 \text{ nC}$  located at  $(-3, 4, 0)$  and a line  $y=1$ ,  $z=1$  carries a uniform charge of  $2 \text{ nC/m}$

b) If  $V = 100 \text{ V}$  at  $B(1, 2, 1)$  find  $V$  at  $C(-2, 5, 3)$ .

← field

← field & ref.

ref is point B

$$V_{BC} = V_C - V_B$$

$$V_C = V_{BC} + V_B$$

$$V_{AB} = V_B - V_A$$

$$V_{AB} - V_{AOA}$$

$$V_B - V_{AO} - V_A + V_{AO}$$

$$= V_B - V_A$$

$$V_{BC} = V_{BCQ} + V_{BCl}$$

$$V_{BCQ} = - \int_P \vec{E} \cdot d\vec{u} = - \int_{r_B}^{r_C} \frac{Q}{4\pi\epsilon_0 r^2} \hat{a}_r \cdot dr \hat{a}_r$$

$$= \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_C} - \frac{1}{r_B} \right)$$

$$r_C = |(-2, 5, 3) - (-3, 4, 0)| = |(1, 1, 3)| = \sqrt{11}$$

$$r_B = |(1, 2, 1) - (-3, 4, 0)| = |(4, -2, 1)| = \sqrt{21}$$

$$V_{BCD} = \int \frac{P_L dl}{4\pi\epsilon \cdot r} \times$$

$$V_{BCD} = - \int \vec{E} \cdot d\vec{l}$$

$$= - \int_{r_B}^{r_C} \frac{P_L}{2\pi\epsilon \cdot r} \hat{a}_r \cdot d\vec{r} \hat{a}_r \dots$$

$$= \frac{-P_L}{2\pi\epsilon} (\ln r_C - \ln r_B)$$

$$\frac{-P_L}{2\pi\epsilon} \ln\left(\frac{r_C}{r_B}\right)$$

$$r_C = |(-2, 5, 3) - (-2, 1, 1)| = |(0, 4, 2)| = \sqrt{20}$$

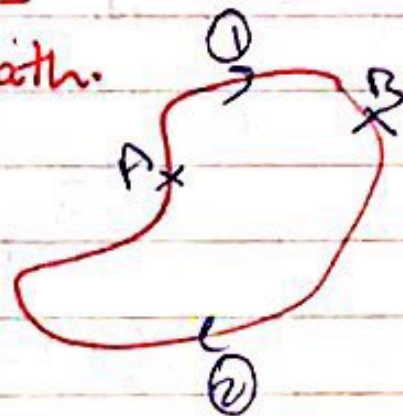
$$r_B = |(1, 2, 1) - (1, 1, 1)| = |(0, 1, 0)| = 1$$

$$V_{BC} = -50 \cdot 175 \text{ V}$$

$$V_C = 49.825 \text{ V} < V_B = 100 \text{ V}$$

\* Relation between  $\vec{E}$  and  $V$  :-

→ voltage over a closed path.



$$V = \oint \vec{E} \cdot d\vec{l}$$

$$= - \int_{r_A}^{r_B} \vec{E} \cdot d\vec{l} + \int_{r_B}^{r_A} \vec{E} \cdot d\vec{l}$$

$$= - \int_{r_A}^{r_B} \vec{E} \cdot d\vec{l} + \int_{r_A}^{r_B} \vec{E} \cdot d\vec{l} = 0$$

$$\oint_C \vec{E} \cdot d\vec{L} = 0 \implies \text{equi-potential surface.}$$

$\nabla = 0$  (2<sup>nd</sup> Maxwell's eq.)  
in integral form.

$$\boxed{\nabla \times \vec{E} = 0} \rightarrow \text{2nd Maxwell's eq. (in a diff form).}$$

$$\oint_C \vec{E} \cdot d\vec{L} = 0 \Rightarrow \text{equi-potential surface.}$$

$$V=0$$

(2<sup>nd</sup> Maxwell's eq.)  
in integral form.

$$\nabla \times \vec{E} = 0$$

→ 2<sup>nd</sup> Maxwell's eq.  
(in a diff form).

$\vec{E}$  is irrotational

$$\nabla \cdot \vec{D} = \rho_v \Rightarrow \nabla \cdot \epsilon_0 \vec{E} = \rho_v$$

$$\nabla \cdot \vec{E} = \frac{\rho_v}{\epsilon_0} \neq 0$$

(\*) To find  $\vec{E}$  from  $V$

$$V = - \int_C \vec{E} \cdot d\vec{L} \Rightarrow dV = -\vec{E} \cdot d\vec{L}$$

in Cart:  $\vec{E} = E_x dx + E_y dy + E_z dz$

$$d\vec{L} = dx \hat{a}_x + dy \hat{a}_y + dz \hat{a}_z$$

$$\vec{E} \cdot d\vec{L} = E_x dx + E_y dy + E_z dz$$

$$dV = \frac{\partial V}{\partial x} dx + \frac{\partial V}{\partial y} dy + \frac{\partial V}{\partial z} dz$$

- equating the x-component.

$$\frac{\partial V}{\partial x} dx = -E_x dx$$

$$E_x = -\frac{\partial V}{\partial x}$$

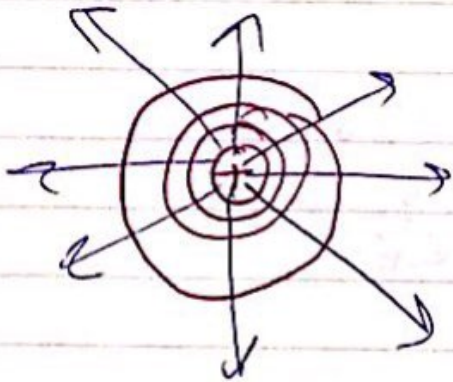


→ equating the y-component:

$$\frac{\partial V}{\partial y} dy = -E_y dy \rightarrow E_y = -\frac{\partial V}{\partial y}$$

→ equating the z-component:

$$\frac{\partial V}{\partial z} dz = -E_z dz \rightarrow E_z = -\frac{\partial V}{\partial z}$$



So :-

$$\vec{E} = -\frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z$$

$$\boxed{\vec{E} = -\nabla V} \rightarrow \text{gradient}$$

$\nabla \times \vec{E} = \text{zero} \rightarrow E$  is irrotational

$\nabla \times (-\nabla V) = \text{zero} \rightarrow \text{Always}$

\* Example: Given  $V = 10 \sin\theta \cos\phi$

Find: a)  $\vec{D}$  at  $(2, \frac{\pi}{2}, 0) r^2$

b) Calculate the work done in moving a 10nC charge from A  $(1, 30^\circ, 120^\circ)$  to B  $(4, 90^\circ, 60^\circ)$

Sol →  
next

$$\vec{E} = -\nabla V \rightarrow \vec{D} = \epsilon \cdot \vec{E}$$

$$\vec{D} = \epsilon \cdot \nabla V$$

$$\vec{E} = \left( \frac{\partial V}{\partial r} \hat{a}_r + \frac{\partial V}{r \partial \theta} \hat{a}_\theta + \frac{\partial V}{r \sin \theta \partial \phi} \hat{a}_\phi \right)$$

$$\vec{E} = \left( \frac{20 \sin \theta}{r^3} (\cos \phi \hat{a}_r - \frac{10}{r^3} \cos \theta \cos \phi \hat{a}_\phi + \frac{10}{r^3} \sin \phi \hat{a}_\phi) \right)$$

$$\vec{D} = \epsilon \cdot \vec{E} = \epsilon \cdot \left( \frac{20}{9} \hat{a}_r \right) = 22.1 \hat{a}_r \text{ C/m}^2$$

(2,  $\frac{\pi}{2}$ , 0)

b)  $W = Q V_{AB}$   
 $= Q (V_B - V_A)$   
 $= 10 \times 10^{-6} \left( \left( \frac{10}{10} * \frac{1}{2} \right) - \left( 10 * \frac{1}{2} * -\frac{1}{2} \right) \right)$

$$= 10 \times 10^{-6} \left( \frac{10}{5} + \frac{5}{2} \right) = 28.125 \text{ MJ}$$

Method 2.

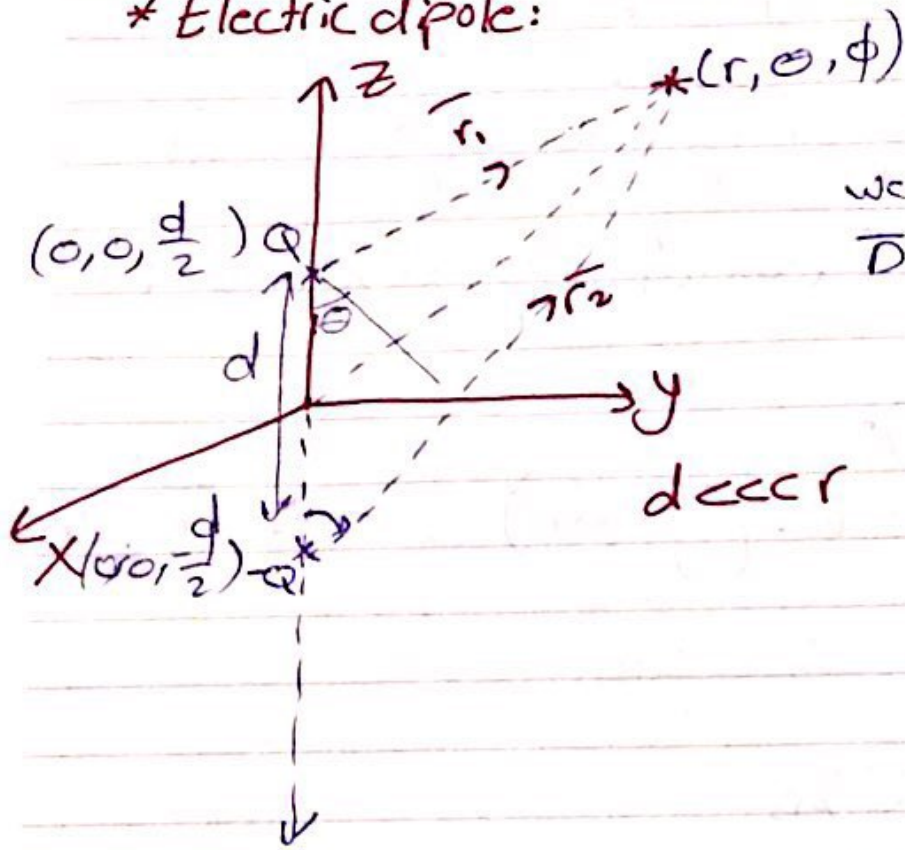
$$W = -Q \int_{r_A}^{r_B} \vec{E} \cdot d\vec{L}$$

$$W = -Q \int_{r_A}^{r_B} (E_r dr + r E_\theta d\theta + r \sin \theta E_\phi d\phi) \Big|_{\theta=30^\circ}^{\theta=60^\circ}$$

$$W = -Q \left[ \int_{r_A}^{r_B} E_r dr \Big|_{\theta=30^\circ}^{\theta=60^\circ} + \int_{30^\circ}^{90^\circ} r E_\theta d\theta \Big|_{\phi=120^\circ}^{\phi=120^\circ} + \int_{120^\circ}^{90^\circ} r \sin \theta E_\phi d\phi \Big|_{r=4}^{r=4} \right]$$

$$= 28.125 \text{ MJ}$$

\* Electric dipole:



we need to find  $\vec{D}$ ,  $\vec{E}$  &  $V$ .

$$V = V_+ \oplus V_-$$

$$= \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{r_1} - \frac{1}{r_2} \right)$$

$$V = \frac{Q(r_2 - r_1)}{4\pi\epsilon_0 \cdot r_1 r_2} \text{ volt} \Rightarrow \textcircled{1}$$

$Q, d$  is not given

to simplify the equation

$$\cos\theta = \frac{r_2 - r_1}{d} \Rightarrow d \cos\theta = r_2 - r_1$$

$$\Rightarrow r_1 r_2 \approx r^2$$

$$V = \frac{Qd \cos\theta}{4\pi\epsilon_0 \cdot r^2} \text{ volt} \Rightarrow \textcircled{2}$$

define the dipole moment  $\vec{p}$  ( $\vec{P}$ ):

$$p = qd \quad \text{in (C.m)}$$

$$V = \frac{p \cos \theta}{4\pi\epsilon_0 r^2} \Rightarrow \textcircled{3}$$
$$p \cos \theta = p \cdot \hat{a}_r =$$

$$V = \frac{\vec{P} \cdot \hat{a}_r}{4\pi\epsilon_0 r^2} \quad \text{volt}$$

→ for point charge:  $V \propto \frac{1}{r}$ ,  $E \propto \frac{1}{r^2}$

→ for two point charge dipole:  $V \propto \frac{1}{r^2}$ ,  $E \propto \frac{1}{r^3}$

$$E = \vec{E}_- \oplus \vec{E}_+ \quad \text{or} \quad \vec{E} = -\nabla V$$

$$\vec{E} = - \left( \frac{\partial V}{\partial r} \hat{a}_r + \frac{\partial V}{r \partial \theta} \hat{a}_\theta + \frac{\partial V}{r \sin \theta \partial \phi} \hat{a}_\phi \dots \right)$$

$$\vec{E} = -\frac{p}{4\pi\epsilon_0 r^3} \left( -\frac{2}{r^3} \cos \theta \hat{a}_r + \frac{\sin \theta}{r^3} \hat{a}_\theta \right)$$

$$= \frac{p}{4\pi\epsilon_0 r^3} (2 \cos \theta \hat{a}_r + \sin \theta \hat{a}_\theta)$$

$$\vec{D} = \vec{E} \cdot \epsilon$$

\* Example: Two dipoles with dipole moments  $-5a\hat{z}$  nC.m and  $9a\hat{z}$  nC.m are located at  $(0,0,-2)$  and  $(0,0,3)$  find  $V$  and  $\vec{E}$  at the origin.

$$V = V_1 + V_2$$

$$= \frac{P_1 \cdot \vec{r}_1}{4\pi\epsilon_0 \cdot r_1^3} + \frac{P_2 \cdot \vec{r}_2}{4\pi\epsilon_0 \cdot r_2^3}$$

$$= -20 \cdot 25V$$

$$\vec{r}_1 = (0,0,0) - (0,0,-2) = 2a\hat{z}$$

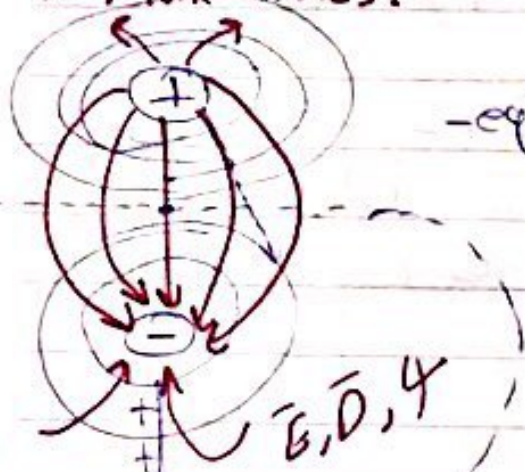
$$\vec{r}_2 = (0,0,0) - (0,0,3) = -3a\hat{z}$$

$$r_1 = 2m, r_2 = 3m$$

\* ref is  $\infty$

$$V_{\infty} = V_0 - V_0 = V_0 - \text{zero} = V_{\text{origin}}$$

\* Flux lines:



- equi-potential surface (in blue)

$\Rightarrow$  Loci for all equi-potential surface.

~~\* Energy Density in Electrostatic Fields:~~

$\vec{E} = \vec{E}_1 + \vec{E}_2$  ,  $\vec{E} = -\nabla V$

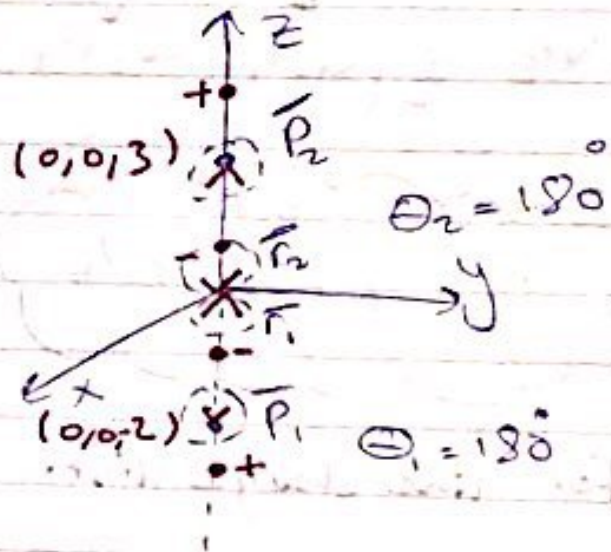
$\vec{E}_1 = \frac{(\vec{P}_1)}{4\pi\epsilon_0 \cdot (r_1)^3} (2\cos\theta_1 \hat{r}_1 + \sin\theta_1 \hat{a}_\theta)$

$P_1 = 5 \text{ nC}\cdot\text{m}$

$P_2 = 9 \text{ nC}\cdot\text{m}$

$r_1 = 2 \text{ m}$

$r_2 = 3 \text{ m}$



\* Energy density in Electrostatic Fields:-

space



$\textcircled{*} W = Q V_{\text{diff}}$

$Q_1 \rightarrow Q_2 \rightarrow Q_3$

electrical energy  $\rightarrow W_E = W_1 + W_2 + W_3$

$= 0 + Q_2 V_{12} + Q_3 (V_{13} + V_{23})$   $\textcircled{1}$

if  $Q_3 \rightarrow Q_2 \rightarrow Q_1$

$$W_E = W_1 + W_2 + W_3$$

$$= Q_1(V_{31} + V_{21}) + Q_2(V_{32}) + 0 \rightarrow (2)$$

$$2W_E = Q_1(V_{31} + V_{21}) + Q_2(V_{12} + V_{32}) + Q_3(V_{13} + V_{23})$$

$$W_E = \frac{1}{2} (Q_1 V_1 + Q_2 V_2 + Q_3 V_3)$$

$$\textcircled{*} \quad W_E = \frac{1}{2} \sum_{k=1}^N Q_k V_k \quad (\text{J})$$

- for line charge dist.

$$W_E = \frac{1}{2} \int P_L v dl$$

- for surface charge

$$W_E = \frac{1}{2} \int_S P_s v ds$$

- for volume charge.

$$W_E = \frac{1}{2} \int_V P_v v dv$$

\* How to relate  $W_E$  with  $\bar{E}$ .

$$W_E = \frac{1}{2} \int_V \rho_v v dv$$

$$\nabla \cdot \bar{D} = \rho_v, \bar{D} = \epsilon \cdot \bar{E}$$

$$W_E = \frac{1}{2} \int_V (\nabla \cdot \bar{D}) v dv$$

- in general:  $\nabla \cdot (v \bar{D}) = v(\nabla \cdot \bar{D}) + \bar{D} \cdot \nabla v$

$$W_E = \frac{1}{2} \int_V [\nabla \cdot (v \bar{D}) - \bar{D} \cdot \nabla v] dv$$

- Apply divergence theorem in (1).

$$W_E = \frac{1}{2} \oint_S v \bar{D} \cdot \bar{D} s - \frac{1}{2} \int_V \bar{D} \cdot \nabla v dv$$

$$E = -\nabla v$$

$$\begin{aligned} N &\propto \frac{1}{r} \\ \bar{D} &\propto \frac{1}{r^2} \\ v \bar{D} &\propto \frac{1}{r^3} \\ ds &\propto r^2 \end{aligned}$$

$$\propto \frac{1}{r}$$

$$W_E = \frac{1}{2} \int_V \bar{D} \cdot \bar{E} dv \quad (J)$$

$$W_E = \frac{1}{2} \int_V \epsilon \cdot E^2 dv \quad (J)$$

$$W_E = \frac{1}{2} \int_V \frac{D^2}{\epsilon} dv \quad (J)$$



$$w_E = \frac{W_E}{\text{Volume}}$$

$$\begin{aligned}
 w_E &= \frac{1}{2} \cdot \vec{D} \cdot \vec{E} \\
 &= \frac{1}{2} \epsilon_0 \cdot E^2 \\
 &= \frac{1}{2} \frac{D^2}{\epsilon_0}
 \end{aligned}
 \rightarrow \text{J/m}^3$$
  

$$W_E = \int_V w_E dV \rightarrow (\text{J})$$

$\downarrow$   $\text{J/m}^3$       $\downarrow$   $\text{m}^3$

\*example: The point charge  $-1 \text{ nC}$ ,  $4 \text{ nC}$  and  $3 \text{ nC}$  are located  $(0,0,0)$ ,  $(0,0,1)$  and  $(1,0,0)$ . find the energy in the system

$$W_E = \frac{1}{2} \sum_{k=1}^N Q_k V_k, \text{ or } W_E = \frac{1}{2} \int \epsilon_0 E^2 dV$$

$$N=3$$

$$W_E = \frac{1}{2} (Q_1 V_1 + Q_2 V_2 + Q_3 V_3)$$

$$\Rightarrow \frac{1}{2} \left[ Q_1 \left( \frac{Q_2}{4\pi\epsilon_0 \cdot (1)} + \frac{Q_3}{4\pi\epsilon_0 \cdot (1)} \right) + \frac{Q_2 (Q_1 + Q_3)}{4\pi\epsilon_0 \cdot (1)} \right]$$

$$+ \frac{Q_3 (Q_1 + Q_2)}{4\pi\epsilon_0 \cdot (1)} \Big] = 13.37 \text{ nJ}$$

## Chapter 5 :- Electric fields in Materials.

\* Types of materials based on its electrical properties

- ↳ conductors (metals),  $\sigma \gg \gg 1$   $\sigma \approx 10^8 \text{ S/m}$
- ↳ semi-conductor  $\sigma > 1$
- ↳ Dielectrics (Insulators)  $0 < \sigma \ll \ll 1$

$\sigma$  = conductivity S/m or  $(\Omega \cdot m)^{-1}$ , V/m

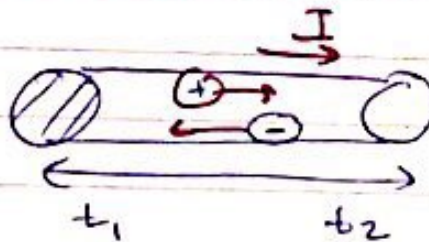
$\rho = \frac{1}{\sigma}$   $\rightarrow$  resistivity ( $\Omega \cdot m$ )

$\sigma$  depends mainly on:  $\sim$  temperature  $\sim$  frequency  
(CH 10)

\* types of currents:

- 1) conduction current
- 2) convection current.
- 3) displacement current.  $\Rightarrow$  CH 9

$$* I = \frac{dQ}{dt}$$



define the current density ( $\vec{J}$ ) in  $A/m^2$

$$dI = J dS = \int dI = \int J dS \Rightarrow I = \int_S \vec{J} \cdot d\vec{s}$$

$$* \bar{I} = \frac{DQ}{Dt}, \quad Q = \int_V \rho dv \quad DQ = \rho v DV$$

$$DQ = \rho v DV = \rho v \Delta x \Delta y \Delta z$$

$$\bar{I} = \rho v \Delta x \Delta y \Delta z \quad A$$

\* How to relate  $\bar{J}$  with  $\bar{E}$ ?

$$F = Q E_{\text{ext}} \Rightarrow \text{the force on one electron}$$

$$\bar{F} = -e \bar{E} = m \bar{u} = m \frac{\bar{u}}{\tau} \quad Q = -e$$

\*  $\tau$ : time between collisions and its constant at constant temperature.

$$(\tau \uparrow, T \uparrow) \quad \tau \uparrow T \downarrow$$

$$\bar{u} = \left( \frac{-e\tau}{m} \right) \bar{E}, \quad \bar{u} = \mu \bar{E}$$

↳ mobility

$$\bar{u} = v_d = \mu \bar{E}$$

↳ drift velocity; if  $\rho v = -ne \rightarrow n$  is  $1/m^3$

$$\bar{J} = \rho v \bar{n}$$

$$\bar{J} = -ne \bar{u} \Rightarrow \bar{J} = -ne \left( \frac{-e\tau}{m} \right) \bar{E} = \left( \frac{n^2 e^2 \tau}{m} \right) \bar{E}$$

$$\bar{J} = \sigma \bar{E}$$

→ conduction current density  
→ point form of ohm's law.

$$I = GV \Rightarrow I = \frac{V}{R}$$

$$I = \int \vec{J} \cdot d\vec{s}, \quad V = \int E dU$$

$$I = J_s, \quad V = El$$

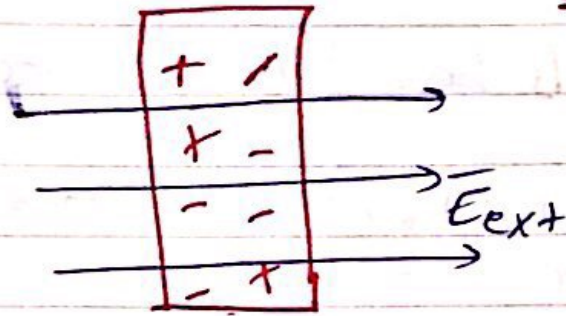
$$R = \frac{V}{I} = \frac{El}{J_s} = \frac{El}{\sigma_s \epsilon_s}$$

$$R = \frac{\rho}{\sigma_s} = \frac{\rho L}{s}$$

$$\rho = \frac{\sigma}{M}$$

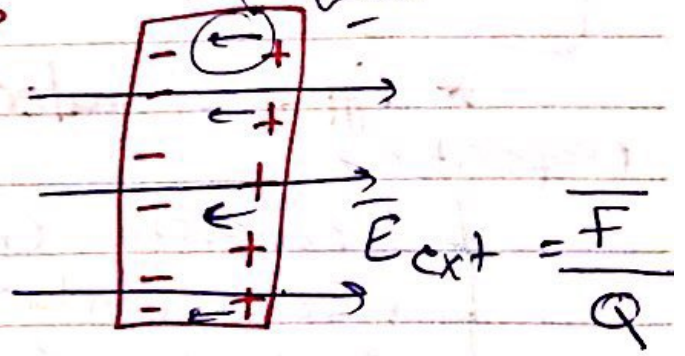
\* Conductors :

$\vec{E}_{\text{internal}}$   
 محال  
 عمربا  
 داخله

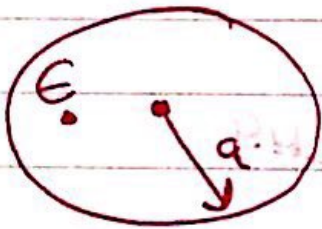
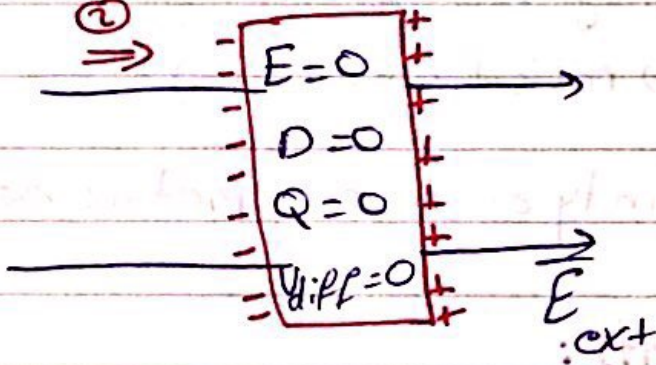


$Q = 0$

Neutralized



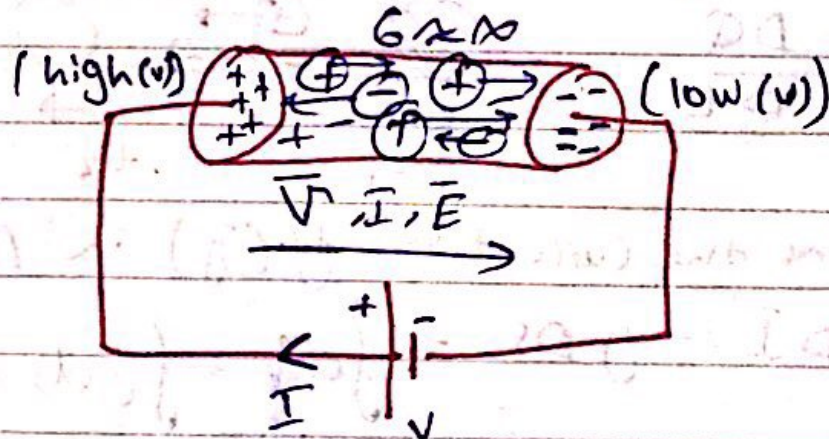
②



$E = E_0$

conductors ( $\epsilon = \infty$ )

Free space ( $\epsilon = 0$ )



↑

## - Resistance (R)

$$R = \frac{V}{I} = - \int_{\rho} \vec{E} \cdot d\vec{L}$$

$$R = \frac{PL}{A} = \frac{1}{\sigma A}$$

$$R = \frac{\rho L}{\sigma \epsilon S}$$

$$\int \underbrace{\sigma \vec{E}}_{\vec{J}} \cdot d\vec{s}$$

\*only (uniform)

\*Power :-  $P = VI$  (watt)

$$P = \frac{\text{work}}{\text{time}}, \left( \frac{J}{s} = W \right)$$

$$= - \frac{Q \int_{\rho} \vec{E} \cdot d\vec{L}}{dt}, \quad \alpha = \int_{\nu} P_{\nu} d\nu$$

$$= + Q \vec{E} \cdot \vec{V}$$

$$P = \int_{\nu} P_{\nu} E \nu d\nu = \int_{\nu} \vec{J} \cdot \vec{E} d\nu, \quad \vec{J} = \sigma \vec{E}$$

$$P = \int_{\nu} \vec{J} \cdot \vec{E} d\nu$$

$$= \int_{\nu} \sigma E^2 d\nu$$

$$= \int_{\nu} \frac{J^2}{\sigma} d\nu$$

$$\vec{J} = \sigma \vec{E}$$

in (W)

$w_p \equiv$  Power density ( $W/m^3$ )

$$\text{power density} \equiv W_p = \frac{P}{\text{volume}}$$

$$\begin{aligned} W_p &= \vec{J} \cdot \vec{E} \\ &= G E^2 \\ &= \frac{J^2}{G} \end{aligned}$$

in uniform:

$$P = \int_V \vec{J} \cdot \vec{E} dV \Rightarrow \text{joule's law.}$$

$$dV = ds dl$$

$$P = \int_V \vec{J} \cdot \vec{E} dV$$

$$P = \int_S \vec{J} \cdot d\vec{s} \int_L \vec{E} \cdot d\vec{l}$$

$$P = I * V$$

$$P = G V^2 = \frac{V^2}{R}$$

$$= \frac{I^2}{G} = R I^2$$

$$\Phi = \int \vec{J} \cdot d\vec{\Sigma}, \quad V = - \int \vec{E} \cdot d\vec{l}$$

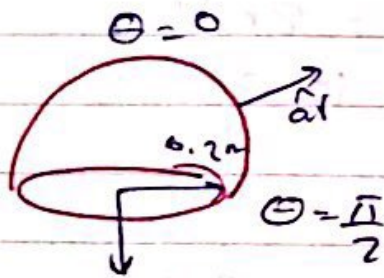
$A/m^3$

\* example: If  $\vec{J} = \frac{1}{r^3} (z \cos \theta \hat{a}_r + z \sin \theta \hat{a}_\theta)$   
Find the current passing through:

- a) A hemi-spherical shell of radius = 20 cm  
 $0 < \theta < \frac{\pi}{2}$ ,  $0 < \phi < 2\pi$
- b) A spherical shell of  $r = 10$  cm.

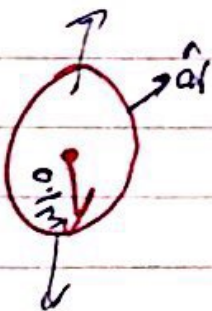
Sol.

a)



$$I = \int_S \vec{J} \cdot d\vec{s}$$
$$d\vec{s} = r^2 \sin \theta d\theta d\phi \hat{a}_r$$
$$I = \frac{1}{r} \int_0^{2\pi} \int_0^{\frac{\pi}{2}} z \sin \theta \cos \theta d\theta d\phi \Big|_{r=0.2 \text{ m}}$$
$$= 10\pi \text{ A}$$
$$= 31.4 \text{ A}$$

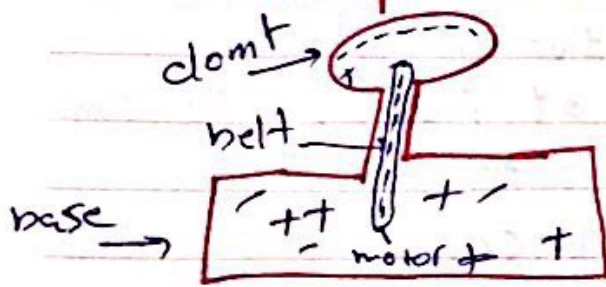
b)



$$d\vec{s} = r^2 \sin \theta d\theta d\phi \hat{a}_r$$
$$I = \oint_S \vec{J} \cdot d\vec{s} = \int_V \nabla \cdot \vec{J} dV$$
$$\nabla \cdot \vec{J} = 0$$



\* example: In Van de Graaff generator:



if  $P_s = 10^{-7} \text{ C/m}^2$ ,  $u = 2 \text{ m/s}$   
width of the belt = 10 cm  
calculate the charge.

$$\dot{I} = \frac{dQ}{dt} = \frac{P_s P_b}{P_b}$$

$$P_s = \frac{W_b}{P_b} \Rightarrow I = P_s W_b u$$
$$Q = I t$$

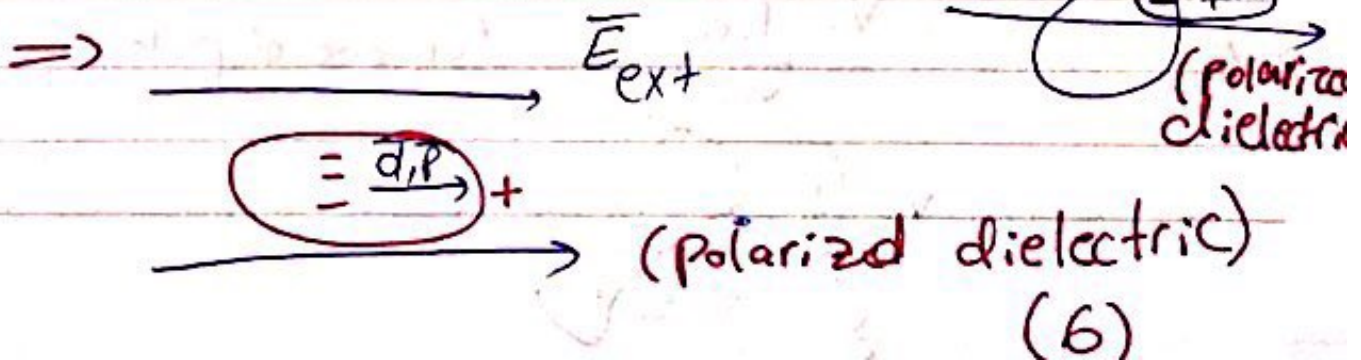
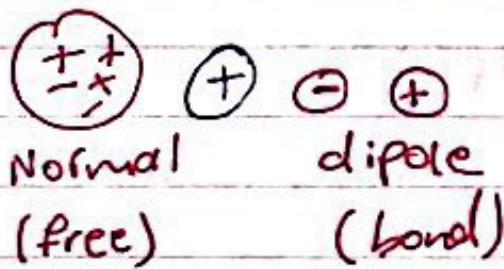
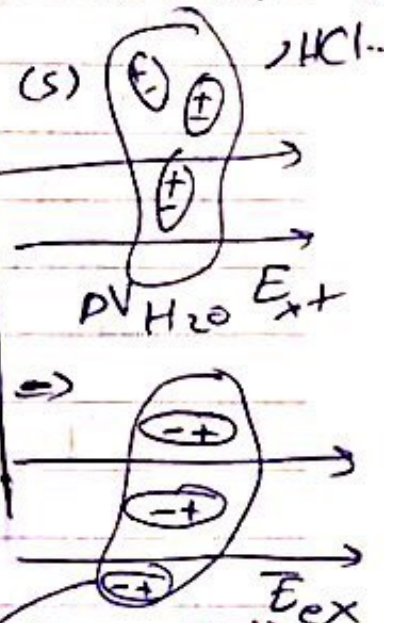
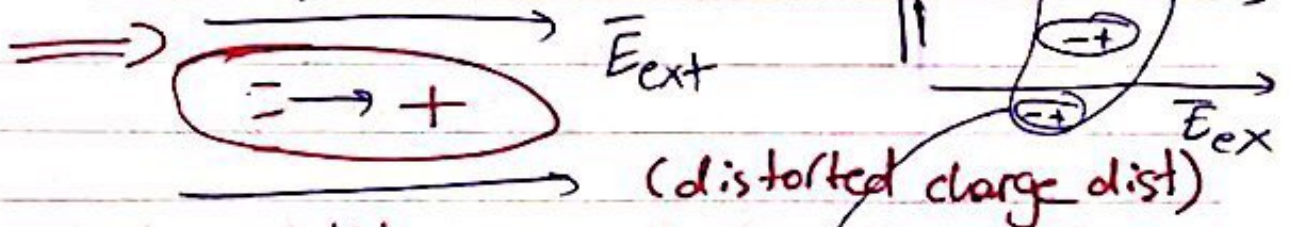
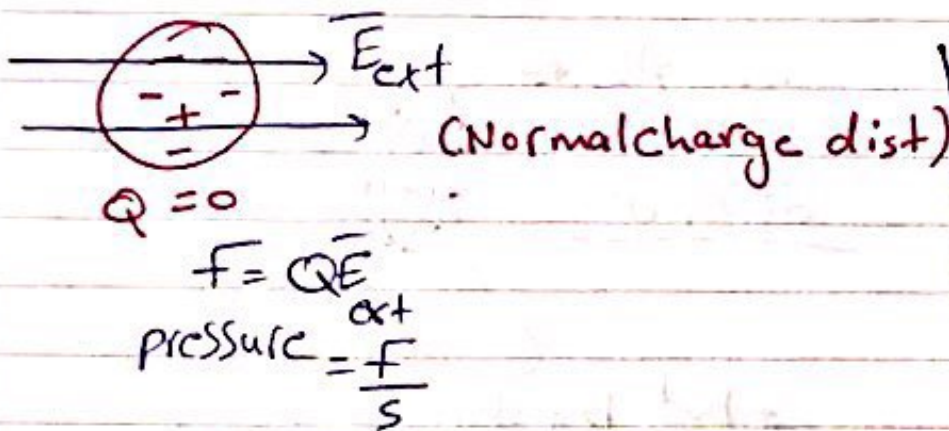
$$Q = P_s W_b u t$$

$$Q = 100 \text{ nC.}$$

\* Polarization in dielectrics:

- Types of dielectrics:

- non-polar  
 $O_2, H_2, N_2, \text{Rare gases}, Xe, Ne, Kr.$
- polar (Permanent dipoles) - ex.  $H_2O, NH_3$



- define polarization ( $\vec{P}$ )

$$\vec{P} = \lim_{\Delta V \rightarrow 0} \frac{\sum_{k=1}^N Q_k \vec{d}_k}{\Delta V} \quad \text{in } (\text{C/m}^3)$$

\* for N-dipoles

$$\vec{P} = \sum_{k=1}^N Q_k \vec{d}_k \quad (\text{C.m})$$

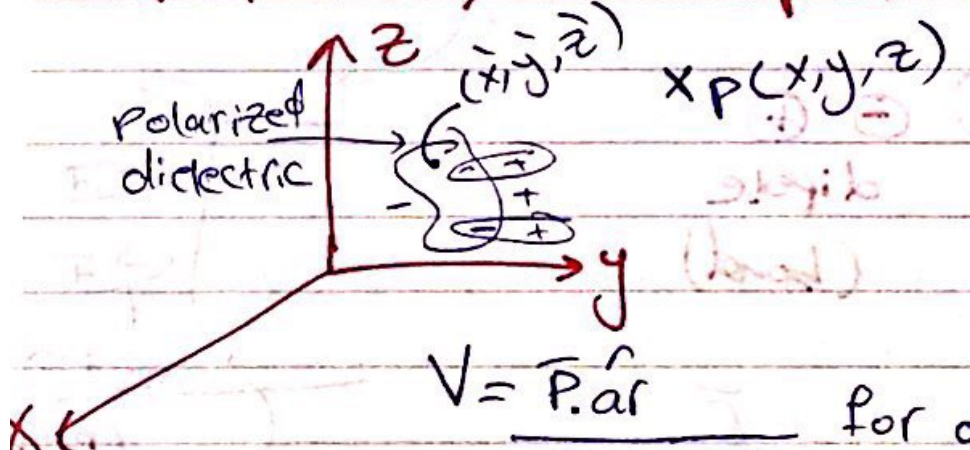


angle as  $\vec{d}_k$  dipoles



but by shrinking and taking only one dipole

\* find  $V, \vec{E}, \vec{D}$  for a polarized dielectric.



$$V = \int \frac{\vec{P} \cdot \hat{a}_r}{4\pi\epsilon_0 r^2} dv$$

→ for dipole charges.

$$V = \oint \frac{\vec{P} \cdot \hat{a}_n}{4\pi\epsilon_0 r} ds \quad \ominus \quad \int \frac{\nabla' \cdot \vec{P}}{4\pi\epsilon_0 r} dV$$

→ for free charge:

from Ch. 4

$$V = \int \frac{P_s ds}{4\pi\epsilon_0 r}, \quad V = \int \frac{P_v dV}{4\pi\epsilon_0 r}$$

- equating terms:

$$P_s = \vec{P} \cdot \hat{a}_n$$

↳ polarized (bound) surface charge dist.

$$P_v = -\nabla \cdot \vec{P}$$

↳ polarized (bound) volume charge dist.

**- bound charge** :-  $(Q_b)$

$$Q_{bt} = \int_s P_s ds, \quad Q_b = \int_v P_v dV$$

$$Q_{btotal} = Q_{bt} + Q_b = 0$$

↳ must (Neutralized).

$$\vec{E} = -\nabla V, \quad \vec{P} = \epsilon \cdot \vec{E}$$

\* For some dielectrics (Linear Dielectrics)

$$* \boxed{\vec{P} = \chi_e \epsilon \cdot \vec{E}}$$

$\chi_e \equiv$  (electrical susceptibility).  
(constant)

Mat.	$\chi_e$	
Air	0	$\rightarrow \vec{P} = 0$
good cond	0	$\rightarrow \vec{P} = 0$
:		

\* polarized in dielectrics:

$$P_{ps} = \vec{P} \cdot \hat{a}_n$$

$$P_{pv} = -\nabla \cdot \vec{P}$$

$D = \epsilon \cdot \vec{E}$  in free space and conductors.

$$P_{v \text{ total}} = (\vec{P}_v) + P_{pv} = \nabla \cdot \vec{P}$$

$$P_v = P_{v \text{ total}} - P_{pv} = \nabla \cdot \vec{P} - (-\nabla \cdot \vec{P})$$

$$P_v = \nabla \cdot (\vec{P} + \vec{P})$$

$$P_v = \nabla \cdot (\epsilon \cdot \vec{E} + \vec{P}) = \nabla \cdot \vec{P}$$

for some dielectrics (Linear dielectric)

$$\vec{P} = \chi_e \epsilon \cdot \vec{E}$$

$\chi_e \equiv$  electrical susceptibility. (constant)

Material	$\chi_e$
Air	0
conductors	0

$$\boxed{\vec{D} = \epsilon \cdot \vec{E} + \vec{P}} \rightarrow \text{in general}$$

$D| > D|$   
dielectric conductors  
& freespace.

$$\begin{aligned} \vec{D} &= \epsilon \cdot \vec{E} + \chi_e \epsilon_0 \cdot \vec{E} \\ &= (1 + \chi_e) \epsilon_0 \cdot \vec{E} \\ \vec{D} &= \epsilon_r \epsilon_0 \cdot \vec{E} \\ \vec{D} &= \epsilon \vec{E} \end{aligned} \quad \left\| \begin{array}{l} \epsilon = \text{permittivity F/m} \\ \epsilon_r = \text{relative permittivity} \\ \text{(Dielectric constant)} \\ \epsilon_r = \frac{\epsilon}{\epsilon_0} \text{ or } 1 + \chi_e \end{array} \right.$$

- bound charge ( $Q_b$ )

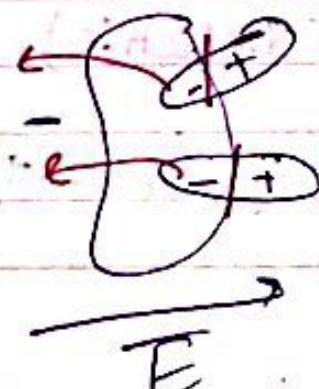
$$Q_{b+} = \int_s P_{ps} ds$$

$$Q_{b-} = \int_v P_{pv} dv$$

$$Q_{b\text{total}} = Q_{b+} + Q_{b-} = \boxed{0}$$

\* Dielectric breakdown.

if  $Q_{b\text{total}} \neq 0$

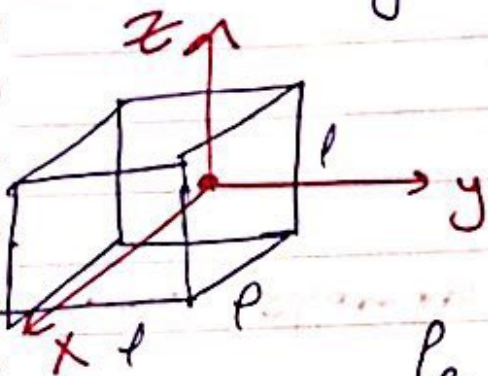


\* breakdown depends on:

- 1) The nature of the material,
- 2) Temperature  $T \downarrow$
- 3) Humidity  $\uparrow$
- 4) The applied  $\vec{E}_{\text{ext}} \uparrow$

5) The time that  $\vec{E}_{ext}$  is applied  $\uparrow$ .

\* **Example:** A dielectric cube of length ( $l$ ) is centered at the origin has  $\vec{P} = a\vec{r}$  where ( $a$ ) is constant and  $\vec{r} = x\hat{a}_x + y\hat{a}_y + z\hat{a}_z$   
**Find:** All bound charge dist. and the total bound charge



$$P_{fs} = \vec{P} \cdot \hat{a}_n, \hat{a}_n = \hat{a}_x$$

$$= ax \Big|_{x=-\frac{l}{2}} = \frac{al}{2} \text{ C/m}^2$$

$$P_{fs} = -ax \Big|_{x=\frac{l}{2}} = \frac{al}{2} \text{ C/m}^2$$

$$= \vec{P} \cdot (-\hat{a}_x)$$

$\Rightarrow$  All  $P_{fs} = \frac{al}{2} \text{ C/m}^2$

$$P_{v} = -\nabla \cdot \vec{P}$$

$$= -\left(\frac{\partial P_x}{\partial x} + \frac{\partial P_y}{\partial y} + \frac{\partial P_z}{\partial z}\right)$$

$$= -(a + a + a)$$

$$P_{v} = -3a \text{ C/m}^3$$

$$Q_{bt} = 6 \int P_{fs} ds = 6 \int_{-\frac{l}{2}}^{\frac{l}{2}} \int_{-\frac{l}{2}}^{\frac{l}{2}} \frac{al}{2} dy dz$$

$$Q_{bt} = 3al^3 \text{ C}$$

$$\Phi_{b-} = \int \rho_{b-} dv$$

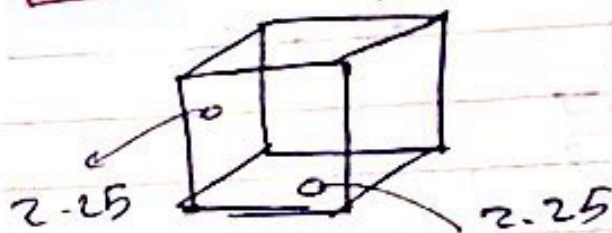
$$= \int_{-\frac{f}{2}}^{\frac{f}{2}} \int_{-\frac{f}{2}}^{\frac{f}{2}} \int_{-\frac{f}{2}}^{\frac{f}{2}} -3a \, dx \, dy \, dz$$

$$\Phi_{b-} = -3a \rho^3$$

$$\Phi_{b \text{ total}} = 0$$

5.7 → linear, isotropic, homogenous.

$\epsilon_r$



$$\epsilon_r = 2.25 \times r$$

$$\begin{aligned} \nabla \cdot \bar{D} &= \nabla \cdot \epsilon \bar{E} = \nabla \cdot \epsilon_r \bar{E} \\ &= \epsilon_r \nabla \cdot \bar{E} \end{aligned}$$

5.8 → conductivity equation & relaxation time.

$$\boxed{kcl} : I_{out} = I_{in}$$

$$I_{out} = \oint_S \bar{J} \cdot d\bar{s}, \quad I_{in} = -\frac{dQ_{in}}{dt}$$





$$\oint_S \bar{J} \cdot d\bar{s} = -\frac{dQ_{in}}{dt}, \quad Q_{in} = \int_V \rho_V dv$$

$$\oint_S \bar{J} \cdot d\bar{s} = -\frac{dQ}{dt} = \int_V \rho_V dv$$

$$\oint_S \bar{J} \cdot d\bar{s} = \int_V \frac{\partial \rho_V}{\partial t} dv \rightarrow \rho_V(x, y, z; t)$$

$$\int_V \nabla \cdot \bar{J} dv = -\int_V \frac{\partial \rho_V}{\partial t} dv$$

$$\boxed{\nabla \cdot \bar{J} = -\frac{\partial \rho_V}{\partial t}} \rightarrow \text{continuity of Eq.}$$

start from  $\nabla \cdot \bar{J} = -\frac{\partial \rho_V}{\partial t}$

with:  $\nabla \cdot \bar{D} = \rho_V$ ,  $\bar{D} = \epsilon \bar{E}$ ,  $\bar{J} = \sigma \bar{E}$

$\nabla \cdot \epsilon \bar{E} = \rho_V$  if  $\epsilon$  is homogeneous

$$\boxed{\nabla \cdot \bar{E} = \frac{\rho_V}{\epsilon}}$$

$$\nabla \cdot \sigma \bar{E} = -\frac{\partial \rho_V}{\partial t}$$

$$\sigma \frac{\rho_V}{\epsilon} = -\frac{\partial \rho_V}{\partial t}$$

$$\int_{\rho_{V_0}}^{\rho_V} \frac{\partial \rho_V}{\rho_V} = \int_{t_0}^t -\frac{\sigma}{\epsilon} dt$$

I.e.  
 $\rho_V(t=t_0) = \rho_{V_0}$

$$\ln P_V - \ln P_{V_0} = \frac{-G}{G} (t - t_0)$$

$$\ln\left(\frac{P_V}{P_{V_0}}\right) = -\frac{\sigma}{G} (t - t_0)$$

~~$$\ln\left(\frac{P_V}{P_{V_0}}\right) = -\frac{\sigma}{G} (t - t_0)$$~~

$$\frac{P_V}{P_{V_0}} = e^{-\frac{\sigma}{G} (t - t_0)}$$

$$P_V = P_{V_0} e^{-\frac{\sigma}{G} (t - t_0)}$$

$$P_V = P_{V_0} e^{-\frac{\sigma}{G} (t - t_0)}$$

$$P_V = P_{V_0} e^{-\frac{\sigma}{G} (t - t_0)}$$

$$T_r = \frac{G}{\sigma}$$

$$t = T_r \rightarrow e^{-1} = 36.8$$

\* for copper  $\epsilon_r = 1$ ,  $G = 5.7 \times 10^8$

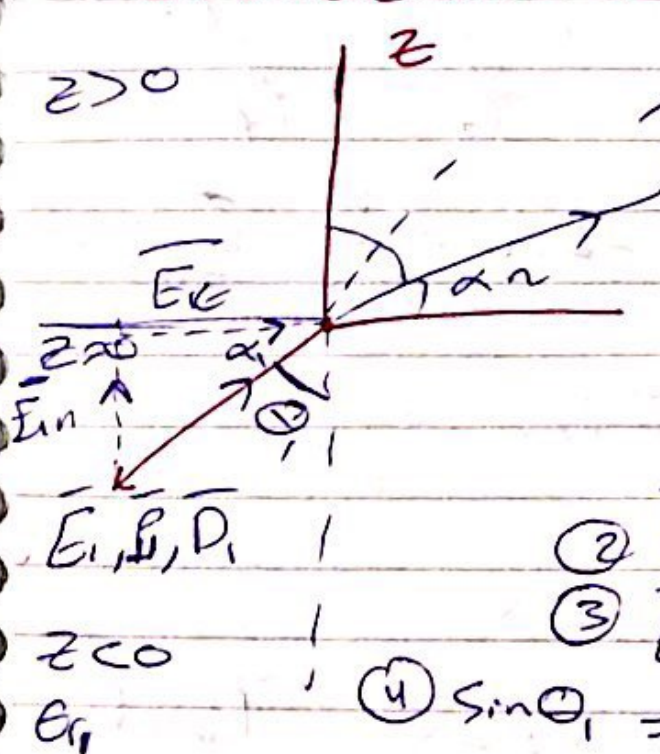
$$T_r = \frac{G \cdot \epsilon_r}{\sigma} = 1.53 \times 10^{-17}$$

for fused

$$T_r = \frac{G \cdot \epsilon_r}{\sigma} = 51.2$$

\* Boundary condition.

\* (1) Dielectric to Dielectric.



Assume  $\vec{E}_1$  is given

(1)  $\vec{E}_1 = \vec{E}_{in} + \vec{E}_{te}$

$\hat{a}_n = +\hat{a}_z$

(2)  $\vec{E}_{in} = (\vec{E}_1 \cdot \hat{a}_n) \hat{a}_n$

(3)  $\vec{E}_{te} = \vec{E}_1 - \vec{E}_{in}$

(4)  $\sin \theta_1 = \frac{E_{te}}{E_1}$

(5)  $\cos \theta_1 = \frac{E_{in}}{E_1}$

(6)  $\tan \theta_1 = \frac{E_{te}}{E_{in}}$  ,  $\alpha_1 = 90^\circ - \theta_1$

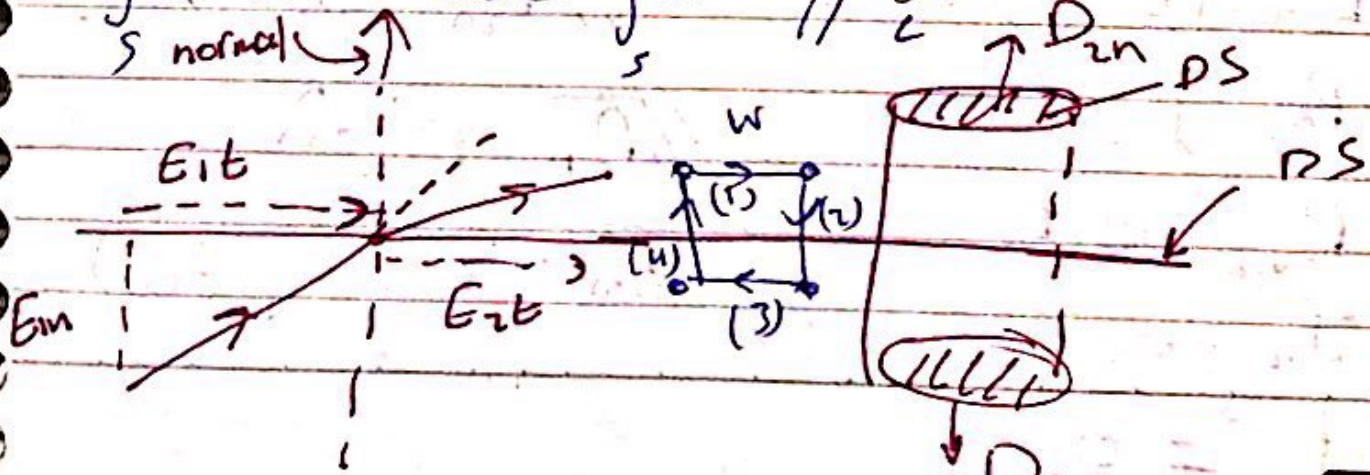
to find  $\vec{E}_2$

$\vec{E}_2 = \vec{E}_{2n} + \vec{E}_{2t}$

\* Apply 1st Maxwell eq. & 2nd.

on the ref. ( $z=0$ )

$\oint_S \vec{D} \cdot d\vec{s} = Q_{enc} = \int_S \rho_s d\vec{s}$  //  $\oint \vec{E} \cdot d\vec{l} = 0$



$$\oint \vec{E} \cdot d\vec{l} = 0, \text{ on } z=0$$

$$\oint \vec{E} \cdot d\vec{l} = \int \vec{E} \cdot d\vec{l}_1 + \int \vec{E} \cdot d\vec{l}_2 + \int \vec{E} \cdot d\vec{l}_3 + \int \vec{E} \cdot d\vec{l}_4 = 0$$

$$E_{zt} W - E_{zn} \frac{h}{2} - E_{in} \frac{h}{2} - E_{nz} W \frac{h}{2} - E_{zn} \frac{h}{2} = 0$$

$$\boxed{E_{zt} = E_{it}} \text{ Always}$$

\* Applying  $\oint \vec{D} \cdot d\vec{s} = \int \rho_s d\vec{s}$

$$D_{zn} Ds - D_{in} Ds = P_s Ds$$

$$\boxed{D_{zn} - D_{in} = P_s} \text{ if } P_s = 0 \Rightarrow \overline{D_{in}} = \overline{D_{zn}}$$

$$\epsilon_1 \epsilon_r \overline{E_{in}} = \epsilon_2 \epsilon_r \overline{E_{zn}}$$

$$\boxed{\overline{E_{zn}} = \frac{\epsilon_1}{\epsilon_2} \overline{E_{in}}}$$

line ①  $E_z = E_{zn} + E_{zt}$

②  $\overline{P_z} = \epsilon_1 \epsilon_r \overline{E_z}$

③  $\overline{P_z} = (\epsilon_2 - 1) \epsilon_r \overline{E_z}$

④  $P_{sz} = \overline{P_z} \hat{a}_n$

⑤  $P_{sz} = \nabla \cdot \overline{P_z}$

⑥  $\overline{J_z} = \sigma_2 \overline{E_z}$

⑦ if  $P_s \neq 0$

$$D_{zn} - D_{in} = P_s$$

$$D_{zn} = D_{in} + P_s, \quad P_{in} = \epsilon_1 \epsilon_r E_{in}$$

$$\overline{D_{zn}} = \overline{D_{in}} \hat{a}_n$$

$$\overline{E_{zn}} = \overline{D_{in}} (\epsilon_1 \epsilon_r)$$

if  $P_s = 0$  (relation between  $\theta_1$  &  $\theta_2$ )

$$E_{1t} = E_{2t}$$

$$E_1 \sin \theta_1 = E_2 \sin \theta_2 \quad \text{--- (1)}$$

$$P_{1n} = P_{2n}$$

$$\epsilon_1 \epsilon_0 E_{1n} = \epsilon_2 \epsilon_0 E_{2n}$$

$$\epsilon_1 E_1 \cos \theta_1 = \epsilon_2 E_2 \cos \theta_2$$

dividing (1) by (2)

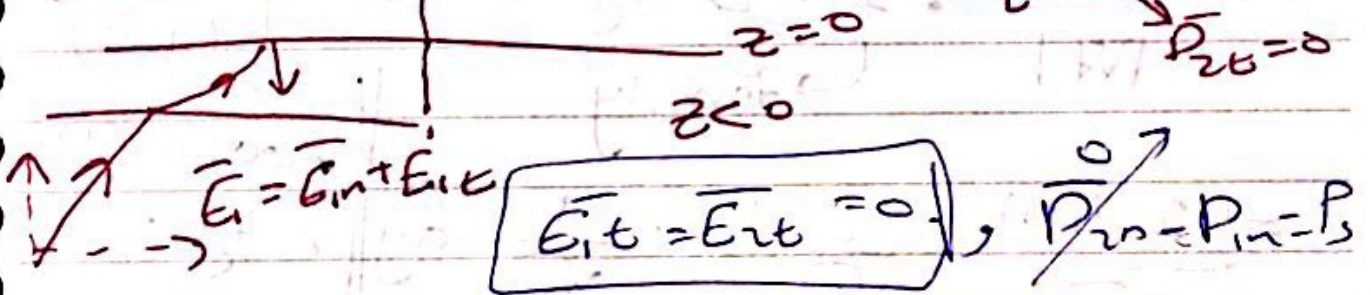
$$\frac{\tan \theta_1}{\epsilon_1} = \frac{\tan \theta_2}{\epsilon_2}$$

(\*) (2) Conductor - to - Dielectric  $E_{2t} = 0$

$\uparrow$  z-normal

$$\vec{E}_2 = 0 \Rightarrow E_{2n} = 0$$

$$\vec{P}_2 = 0 \Rightarrow P_{2n} = 0$$



$$E_n = \frac{P_n}{\epsilon_0 \epsilon_1}$$

$$P_n = -P_s (\hat{a}_n)$$

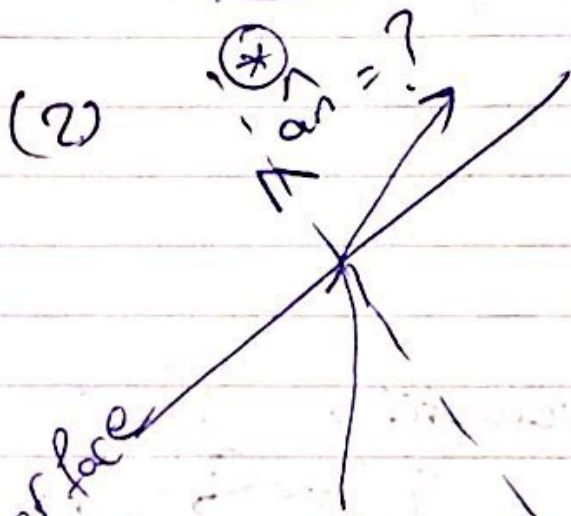
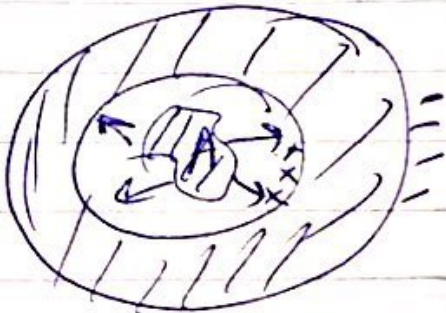
(\*) (C) free space - to conductor :-

$$\vec{E}_{1t} = \vec{E}_{2t} = 0$$

$$D_{1n} = -P_s \hat{a}_n$$

$$\vec{E}_{1n} = \frac{\vec{D}_1}{\epsilon_0}$$

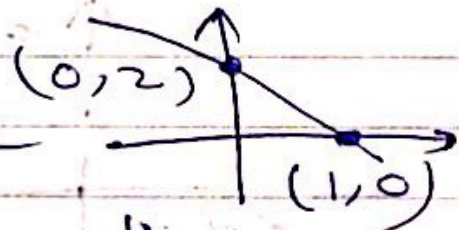
\*Application :-  
Shielding



$$\hat{a}_n = \frac{\nabla F}{|\nabla F|}$$

$$, \quad f = 2x + y - 2$$

↳ family



$$= \frac{(2, 1, 0)}{\sqrt{5}}$$

$$= \frac{2}{\sqrt{5}} \hat{a}_x + \frac{1}{\sqrt{5}} \hat{a}_y$$

medium (1)

$$2x + y - 2 \leq 0$$

(2)

$$2x + y - 2 > 0$$

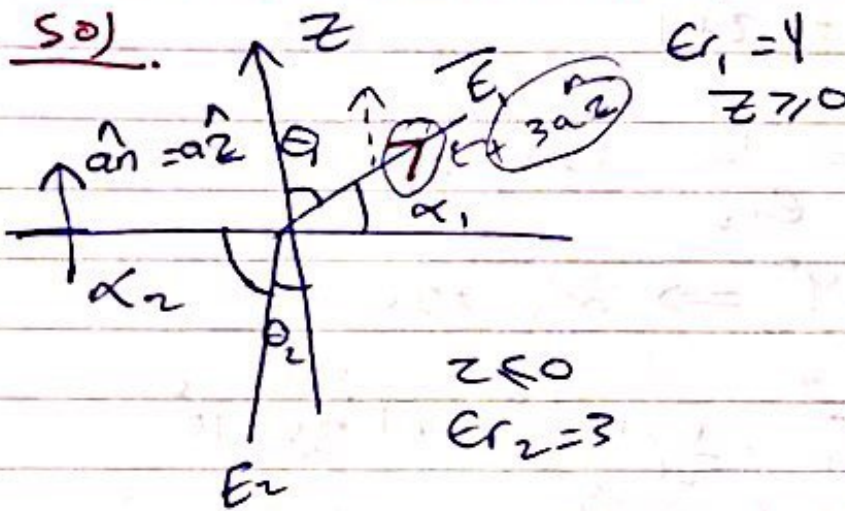
$$\vec{E}_n = (\vec{E}_i \cdot \hat{a}_n) \hat{a}_n$$

\*example: Two homogeneous isotropic dielectrics meet on plane  $z=0$ . for  $z>0$ ,  $\epsilon_r=4$

has  $\vec{E} = 5a\hat{x} - 2a\hat{y} + 3a\hat{z}$  kV/m

find: سأنا بحزن الانتباه

- a)  $E_2$  for  $z \leq 0$  if  $\epsilon_r=3$
- b)  $\phi_1, \phi_2, \alpha_1, \alpha_2$
- c) energy density in both regions.
- d) the energy in a cube of side (2m) centered at (3,4,-5).



$\hat{n} = a\hat{z}$ ,  $\vec{E}_1 = \vec{E}_{1n} + \vec{E}_{1t}$   
 $E_{1n} = (\vec{E}_1 \cdot \hat{n}) \hat{n}$

$\vec{E}_{1n} = 3a\hat{z}$  kV/m

$\vec{E}_{1t} = \vec{E}_1 - \vec{E}_{1n} = 5a\hat{x} - 2a\hat{y}$  kV/m  
 $= \vec{E}_{2t}$

$\vec{E}_{1t} = \vec{E}_{2t}$

$\Rightarrow D_{1n} = D_{2n}, \rho_s = 0$

$D_{1n} = D_{2n}$

$$\vec{E}_{in} = \frac{E_{r1}}{E_{r2}} \vec{E}_{in}$$

$$E_{in} = 4 \hat{a}_z \text{ kV/m}$$

$$\begin{aligned} \vec{E}_2 &= \vec{E}_{ext} + \vec{E}_{in} \\ &= 5 \hat{a}_x + -2 \hat{a}_y + 4 \hat{a}_z \end{aligned}$$

$$b) \theta_1 = \sin^{-1} \left( \frac{E_{yt}}{E_1} \right) = \sin^{-1} \left( \frac{\sqrt{29}}{\sqrt{38}} \right) = 60.9^\circ$$

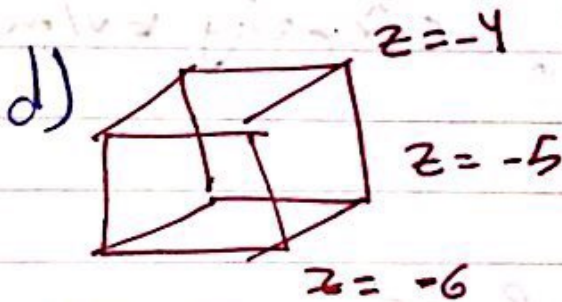
$$\alpha_1 = 90^\circ - \theta_1 = 29.1$$

$$\theta_2 = \frac{\tan \theta_1}{\tan \theta_2} = \frac{E_{r1}}{E_{r2}} \text{ if } \rho_s = 0$$

$$\theta_2 = 53.4^\circ \Rightarrow \alpha_2 = 36.6^\circ$$

$$\begin{aligned} c) w_{E_1} &= \frac{1}{2} E_1 E_1 = \frac{1}{2} \left( \frac{10^9}{36\pi} \right) (4) 38 \times 10^6 \\ &= 672 \text{ MJ/m}^3 \end{aligned}$$

$$\begin{aligned} w_{E_2} &= \frac{1}{2} E_2 E_2 = \frac{1}{2} \left( \frac{10^9}{36\pi} \right) (3) (4J) \times 10^6 \\ &= 597 \text{ MJ/m}^3 \end{aligned}$$



$$W_E = \int_V w_{E_2} dV = \int_{-6}^{-4} \int_{-6}^{-5} \int_{-6}^{-5} 597 \times 10^6 dx dy dz$$

$$= 598 \times 10^6 \times 8$$

in region 2

$$= 4.776 \text{ MJ}$$



$\Rightarrow$  resolve (d) if the center is (0,0,0)

$$W_E = \int_{V_1} w_{E_1} dV + \int_{V_2} w_{E_2} dV$$
$$= \int_{-1}^1 \int_{-1}^1 \int_{-1}^1 672 \times 10^{-6} dx dy dz + \int_{-1}^1 \int_{-1}^1 \int_{-1}^1 597 \times 10^{-6} dx dy dz$$

chapter 6

: electrostatic Boundary value Problems (B.V.P)

Coulomb's law  
Gauss's law }  $\rightarrow$  charge is known

potential

$$\vec{E} = -\nabla \bar{V} \rightarrow \text{potential is given}$$

If the charge or potential is known for part of the surface

$\Rightarrow$  use B.V.P

$$\nabla \cdot \vec{D} = \rho_v$$

$$\vec{E} = -\nabla V \leftarrow \nabla \times \vec{E} = 0$$

$$\vec{D} = \epsilon \vec{E}, \quad \epsilon = \epsilon_0 \epsilon_r$$

$$\nabla \cdot \epsilon (-\nabla V) = \rho_v$$

Poisson's eq. for non-homo.

$\epsilon_r$  is not constant

if  $\epsilon$  is homo

$$\nabla \cdot \nabla V = \frac{-\rho_v}{\epsilon} \rightarrow \nabla^2 V = \frac{-\rho_v}{\epsilon}$$

For surface free region  $\rightarrow \rho_v = 0$

$\nabla \cdot -\epsilon \nabla V = 0 \rightarrow$  Laplace's eq for

$\nabla^2 V = 0$  non-hom media

Poisson's eq. for hom media

$$\nabla = \frac{\partial}{\partial x} \hat{x} + \frac{\partial}{\partial y} \hat{y} + \frac{\partial}{\partial z} \hat{z}$$

\* procedure to solve Laplace's or Poisson's:

1] choose a suitable coordinates (Based on the structure).

2] select the proper partial eq. to solve (based on  $\epsilon_r$  and  $\rho_v$ ).

3] solve the selected eq. using:

a) Direct integral if  $V$  is function of one variable.

b) separation of variables;  $V$  is function of 2 or 3 variables.

4] Apply two boundary (Initial) conditions to find two unknowns.

→ to find the unique solution of  $V$

5] Find  $\vec{E} = -\nabla V$

mainly:

$$6] R = \frac{V}{I} = \frac{-\int \vec{E} \cdot d\vec{L}}{\int \vec{E} \cdot d\vec{s}}$$

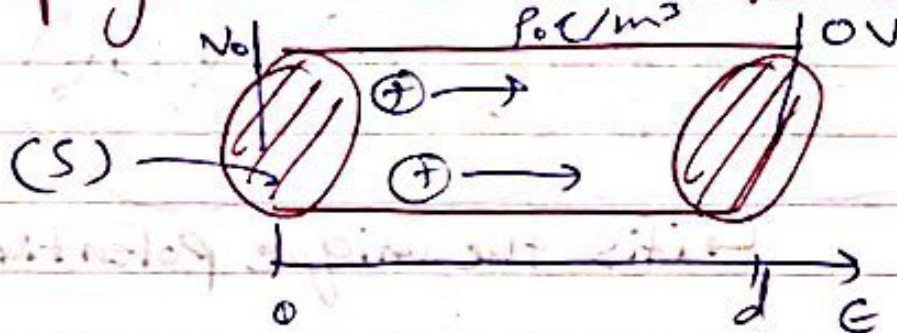
$$C = \frac{Q}{V} = \frac{\int \epsilon \vec{E} \cdot d\vec{s}}{-\int \vec{E} \cdot d\vec{L}}$$

in cart.  $\nabla^2 V = \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} + \frac{\partial^2 V}{\partial z^2}$   
(Scalar)

in cyl.  $\nabla^2 V = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 V}{\partial \theta^2} + \frac{\partial^2 V}{\partial z^2}$   
(given)

in sph.  $\nabla^2 V = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial V}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial V}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 V}{\partial \phi^2}$   
(given)

\* Example: Electrohydrodynamics (EHD) Pumping has  $\rho_0 \text{ C/m}^3$  exists between electrodes



if  $\rho_0 = 25 \text{ mc/m}^3$  and  $V_0 = 22 \text{ kV}$

find the pressure of the pump.

- solve the poissons eq. in cyl. coordinates

$$\nabla^2 V = -\frac{\rho_v}{\epsilon}, \quad \rho_v = \rho_0$$

$$\frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 V}{\partial \theta^2} + \frac{\partial^2 V}{\partial z^2} = -\frac{\rho_v}{\epsilon}$$

$$\int \frac{d^2 V}{dz^2} = \int \frac{-\rho_v}{\epsilon}$$

$$\int \frac{dV}{dz} = \int \left( -\frac{\rho V}{\epsilon} z + A \right)$$

$$V = -\frac{\rho V}{\epsilon} \frac{z^2}{2} + Az + B$$

B.c.s are

$$\begin{cases} V(z=0) = V_0 \\ V(z=d) = 0 \end{cases}$$

$$\boxed{B = V_0}$$

$$0 = -\frac{\rho V}{\epsilon} \frac{d^2}{2} + Ad + V_0$$

$$\boxed{A = \frac{1}{d} \left[ \frac{\rho V}{\epsilon} \frac{d^2}{2} - V_0 \right]}$$

$$V = -\frac{\rho V}{\epsilon} \frac{z^2}{2} + \frac{z}{d} \left( \frac{\rho V}{\epsilon} \frac{d^2}{2} - V_0 \right) + V_0$$

↳ it is the unique potential.

$$\vec{E} = -\nabla V = -\frac{\partial V}{\partial z} \hat{a}_z \quad \text{V/m}$$

$$\vec{E} = - \left( -\frac{\rho V}{\epsilon} + \frac{1}{d} \left( \frac{\rho V d^2}{2\epsilon} - V_0 \right) \right) \hat{a}_z$$

$$\vec{E} = \left( \frac{\rho V z}{\epsilon} - \frac{\rho V d}{2\epsilon} + \frac{V_0}{d} \right) \hat{a}_z$$

$$\vec{F} = Q \vec{E}, \quad Q = \int \rho v dv$$

$$\vec{F} = \int_V \rho v \vec{E} dv, \quad dv = ds dz$$

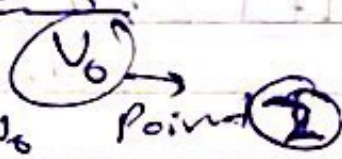
B.V.P

3) Solve Laplace Eq. and apply the B.C.S to find the unique (V)

$$4) \vec{E} = -\nabla V$$

$$5) Q = \oint_S \vec{E} \cdot d\vec{s} \rightarrow C = \frac{Q}{V_0}$$

$$I = \int_S \epsilon \vec{E} \cdot d\vec{s} \rightarrow R = \frac{V_0}{I}$$



Gauss

3) Find  $\vec{E}$  using Gauss.

$$\oint_S \vec{E} \cdot d\vec{s} = Q$$

$$4) V = -\int \vec{E} \cdot d\vec{l}$$

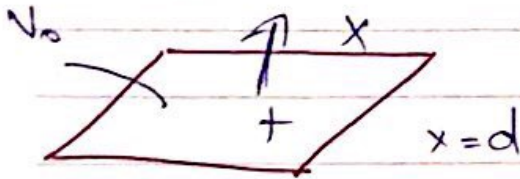
$$5) C = \frac{Q}{V}$$

$$R = \frac{V}{\int_S \epsilon \vec{E} \cdot d\vec{s}}$$

\* types of capacitors:

① parallel plate capacitor

# 1) parallel plate capacitor (Gauss)



Gauss

0V



$$\vec{E} = \frac{Q}{\epsilon_0} (-\hat{x}) \text{ V/m}$$

$$V = -\int_P \vec{E} \cdot d\vec{L} = \frac{QS}{d} \text{ (F)}$$

$$C = \frac{Q}{V}, \quad I = \int_S \vec{E} \cdot d\vec{S}$$

higher (+) side potential

using (B.v.P)

- Assume a  $V_0$  potential diff.
- cart

$$\nabla^2 V = 0 \rightarrow \int \frac{d^2 V}{dx^2} = \int 0$$

$$\int \frac{dV}{dx} = \int A$$

$$V = Ax + B$$

B.C.S  $V(x=0) = 0 \rightarrow \boxed{B=0}$

$$V(x=d) = V_0 \Rightarrow A = \frac{V_0}{d}$$

$$V = \frac{V_0}{d} x \quad (v)$$

$$\vec{E} = -\nabla V = -\frac{dV}{dx} \hat{a}_x$$

$$\vec{E} = -\frac{V_0}{d} \hat{a}_x = \frac{V_0}{d} (-\hat{a}_x) \quad \text{V/m}$$

$$Q = \int \epsilon \vec{E} \cdot d\vec{s} = \int \int \int (\epsilon) \frac{V_0}{d} (-\hat{a}_x) \cdot d\vec{s} (-\hat{a}_x)$$

$$Q = \frac{\epsilon V_0}{d} s (l)$$

$$C = \frac{Q}{V_0} = \frac{\frac{\epsilon V_0}{d} s (l)}{V_0} = \frac{\epsilon s}{d} \quad (F)$$

Energy stored in the Capacitor:

$$W_E = \frac{1}{2} \int \epsilon E^2 dv$$

$$W_E = \frac{1}{2} \frac{\epsilon Q^2}{\epsilon^2 s^2} s d$$

$$= \frac{Q^2}{2\epsilon} \quad , \quad C = \frac{Q}{V} \quad , \quad Q = CV$$

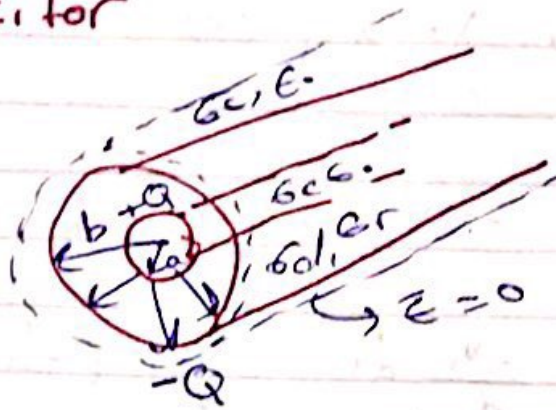
$$= \frac{C^2 V^2}{2\epsilon} = \frac{1}{2} (CV)^2 \quad \text{for uniform}$$

$C = \frac{\epsilon s}{d}$

2) cylindrical capacitor  
(coaxial cable).

$C?$ ,  $R_d?$

$$G = \frac{1}{R_d}$$



using Gauss

$$\oint \epsilon \vec{E} \cdot d\vec{s} = Q$$

$$\vec{E} = E_r \hat{a}_r \cdot d\vec{s} = r d\phi dz \hat{a}_r$$

$$\int_0^l \int_0^{2\pi} \epsilon E_r \hat{a}_r \cdot r d\phi dz$$

$$\epsilon E_r r 2\pi r = Q$$

$$\boxed{E = \frac{Q}{2\pi \epsilon r l} \hat{a}_r} \quad \text{V/m}$$

$$\frac{\rho_H \cdot y}{2\pi \epsilon r} \hat{a}_r$$

$$r_l = \frac{Q}{l}$$

$$V = - \int \vec{E} \cdot d\vec{r}$$

$$= - \int_{r=b}^{r=a} \frac{Q}{2\pi \epsilon r l} \hat{a}_r \cdot dr \hat{a}_r$$

$$= \frac{-Q}{2\pi \epsilon l} \ln\left(\frac{a}{b}\right)$$

$$V = \frac{Q}{2\pi \epsilon l} \ln\left(\frac{b}{a}\right) \quad (V)$$



$$C = \frac{Q}{V} = \frac{Q}{\frac{Q}{2\pi\epsilon l} \ln\left(\frac{b}{a}\right)}$$

$$C = \frac{2\pi\epsilon l}{\ln\left(\frac{b}{a}\right)} \quad (F)$$

\*capacitance per unit length.

$$C/l = \frac{2\pi\epsilon}{\ln\left(\frac{b}{a}\right)} \quad (F/m)$$

$$I = \int \sigma d\vec{E} \cdot d\vec{s} = \int \int \sigma d \frac{Q}{2\pi\epsilon r \rho} \hat{a}_r \cdot \rho d\phi dz \hat{a}_r$$

$$= \frac{\sigma d Q}{2\pi\epsilon l} \hat{a}_r \cdot \rho d\phi dz \hat{a}_r$$

$$I = \frac{\sigma d Q}{\epsilon} A$$

$$R_d = \frac{V}{I} = \frac{\frac{Q}{2\pi\epsilon l} \ln\left(\frac{b}{a}\right)}{\frac{\sigma d Q}{\epsilon}}$$

$$R_d = \frac{\ln\left(\frac{b}{a}\right)}{2\pi\sigma d l} \quad (\Omega)$$

$$R_d C = \frac{\epsilon}{\sigma d} \quad \text{or} \quad \frac{C}{G} = \frac{\epsilon}{\sigma d}$$

$$G/l = \frac{2\pi\sigma d}{\ln\left(\frac{b}{a}\right)} \quad S/m \Rightarrow \frac{G = 2\pi\sigma d l}{\ln\left(\frac{b}{a}\right)} \quad \left\| \quad l = 1 \text{ m} \right.$$

using B.V.P

$$\nabla^2 V = 0$$

$$\frac{1}{r} \int \frac{\partial}{\partial r} \left( r \frac{\partial V}{\partial r} \right) dr = 0$$

$$\int \frac{dr}{r} = \int \frac{A}{r}$$

$$V = A \ln r + B$$

$$\begin{aligned} V(r=b) &= 0 \\ V(r=a) &= V_0 \end{aligned}$$

3) spherical capacitor

$C = ?$ ,  $Rd = ?$

using Gauss:

$$\oint \vec{E} \cdot d\vec{s} = Q$$

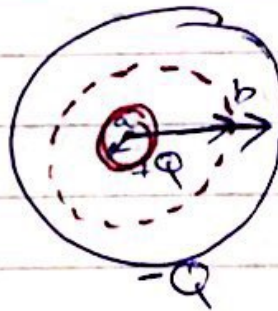
$$\vec{E} = E_r \hat{r}$$

$$d\vec{s} = r^2 \sin\theta d\theta d\phi \hat{r}$$

$$\int_0^{2\pi} \int_0^\pi E_r \hat{r} r^2 \sin\theta d\theta d\phi \hat{r} = Q$$

$$E_r / r^2 (2\pi) (2\pi) = Q$$

$$E = \frac{Q}{4\pi\epsilon_0 r^2} \hat{r} \quad \text{N/m}$$



$$V = - \int E \cdot d\vec{l}$$

$$= - \int_{r=b}^{r=a} \frac{Q}{4\pi\epsilon_0 r^2} \hat{r} \cdot dr \hat{r}$$

$$= \frac{+Q}{4\pi\epsilon_0} \left( \frac{1}{a} - \frac{1}{b} \right) \text{ (v)}$$

$$C = \frac{Q}{V} = \frac{Q}{\frac{Q}{4\pi\epsilon_0} \left( \frac{1}{a} - \frac{1}{b} \right)}$$

$$C = \frac{4\pi\epsilon_0}{\left( \frac{1}{a} - \frac{1}{b} \right)} \text{ (F)}$$

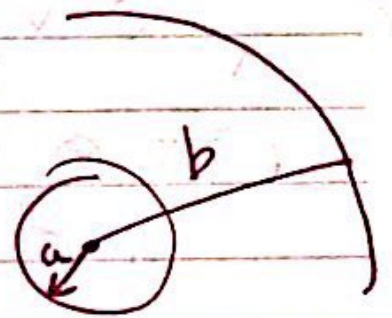
$$I = \int \epsilon_0 d\vec{E} \cdot d\vec{r} = \int_0^{2\pi} \int_0^\pi \frac{\epsilon_0 Q}{4\pi\epsilon_0 r^2} \hat{r} \cdot r^2 \sin\theta d\theta d\phi \hat{r}$$

$$I = \frac{Q}{\epsilon_0} \text{ (A)}$$

$$R_d = \frac{V}{I} = \frac{\frac{1}{a} - \frac{1}{b}}{4\pi\epsilon_0} \text{ (\Omega)}$$

$$G = \frac{4\pi\epsilon_0}{\frac{1}{a} - \frac{1}{b}} \text{ (S)}$$

4) Isolated Capacitor  
when  $b \rightarrow \infty$



$$C = 4\pi\epsilon_0 (F)$$

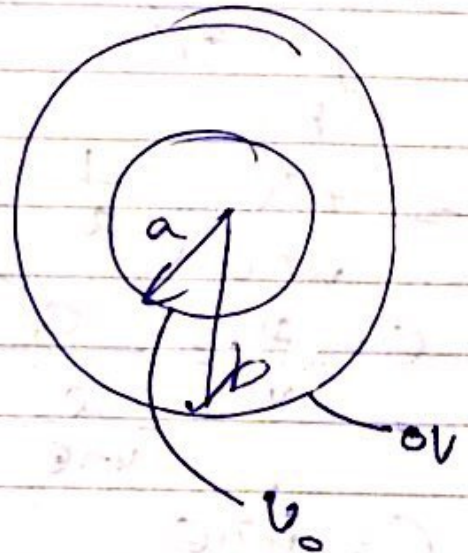
$$R = \frac{1}{4\pi\epsilon_0 a} (-a)$$

Sph Cap. using B.V.P  
Sph.

$$\nabla^2 v = 0$$

$$\frac{1}{r^2} \int \frac{\partial}{\partial r} (r^2 \frac{\partial v}{\partial r}) = \int \rho$$

$$\rho \int \frac{\partial v}{\partial r} = \int \frac{A}{r^2}$$



(Ex.)  $v = \frac{-A}{r} + B$

B.C.s

$$v(r=a) = v_0$$

$$v(r=b) = 0$$

R.C.V.D.I.F.I.I.I

variation w.r.t  $\theta$ .



sph.

$$\nabla^2 v = 0$$

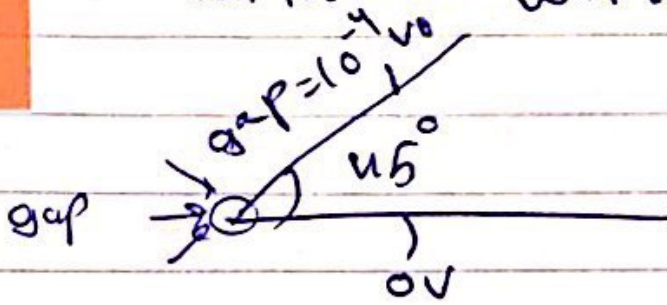
$$\frac{1}{r^2 \sin^2 \theta} \frac{\partial}{\partial \theta} (\sin \theta \frac{\partial v}{\partial \theta}) = 0$$

$$\sin \theta \left( \frac{dv}{d\theta} \right) = \int A \cos \theta$$

$$V(\theta = \theta_2) = V_0$$

$$V(\theta = \theta_1) = 0$$

Variation w.r.t  $\phi$

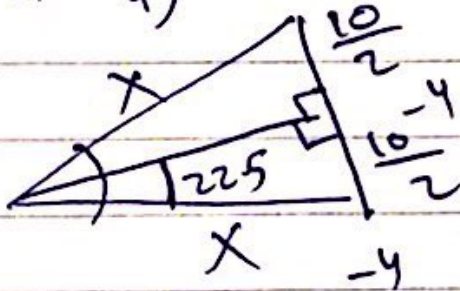


$$\frac{1}{P_2} \frac{d^2 V}{d\phi^2} = 0$$

$$V = A\phi + R$$

$$V(\theta = 0) = 0$$

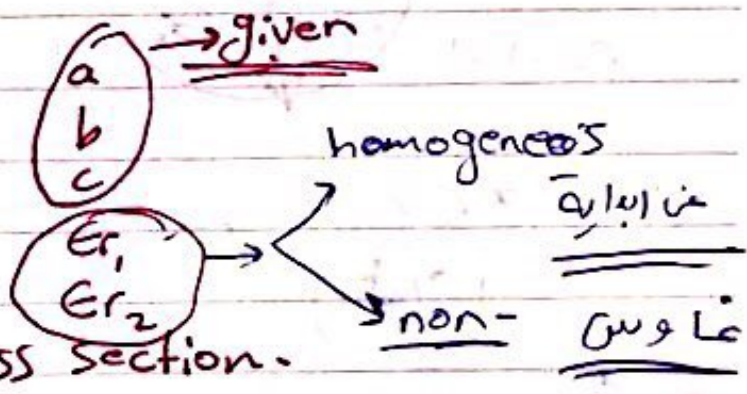
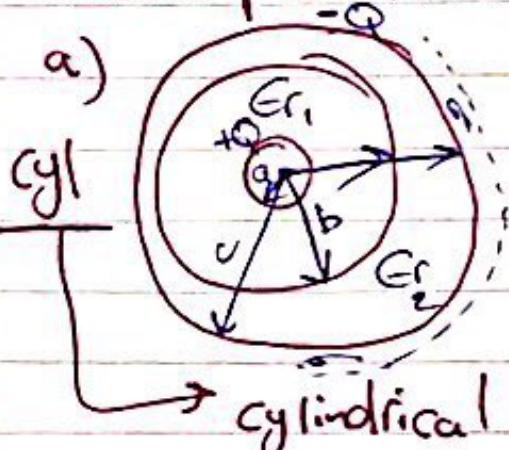
$$V(\phi = \frac{\pi}{4}) = V_0$$



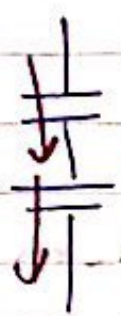
$$\sin(22.5) = \frac{10^{-4}}{2}$$

$$Q = \oint_S \epsilon \vec{E} \cdot d\vec{s} = \int_0^{\phi} \int_x^{x+1} \epsilon E_{\phi} \hat{a}_{\phi} d\rho dz d\phi$$

\* example: find the capacitance of the following

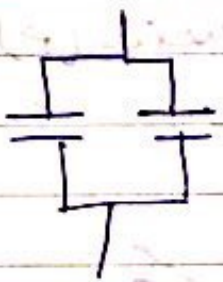


cylindrical cross section.



$$C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$$

في الحالة فوق قطع ال capacitor  
① + capacitor ②  
So series.

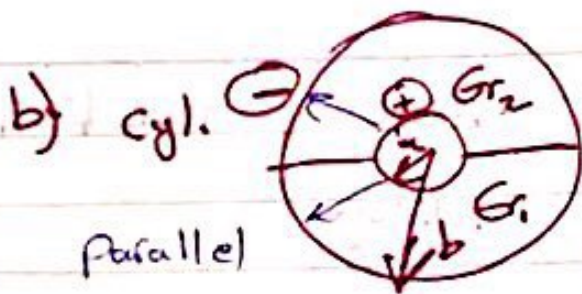


$$C_{eq} = C_1 + C_2$$

$$C = \frac{2\pi \epsilon f}{\ln\left(\frac{b}{a}\right)}$$

$$\rightarrow C_1 = \frac{2\pi \epsilon_c \epsilon_{r1} f}{\ln\left(\frac{b}{a}\right)} \text{ (f)}$$

$$\rightarrow C_2 = \frac{2\pi \epsilon_c \epsilon_{r2} f}{\ln\left(\frac{c}{b}\right)}$$



$$C_1 = \frac{\pi \epsilon_0 \epsilon_1 l}{\ln\left(\frac{b}{a}\right)} \text{ (F)}$$

$$C_2 = \frac{\pi \epsilon_0 \epsilon_2 l}{\ln\left(\frac{b}{a}\right)} \text{ (F)}$$

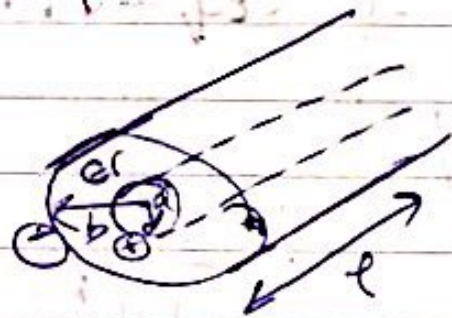
\*example: A coaxial cable has  $a = 1 \text{ cm}$   
 $b = 2.5 \text{ cm}$ , if the dielectric between the  
two conductors has  $\epsilon_r = \frac{10 + P}{P}$ , where  $P$   
is in cm.

Find  $C/P$ ?

⇒ Gauss

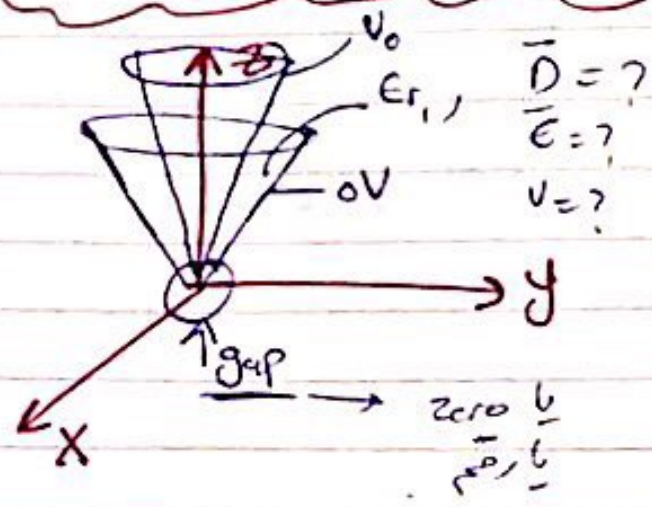
$$\oint \vec{E} \cdot d\vec{s} = Q$$

$$\int_0^l \int_0^{2\pi} \epsilon_0 \epsilon_r E_p r dr dz = Q$$

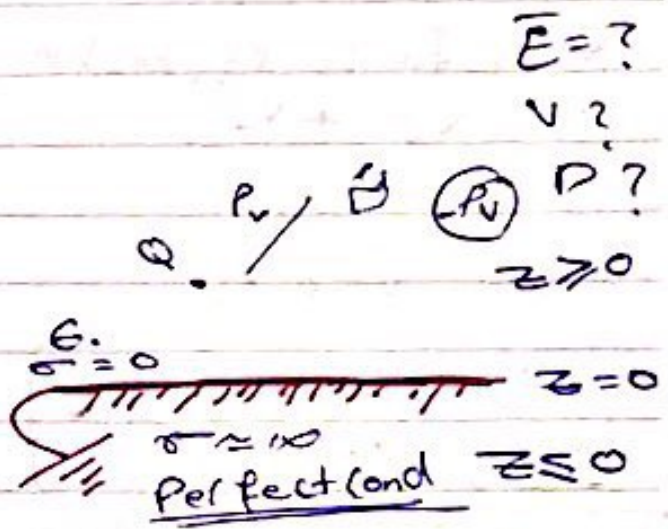


$$\vec{E} = \frac{Q}{2\pi \epsilon_0 \epsilon_r r l} \hat{a}_r \text{ V/m}$$

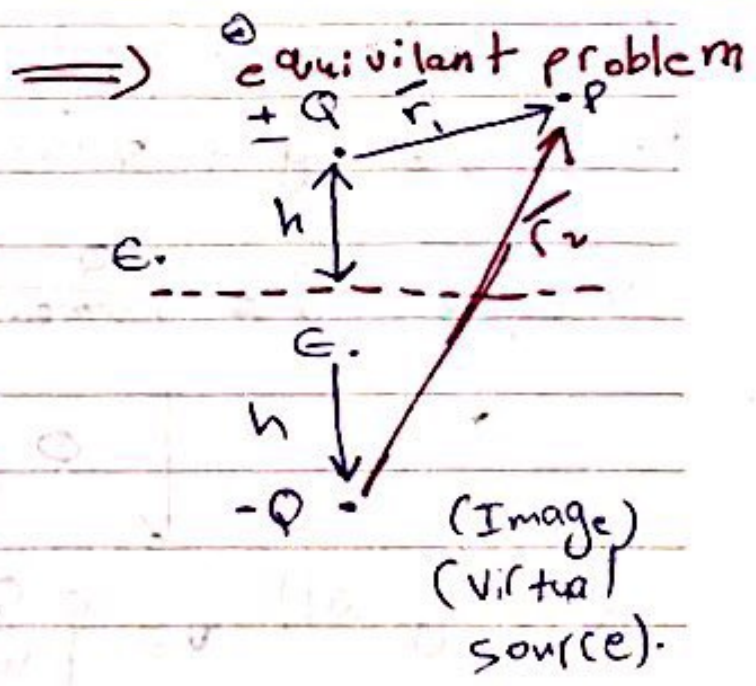
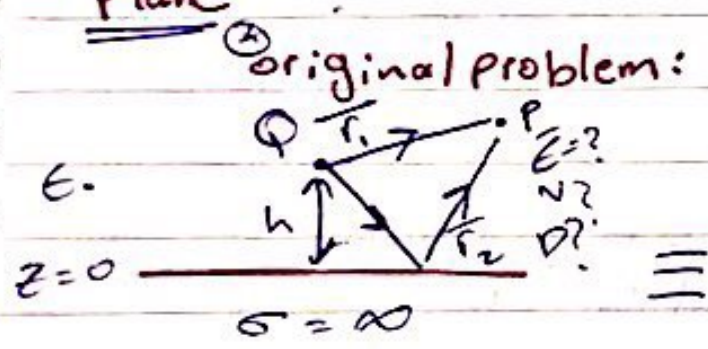
- variation w.r.t  $\Theta$  or  $\phi$  :-



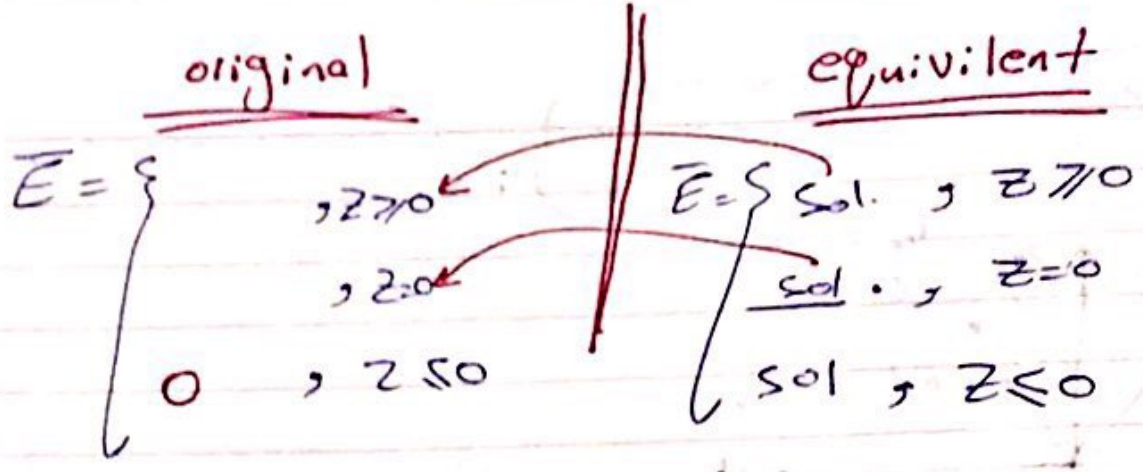
\* Method of Images:  
(electric field  $\vec{E}$ ,  $\vec{D}$ ,  $\vec{V}$   $\equiv$   $\vec{E}$ ,  $\vec{D}$ ,  $\vec{V}$ )



A) Point charge above perfect ground conducting plane







Sol. for the eq. problem

$$V = V_+ + V_-$$

$$= \frac{Q}{4\pi\epsilon \cdot r_1} + \frac{-Q}{4\pi\epsilon \cdot r_2}$$

$$= \frac{Q}{4\pi\epsilon} \left( \frac{1}{r_1} - \frac{1}{r_2} \right) \quad , z > 0$$

$$r_1 = (x, y, z) - (0, 0, h) = (x, y, z-h)$$

$$r_2 = (x, y, z) - (0, 0, -h) = (x, y, z+h)$$

$$r_1 = \sqrt{x^2 + y^2 + (z-h)^2}$$

$$r_2 = \sqrt{x^2 + y^2 + (z+h)^2}$$

$$V(\text{equivalent}) = \begin{cases} \frac{Q}{4\pi\epsilon} \left( \frac{1}{r_1} - \frac{1}{r_2} \right) , z > 0, z < 0 \\ 0 , z = 0 \end{cases}$$

$$V(\text{original}) \quad V = \begin{cases} \frac{Q}{4\pi\epsilon} \left( \frac{1}{r_1} - \frac{1}{r_2} \right) , z > 0 \\ 0 , z \leq 0 \end{cases}$$

$$\vec{E} = \vec{E}_+ + \vec{E}_-$$

$$= \frac{Q\vec{r}_1}{4\pi\epsilon_0 r_1^3} + \frac{Q\vec{r}_2}{4\pi\epsilon_0 r_2^3}$$

$$= \begin{cases} \frac{Q}{4\pi\epsilon_0} \left( \frac{\vec{r}_1}{r_1^3} - \frac{\vec{r}_2}{r_2^3} \right), & z > 0 \end{cases}$$

$$\begin{cases} \frac{Q}{4\pi\epsilon_0} \frac{(-zh\hat{a}_z)}{(x^2+y^2+h^2)^{\frac{3}{2}}}, & z=0 \end{cases} \quad \text{En}$$

$$0, \quad z < 0$$

$$\vec{D} = \epsilon_0 \cdot \vec{E}$$

$$P_s = \vec{D} \cdot \hat{a}_n$$



$$= -\frac{Qh}{2\pi\epsilon_0 (x^2+y^2+h^2)^{\frac{3}{2}}} \quad \text{C/m}^2$$

$Q_i \equiv$  induced charge

$$Q_i = \int_s P_s ds = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} P_s dx dy$$

convert to cyl ( $z$ ) is common

$$ds = \rho d\tau d\phi$$

$$x^2 + y^2 = \rho^2$$

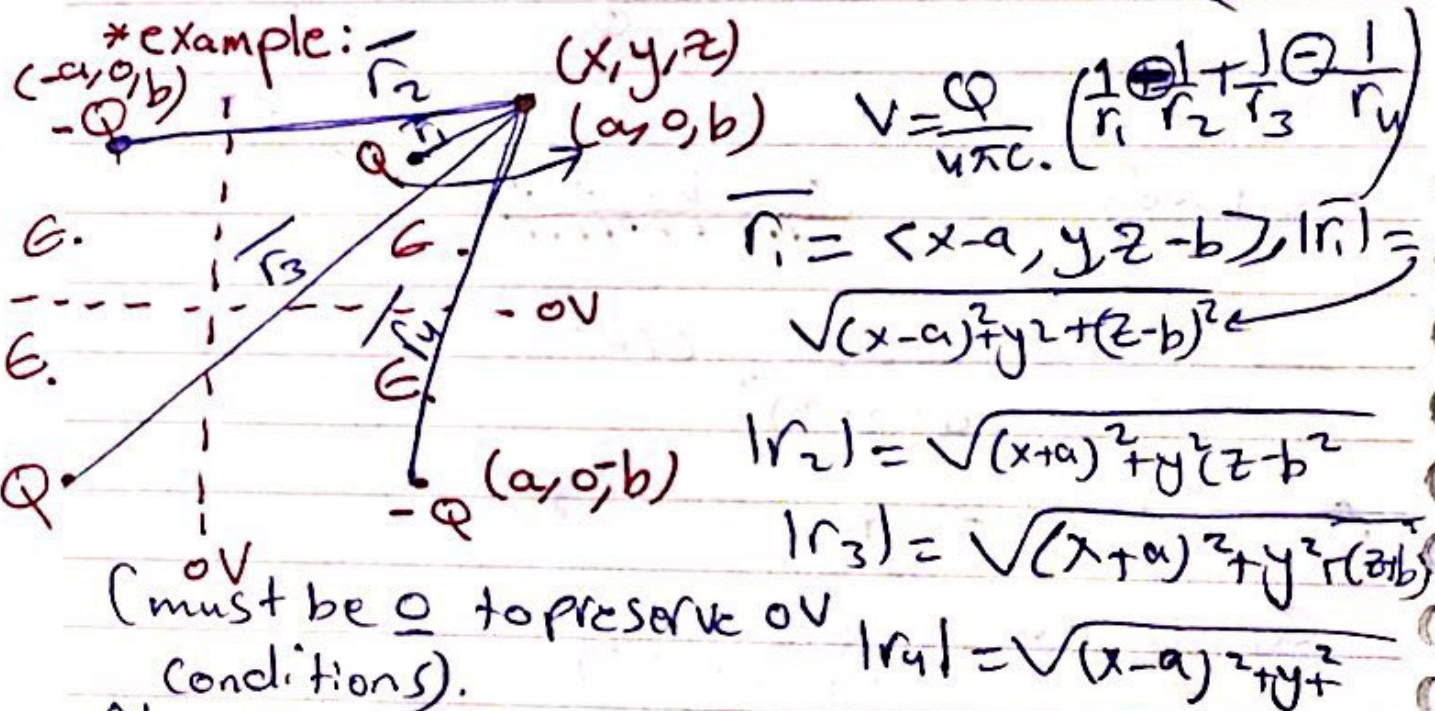
$$Q_i = \int_0^{2\pi} \int_0^{\infty} \frac{-hQ}{2\pi\epsilon_0 (\rho^2+h^2)^{\frac{3}{2}}} \rho d\rho d\phi$$

$$\text{let } \rho^2 + h^2 = u \rightarrow \rho d\rho = \frac{du}{2}$$

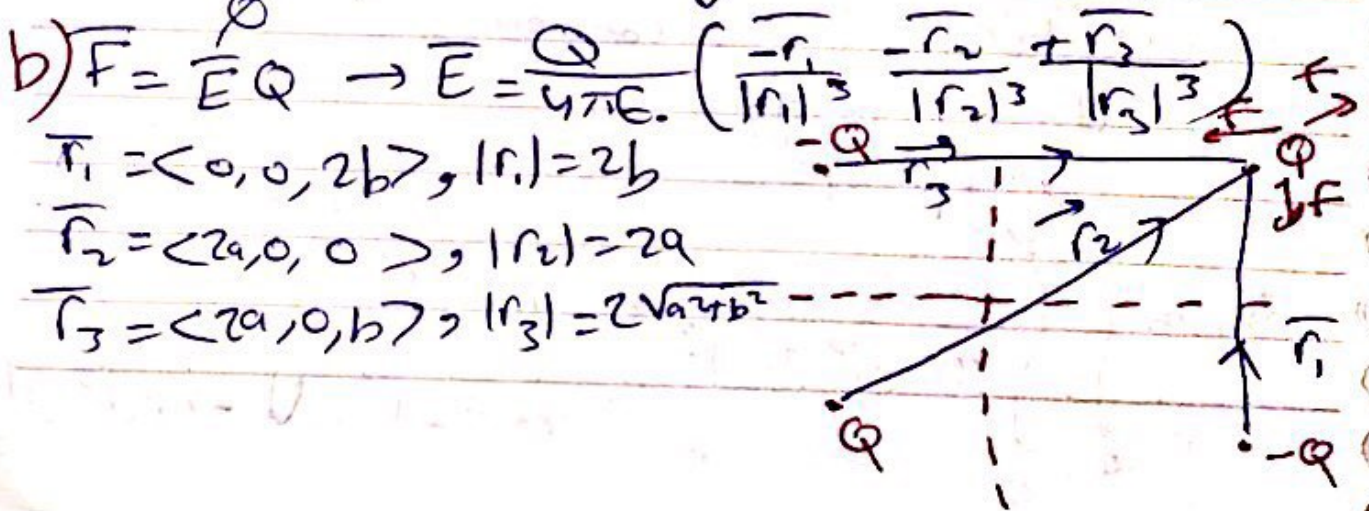
$$\Phi_i = \frac{-kQ}{(z)} \int \frac{dd}{u^{\frac{3}{2}}}$$

$$\Phi_i = \frac{+kQ}{z} \frac{u^{-\frac{1}{2}}}{\frac{1}{z}}$$

$$\Phi_i = kQ * \frac{1}{\sqrt{p^2 + u^2}} \Big|_0^\infty = kQ \left( 0 - \frac{1}{u} \right) = -Q$$



$$N = \frac{360}{\phi} \neq -1 = 3 \text{ images}$$



# \* Chapter 7 :

Duality :

Electrostatic

$$E \equiv V/m$$

$$D \equiv C/m^2$$

$$\epsilon \equiv F/m$$

$$D = \epsilon \cdot \bar{E}$$

$$\bar{E} = -\nabla V$$

$$W_E = \frac{1}{2} \int_V \bar{E} \cdot \bar{D} \, dV$$

MegretoStatic

$H \rightarrow$  Magnetic field intensity

$$H \equiv A/m$$

$B \rightarrow$  Magnetic flux density

$$B \equiv Wb/m^2 \text{ or } (T)$$

$$\mu_0 = 10^{-12} T$$

$M \equiv$  Permeability (H/m)

$$B = \mu H$$

$$\bar{H} = -\nabla \psi/m$$

$$W_M = \frac{1}{2} \int_V \bar{H} \cdot \bar{B} \, dV$$

$$\gamma = \oint_S \bar{D} \cdot d\bar{s} \rightarrow \gamma = \oint_S \bar{B} \cdot d\bar{s}$$

Gauss law

$\rightarrow$  Sources for magnetostatic :-

1) permanent magnet (Neoduminium Nd).

2) Charge moving with constant velocity.

(uniform)  $\Rightarrow$  0 acceleration

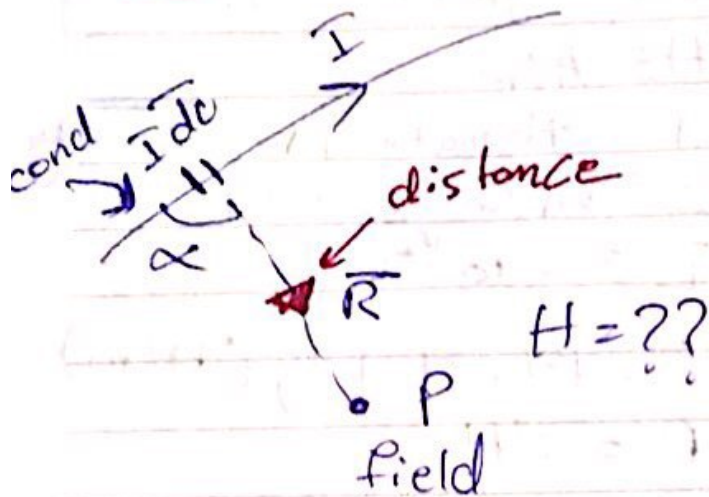
3) DC current flowing in the wire-



\* Major laws:

- 1 → Biot-Savart's law:
- 2 → Ampere's

1 Biot-Savart's law: by exp



$$dH \propto \frac{Idl \cdot \sin \alpha}{R^2} \rightarrow \int dH = \int \frac{\mu_0 I dl \sin \alpha}{4\pi R^2}$$

$$\mu_0 = \frac{1}{\epsilon_0 \epsilon_r}$$

$$H = \int \frac{I dl \sin \alpha}{4\pi R^2} \equiv A/m$$

magnitude only.

→ to find the direction:-

$$I dl \sin \alpha = |I dl \times \hat{r}|$$

$$\vec{H} = \int \frac{I dl \times \hat{r}}{4\pi R^2} \rightarrow \vec{E} = \int \frac{\rho dv}{4\pi \epsilon_0 R^2}$$

Any 1-D segment,

$$= \int_L \frac{I d\vec{L} \times \vec{R}}{4\pi R^3}, \quad d\vec{L} = dl \hat{a}_L$$

\* note that:

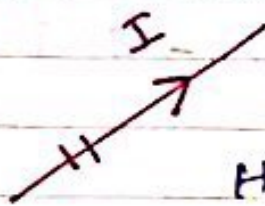
$$\vec{A} \times \vec{B} = |\vec{A}| |\vec{B}| \sin \theta$$

$$\vec{A} \times \vec{B} = -\vec{B} \times \vec{A}$$

$$\vec{H} = \int_L \frac{I \hat{a}_L \times \vec{R}}{4\pi R^3} dL$$

\* current distribution:-

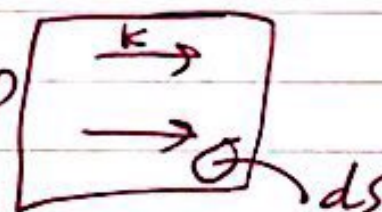
① line current.



$$I dL \equiv A \cdot m$$

$$H = \int_L \frac{I d\vec{L} \times \vec{R}}{4\pi R^3}$$

② surface current:

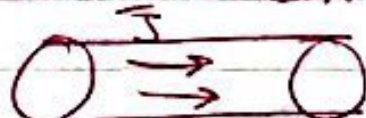


$$\vec{k} ds \equiv A \cdot m$$

$$L, m^2$$

$$\vec{H} = \int_S \frac{\vec{k} ds \times \vec{R}}{4\pi R^3} \equiv A/m$$

③ volume current distribution:



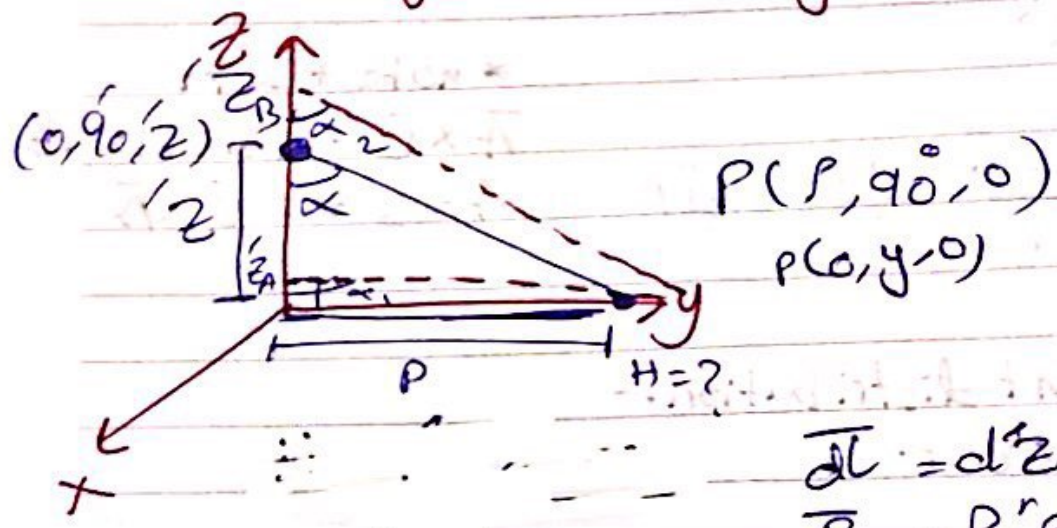
$$\vec{J} dv \equiv A \cdot m$$

$$L, m^3$$

$$\rightarrow A/m^2$$

$$\vec{H} = \int_V \frac{\vec{J} dv \times \vec{R}}{4\pi R^3}$$

\* example: find  $\vec{H}$  due to straight finite wire along  $-z$  axis carry  $I$ .



$$d\vec{l} = dz \hat{z}$$

$$\vec{R} = p\hat{x} - z\hat{z}$$

$$\vec{H} = \int \frac{I d\vec{l} \times \vec{R}}{4\pi R^3}$$

$$\vec{H} = \frac{I}{4\pi} \int_{z_A}^{z_B} \frac{dz \hat{z} \times (p\hat{x} - z\hat{z})}{(p^2 + z^2)^{3/2}}$$

$$H = \frac{I}{4\pi} \int_{z_A}^{z_B} \frac{p dz \hat{\phi}}{(p^2 + z^2)^{3/2}}$$

$$\sin \alpha = \frac{p}{R}$$

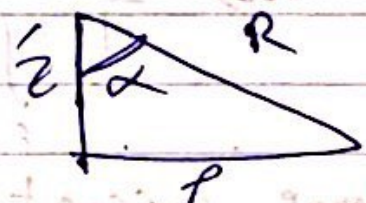
$$\cos \alpha = \frac{z}{R}$$

$$\tan \alpha = \frac{p}{z} \rightarrow z = p \cot \alpha$$

$$R^2 = p^2 + z^2 = p^2 + p^2 \cot^2 \alpha$$

$$R^2 = p^2 \csc^2 \alpha$$

$$R^3 = p^3 \csc^3 \alpha$$



$$H = \frac{I}{4\pi r} \int_{\alpha_1}^{\alpha_2} \frac{r^2}{r^2 \csc^3 \alpha} (-r \csc^2 \alpha d\alpha) \hat{a}_\phi$$

$$H = \frac{I}{4\pi r} \int_{\alpha_1}^{\alpha_2} -\sin \alpha d\alpha \hat{a}_\phi$$

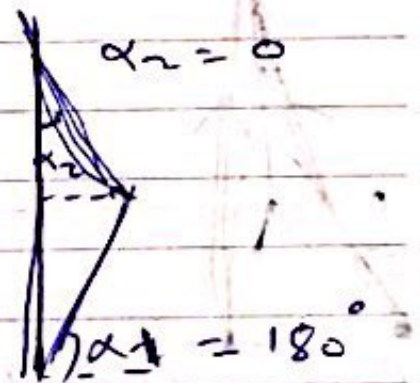
$$H = \frac{I}{4\pi r} (\cos \alpha_2 - \cos \alpha_1) \hat{a}_\phi$$

→ for any finite straight wire.

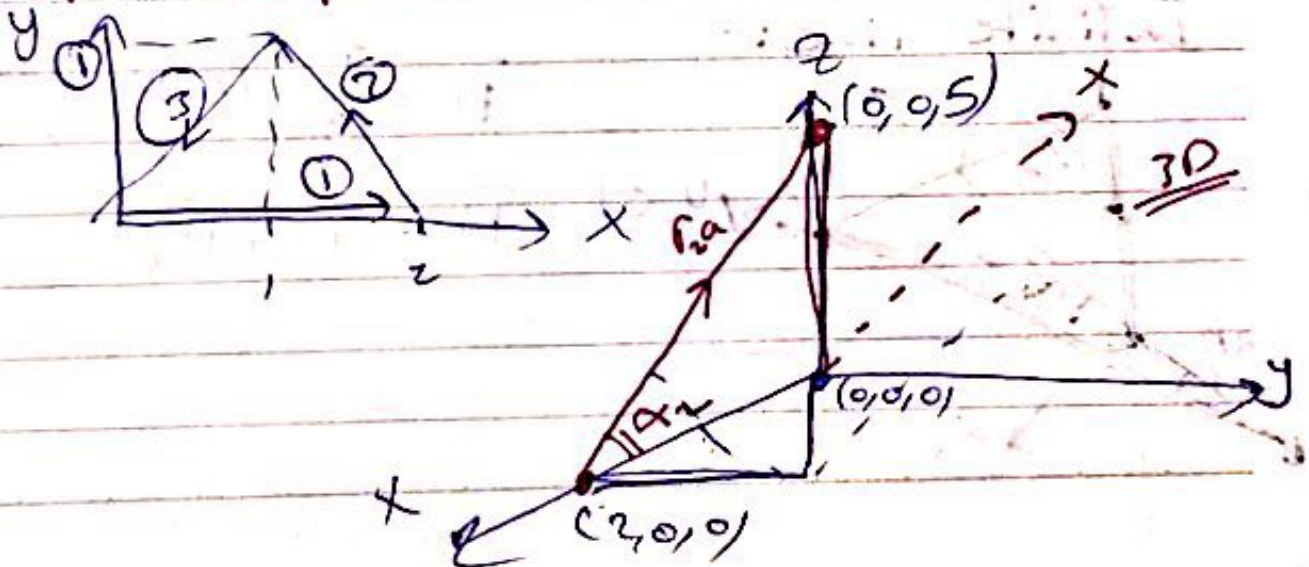
$$\hat{a}_\phi = \hat{a}_L \times \hat{a}_r$$

for an infinite line:-

$$\boxed{H = \frac{I}{2\pi r}} \Rightarrow \text{always}$$



→ example: find  $H$  at  $(0,0,5)$  due to side ① of the loop.





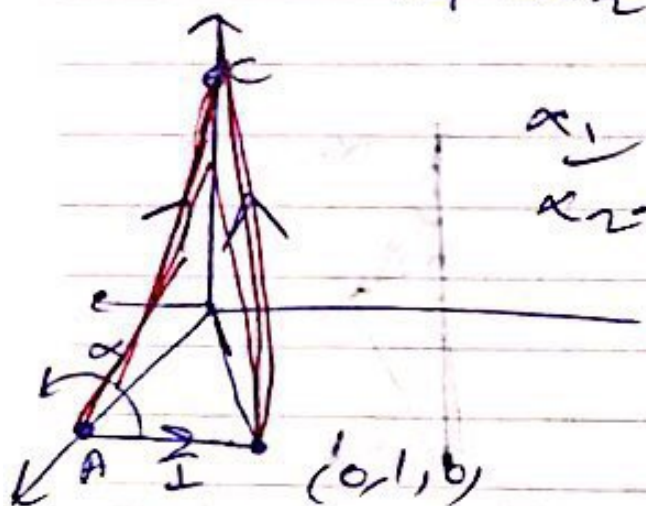
$$H = \frac{I}{4\pi P} (\cos\alpha_2 - \cos\alpha_1) \hat{a}_\phi$$

$$\begin{cases} P=5 \\ \alpha_1 = 20^\circ \\ \alpha_2 \rightarrow \cos\alpha_2 = \frac{2}{\sqrt{29}} \end{cases}$$

$$\begin{aligned} \hat{a}_\phi &= \hat{a}_L \times \hat{a}_P \\ &= \hat{a}_x \times \hat{a}_z \\ &= -\hat{a}_y \end{aligned}$$

$$H = -59 \cdot 1 \hat{a}_y \text{ mA/m}$$

$$\theta_1 + \alpha_2 = 120^\circ$$



$\alpha_1$   
 $\alpha_2$

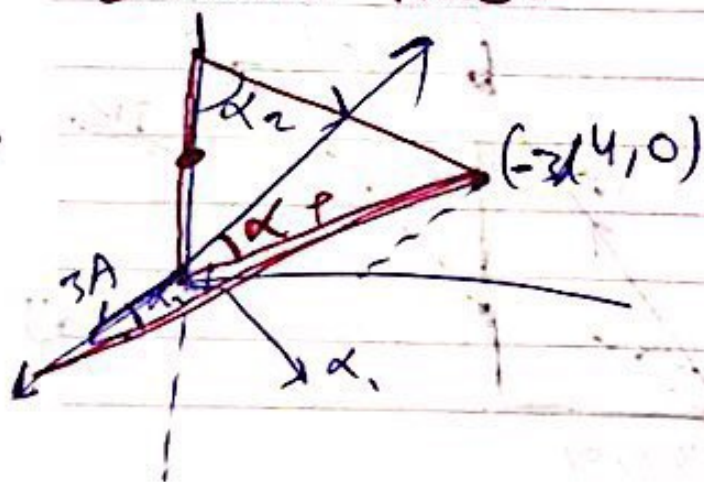
$$\overline{BA} \cdot \overline{BC} = |\overline{BA}| |\overline{BC}| \cos\alpha_2$$

$$\overline{AB} \cdot \overline{AC} = |\overline{AB}| |\overline{AC}| \cos\alpha_1$$

$$\cos\alpha_1 = -\cos\theta_1$$

\* example: find  $\overline{H}$  at  $(-3, 4, 0)$

Infinite line:-



$$\overline{H} = \frac{I}{4\pi P} (\cos\alpha_2 - \cos\alpha_1) \hat{a}_\phi$$

$$\overline{H} = \overline{H}_1 + \overline{H}_2$$

for line 1: -

$$P^2 = (-3, 4, 0) \rightarrow P = 5$$

$$\alpha_1 = 90$$

$$\alpha_2 = 0$$

$$a\phi = a_1 \times a_2 \\ = -\hat{a}_2 \times \frac{(-3, 4, 0)}{5}$$

$$\frac{3}{5} \hat{a}_y + \frac{4}{5} \hat{a}_x$$

$$\vec{H}_1 = \frac{I}{4\pi r P} a\phi = 32.2 \hat{a}_x + 28.65 \hat{a}_y \text{ mA/m}$$

for line 2:

$$P = 4$$

$$\alpha_2 = 0$$

$$\cos \alpha_1 = \frac{-3}{5}$$

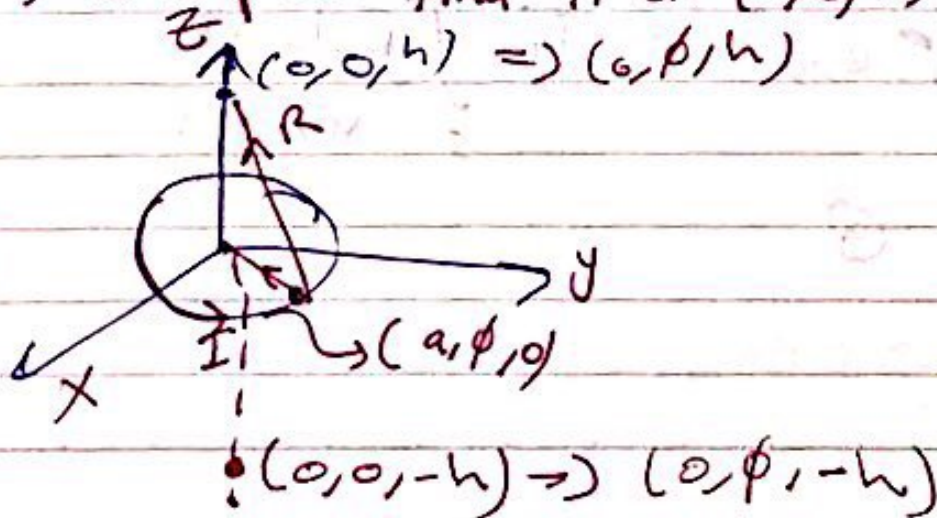
$$a\phi = \hat{a}_1 \times \hat{a}_2$$

$$= \hat{a}_x \times \hat{a}_y = \hat{a}_z$$

$$\vec{H}_2 = \frac{I}{4\pi r P} \left(\frac{3}{5}\right) a\phi$$

$$H_2 = 23.88 \hat{a}_z \text{ mA/m.}$$

\* example: find  $\vec{H}$  at  $(0, 0, h)$



$$H = \int \frac{I d\vec{l} \times \vec{R}}{4\pi R^3}$$

$$d\vec{l} = R d\phi \hat{a}_\phi = a d\phi$$

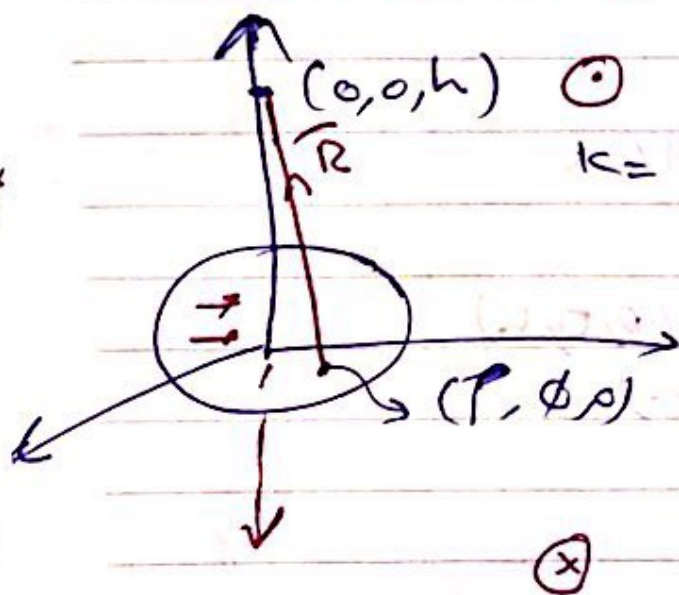
$$\vec{R} = -a \hat{a}_\rho + h \hat{a}_z$$

$$H = \frac{Ia}{4\pi} \int_0^{2\pi} \frac{\hat{a}_\phi \times (-a \hat{a}_\rho + h \hat{a}_z) d\phi}{(a^2 + h^2)^{3/2}}$$

$$H = \frac{Ia^2}{4\pi} \int_0^{2\pi} \frac{(\hat{a}_z + h \hat{a}_\rho) d\phi}{(a^2 + h^2)^{3/2}}$$

$$H = \frac{Ia^2}{2(m^2 + h^2)^{3/2}} \hat{a}_z \quad \text{A/m}$$

$\vec{H}$  for an infinite sheet.



$$\vec{H} = \int_S \frac{K d\vec{s} \times \vec{R}}{4\pi R^3}$$

~~$ds = \rho d\ell \times \hat{R}$~~   
 ~~$\frac{1}{R^2}$~~

$ds = \rho d\ell d\phi$   
 $\hat{R} = -\rho \hat{a}_\rho + h \hat{a}_z$   
 $R = \sqrt{\rho^2 + h^2}$

$\frac{h}{\sqrt{\pi}} \int_0^{2\pi} \int_0^{\alpha} \frac{\hat{a}_\phi \times (-\rho \hat{a}_\rho + h \hat{a}_z)}{(\rho^2 + h^2)^{\frac{3}{2}}} \rho d\rho d\phi$

**[2] \*\* Ampere's law: -**

$\oint \vec{H} \cdot d\vec{L} = I_{\text{enclosed}}$

\* 3rd maxwell's eq. in integral form.



\* Apply Stokes's theorem: -

$\oint \vec{H} \cdot d\vec{L} = \int \nabla \times \vec{H} \cdot d\vec{s} = I_{\text{enclosed}} = \int \vec{J} \cdot d\vec{s}$

\*  $\nabla \times \vec{H} = \vec{J}$   
 → 3rd maxwell's eq in diff form.

**[2] Duality:**

1  $\oint \vec{D} \cdot d\vec{s} = Q_{\text{enc}} \rightarrow \oint \vec{B} \cdot d\vec{s} = 0$

2  $\oint \vec{E} \cdot d\vec{L} = 0 \rightarrow \oint \vec{H} \cdot d\vec{L} = I_{\text{enclosed}}$

\* 4th maxwell's eq. in integral form.

\* Application on Ampere's law: -

1)  $\vec{H}$  due to an inf line of current

$$\oint_L \vec{H} \cdot d\vec{L} = I_{enc} = I$$

R.H.R  $\rightarrow \vec{H} = H_\phi \hat{a}_\phi$

$$d\vec{L} = \rho d\phi \hat{a}_\rho$$

$\hookrightarrow$  Amperian path

$$\int_0^{2\pi} H_\phi \rho d\phi = I$$

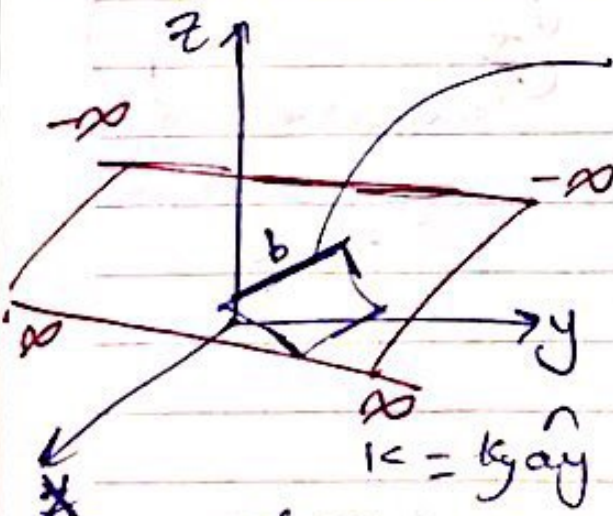
$$\Rightarrow 2\pi \rho H_\phi = I$$

$$\vec{H} = \frac{I}{2\pi \rho} \hat{a}_\phi$$



2)  $\vec{H}$  for an inf sheet of current.

$\hookrightarrow$   $z$  plane (Amperian path  $\perp y$ )



$$\oint_L \vec{H} \cdot d\vec{L} = I_{enc}$$

$$\text{R.H.R} \rightarrow \vec{H} = \begin{cases} H(\hat{a}_x), & z > 0 \\ H(-\hat{a}_x), & z < 0 \end{cases}$$

$$\oint_C \vec{H} \cdot d\vec{L} = \int_{L_1} \vec{H} \cdot d\vec{L}_1 + \int_{L_2} \vec{H} \cdot d\vec{L}_2 + \int_{L_3} d\vec{L}_3 \cdot \vec{H} + \int_{L_4} \vec{H} \cdot d\vec{L}_4$$

$$\int_0^b \vec{H} \cdot \hat{a}_x \cdot dx \hat{a}_x + \int_b^0 \vec{H} \cdot (-\hat{a}_x) \cdot dx \hat{a}_x$$

$$H \cdot b + H \cdot b + k_y \cdot b$$

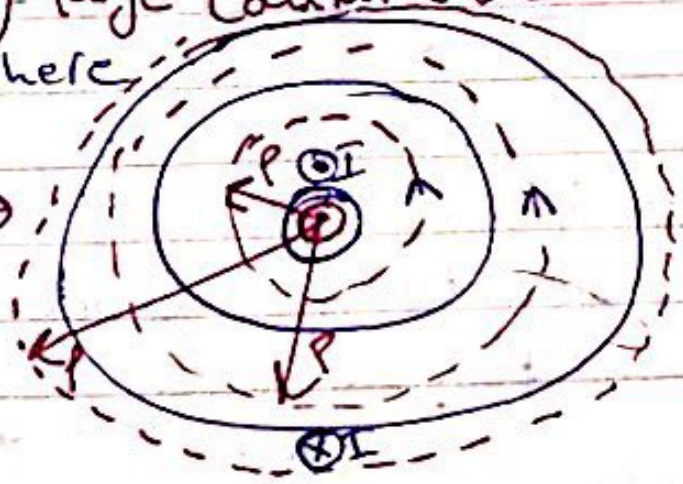
$$H_0 = \frac{k_y}{2} \text{ A/m}$$

$$H = \begin{cases} k_y (\hat{a}_x), & z > 0 \\ \frac{k_y}{2} (-\hat{a}_x), & z < 0 \end{cases}$$

(\*) In general  
 $\vec{H} = \frac{1}{2} \vec{T}_c \times \hat{a}_n$   
 in this example.  
 $= \frac{1}{2} k \hat{a}_x$   
 $\frac{1}{2} k \hat{a}_y \times -\hat{a}_z$   
 $= \frac{1}{2} k \hat{a}_x$

[3] For an infinitely large coaxial cable:-  
 - find  $\vec{H}$  everywhere

Ampere's path →



by R.H.R

$$\vec{H} = H_{\phi} \hat{\phi}$$

$$d\vec{l} = \rho d\phi \hat{\phi}$$

$$\oint_C \vec{H} \cdot d\vec{l} = I_{\text{enclosed}}$$

$\vec{e}_r$  for  $0 < \rho < a$

$$\int_0^{\rho} H_{\phi} \hat{\phi} \cdot \rho d\phi \hat{\phi} = I_{\text{enclosed}}$$

$$2\pi \rho H_{\phi} = I_{\text{enclosed}} = \int \vec{J} \cdot d\vec{s}$$

$$\text{at } \rho = a \rightarrow I_{\text{enclosed}} = \int \vec{J} \cdot d\vec{s}$$

$$I = \int_0^a \int_0^{2\pi} J_z \hat{z} \cdot \rho d\rho d\phi \hat{z}$$

$$I = J_z \pi a^2 \rightarrow J = \frac{I}{\pi a^2} \hat{z} \text{ A/m}^2$$

$$2\pi \rho H_{\phi} = \int_0^{\rho} \int_0^{2\pi} \frac{I}{\pi a^2} \hat{z} \cdot \rho d\rho d\phi \hat{z}$$

$$\vec{H} = \frac{I \rho}{2\pi a^2} \hat{\phi} \text{ (A/m)} \rightarrow \text{for } 0 < \rho \leq a$$

$\rightarrow$  for  $a < \rho < b$

$$2\pi \rho H_{\phi} = I_{\text{enclosed}} = I$$

$$H = \frac{I}{2\pi \rho} \hat{\phi} \text{ A/m}$$

→ for  $b < P < c$

$$2\pi r H_\phi = I_{enc} = \int \bar{J} \cdot d\bar{s} = \int_0^a \bar{J} \cdot \hat{z} \, d\bar{s} + \int_a^b \bar{J} \cdot d\bar{s} + \int_b^c \bar{J} \cdot d\bar{s}$$

at  $P=c$ :  $I_{enc} = I$

$$I = \int \bar{J} \cdot d\bar{s} = \int_0^c \int_b^c \int_0^{2\pi} J_z (-a\hat{z}) \cdot \rho d\rho d\phi \hat{z}$$

$$I = \int_0^c \int_b^c \int_0^{2\pi} J_z \rho d\rho d\phi$$

$$\bar{J} = \frac{I}{\pi(a^2 - b^2)} (-a\hat{z}) \rightarrow \text{wb. n}$$

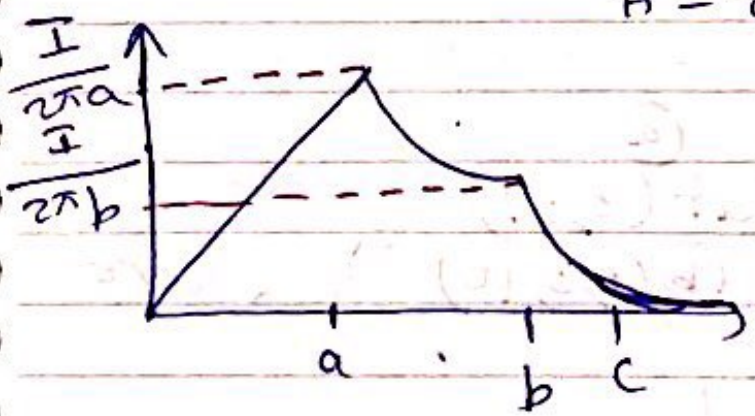
$$2\pi r H_\phi = I - \int_b^c \int_0^{2\pi} \frac{I}{\pi(a^2 - b^2)} \rho d\rho d\phi$$

$$2\pi r H_\phi = I - \frac{I}{\pi(a^2 - b^2)} \times \pi(r^2 - b^2)$$

$$H = \frac{I}{2\pi r} \left(1 - \frac{r^2 - b^2}{a^2 - b^2}\right) \hat{\phi} \quad \text{A/m}$$

↪  $b \leq r \leq c$

→ for  $r > c \Rightarrow 2\pi r H_\phi = I_{enc} = I - I = 0$   
 $H = \text{zero}, r > c$





4 Toroid:-

- find  $\vec{H}$  everywhere.

$H = H_\phi \hat{a}_\phi$   
for  $0 < \rho < a$

$\oint \vec{H} \cdot d\vec{L} = I_{enc}$   
 $= \text{zero}$

$H = \text{zero}$

for  $\rho > a + 2t$

$2\pi \rho H_\phi = I_{enc} = I - I = \text{zero}$

$H = \text{zero}$

→ for  $a < \rho < a + 2t$

$2\pi \rho H_\phi = I_{enc} = NI$

$\uparrow$   
Circuit

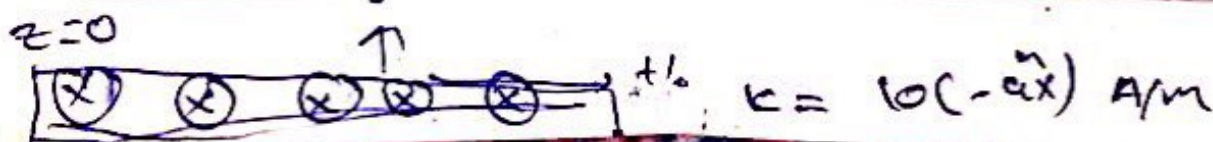
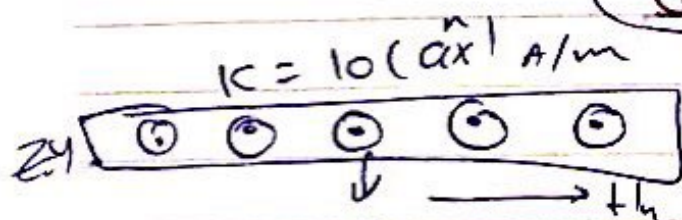
$$\vec{H} = \frac{NI}{2\pi \rho} \hat{a}_\phi \text{ A/m}$$

$H L = NI$

$\oint \vec{H} \cdot d\vec{L} = NI$

\* example: find  $\vec{H}$  at (a)

(b)  $(0,0,10)$  → zero



$$\vec{H} = \frac{1}{2} k a \hat{a}_n$$

$$\text{at } (0,0) \vec{H}_1 = \vec{H}_0 + \vec{H} :-$$

$$= \frac{1}{2} (10(-\hat{a}_x) \times a\hat{z}) + \frac{1}{2} (10(a\hat{y}) \times -a\hat{z})$$

$$= 5a\hat{y} + 5a\hat{y}$$

$$= 10a\hat{y} \text{ (A/m)}$$

\* Magnetic flux density ( $\vec{B}$ ):-

$$\vec{B} = \mu_0 \vec{H} \rightarrow \text{constitutive relation.}$$

$\mu_0 \equiv$  free space permeability

$$= 4\pi \times 10^{-7} \text{ H/m}$$

$$\rightarrow \text{unit: } \frac{\text{H}}{\text{m}} \cdot \frac{\text{A}}{\text{m}} = \frac{\text{H A}}{\text{m}^2}$$

$$\text{or } \frac{\text{Wb}}{\text{m}^2}, \text{ Wb} = \text{weber}$$

or T

$$\text{or } 1 \text{ T} = 10^{-5} \text{ T (old unit)}$$

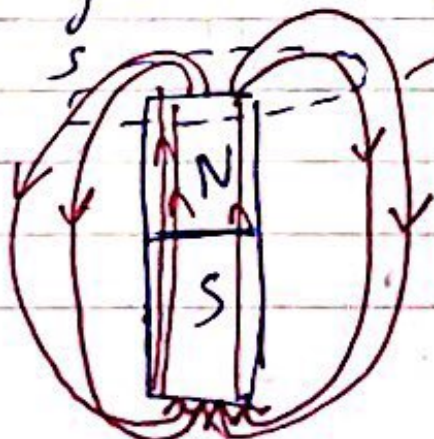
\* Magnetic flux ( $\Psi_m$ ): - (scalar)

$$\Psi = \int \vec{B} \cdot d\vec{s} \neq \text{zero}$$

$$\Psi = \oint \vec{B} \cdot d\vec{s} = 0$$

magnetic Gauss law

Magnetic flux lines



$$\Psi_e = \int \vec{D} \cdot d\vec{s}$$

$$\Psi_e = \oint \vec{D} \cdot d\vec{s} = Q_{enc}$$

Gauss law.

$$\oint \vec{B} \cdot d\vec{s} = \text{zero}$$

↳ 4th Maxwell's eq. in integral form

Apply divergence thm.

$$\oint \vec{B} \cdot d\vec{s} = \int \nabla \cdot \vec{B} dV = \text{zero}$$

↳  $\nabla \cdot \vec{B} = \text{zero}$   
 ↳ 4th Maxwell's eq. in diff form

**\*\* Magnetic potential :-**

↳ ~~Scalar~~ :  $V_m$  (CA)

↳ vector :  $\vec{A}$  ( $\text{wb/m}$ )

we know:

↳ 4th Maxwell eq.  
 $\nabla \cdot \vec{B} = 0$   
 $\nabla \times \vec{H} = \vec{J}$   
 ↳ 3rd Maxwell eq.

So

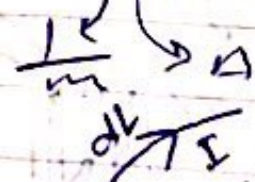
$$\vec{B} = \nabla \times \vec{A}, \quad \vec{H} = \frac{\vec{B}}{\mu_0}$$

$$\frac{\text{wb}}{\text{m}^2} \quad \frac{1}{\text{m}} \quad \left( \frac{\text{wb}}{\text{m}} \right)$$

(magnetic flux density)

$$\vec{H} = -\nabla V_m \equiv \vec{E} = -\nabla V$$

if  $\vec{J} = \text{zero}$  → since free region



What is  $\vec{A}$  :-

$$\vec{B} = \int \frac{\mu_0 I d\vec{L} \times \vec{r}}{4\pi r^3}$$

$$\frac{\vec{r}}{r^3} = \frac{\nabla}{r^2} = \nabla \times \left( \frac{1}{r} \right)$$

$$B = \frac{\mu_0 I}{4\pi} \int dL \times \nabla \left( \frac{1}{R} \right)$$

Identity:

\* Apply the vector Identity:

$$\nabla \times (f \bar{A}) = f \nabla \times \bar{A} + \nabla f \times \bar{A}$$

$$f = \frac{1}{R} = \bar{A} \equiv dL$$

$$B = \frac{\mu_0 I}{4\pi} \int \nabla \times \frac{dL}{R}$$

$$\bar{B} = \nabla \times \left[ \frac{\mu_0 I dL}{4\pi R} \right]$$

$$\boxed{\bar{B} = \nabla \times \bar{A}}$$

So  $\rightarrow \bar{A} = \int \frac{\mu_0 I dL}{4\pi R} \rightarrow \text{line}$

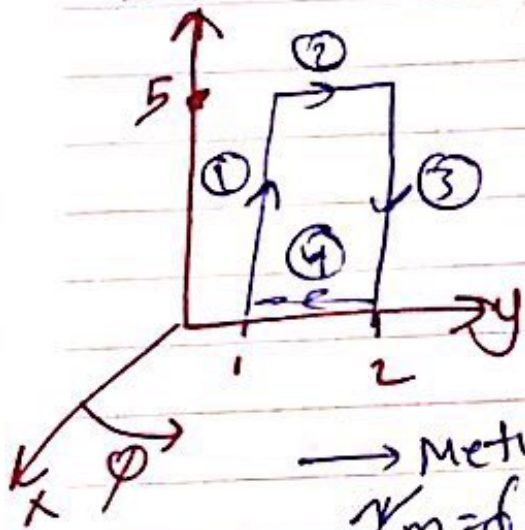
$\bar{A} = \int \frac{\mu_0 I dS}{4\pi R} \rightarrow \text{surface}$

$\bar{A} = \int \frac{\mu_0 I dV}{4\pi R} \rightarrow \text{Volume}$

$$\gamma_m = \int_S \bar{B} \cdot d\bar{s} = \int_S \nabla \times \bar{A} \cdot d\bar{s}, \quad B = \nabla \times \bar{A}$$

$$\gamma_m = \oint_S \bar{A} \cdot d\bar{L} \quad \leftarrow \text{Stokes}$$

\* example: Given  $\vec{A} = \frac{\rho^2}{4} \hat{z}$  w/m  
 Calculate the magnetic flux crossing the surface  $\phi = \frac{\pi}{2}$ ,  $1 \leq \rho \leq 2$  m,  $0 \leq z \leq 5$  m.



$$\begin{aligned} d\vec{L}_1 &= dz \hat{a}_z \\ d\vec{L}_2 &= d\rho \hat{a}_\rho \\ d\vec{L}_3 &= dz \hat{a}_z \\ d\vec{L}_4 &= d\rho \hat{a}_\rho \end{aligned}$$

→ Method 1

$$\Psi_m = \oint \vec{A} \cdot d\vec{L}$$

$$\Psi_m = \int_{L_1} \vec{A} \cdot d\vec{L}_1 + \int_{L_2} \vec{A} \cdot d\vec{L}_2 + \int_{L_3} \vec{A} \cdot d\vec{L}_3 + \int_{L_4} \vec{A} \cdot d\vec{L}_4$$

$$\Psi_m = \int_0^5 \frac{-\rho^2}{4} dz + \int_1^2 \frac{-\rho^2}{4} dz$$

$$\boxed{\Psi_m = \frac{15}{4} \text{ W}_b}$$

→ Method 2:

$$\Psi_m = \int \vec{B} \cdot d\vec{s} \rightarrow ds = d\rho dz \hat{a}_\phi$$

$$\vec{B} = \nabla \times \vec{A} = \frac{1}{\rho} \begin{vmatrix} \hat{a}_\rho & \rho \hat{a}_\phi & \hat{a}_z \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ A_\rho & A_\phi & A_z \end{vmatrix}$$

$$= \frac{1}{\rho} (0-0) \hat{a}_\rho - (-\frac{\rho}{z}) \rho \hat{a}_\phi + (0) \hat{a}_z$$

$$= \vec{B} = \frac{\rho}{z} \hat{a}_\phi \Rightarrow \Psi_m = \int_0^5 \int_1^2 \frac{\rho}{z} d\rho dz = \frac{15}{4} \text{ W}_b$$