

# Amplifiers Summary

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# Electronics II

## Summary

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# First Material

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\* Mode of Operations for BJT:

① Forward-active mode  $\begin{cases} \rightarrow BE \text{ forward.} \\ \rightarrow BC \text{ reverse.} \end{cases} \Rightarrow (\text{Amplifier}).$

② Saturation mode  $\begin{cases} \rightarrow BE \rightarrow \text{Forward.} \\ \rightarrow BC \rightarrow \text{Forward.} \end{cases} \Rightarrow (\text{switch}).$

③ Inverse-active mode  $\begin{cases} \rightarrow BE \text{ reverse.} \\ \rightarrow BC \text{ forward.} \end{cases}$

④ Cutoff mode  $\begin{cases} \rightarrow BE \rightarrow \text{Reverse.} \\ \rightarrow BC \rightarrow \text{Reverse.} \end{cases}$

\* How To Find The Mode of Operation:

① Assume forward-active mode: I/p: To find  $I_B$  then  $I_C$   
 $\hookrightarrow$  use  $V_{BE} = 0.7$  &  $I_C = \beta I_B$  O/p: To find  $V_{CE}$

CHECK:  $V_{CE} \stackrel{?}{>} V_{CE(sat)}$   $\begin{cases} \rightarrow \text{if yes (F.W.)} \\ \rightarrow \text{if No (wrong assumption).} \end{cases}$

② Assume Saturation mode:

$\begin{cases} \text{Warning: DO NOT USE } I_C = \beta I_B & \text{I/p: To find } I_B \\ \text{use } V_{CE(sat)} = 0.2 \text{ or } 0.3, V_{BE(sat)} = 0.7 & \text{O/p: To find } I_C \end{cases}$

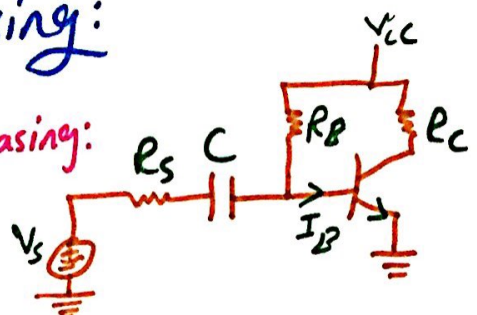
CHECK:  $I_C \stackrel{?}{<} \beta I_B$   $\begin{cases} \rightarrow \text{if yes (sat. mode).} \\ \rightarrow \text{if No (cut off mode).} \Rightarrow I_C = I_B = I_E = \phi \end{cases}$

\* DC-load line: Take output loop to find the relation between  $V_I$  &  $V_{CE}$

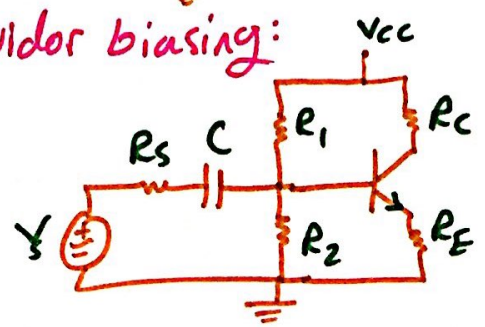
\*  $V_O$  &  $V_I$ : check the effect on transistor ( $V_O$  &  $V_I$ ) in the three modes (FW/sat/cutoff)  
Then draw the graph.

# \* Types of Biasing:

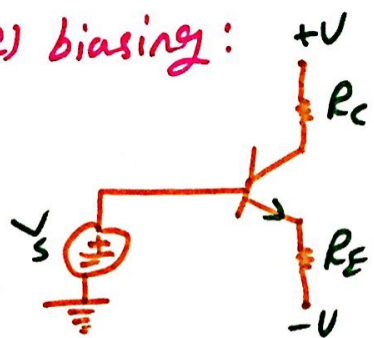
① single base-resistor biasing:



② Voltage divider biasing:



③ (+ve) & (-ve) biasing:



## Disadvantages:

- ①  $R_B$  high value (M $\Omega$ )
- ② Non-stable Q-point.

## Advantages:

- ① stable Q-point.
- ② Low values of resistors.

## Advantages:

- ① stable Q-point.
- ② No need for coupling capacitor.

# \* Amplifier Circuit:

\* To design Amplifier circuit:

- ① the transistor should be FW.
- ② AC signals should be small to get linear amplifier.

\* What does mean Linear amp.?

$$V_o = (\text{constant}) V_i$$

$\downarrow$   
 $> 1$

\* How to get Linear amp?

All components in the amp. ckt. must be linear.

\* What is the way to make transistor linear to get amp ckt? if the AC signals in the amp ckt are small.

see the proves

graphically mathematically

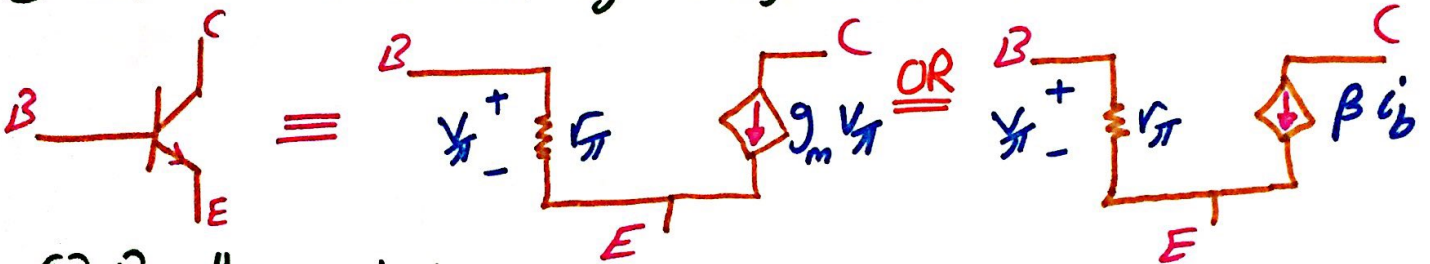
# \* Analysis of Amplifier Circuit:

## \* step 1: DC analysis:

- ① Replace all capacitors by Open Circuit.
- ② Replace all (AC sources) by Short Circuit.
- ③ find  $I_{CQ}$ ,  $I_{BQ}$ ,  $V_{CEQ}$ .

## \* step 2: AC analysis:

- ① Replace all capacitors by short circuit.
- ② Replace all (DC sources) by short circuit.
- ③ Replace the transistor by its Hybrid- $\pi$  model



④ Do the analysis.

$$r_{\pi} = \frac{V_{\pi}}{I_{BQ}} \rightarrow 0.026 \text{ volt.}$$

$$g_m = \frac{I_{CQ}}{V_T}$$

$$\beta = g_m r_{\pi}$$

voltage gain:

$$A_V = \frac{V_o}{V_s}$$

take loops to find  $V_o$  &  $V_s$  as functions of  $(V_{\pi})$ .

current gain:

$$A_i = \frac{i_o}{i_i}$$

To find  $R_i$  &  $R_o$ :

use Thevenin equivalent ckt.

↳ Kill the independent sources & put a voltage test source  $V_x$  with  $I_x$ .

\* Notes:

$i_B, i_c, V_{CE}, v_o \Rightarrow (AC+DC \text{ value})$

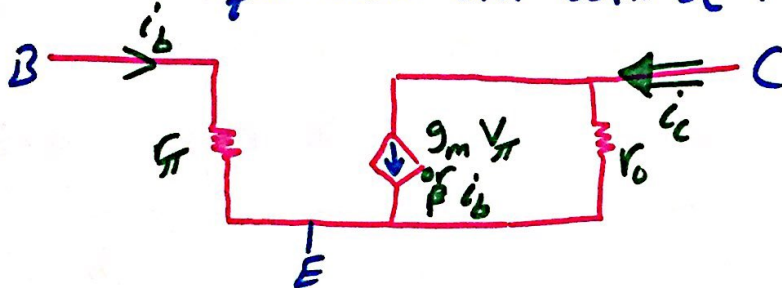
$i_B = i_b + I_{BQ}, i_c = i_c + I_{CQ}, V_{CE} = v_{ce} + V_{CE}, v_o = v_o + V_o$

\* Hybrid- $\pi$  with the early effect:

→ without early effect:  $I_c$  is independent on  $V_{CE}$ .

→ with early effect:  $I_c \propto V_{CE}$  & the junction C-E has resistance called  $r_o$ .

⇒ the equivalent ckt will be :



$r_o = \frac{V_A}{I_{CQ}}$  (high value)  
will be given.

\* So, Now if he say the ckt with early effect

⇒ You must add the part ( $r_o$ ) to the Hybrid- $\pi$  ckt.

\* Note:  $\downarrow \begin{matrix} g_m v_{\pi} \\ \text{or} \\ \beta i_b \end{matrix}$  ⇒ The best use for  $g_m v_{\pi}$  when  $R_E$  is Not existing.  
The best use for  $\beta i_b$  when  $R_E$  is exist.

\* Basic BJT Amp. Configurations:

- Common Collector Amplifier (CC).
- Common Base Amplifier (CB).
- Common Emitter Amplifier (CE).

- Basic CE Amp.
- CE with  $R_E$ .
- CE with  $R_E$  & bypass Capacitor.
- Advanced CE Amp.

# \* Common Emitter Amplifier:

## ① Basic CE Amplifier:

\* **Advantages:** High gain.

\* **Disadvantages:**

① High loading effect due to small  $R_i$  ( $V_i < V_s$ ).

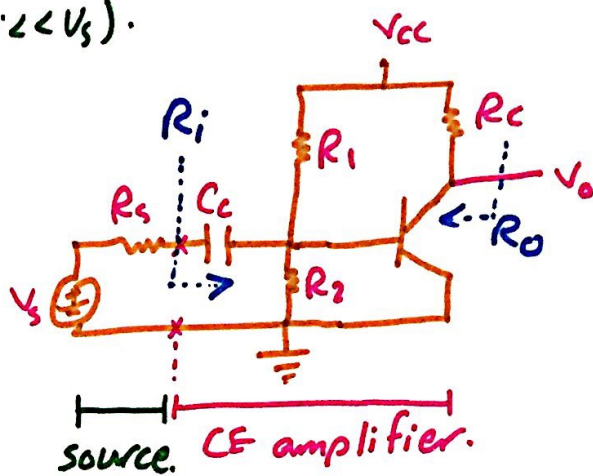
② Highly sensitive to  $V_{BE}$  (i.e.)

$R_s$ : internal resistance of the source.

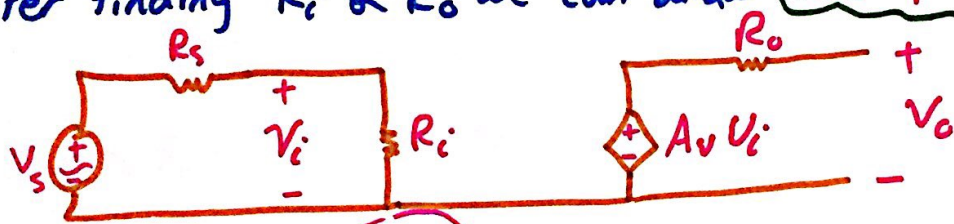
$C_c$ : coupling capacitor.

↳ it is used before & after the amplifier ckt. (why)?

To block any DC component from the user that may change the position of the Q-point (change the mode of operation).



\* After finding  $R_i$  &  $R_o$  we can draw **Two-port equivalent ckt.**



$$V_i = V_s \frac{R_i}{R_i + R_s}$$

This value represents: "Loading effect"

\* To reduce loading effect: need high  $R_i$  & small  $R_o$

\* To have a good voltage Amp. ckt: ① High  $R_i$  ② small  $R_o$  ③ High  $A_v$

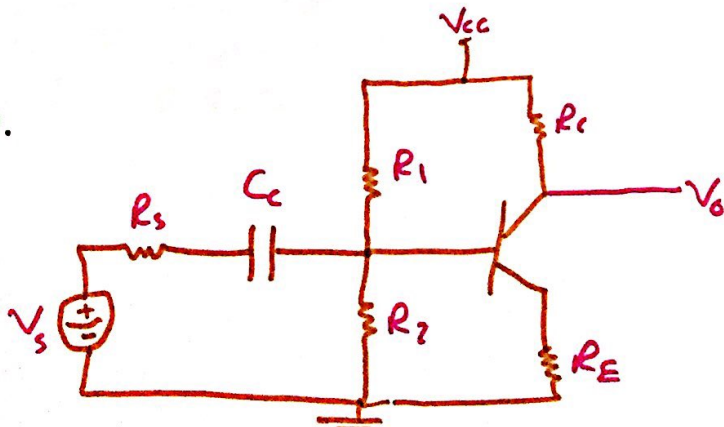
## ② CE with $R_E$ :

\* **Advantages:**

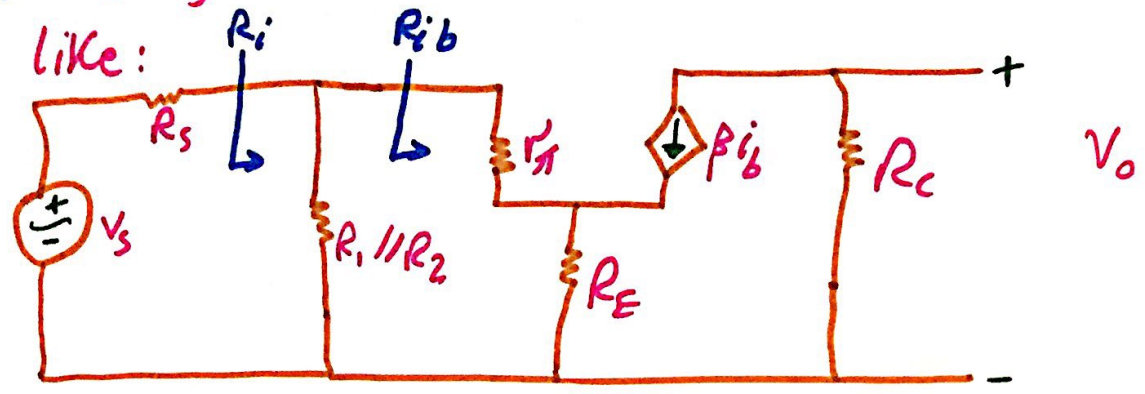
- ① small loading effect.
- ② stable Q-point (less sensitive to  $\beta$ ).

\* **Disadvantages:**

small gain.



⇒ Notice that: The hybrid- $\pi$  for CE with  $R_E$  would be like:



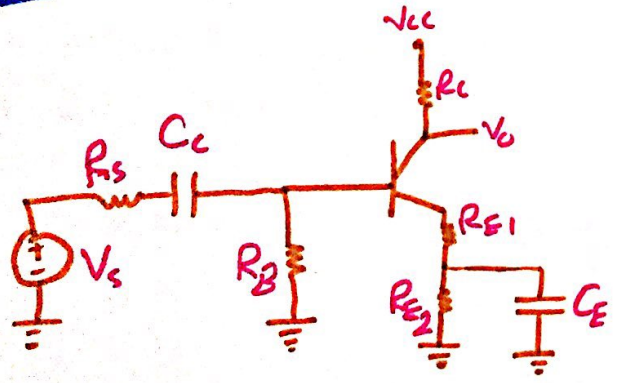
⇒ Also for this type of circuits for finding the voltage gain you can simply use the following relation:

$$A_v = -\frac{R_c}{R_E} \quad \text{***}$$

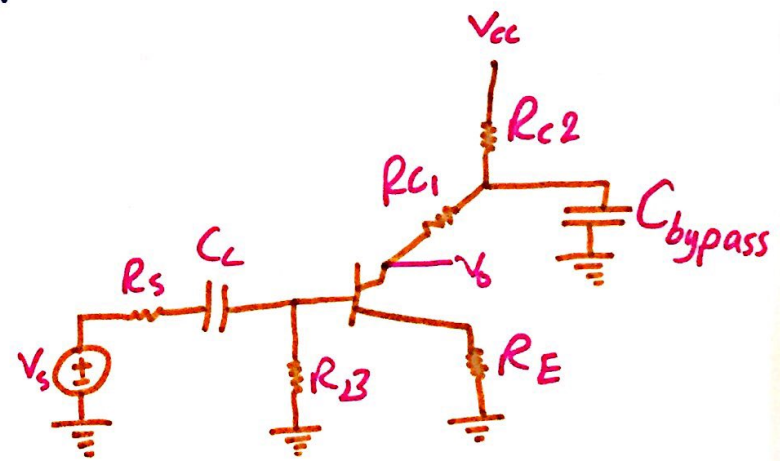
\* Note: Finding  $R_{ib}$  then find  $R_i$  will be the easiest way to solve.

\* stability rule:  $R_{th} = 0.1(1+\beta)R_E$  \*\*\*

3 CE with  $R_E$  & bypass capacitor:



OR



$C_E$ : Bypass Capacitor.

↳ What is the advantage of  $C_E$ ?

AC requirement, need  $R_E$  small  
 DC " " , need  $R_E$  high } ⇒

so, bypass capacitor simplifies the design process (satisfies AC & DC requirements)

\* AC req.: (i.e)  $A_v, R_i \dots$

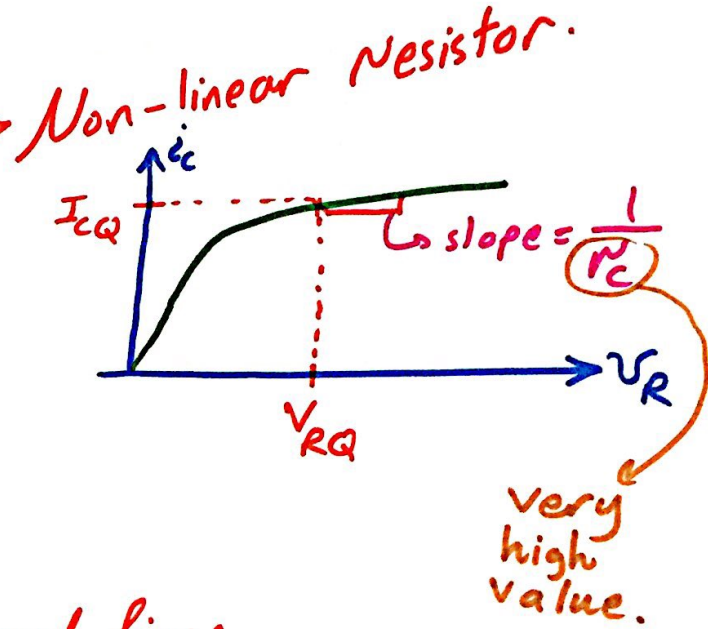
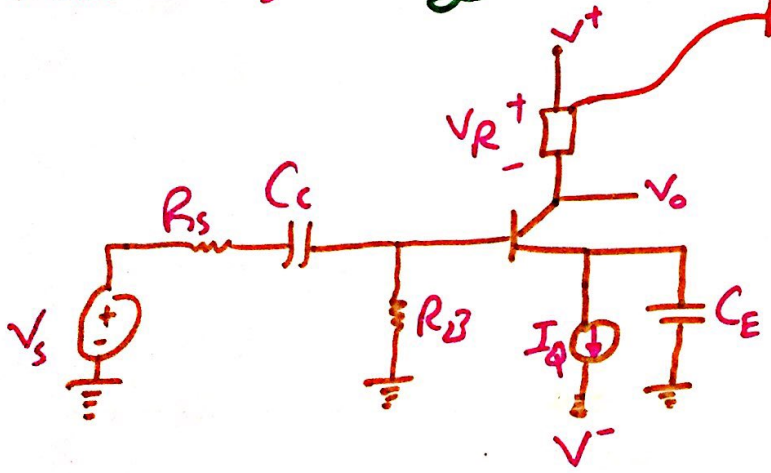
\* DC req.: (i.e)  $I_{CQ}, V_{CEQ} \dots$



Note: if we solve in an example on ordinary CE with  $R_E$ , and we had a confliction between AC & DC req.  $\Rightarrow$  Bypass Capacitor will solve this. (so, solve CE with  $R_E$  & bypass capacitor.)

**4** Advanced CE Amplifier:

\* Advantage: very high  $A_v$ .

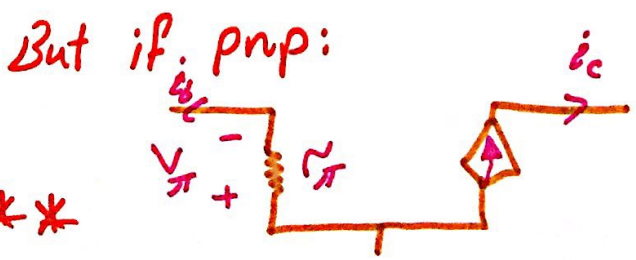
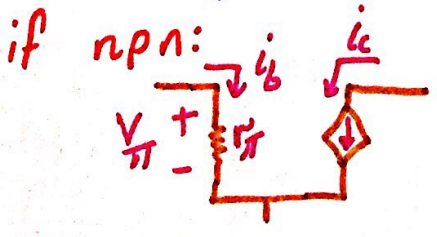


\* DC load line & AC load line:

draw DC equivalent ckt then from output loop find relation between  $(I_C \propto V_{CE})$

Draw AC equivalent ckt then find a relation between  $(i_c \propto v_{ce})$

Note: in AC equivalent ckt:



# Common Collector Amplifier:

## Features:

- ① High input impedance.
- ② Low output impedance.
- ③  $A_V \approx 1$

small loading effect in the input side.  
 small loading effect in the output side.

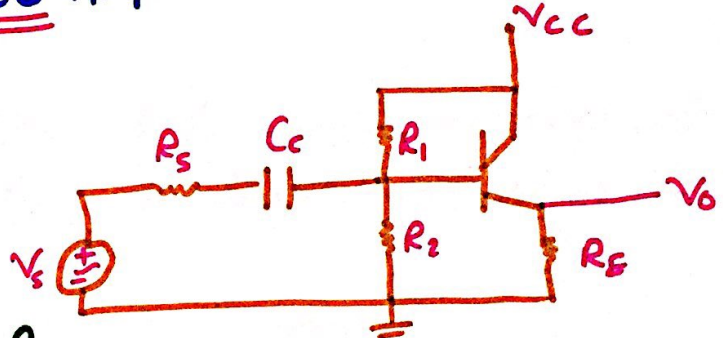
so, CC Amp. is called buffer or impedance transformer & it is equivalent to ideal voltage source.

$(V_o \approx V_s)$  so, it is called emitter follower.

- ④ used as the final stage in multi-stage Amplifier.
- ⑤  $R_1$  &  $R_2$  should be high value  $\Rightarrow$  To exploit the advantage of high  $R_{iB}$
- ⑥  $A_i \approx 1 + \beta \approx \beta$

\* if you have a standard CC Amp like that shown in the figure:

you can directly use the features  $A_V \approx 1$ ,  $A_i \approx 1 + \beta \approx \beta$



under conditions:

$R_1, R_2$  High and  $R_i \gg R_s$  and  $R_1 // R_2 \gg R_{iB}$

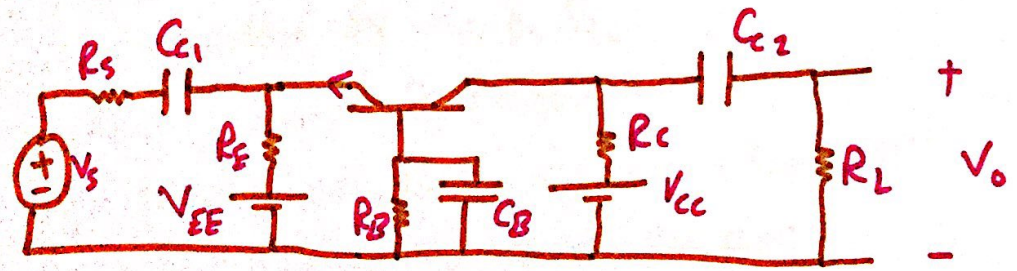
Be careful: if the conditions weren't true you have to calculate  $A_V$  or  $A_i$  by circuit analysis methods.

# Common Base Amplifier:

## Features:

## Standard form:

- ① small  $R_i$
- ② High  $R_o$
- ③  $A_i \approx 1$
- ④  $A_V > 1$



you can use the features ( $A_i \approx 1$ ) under conditions: - standard form.

- must be said that  $R_L \rightarrow 0$   
 $R_C \rightarrow \infty$

\* Here some techniques could be useful in calculations:

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- ① To find  $R_i$ , separate  $R_i$  by finding  $R_{i_b}$  at first if it is CE or CC,  $R_{i_e}$  if it is CB.
- ②  $v_i = v_s \frac{R_i}{R_s + R_i}$  could be useful sometimes in relations.
- ③ Always put in mind voltage division / current division / Nodal analysis; to connect the variables with each other.

\* Multi-stage Amplifier:

↳ Why we need it? To satisfy certain requirements that can not be satisfied by single stage amplifier.

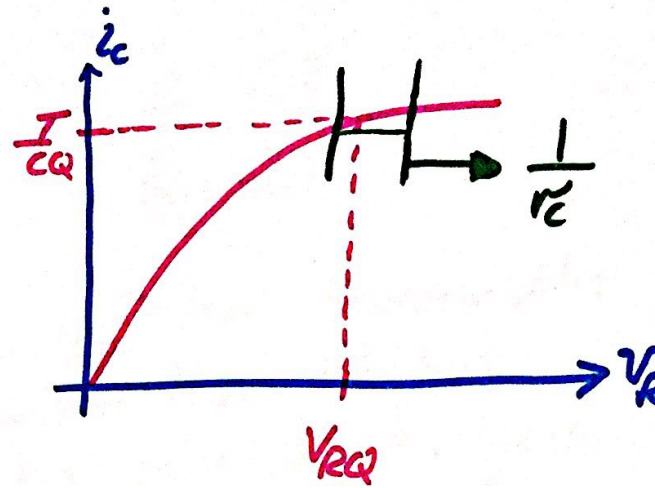
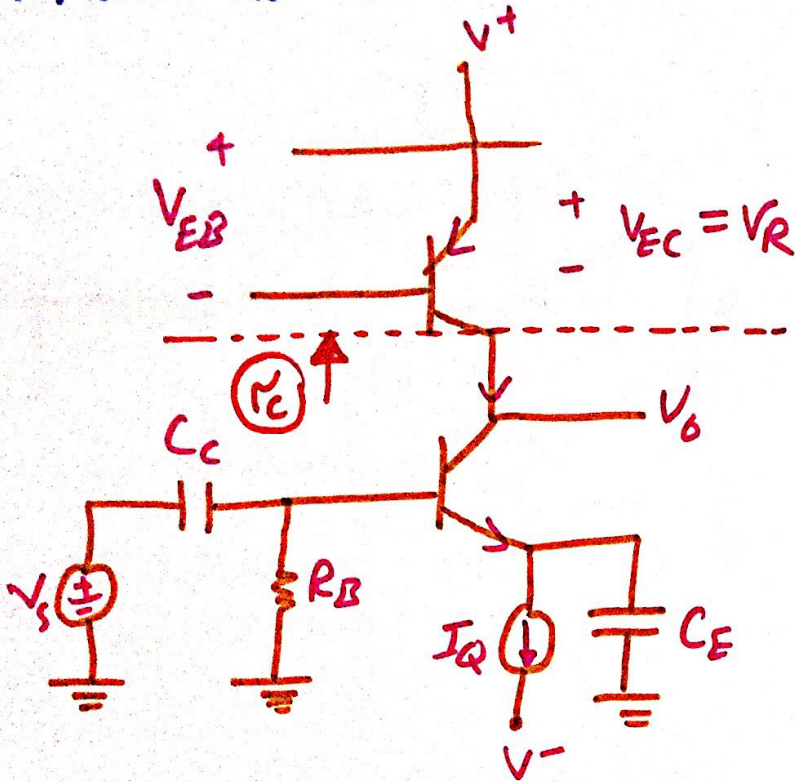
\* Could ask to find overall voltage gain:

Here you need to do the analysis for each stage alone to find  $A_{v_1}$  &  $R_{o_1}$ , then  $R_{o_1}$  will be  $R_s$  for the next stage with voltage source  $v_s A_{v_1}$  and so on, Then find  $A_{v_{total}}$  from the last stage.

\* Also if he asked about  $R_o(\text{total})$ :  
Do the same, then  $R_o(\text{total})$  found from the last stage since it is included by  $R_{o_1}$  &  $R_{o_2}$ .

\* Also if he asked about  $R_i(\text{total})$ :  
some of the techniques that find  $R_i$  for stage(3) the make it load for stage(2) and so on until you find  $R_i(\text{total})$ .

\* Advanced CE with active load:



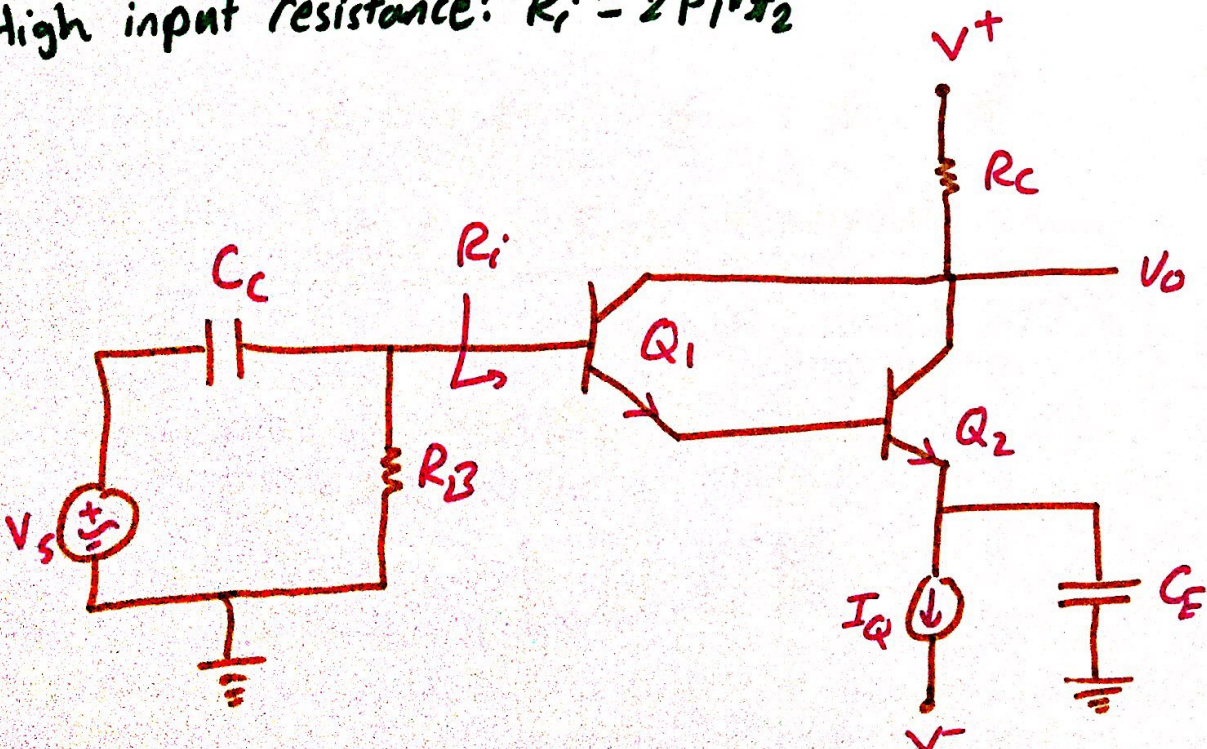
\* Advantages:

- ①  $r_c$ : high value  $\Rightarrow$  very high  $A_v$
- ② small size so it is used in ICs.
- ③ No need for bypass capacitor.

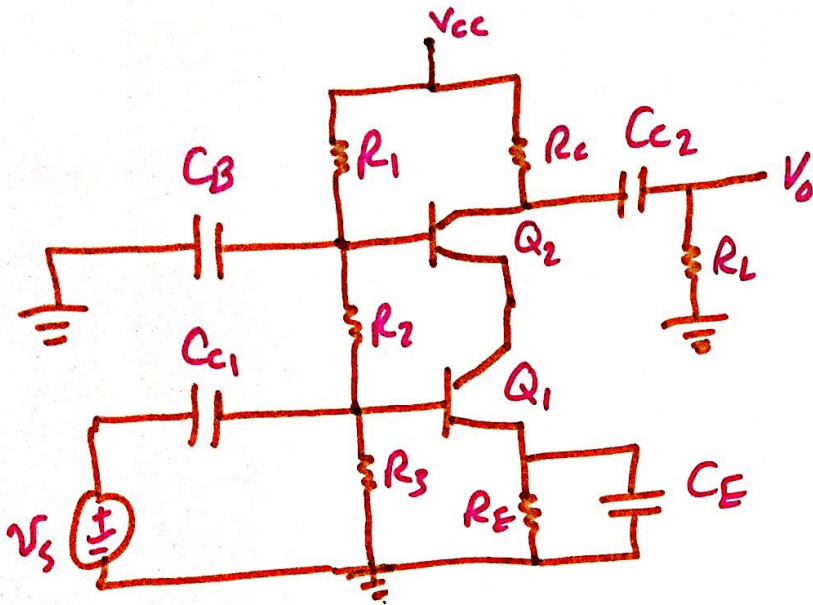
\* Darlington Pair Circuit:

\* features:

- ① High Current gain:  $A_i = \beta_1 \beta_2$
- ② High input resistance:  $R_i \approx 2 \beta_1 r_{\pi 2}$



# \* Cascade Configuration:



Q<sub>1</sub>: CE.  
Q<sub>2</sub>: CB.

CB: has bandwidth wider than CE but CB has low input impedance. So, cascade config. will have wide bandwidth & high input impedance.

⇒ These special ckts.

Darlington Pair & Cascade config.

↳ he could ask you: about the type of configuration for the transistors that used in the ckt or ask about the features for the ckt.

\* \* \* \* \*

End of First Material.

GOOD 😊  
😊 LUCK

# Second Material

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## \* Field Effect Transistor Amplifier:

⇒ we will focus on the type MOSFET in enhancement mode

⇒ MOSFET  n-channel  
p-channel.

## \* Advantages of MOSFET <sup>using</sup> instead BJT:

① Small size.

② low power consumption.

③ High input impedance

## \* Disadvantage:

$g_m$  of MOSFET  $\ll$   $g_m$  of BJT so,  $A_v$  (MOSFET)  $\ll$   $A_v$  (BJT)

## \* Always in MOSFET:

$I_G = 0$ ,  $I_D = I_S$

\* Note: FET to work as amplifier should be in saturation mode  $\Rightarrow V_{DSQ} > V_{DS(sat)}$

## \* Analysis of FET-Amplifiers:

### \* step 1: DC analysis:

① Draw DC eq. ckt.

② find  $V_{GSQ}$ ,  $I_{DQ}$ ,  $V_{DSQ}$

I/P loop.  
o/p loop.

\* Note:

$V_{TN} > 0$

$V_{TP} < 0$

### \* n-channel:

$$I_{DQ} = K_n (V_{GS} - V_{TN})^2, \quad V_{DS(sat)} = V_{GS} - V_{TN}$$

### \* p-channel:

$$I_{DQ} = K_p (V_{GS} + V_{TP})^2, \quad V_{SD(sat)} = V_{SQ} + V_{TP}$$

\* step 2: AC analysis:

- ① Draw AC eq. ckt.
- ② find  $g_m, r_o$ .

$$r_o = \left[ \lambda I_{DQ} \right]^{-1}$$

n-channel:

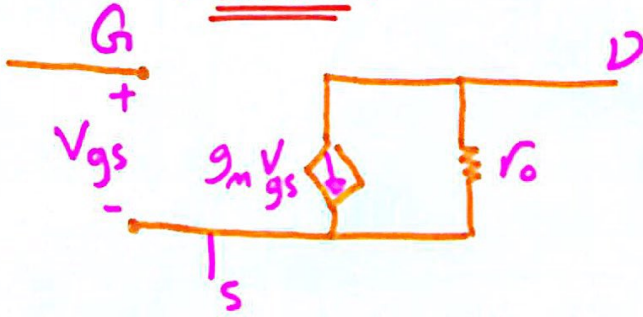
$$g_m = 2K_n (V_{GSQ} - V_{TN})$$

p-channel:

$$g_m = 2K_p (V_{SGQ} + V_{TP})$$

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\* NMOS:



\* PMOS:



\* Basic FET-Amplifier Configurations:

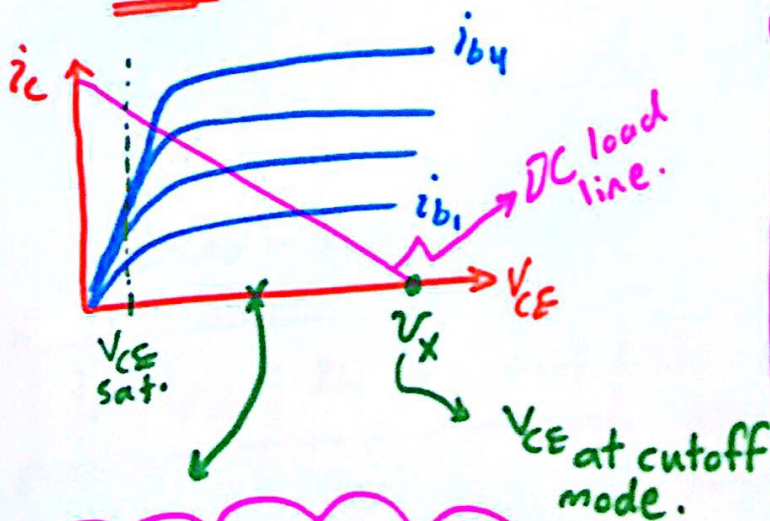
- Common Source.
- Common Drain.
- Common Gate.

\* DC load line:  $I_D \propto V_{DS}$

\* AC load line:  $i_d \propto V_{ds}$

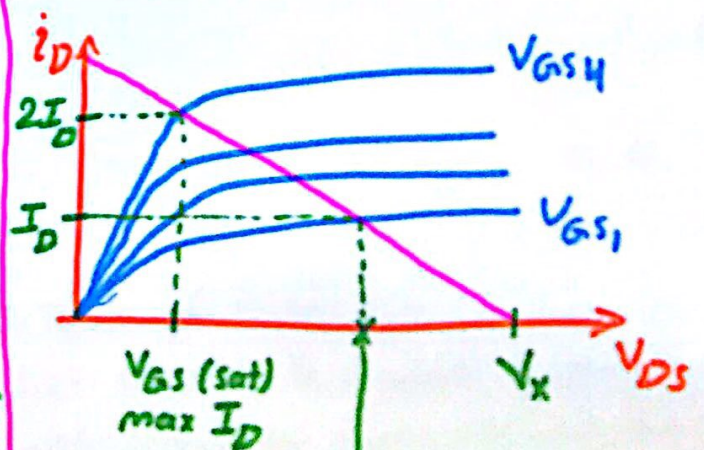
\* How to select the best value of  $V_{CEQ}$  &  $V_{DSQ}$ :

\* BJT:



$$V_{CE} = \frac{V_x + V_{CE(sat)}}{2}$$

\* FET:

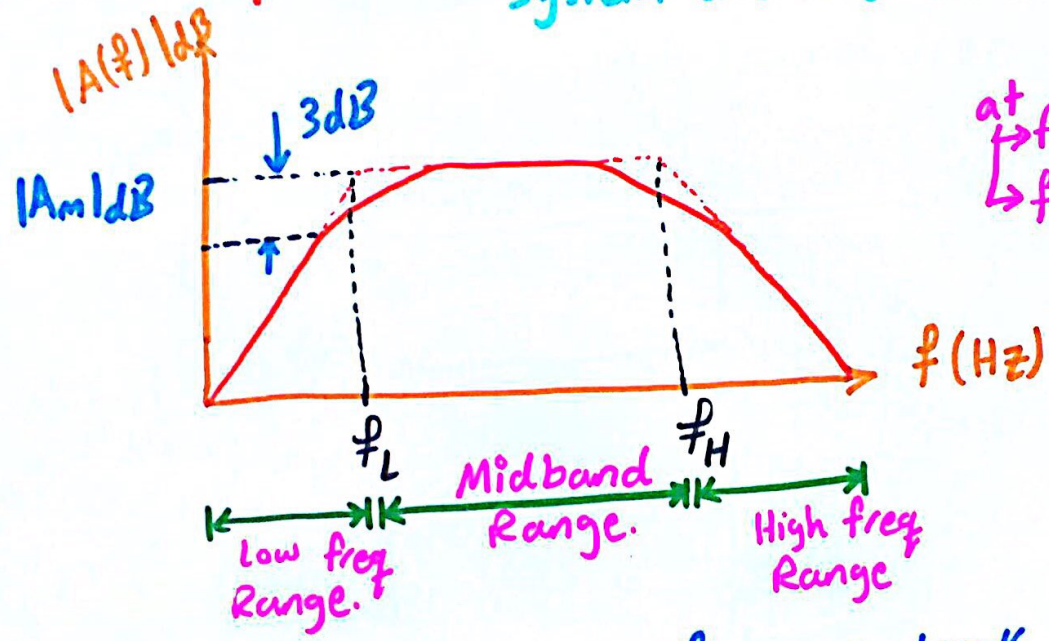


$$V_{DSQ} = \frac{V_x + V_{GS(sat) \max I_D}}{2}$$

Note: You have to solve examples from the book on Common source, Common drain, common gate and they are similar to BJT examples.

## Frequency Response:

what is freq. response? it is the steady state output of linear system due to a sinusoidal input.



at  $f=0$  (DC analysis).  
 $f > 0$  (AC analysis).

$f_L$ : Lower freq. or corner freq. or break point or 3dB freq.  
 $f_H$ : Higher freq. or " " or " " or " " or " " or " "

$f_L = \frac{1}{2\pi\tau_L}$  ,  $f_H = \frac{1}{2\pi\tau_H}$

where:  $\tau$ : Time Constant.

\* Bandwidth of Amplifier:  $BW = f_H - f_L$  \*\*

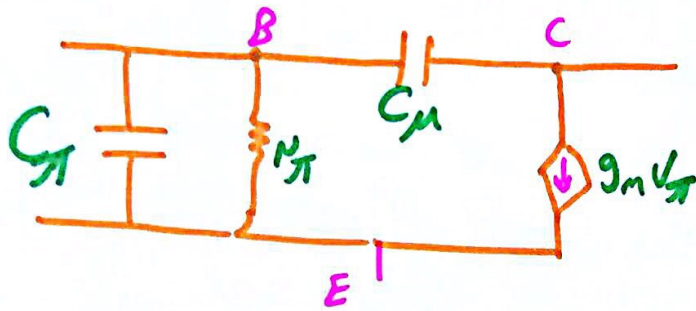
$|A_V|_{dB} = 20 \log_{10} |A_V|$

- \* Types of capacitors in Amp. CKT:
- ① group 1: coupling & bypass capacitors.
  - ② group 2: Transistor Capacitors ( $C_{\pi}$  &  $C_{\mu}$ ) and Load capacitor.



\*  $C_{\pi}$  &  $C_{\mu}$  in the transistor:

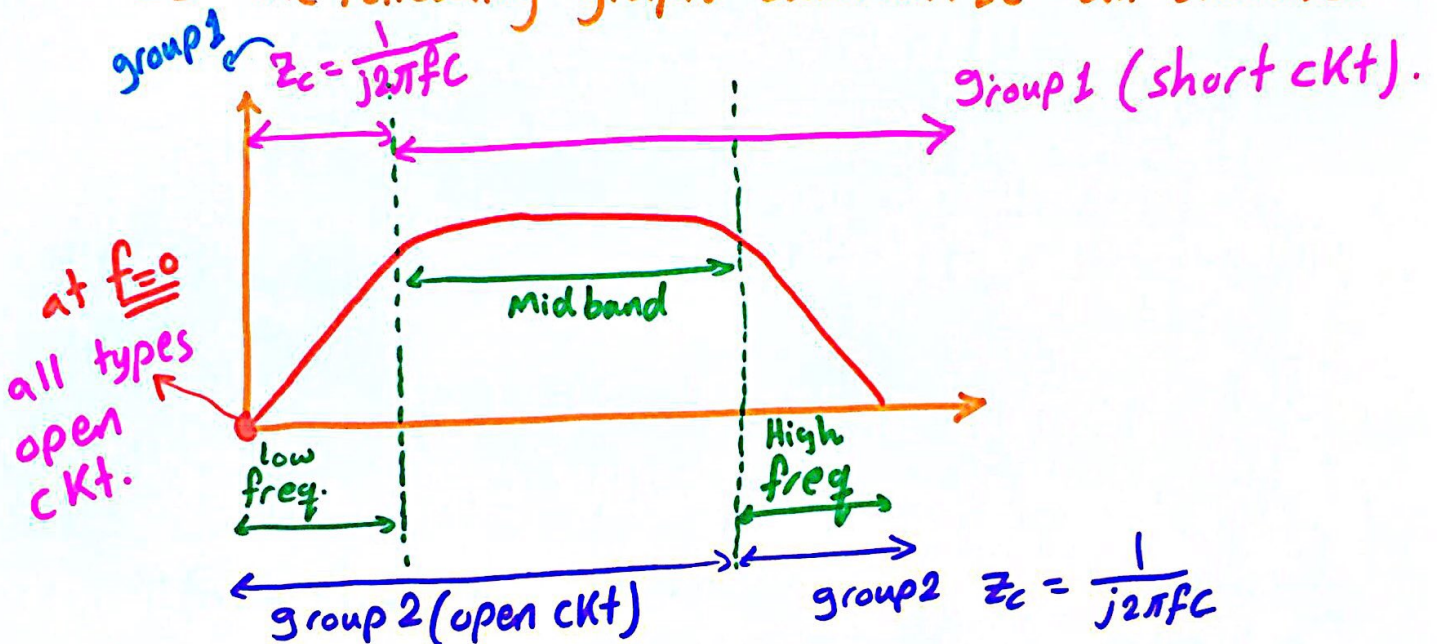
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\* Note:  
 values of group 1 > values of group 2

\* The capacitors could be open ckt or short ckt or have impedance:

⇒ The following graph summarize all statuses:



\* Transfer function of a system  $\equiv \frac{\text{output}}{\text{input}}$

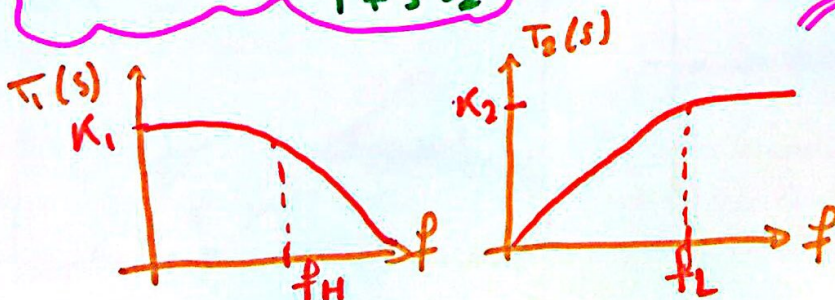
\* Complex freq. of a system  $\equiv s = j\omega$

$$Z_c = \frac{1}{sC}$$

$$T_1(s) = K_1 \frac{1}{1 + s\tau_1}$$

$$T_2(s) = K_2 \frac{s\tau_2}{1 + s\tau_2}$$

⇒ see the prove in Notebook.



from them we can know the corner freq.

# \* What is "Bode Plot" ?

a simplified technique for obtaining approximate plots of the magnitude & phase of a transfer function given the poles & zeros or equivalent time constant.

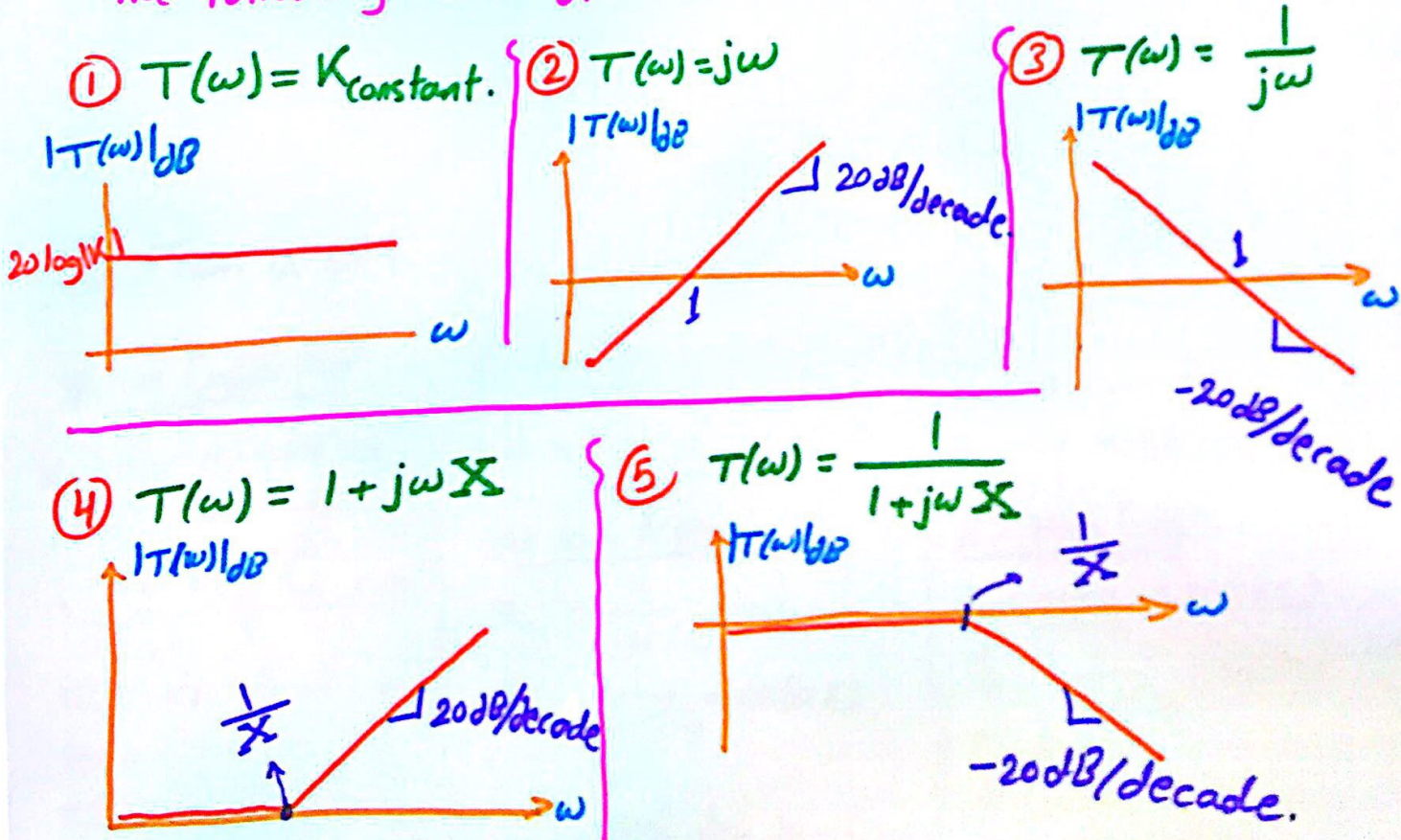
\* To draw the Bode Plot:

- ① write the function in log form.
- ② You will have multi-part; draw each one alone.
- ③ To draw the main function find the sum of slopes on the left & the right of the point when  $|T(f)|_{dB} = 0$

→ it will be the sum of the points on the vertical line at that point  $|T(f)|_{dB} = 0$

## \* Short method to draw Bode Plot:

By writing the function similar to one or more of the following five types:



# \* How to find the time Constant:

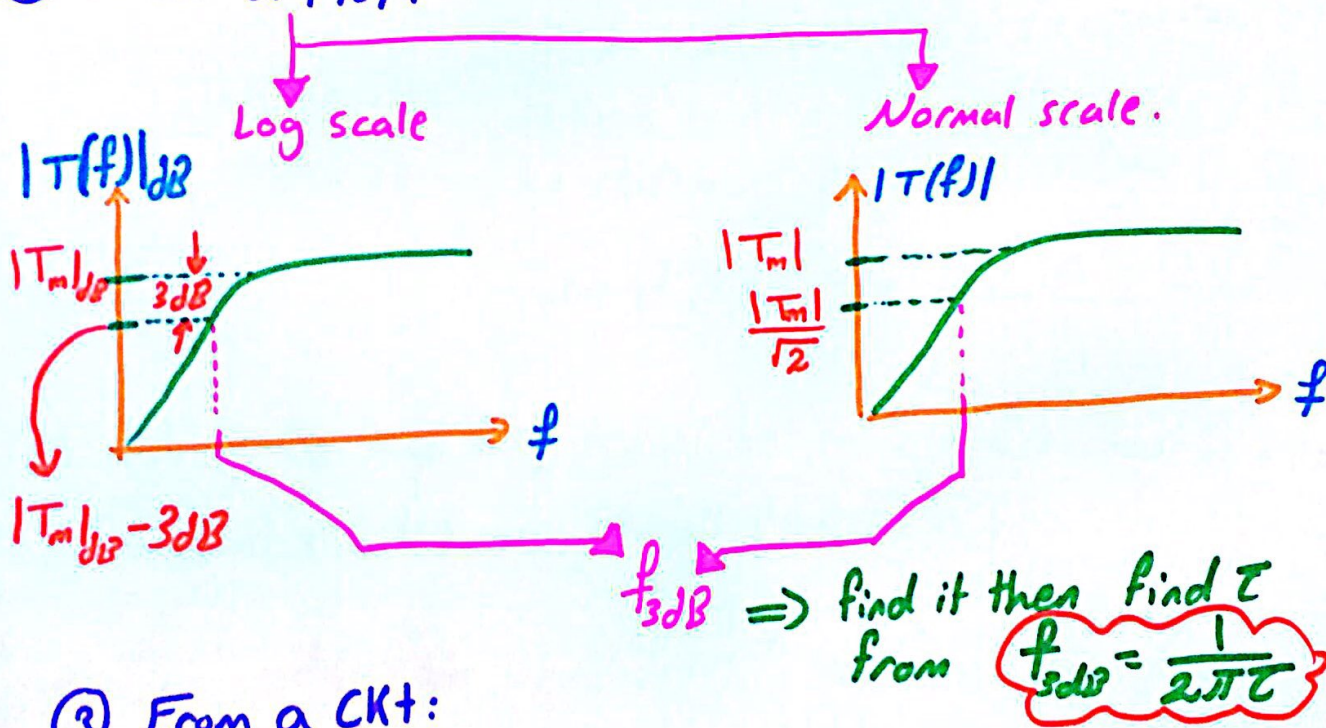
- from a transfer function.
- from a Plot.
- from a circuit.

## ① From a Transfer Function:

⇒ write the given function on the form of

$$T_1(s) = K \frac{1}{1+s\tau} \quad \text{or} \quad T_2(s) = K \frac{s\tau}{1+s\tau} \quad \Rightarrow \text{then find } \tau.$$

## ② From a Plot:



## ③ From a CKT:

### \* One Capacitor:

\* Draw the CKT in AC form then:

$$\tau = R_{eq} C$$

it is  $R_{th}$  that seen from the one capacitor.

### \* Two Capacitors: [ $C_1 > C_2$ ]

\* it will be two time constant

↙ at low freq.  
↘ at high freq.

At low freq:

$$Z_{C_1} = \frac{1}{j2\pi f C_1} \equiv \text{value}$$

$$Z_{C_2} = \frac{1}{j2\pi f C_2} \equiv \infty (O.C)$$

$$\tau = R_{eq} C_1$$

it is called O.C time Const.

At High freq:

$$Z_{C_1} = \frac{1}{j2\pi f C_1} = 0 (S.C)$$

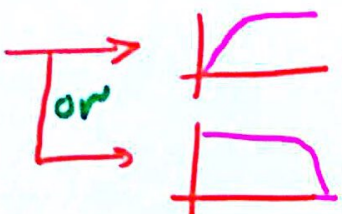
$$Z_{C_2} = \frac{1}{j2\pi f C_2} \equiv \text{value}$$


$$\tau = R_{eq} C_2$$

it is called S.C time constant.

\* Drawing the transfer func. to a given ckt:

7

① if one capacitor   $\Rightarrow$  find  $f_L$ .  
or  $\Rightarrow$  find  $f_H$ .

or  
if two capacitors   $\Rightarrow$  Need  $f_L$  &  $f_H$ .

② Find the max value then draw.

$\rightarrow$  if just  $f_L$ : find max when  $f = \infty$  (capacitor s.c)  
 $\rightarrow$  if just  $f_H$ : find max when  $f = 0$  (capacitor o.c)  
 $\rightarrow$  if  $f_L$  &  $f_H$ : take a point in the middle and see the statement of the capacitors [are they open ckt or short ckt] depending on the value of capacitors then find max.

\* Why in the high freq transistor small devices must be used?  
since it must have small capacitors.

\*  $f_T$ : "unity gain bandwidth" or "Cutoff freq".

\*  $f_{sdb}$  or  $f_\beta$ : "beta Cutoff freq" or

$$f_\beta = \frac{1}{2\pi \beta (C_{\pi} + C_{\mu})}$$

"the Bandwidth of the transistor"

\* Why in BJT  $C_{\mu}$  or  $C_{gd}$  in FET can't be ignored at High freq?

$\Rightarrow$  Due to Miller Effect.

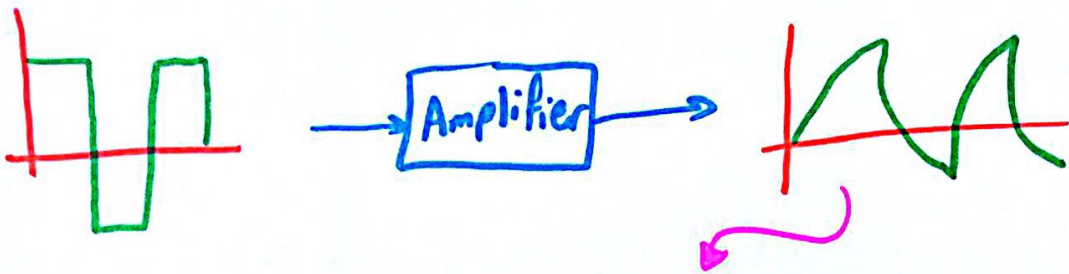
$$f_T = \beta f_\beta$$

# \* Frequency Response for BJT & FET Amplifiers At High Frequency:

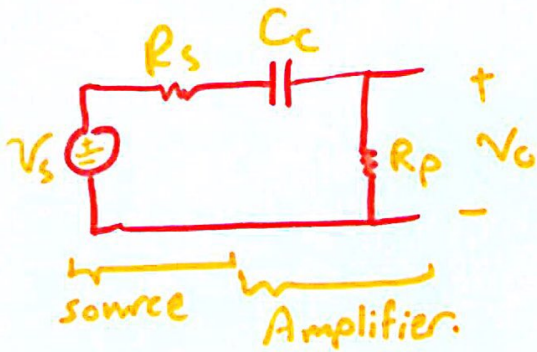
	BJT	FET.
AC CKT.		
$f_T$	$f_T = \frac{\beta}{2\pi r_{\pi} (C_{\pi} + C_{\mu})}$	$f_T = \frac{g_m}{2\pi (C_{gd} + C_{gs})}$
AC CKT with Miller Effect		
$C_M$	$C_M = C_{\mu} * [1 + g_m (R_C // R_L)]$	$C_M = C_{gd} * [1 + g_m R_L]$

## \* Time Response:

\* Why we study it? since sometime we need to amplify non-sinusoidal signal such as square wave signal. (Digital Signal).



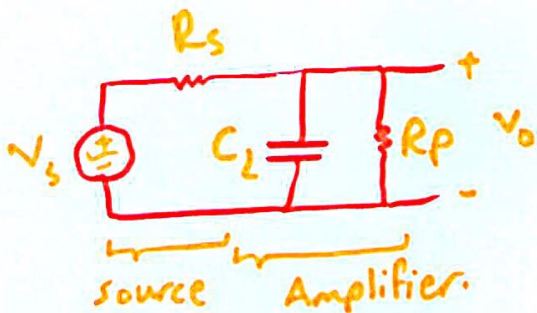
due to charging & discharging of capacitors.  
( $C_c$  &  $C_L$ ).



$\Rightarrow$  for this ckt: need  $\tau \geq 10T$   
where  $T = \frac{1}{2} T_s$   
 $\tau = C_c (R_p + R_s)$

$\Rightarrow$  we need High  $C_c$ :

Rule:  $C_c \geq \frac{5 T_s}{R_p + R_s}$



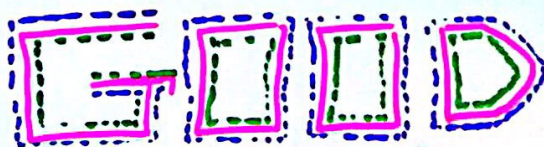
$\Rightarrow$  for this ckt: need  $\tau \leq \frac{T}{10}$   
where  $T = \frac{1}{2} T_s$ ,  $\tau = C_L (R_p // R_s)$

$\Rightarrow$  we need  $C_L$  such that:

Rule:  $C_L \leq \frac{T_s}{20 (R_p + R_s)}$



End of Second Material.



# Final Material

11

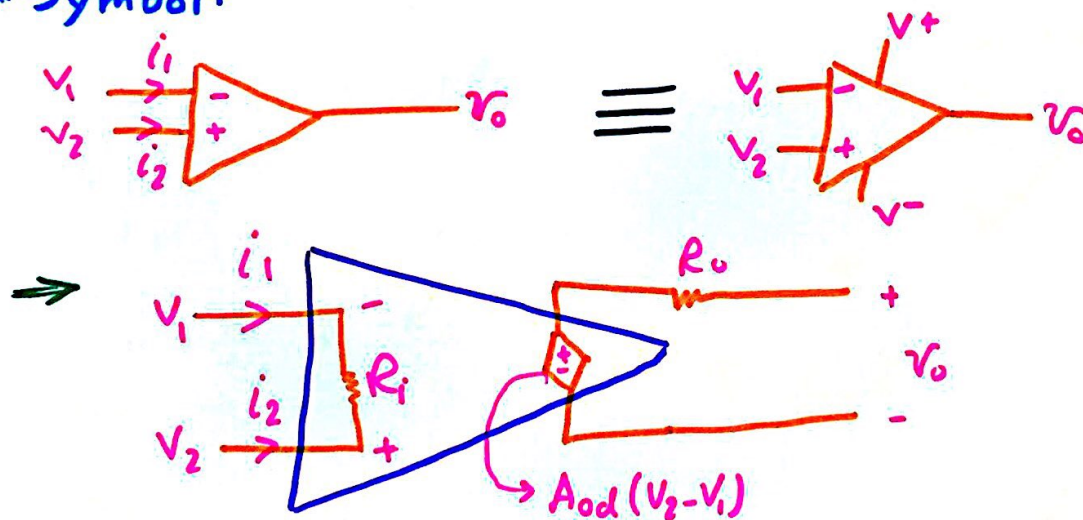
## \* Operational Amplifier [OP-Amp]:

↳ What is op-amp? it is an integrated ckt that amplifies the difference between two input signals & produces one output signal (This is the basic function).

Why we use it? it was used in analog computers to perform mathematical operations to solve differential & integral equ.

What is the number of transistors that op-amp consists? it consists of 20-30 transistors.

## \* Symbol:



$V_1$  is called: inverting terminal  
 $V_2$  is called: Non-inverting terminal.

$A_{od}$ : open-loop differential voltage gain.

## \* Ideal Op-Amp:

①  $R_i = \infty$

⇒  $i_1 = i_2 = 0$

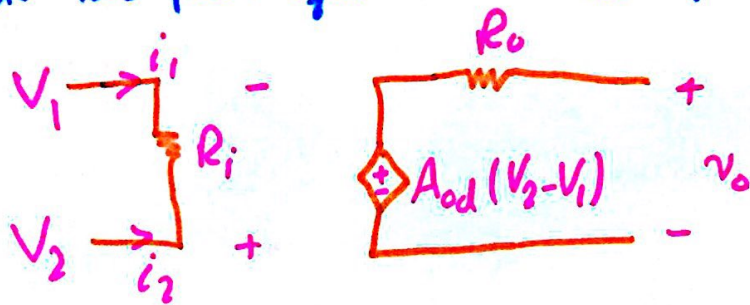
②  $R_o = 0 \Rightarrow V_0 = V_{od}(V_2 - V_1)$

$V_{od} = \infty$

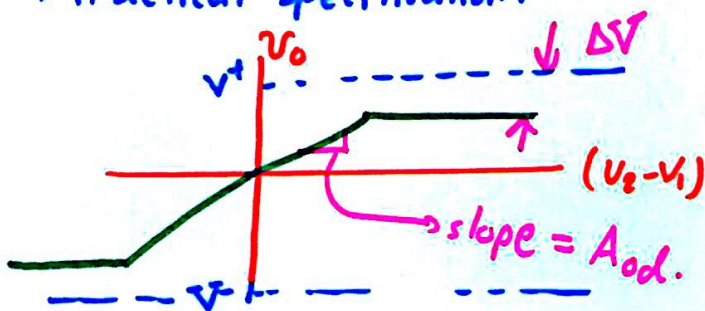
⇒  $V_1 = V_2$

③  $V_1$  &  $V_2$  could be DC or AC or both.

\* Two-port equivalent ckt for Op-Amp:



\* Practical specification:

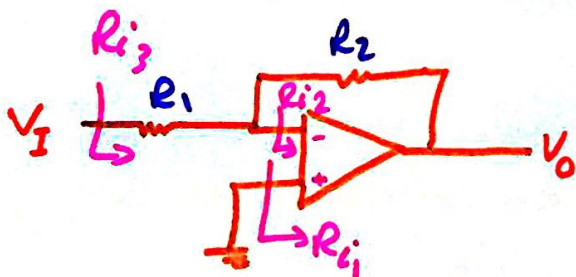
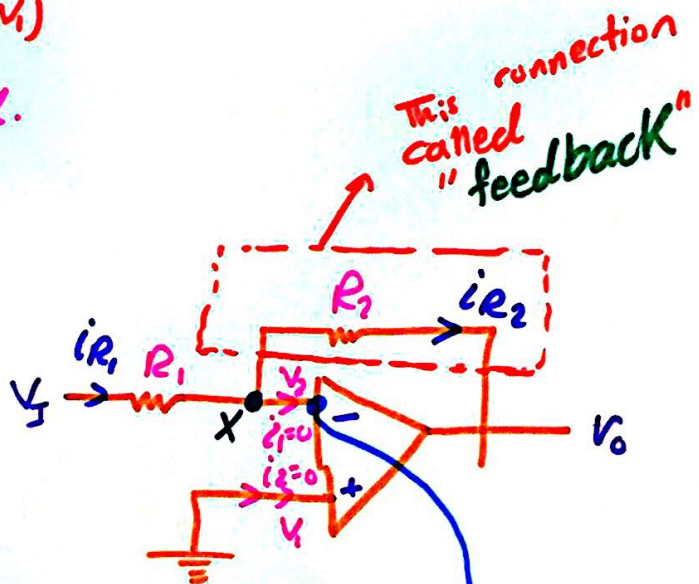


\* Op-Amp Applications:

① Inverting Amplifier:

if it is an ideal op-amp.

$$A_v = \frac{V_o}{V_i} = -\frac{R_2}{R_1} \Rightarrow \text{do KCL at X.}$$



$$\begin{aligned} R_{i1} &= \infty \\ R_{i2} &= \infty \\ R_{i3} &= R_1 \end{aligned}$$

it is called virtual ground.  
(why?)

the voltage at this point = 0  
(as actual ground)  
but the current in this point = 0 (so virtual ground).



## ② Amplifier with T-network:

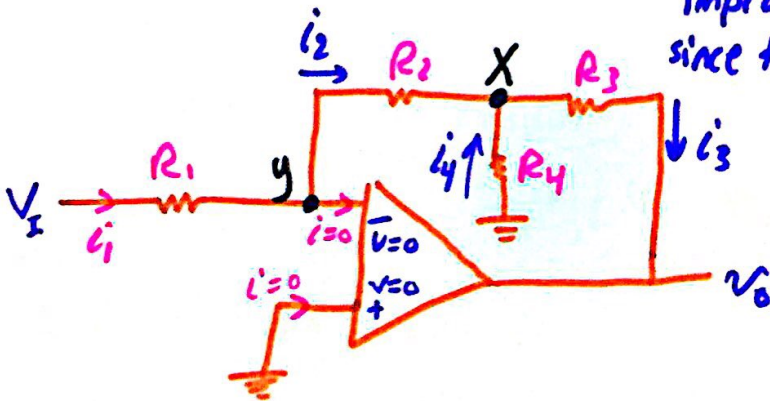
\* Why we used it?

since sometime in first application if we have

$R_i = 50k\Omega$  &  $A_V = -100$

$R_i = R_1 = 50k \Rightarrow A_V = -\frac{R_2}{R_1} \Rightarrow R_2 = 5M\Omega$

this impractical value since that we use it.



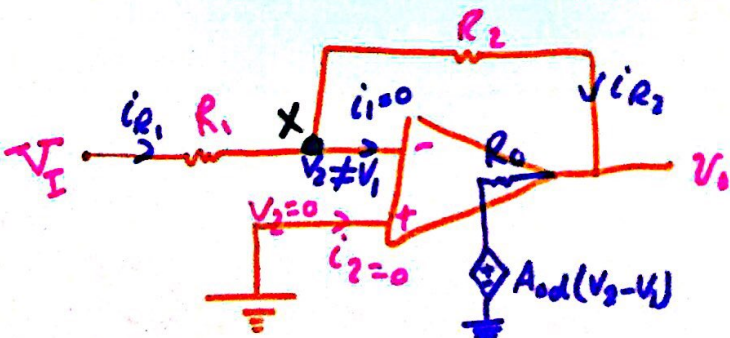
\* You have to know how to use nodal analysis at x and y.

you can reach that:

$$A_V = \frac{V_O}{V_I} = -\frac{R_2}{R_1} \left( 1 + \frac{R_3}{R_4} + \frac{R_3}{R_2} \right)$$

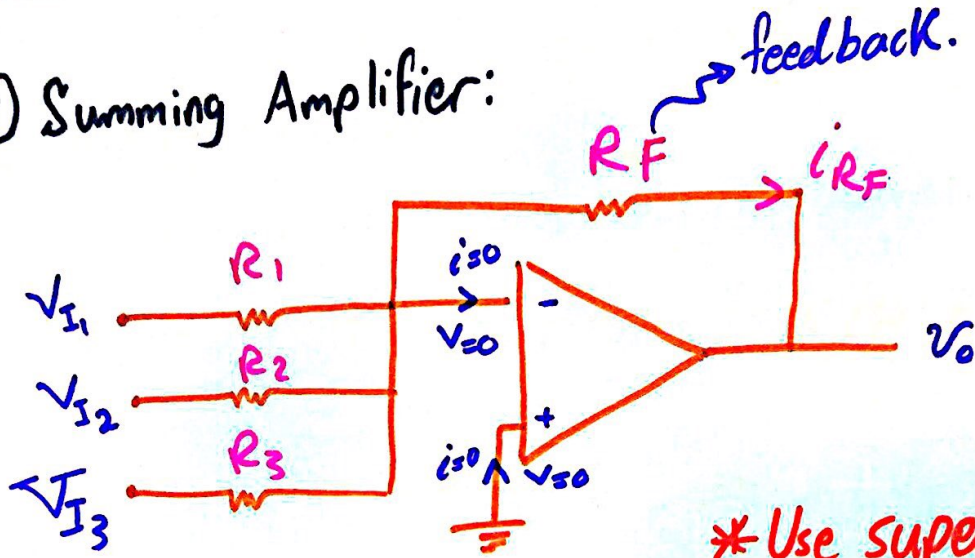
حقيقه . لكن يجب ان تعرف مواقع المقاومات الأربعة بالزبط كما مبين بالشكل التالي .

\* The previous ckt's was ideal op-amp, now if an inverting amplifier wasn't ideal:



Do KCL at (x) and find  $A_V = \frac{V_O}{V_I}$ .

③ Summing Amplifier:

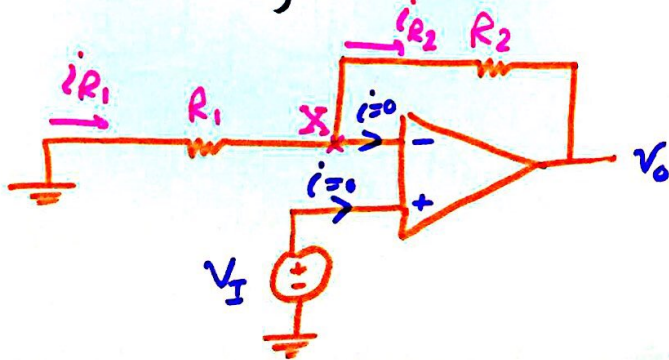


\* Use super position To solve.

⇒ You can reach: if  $R_1 = R_2 = R_3 = R$

$$* \quad V_O = -\frac{R_F}{R} [V_{I_1} + V_{I_2} + V_{I_3}] \quad *$$

④ Noninverting Amplifier:



\* KCL @ X:

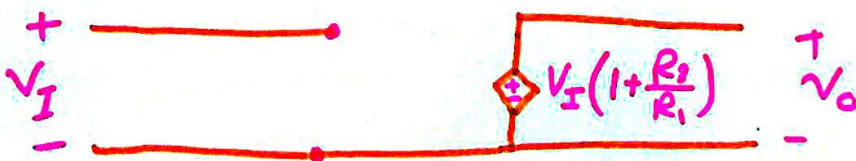
where:  $v_2 = v_I = v_1$

$$\Rightarrow * \quad A_V = 1 + \frac{R_2}{R_1} \quad *$$

\* Note that  $A_V > 1$  in this Application.



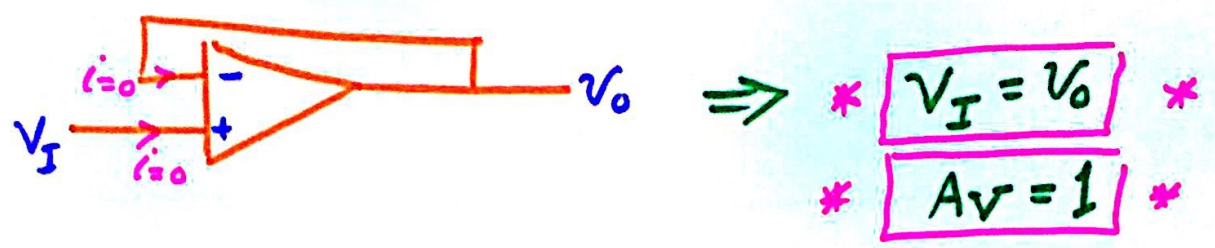
The two-port equivalent network:



⑤ Voltage Follower:

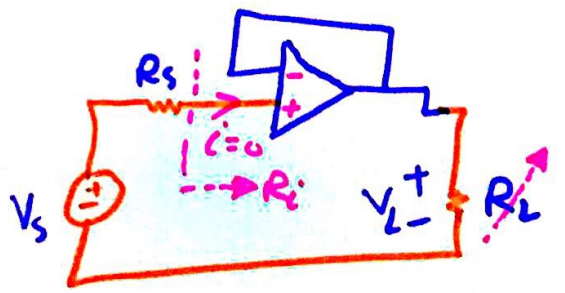
↳ similar to common collector amplifier.

\* other names: Buffer, Impedance Transformer.



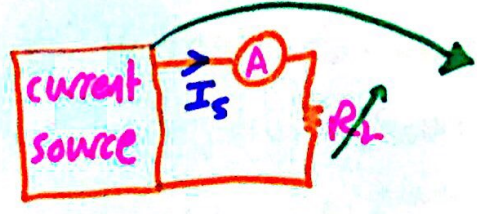
\* Where we use it ?

⇒ we use it with ckt that has High-loading effect  
 ⇒ it will make the ckt has No loading effect.

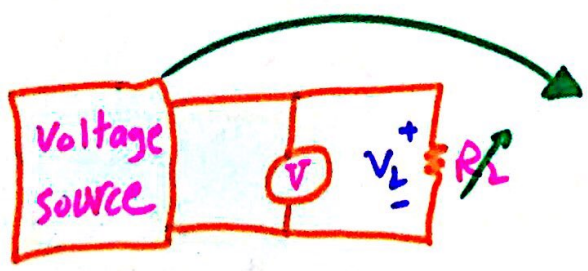


⇒  $R_i = \infty$   
 $V_2 = V_1 = V_s = V_L$   
 ⇒  $V_s = V_L$  even if  $R_L$  is changed.

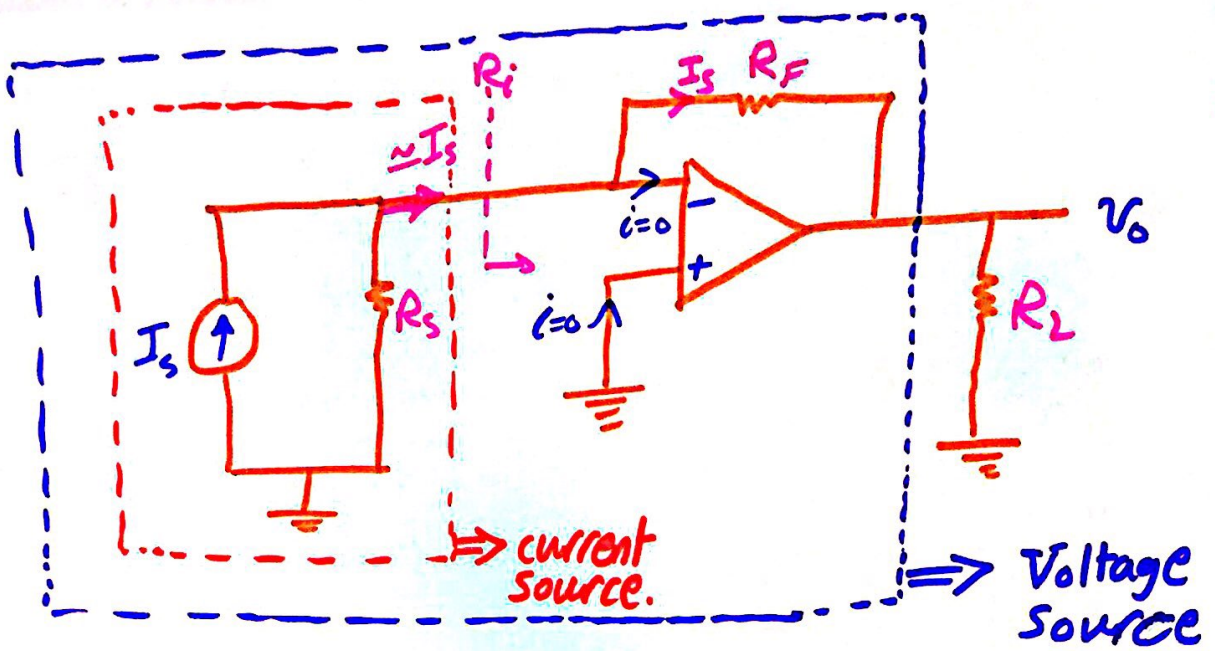
⑥ Current-to-Voltage Converter:



it is current source if  $I_s$  is fixed and independent on  $R_L$ .



it is voltage source if  $V_L$  is fixed and independent on  $R_L$ .

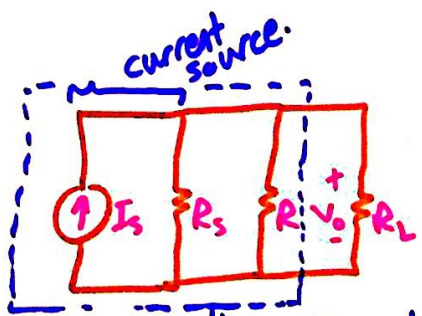


$V_1 = V_2 = 0$   
 $R_i = 0$

$\Rightarrow I_s = \frac{0 - V_o}{R_F}$

$V_o = -R_F I_s$

independent on  $R_L$   
 so, yes it is voltage source.

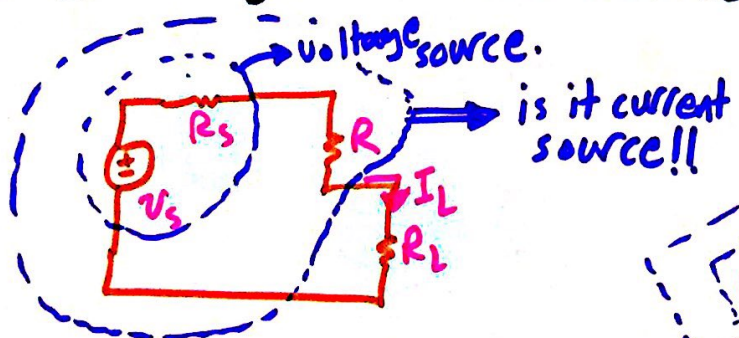


it is not voltage source.

since:  $V_o = I_s (R_s || R || R_L)$

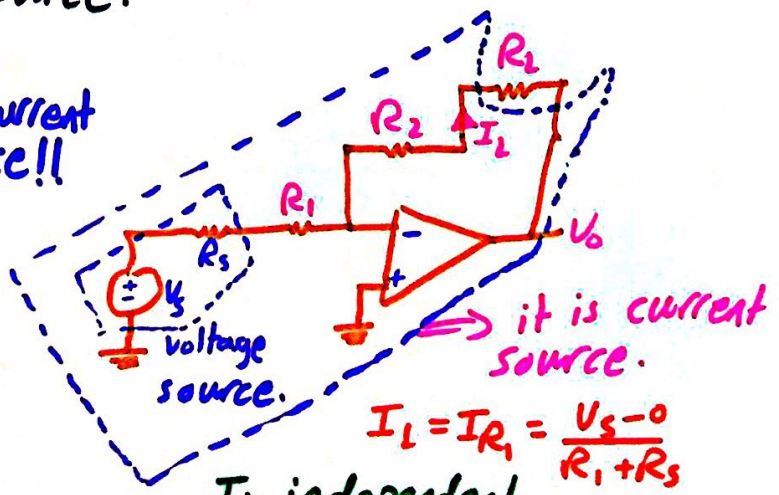
$V_o$  depend on  $R_L$   
 so it is not voltage source.

⑦ Voltage-to-Current Source:



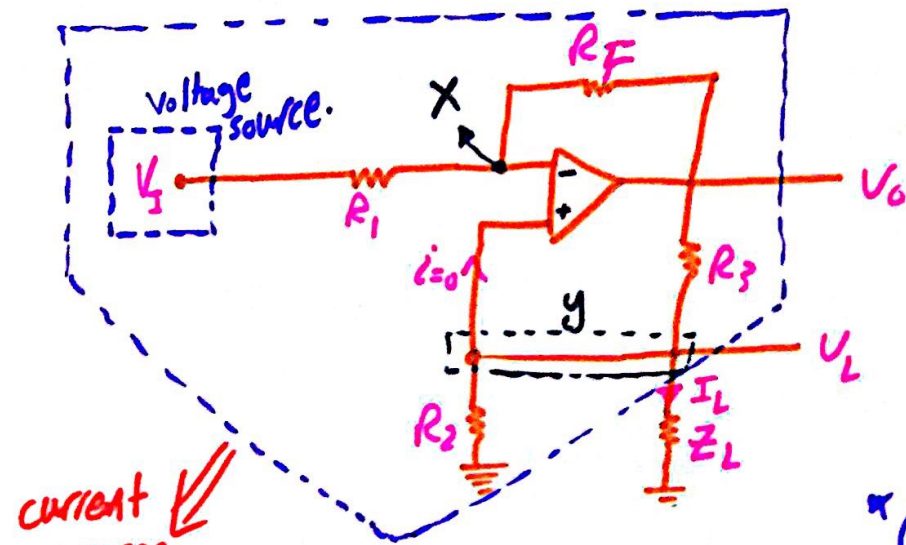
$I_L = \frac{V_s}{R_s + R + R_L}$

$\Rightarrow I_L$  depends on  $R_L$   
 so Not a current source.



$I_L = I_{R_1} = \frac{V_s - 0}{R_1 + R_s}$

$I_L$  independent on  $R_L$ .



⇒ Do KCL @ x & y:

$$i_i = -V_I \frac{R_F}{R_1 R_3}$$

we choose

$$\frac{R_F}{R_1 R_3} = \frac{1}{R_2}$$

⇒ To cancel  $Z_L$

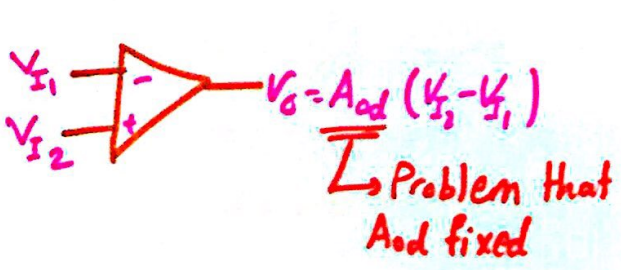
current source  
\* under the condition \*

$$i_i = -\frac{V_I}{R_2}$$

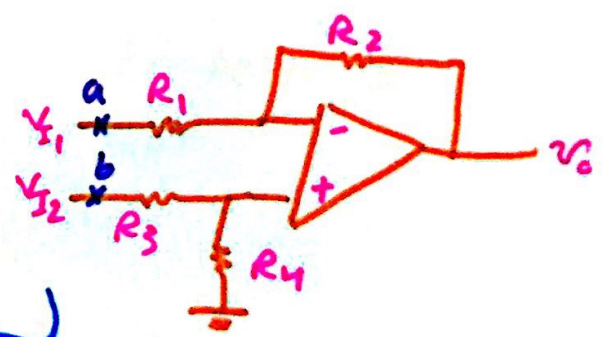
so under this condition.

→ so always check for the condition to use this relation.

### ⑧ Difference Amplifier:



solution. ⇒



use super position.

$$V_O = \left(1 + \frac{R_2}{R_1}\right) \left(\frac{R_4/R_3}{1 + R_4/R_3}\right) V_{I2} - \frac{R_2}{R_1} V_{I1}$$

we choose:  $\frac{R_4}{R_3} = \frac{R_2}{R_1}$

$$V_O = \frac{R_2}{R_1} (V_{I2} - V_{I1})$$

↳ The easiest to select:

$$R_3 = R_1$$

$$R_4 = R_2$$

$R_i$  between a & b:  
 $R_i = R_1 + R_3$  if the condition true  
 ⇒  $R_i = 2R_1$

Note: if he asked to find  $R_i$  between two points  
 $\Rightarrow$  put voltage source  $V_x$  with  $I_x$  between these two points.

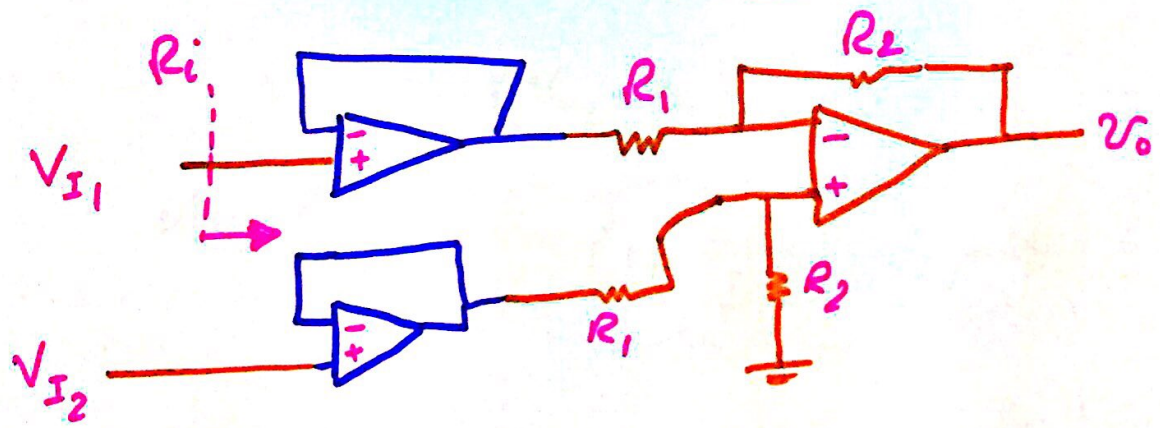
if he asked to find  $R_i$  @ some point  
 $\Rightarrow$  put  $V_x$  with  $I_x$  between this point and the ground.

\* Two problems face application number 8:

① if we want to change the gain  $V_o = \frac{-R_2}{R_1} (V_{I_2} - V_{I_1})$   
we take  $R_1$  fixed & change  $R_2$  but there is (two  $R_2$ )  $\Rightarrow$  we should keep them equal (practical problem)  
 $\Rightarrow$  we solve this By Application 9.

$\hookrightarrow$  Instrumentation Amplifier.

②  $A_v = \frac{R_2}{R_1}$ , we need  $R_i = 2R_1$  to be High  
 $\Rightarrow$  This will cause  $A_v$  to be low  
 $\Rightarrow$  we solve this by Buffer.

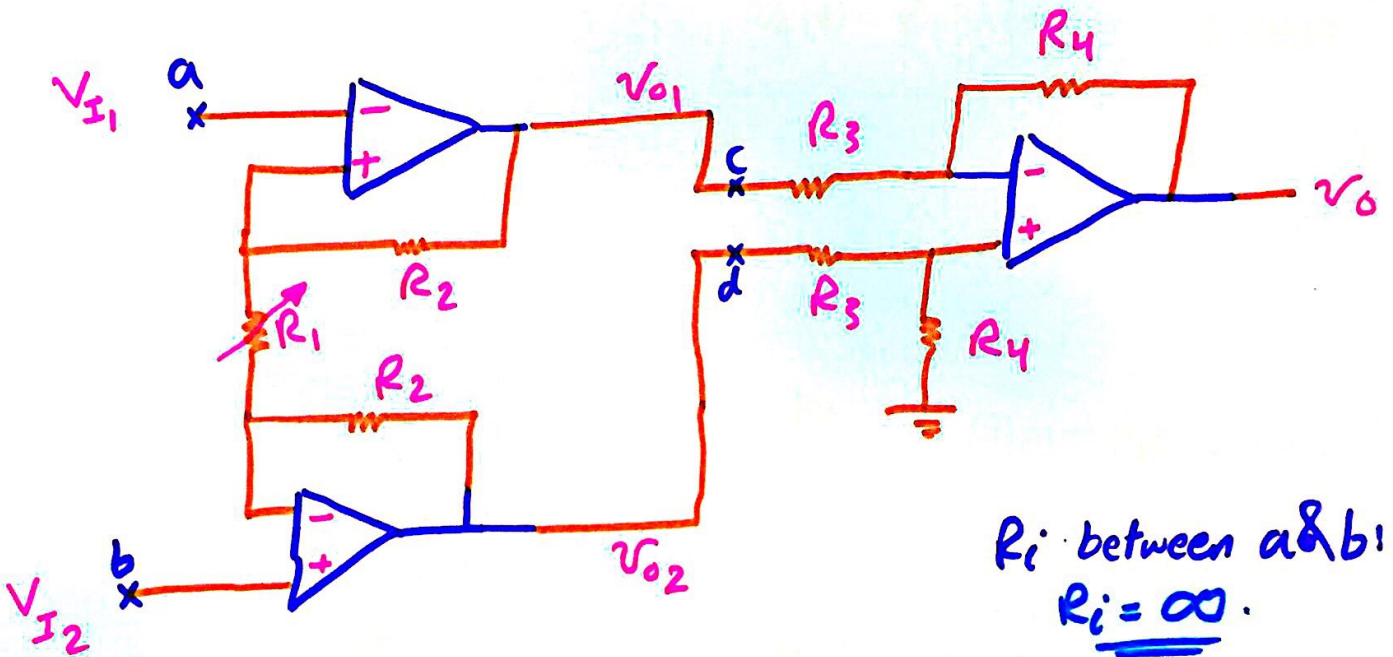


$\Rightarrow R_i = \frac{V_x}{I_x}$  where  $I_x = 0$   
so  $R_i = \infty$  (High value)

# ⑨ Instrumentation Amplifier:

\* Advantages:

- ①  $R_i = \infty$ .
- ② We can change the gain via one resistor.



$R_i$  between a & b:  
 $R_i = \infty$ .

$R_i$  between c & d:  
 $R_i = 2R_3$

⇒ After doing the analysis:

$$v_0 = \frac{R_4}{R_3} (v_{02} - v_{01})$$

also \*

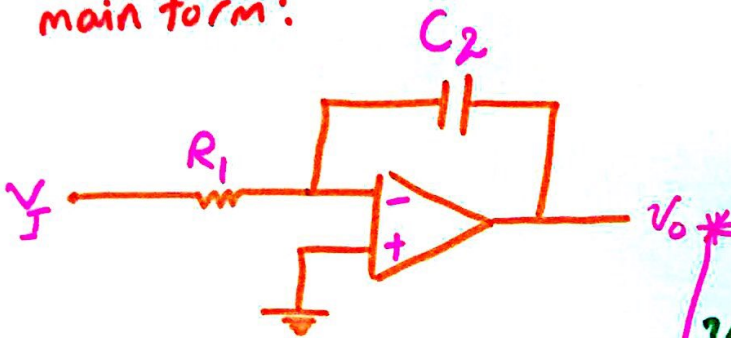
$$v_0 = \frac{R_4}{R_3} \left( 1 + \frac{2R_2}{R_1} \right) (V_{I2} - V_{I1})$$

\*

\* Note: You have to know how to find  $R_i$  between any two points or @ any point.

⑩ Integrator:

main form:

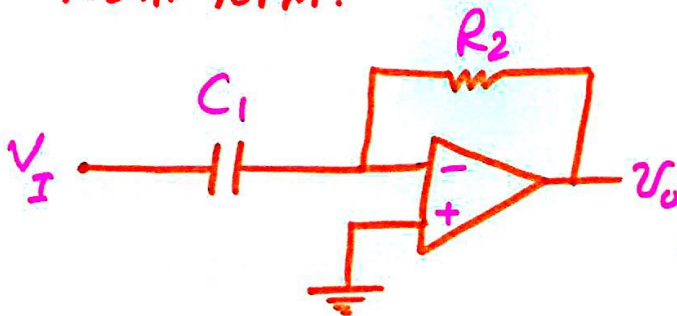


$$\Rightarrow * v_o(s) = \frac{-1}{sR_1C_2} v_I(s) *$$

$$* v_o(t) = v_o(t=0) - \frac{1}{R_1C_2} \int_0^t v_I(t') dt' *$$

⑪ Differentiator:

main form:

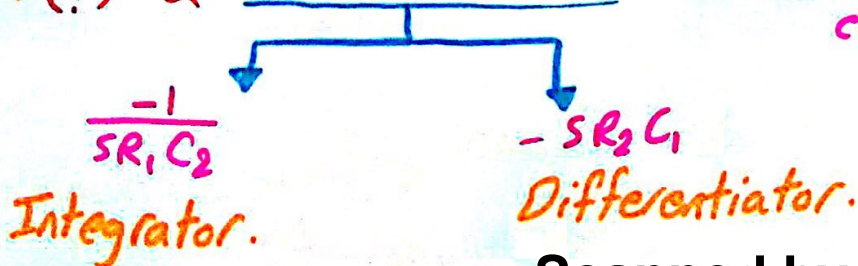


$$\Rightarrow * v_o(s) = -R_2C_1 s v_I(s) *$$

$$* v_o(t) = -R_2C_1 \frac{dv_I(t)}{dt} *$$

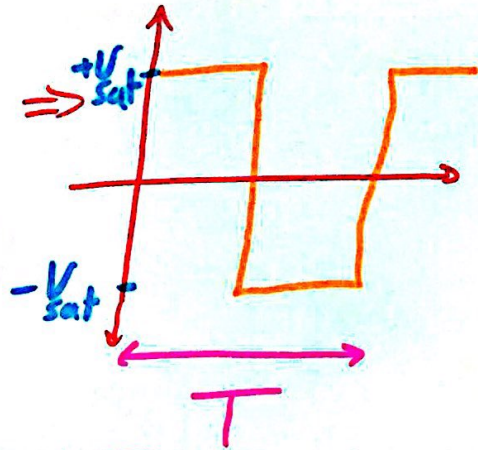
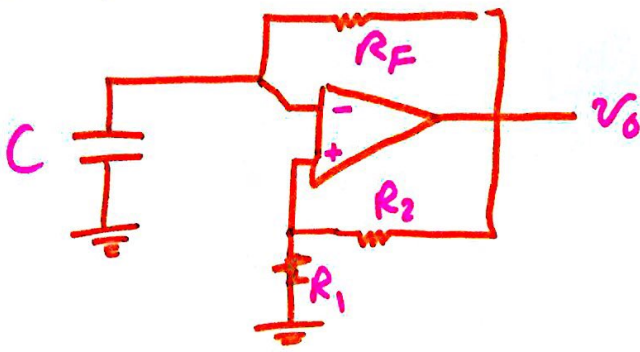
\* An important NOTE on both applications ⑩ & ⑪:

You have to know the main condition that make a ckt Integrator or differentiator so if he add any component to the ckt and ask what will make it integrator or differentiator just find  $v_o(s) = ? v_i(s)$  Then compare between (?) & the main condition.  $\Rightarrow$  Then find the new condition.





## ⑫ Square-Wave Generator:



- if  $v_2 > v_1 \Rightarrow v_o = +V_{sat}$
- if  $v_1 > v_2 \Rightarrow v_o = -V_{sat}$
- if  $v_o > v_c \Rightarrow C$  is charged.
- if  $v_c > v_o \Rightarrow C$  is discharged.

$$T = 2R_F C \ln\left(\frac{1+\lambda}{1-\lambda}\right)$$

$$\lambda = \frac{R_1}{R_1 + R_2}$$

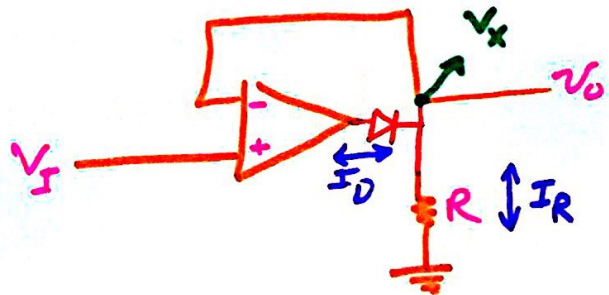
## ⑬ Precision Half-wave Rectifier:

Why we use it?

To save the 0.7 voltage that was lost in Diode half-wave rectifier.

we have two assumptions:

$$v_I < 0 \text{ or } v_I > 0$$



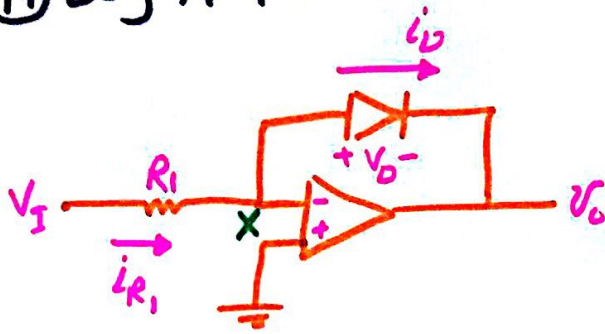
case ( $v_I < 0$ ):

- if the diode ON:  $\Rightarrow$  voltage follower ( $v_o = v_I$ )
- if the diode OFF:  $\Rightarrow v_x < 0 \Rightarrow I_R \uparrow = I_D$  (wrong assumption)
- $\Rightarrow$  No feedback ( $v_o = 0$ )

case ( $v_I > 0$ ):

- if the diode ON:  $\Rightarrow$  voltage follower  $\Rightarrow v_x > 0$  (correct assumption)
- $\Rightarrow I_R \downarrow = I_D$

⑭ Log Amplifier:



remember:

$$i_D = I_S e^{V_D/V_T}$$

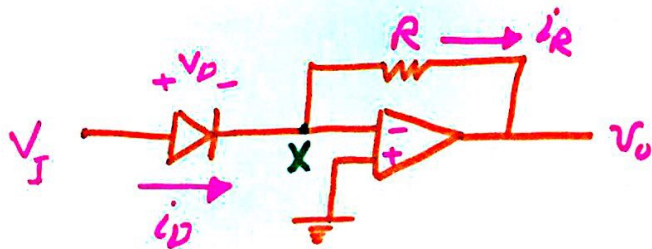
@ X:

$$i_{R_I} = i_D$$

$$\frac{V_I}{R_I} = I_S e^{V_D/V_T} ; \underline{V_D = -V_O}$$

$$\Rightarrow V_O = -V_T \ln\left(\frac{V_I}{I_S R_I}\right)$$

⑮ Antilog or Exponential Amplifier:



Kcl @ X:

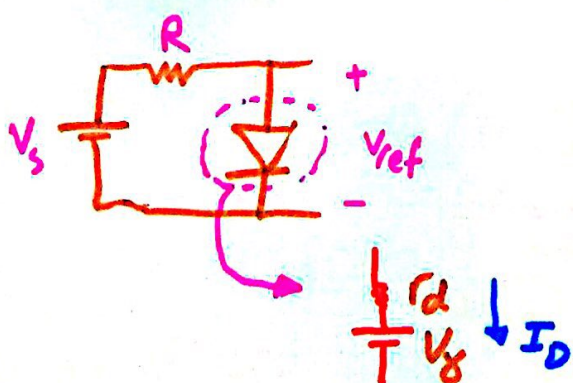
$$\Rightarrow V_O = -I_S R e^{V_I/V_T}$$

⑯ Reference Voltage Source Design:

- Temperature effect on the typical voltage source  
 => so we use this application to have a fixed reference voltage.

\* We have 2 solutions:

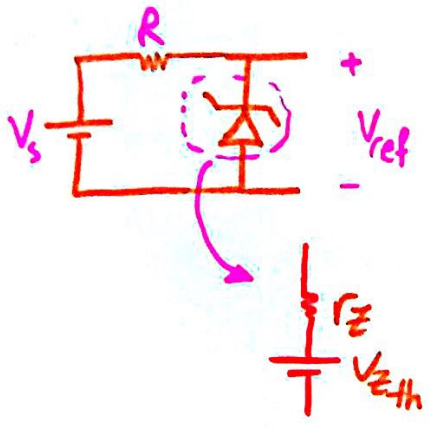
solution (1): using pn Diode.



$$\Rightarrow V_{ref} = V_f + r_d \left( \frac{V_S - V_f}{r_d + R} \right)$$

\* NOT a strong solution  
 Need another one.

solution(2): using Zener diode.



$$\Rightarrow V_{ref} = V_{Z_{th}} + r_Z \left( \frac{V_s - V_{Z_{th}}}{r_Z + R} \right)$$

$r_Z$  is very small so however  $V_s$  changes it won't effect a lot in  $V_{ref}$

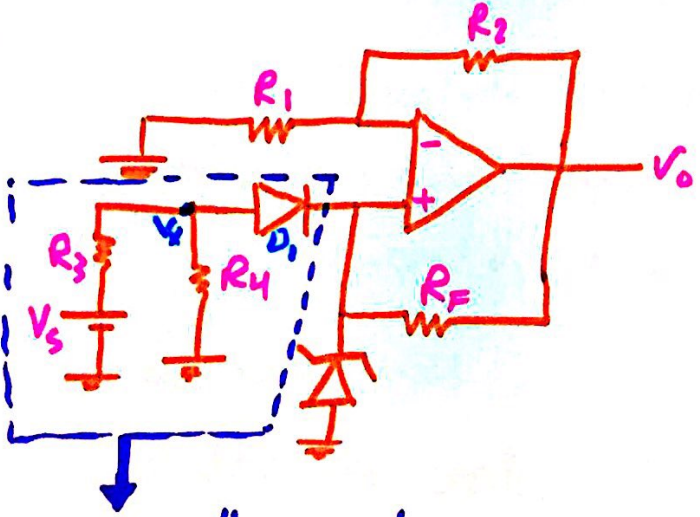
$\Rightarrow$  so solution 2 better than solution 1.

\* Disadvantages of solution(2):

- ①  $V_s$  changes slightly with  $V_{ref}$ .
- ② in some cases, we need  $V_{ref} >$  or  $<$  than  $V_{Z_{th}}$ .

solution(3):

using op-amp, PN diode & Zener diode.



\* when  $D_1$  is on.  
 $(V_x - V_Z) > V_Y$

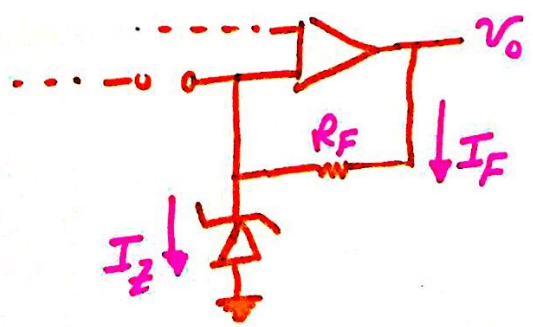
$$V_s \frac{R_4}{R_3 + R_4} - V_Z > V_Y$$

$\Rightarrow$  we decrease  $V_s$  such that  $D_1$  is off (open ckt)

we use this part:  
 To start-up the circuit.

$$V_o = V_Z \left( 1 + \frac{R_2}{R_1} \right)$$

$$I_Z = \frac{R_2 V_Z}{R_1 R_F}$$



## \* Feedback & Stability:

### \* Types of feedback:

① **Positive Feedback:** a portion of the output signal is added to the input signal  
 ⇒ used in The design of oscillators  
 e.g. square-wave-generator.

② **Negative Feedback:** a portion of the output signal is subtracted from the input signal.

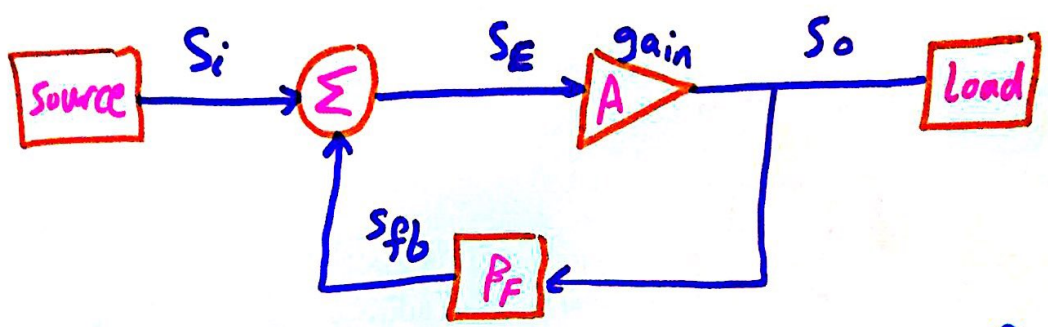
### \* Advantages of (-ve) Feedback:

- ① **Gain Stability:** the gain is independent on the parameters of the transistor or the op-amp (ex.  $\beta$ )  
 e.g. Inverting Amplifier.
- ② **Bandwidth Extension:** increase the bandwidth.
- ③ **Increase Signal-to-Noise Ratio (SNR).**
- ④ **Reduce the Non-Linear Distortion.**
- ⑤ **Control the Input & Output Impedances.**

### \* Disadvantages:

- ① **Reduce the Gain.**
- ② **There is a possibility that the feedback ckt may become unstable (oscillate) @ high frequency.**

\* Basic Feedback Concepts:



$$A_f = \frac{S_o}{S_i} = \frac{A}{1 + \beta_f A}$$
 gain with feedback.

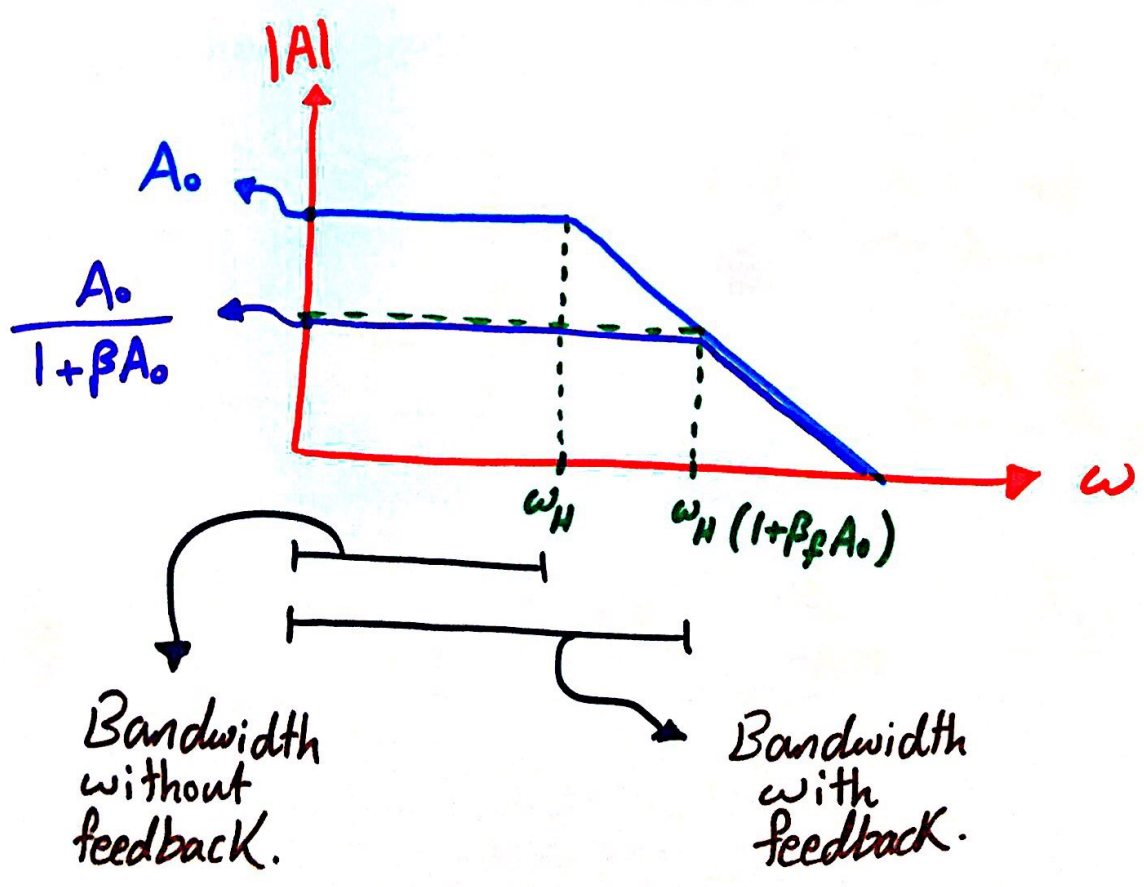
$$A = \frac{S_o}{S_e}$$
 gain without feedback

usually  $\beta_f A \gg 1$

$$A_f = \frac{1}{\beta_f}$$
 "stable gain"

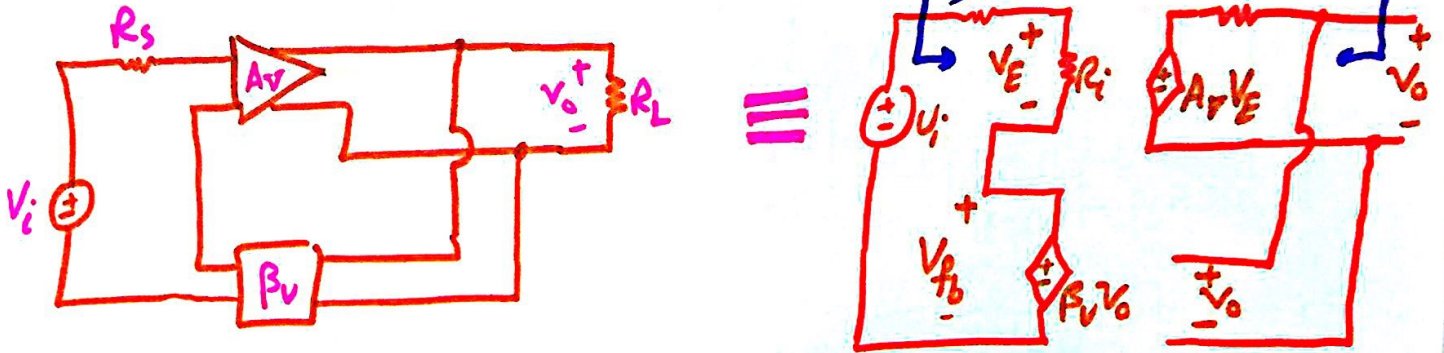
\* Bandwidth Extension:

Gain \* Bandwidth = Constant



# \* 4 - Topologies (Configuration):

## ① Series - Shunt.

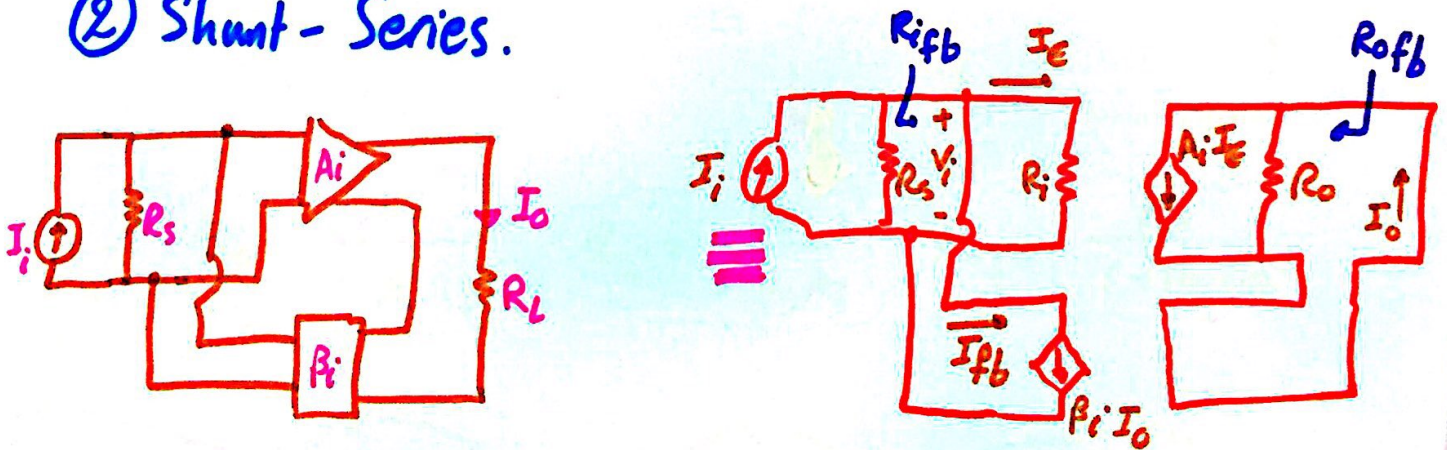


$\frac{V_o}{V_i}$  →  $A_{V_{fb}} = \frac{A_V}{1 + A_V \beta_V}$   
 reduce the voltage gain.

$R_{i_{fb}} = R_i (1 + \beta_V A_V)$   
 increase the input impedance.

$R_{o_{fb}} = \frac{R_o}{1 + A_V \beta_V}$   
 reduce the output impedance.

## ② Shunt - Series.

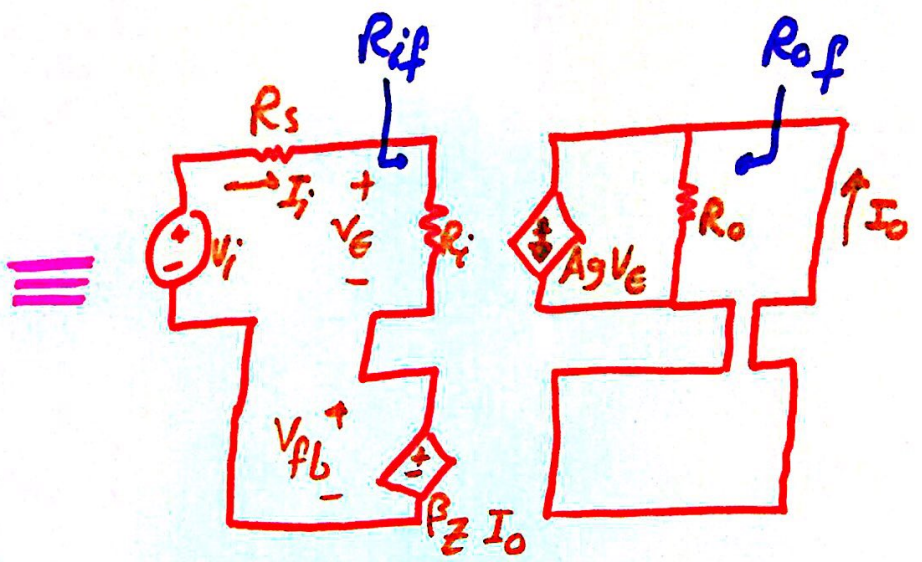
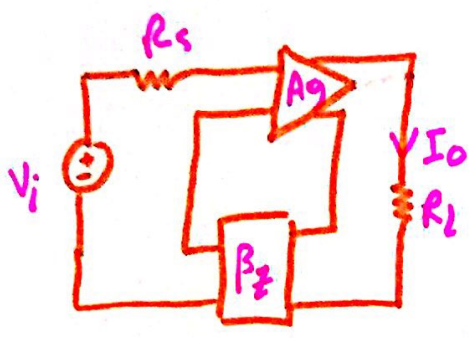


$\frac{I_o}{I_i}$  →  $A_{i_{fb}} = \frac{A_i}{1 + \beta_i A_i}$

$R_{i_{fb}} = \frac{R_i}{1 + \beta_i A_i}$

$R_{o_{fb}} = (1 + \beta_i A_i) R_o$

③ Series-Series.

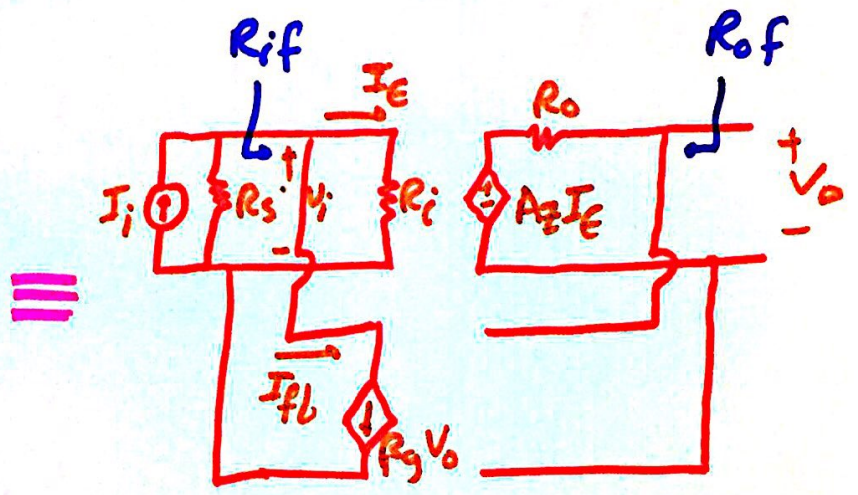
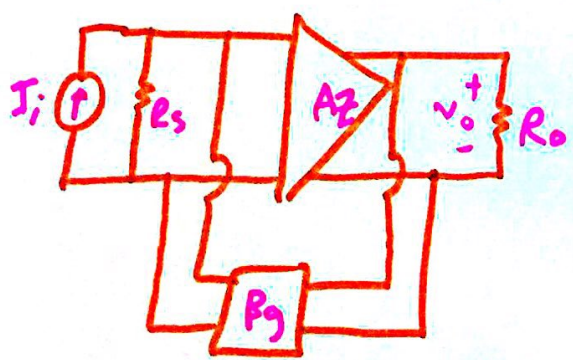


$\frac{I_o}{V_i} \rightarrow A_{gf} = \frac{A_g}{1 + \beta_z A_g}$

$R_{if} = R_i (1 + \beta_z A_g)$

$R_{of} = R_o (1 + \beta_z A_g)$

④ Shunt-Shunt.



$\frac{V_o}{I_i} \rightarrow A_{zf} = \frac{A_z}{1 + \beta_g A_z}$

$R_{if} = \frac{R_i}{1 + \beta_g A_z}$

$R_{of} = \frac{R_o}{1 + \beta_g A_z}$



End of Final Material.



**GOOD LUCK**

